BLYTHE SOLAR POWER PROJECT (09-AFC-6C)
RIVERSIDE COUNTY, CALIFORNIA

NUMERICAL GROUNDWATER FLOW MODEL OF THE PALO VERDE VALLEY and PALO VERDE MESA (SOIL&WATER–16)

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TABLE OF CONTENTS

Section **Page**

Executive Summary **1**

1.0 Introduction **3**
- 1.1 Project Description 3
- 1.2 Project Phasing 5
- 1.3 Project Water Use Requirements 5
- 1.4 Report Organization 5

2.0 Previous Studies and Summary of Available Data **7**
- 2.1 Summary of Previous Studies 7
- 2.2 Summary of Available Information 10
- 2.3 Additional Project Site Investigation 12

3.0 Hydrogeology and Conceptual Flow Model for Palo Verde Valley **13**
- 3.1 Physiography 13
- 3.2 Climate 14
- 3.3 Geology of Palo Verde Valley 14
  - 3.3.1 Hydrostratigraphy 15
  - 3.3.2 Structure 17
- 3.4 Groundwater Occurrence and Flow 17
  - 3.4.1 Groundwater Occurrence 17
  - 3.4.2 Groundwater Flow 19
- 3.5 Groundwater Geochemistry 23
  - 3.5.1 Valley Basin Geochemistry 23
  - 3.5.2 Mesa Basin Geochemistry 24
- 3.6 Palo Verde Valley Aquifer Characteristics 24
- 3.7 Water Balance for the Palo Verde Valley 25
  - 3.7.1 Recharge 27
  - 3.7.2 Discharge 29

4.0 Model Development and Calibration Data **32**
- 4.1 Model Construction 32
  - 4.1.1 Code Selection 32
  - 4.1.2 The Model Grid 33
  - 4.1.3 Boundary Conditions 34
  - 4.1.4 Model Parameters 35
- 4.2 Model Calibration Concepts 36
- 4.3 Calibration Results 37

5.0 Model Simulations **39**

6.0 Sensitivity Analyses **41**

7.0 Conclusions **42**

8.0 References **44**

List of Tables

Table-1 Forecasted Construction Phasing Summary
Table-2 Water Balance
Table-3 Mass Balance Non-Pumping and Pumping Condition (Steady State Model)
Table-4 Mass Balance – Sensitivity Analysis

List of Figures

Figure 1 Map of the Palo Verde Valley
Figure 2 Wells Identified in the USEG NWIS Database
Figure 3 Surface Water Gauging Stations along the Colorado River
Figure 4 PVID Well Locations
Figure 5 PVID Diversion, Spills and Returns
Figure 6 Geologic Map of the Palo Verde Valley and Mesa
Figure 7 Site Map Showing Test Wells and Planned Operational Wells
Figure 8 Isopach Map of the Colorado River Sediments
Figure 9 Hydrographs – Valley Basin
Figure 10 Hydrographs – Mesa Basin
Figure 11 Water Level Contours – Shallow Zone
Figure 12 Water Level Contours – Deep Zone
Figure 13 Boron Concentrations in the Valley and Mesa Basins
Figure 14 Model Domain
Figure 15 Model Grid
Figure 16 Colorado River Transects (USBR)
Figure 17 PVID Drains and DEM Locations
Figure 18 Hydraulic Conductivity Zonation
Figure 19 Calibration – Actual vs. Predicted Water Levels
Figure 20 Model Predicted Water Levels
Figure 21 Model Predicted Zone of Influence
Figure 22 Model Predicted Flow Vectors and Magnitude

List of Appendices

Appendix A Groundwater Wells and Water Level Database (USGS)

Appendix B Water Quality Database

Appendix C Colorado River Gauging Data (USGS)

Appendix D Summary Of Palo Verde Irrigation District Water Level Data

Appendix E Summary of Palo Verde Irrigation District Diversion Data

Appendix F Geophysical Investigation at the Solar Millennium Project

Appendix G Analysis of the Depth of Bedrock in the Lower Colorado River Valley

Appendix H Electronic Groundwater Modeling Files (CD)

List of Acronyms

°F	Degrees Fahrenheit
af	acre-feet
afy	acre-feet per year
ASTM	American Standard Testing Materials
bgs	below ground surface
BLM	Bureau of Land Management
CEC	California Energy Commission
COC	Condition of Certification
DEM	Digital Elevation Model
DWR	Department of Water Resources
ET	evapotranspiration
ft/d	feet per day
ft/ft	groundwater gradient in feet per foot
ft^2/d	feet squared per day
GHB	general head boundary
gpd/ft	gallon per day per foot
gpm	gallons per minute
gpm/ft	gallons per minute per foot of drawdown
HTF	heat transfer fluid
I-10	Interstate 10
Mesa Basin	Palo Verde Mesa Groundwater Basin (USGS Definition)
msl	mean sea level
MW	megawatt
NWIS	National Water Information System
Palo Verde Valley	Palo Verde and Cibola Valleys
Project	Blythe Solar Power Project
PVID	Palo Verde Irrigation District
PVSI	Palo Verde Solar I, LLC
ROW	right-of-way
SCE	Southern California Edison
SCM	site conceptual model
TEM	transient electromagnetic
USBR	United States Bureau of Reclamation
USEPA	United States Environmental Protection Agency
USGS	United States Geological Survey
Valley Basin	Palo Verde Valley Groundwater Basin (USGS Definition)

EXECUTIVE SUMMARY

A numerical groundwater model was developed as required under California Energy Commission final licensing condition SOIL&WATER-16 to estimate the increase in discharge from surface water to groundwater that affects recharge from the Palo Verde Valley Groundwater Basin (Valley Basin) to the Palo Verde Mesa Basin (Mesa Basin) from Project pumping after 30 years. SOIL&WATER-2 requires that the Project offset the amount of water equal to the change in surface water discharge predicted by the model. The key surface water bodies are east of the Project site and include Palo Verde Irrigation District (PVID) drains and the Colorado River, both located in the Valley Basin.

The model was constructed to include both the floodplain of the Colorado River (Valley Basin) and the Palo Verde Mesa (Mesa Basin). The model was constructed as a single-layer numerical model in MODFLOW with the domain encompassing both the younger and older alluvium of the Colorado River. The numerical model was developed in consideration of the water balance for the Palo Verde Valley (both Valley and Mesa Basins), which shows that water levels have not fluctuated significantly indicating a balance between water diverted for irrigation and groundwater discharged through the PVID drains back to the Colorado River. The model was calibrated to steady-state conditions from 1980 to 2009 and assumed unconfined conditions for both the younger and older alluvium. Transient calibration was not attempted given the relative stability of the water levels over the last 30 years.

The model calibration was within acceptable tolerances and the model was used to evaluate the effect from Project pumping after 30 years and a volume of 22,250 acre feet. From the modeling the following conclusions are offered:

- The influence to a predicted drawdown of 0.1 foot is within the Palo Verde Mesa and does not extend into the floodplain or to the Colorado River. Groundwater flow vectors after 30 years of pumping show that groundwater flows to the pumping wells largely from areas on the Palo Verde Mesa, the McCoy Wash and from westerly flow into the Palo Verde Mesa in the northern portion of the floodplain. These results suggest little to no significant influence on the surface water in the PVID drains and no influence on the Colorado River as the cone of depression does not reach these features.

- A comparison of the mass balance between the pumping and non-pumping condition shows that there is no change in the flow of water from the Colorado River to the groundwater, indicating that the Project pumping does not affect a change in the river discharge during the 30 year period.

- A comparison of the mass balance to the PVID drains shows that there is a small change in the mass balance of about 20 acre-feet at the end of construction and 1,785 acre-feet total after 30 years of pumping. This change represents about 0.014% of the flow through the drains in the model over 30 years. A value of this magnitude is insignificant and could not be verified by measurement given the average annual drain flow over the last 10 years is about 353,000 acre-feet per year and the total drain flow in the model is 12,800,000 acre-feet. The amount of change in the drain flow is about 8% of the total groundwater pumped during 30 years for the Project, which is a reflection of the change in recharge from the Valley Basin to the Mesa Basin.

- The predictive sensitivity analysis shows that hydraulic conductivity is the most sensitive variable. Modeling a range of values around the calibrated variable yields changes in the PVID drain discharge of between 1,077 and 3,315 acre-feet after 30 years of pumping. The largest changes in PVID drain discharge were predicted when both the hydraulic conductivity and drain conductance were twice their calibrated value. These model scenarios may be overly conservative and beyond a reasonable predictive estimate of impacts from Project pumping, as the drain flow is 100,000 acre-feet per year more than the measured average in the PVID drain since 1993. The model prediction from the calibrated model appears to be a better representation of potential impacts from Project pumping through the operational life of 30 years.

1.0 INTRODUCTION

This report documents the results of a numerical groundwater flow model developed to fulfill Conditions of Certification (COC) SOIL&WATER-2 and SOIL&WATER-16 included in the Final Decision issued by the California Energy Commission (CEC) on September 15, 2010 for the Blythe Solar Power Project (Project) proposed by Palo Verde Solar I, LLC (PVSI). The Project is located in the Palo Verde Mesa and is west of the Palo Verde Valley north of the Blythe Airport**.** The United States Geological Survey (USGS) in their investigation of groundwater resources has defined the Palo Verde Valley groundwater sub-basin (hereafter Valley Basin) to be coincident with the floodplain of the Colorado River and the Palo Verde Mesa groundwater sub-basin , to be coincident with the mesa above the floodplain to the west (**Figure 1**). The numerical groundwater model developed in response to the COCs is inclusive of both these groundwater sub-basins west of the Colorado River and is hereafter the "Palo Verde Valley Groundwater Model". Additionally, reference to Palo Verde Valley in this document will include both the floodplain and mesa areas.

Condition of Certification SOIL&WATER-2 stipulates that the Project shall offset the potential effects of groundwater pumping as it may increase recharge from surface water to groundwater from the Valley Basin to the Mesa Basin. The Valley Basin is present to the east and contains the surface water features referenced in Condition of Certification SOIL&WATER-2, including canals and drains that are managed by the Palo Verde Irrigation District (PVID) and the Colorado River, which is about 10 miles east from the Project. The significant component of groundwater recharge in the Valley Basin is deep percolation from agricultural irrigation water in the floodplain, whereas the significant component of outflow is the discharge of groundwater back to the Colorado River through the PVID drains. Condition of Certification SOIL&WATER-16 requires that a numerical groundwater flow model be developed to evaluate the increase in recharge from surface water features that are located in the Valley Basin. The development of potential offset options and a plan of implementation is not part of this document and will be submitted separately as required under Condition of Certification SOIL&WATER-2 to the CEC Compliance Project Manager.

In the development of the Palo Verde Valley Groundwater Model, a site conceptual model (SCM) of the Palo Verde Valley was developed from a review of available literature and surface water and groundwater data from PVID, the United States Bureau of Reclamation (USBR), and USGS, and additional field investigations of the Project site. From the SCM, a calibrated two-dimensional computer-based numerical model of the younger and older Colorado River alluvium in the Palo Verde Valley (floodplain and mesa) was constructed using MODFLOW-2000 (McDonald and Harbaugh 2000).

1.1 Project Description

The Blythe Solar Power Project site is located in the southern California inland desert, approximately 8 miles west of the city of Blythe and 2 miles north of Interstate Highway 10

(I-10) in Riverside County, California (**Figure 1**). The Project will be located on a 7,541-acre right-of-way (ROW) on Federally-controlled public lands managed by the U.S. Bureau of Land Management (BLM), pursuant to an ROW grant issued to PVSI from BLM and the parallel thermal electric power plan license to be issued by CEC.

The Project is a commercial solar thermal power generating facility. The total Project Disturbance Area (the Project facilities footprint plus additional areas that will be disturbed by construction and operation) will be 7,025 acres. The Project will have a nominal output of 1,000 megawatts (MW) consisting of four independent 250-MW power plants (Units #1, #2, #3, and #4). The units will be developed in phases, with construction scheduled to begin in late 2010 on Unit #1; that unit will come on line in mid-2013, and subsequent units will come on line in each of the following 3 years.

Each of the four units will have its own solar field using parabolic trough technology that involves rows of parabolic mirrors with piping containing a heat transfer fluid (HTF) at the focal point of the parabola. Each unit will have its own power block, centrally located within the solar field. Each power block will have its own HTF pumping and freeze-protection system, solar steam generator, steam turbine generator, air-cooled condenser (dry cooling tower), and ancillary equipment (e.g., water treatment system and emergency generators). Each power block will have two 4-acre evaporation ponds to manage the cooling tower blow-down stream (a portion of the continuously circulated cooling water discarded to prevent the excessive buildup of salts). Two Land Treatment Units (one 12-acre and one 4-acre) will be used to bio-remediate or land farm soil contaminated by release of HTF. Each unit will have a natural gas-fired auxiliary boiler; natural gas will be supplied by a new 10-mile (2 miles off site) pipeline connecting to an existing Southern California Gas main located south of I-10. Water for the Project will be supplied from on site wells.

The Project will require a new double-circuit 230-kilovolt transmission line to interconnect Project electrical output with the Southern California Edison (SCE) regional system. Transmission line features (e.g., crossing structures, pole pads, crane pads, pull sites, splice sites, spur roads, and an access road) will be located along an 8-mile transmission line corridor that extends south from the Project site to a point south of I-10 and then turns west. The transmission line will be connected to the planned Colorado River Substation, which will be developed by SCE as part of upgrading its transmission network to support integration of renewable energy projects. Development of the substation will be the responsibility of SCE.

Access to the Project site will be via a new road heading north from the existing frontage road that parallels I-10. Only a small portion of the overall facility footprint will be paved, primarily the site access road, the service roads to the power blocks, and 6 acres of each of the 18-acre power blocks. The solar fields will be compacted earth but will remain unpaved and without a gravel surface to prevent mirror damage. Soil and water stabilizers will be used to reduce dust deposition on the collectors and minimize soil erosion. The perimeter of the Project site will be secured with chain-link metal-fabric security fencing and controlled-access gates.

1.2 Project Phasing

Project construction will occur in phases that follow development of the solar units, beginning with Units #1 and #2 in the north portion of the Project site. Construction of Units #1 and #2 will be further subdivided into Phases 1a and 1b to facilitate development beginning in the fall of 2010 through the first half of 2011.

Phase 1a will consist of two types of construction areas, which are (1) linear facilities, including the access road, gas line, and communication lines and (2) nonlinear facilities to include a staging/laydown area, the Unit #1 power block, and a portion of the Unit #1 solar field. The total disturbance area proposed for Phase 1a is less than 10 percent of the total area for the Project and constitutes those critical Project areas that need to be constructed in 2010 and early 2011. Phase 1b will include remaining portions of Unit #1 as well as Unit #2 and the gen-tie line. Phase 2 will include all of Units #3 and #4.

Descriptions of the facilities to be constructed during the remaining phases of the Project, as well as the related acreages for each phase are summarized in **Table 1**.

1.3 Project Water Use Requirements

The Project proposes to use dry cooling in the steam cycle for power plant cooling. Water for cooling tower makeup, process water makeup, and other industrial uses such as mirror washing will be supplied by up to 10 on-site wells, most located northern and southern ends of the four power blocks (**Figure 1**). This groundwater source will also be used to supply water for employee use (e.g., drinking, showers, sinks, and toilets).

The Project will use about 4,100 af over the construction period.[1] The construction phase water demand is primarily for soil compaction and fugitive dust control. The Project will use about 600 afy (150 afy per 250 MW unit) of groundwater upon full build out of the four units for operations, which equates to an average pumping rate of about 390 gallons per minute (gpm). Over the Project's 30-year operational life, water use will total about 18,000 af. In total, about 22,100 af of water will be used for the Project.

Groundwater wells will be completed in the older alluvial deposits of the Colorado River above the Bouse Formation under permits from the County of Riverside.

1.4 Report Organization

The report was prepared following the requirements of SOIL&WATER-16. The following is a summary of the various sections that makeup this report.

1. A yearly volume of 713 af equates to an average pumping rate of about 440 gpm of water for construction activities (assuming a continuous uninterrupted supply and continuous usage).

1.0 - Introduction	Outlines the CEC condition requirements and purpose of the numerical groundwater model. Provides the Project description and general approach to the model development and execution.
2.0 - Previous Investigations	Presents and summarizes the prior investigations conducted for the Palo Verde Valley pertinent to the development of this groundwater model. Summarizes the available data gathered from PVID, USBR, and USGS, and summarizes the additional Project site investigation work conducted in support of model development.
3.0 - Site Conceptual Model	Establishes the hydrogeologic framework for the Palo Verde Valley and the Mesa and Valley Basins. Presents the hydrostratigraphy, structure, aquifer distribution and physical properties, and the groundwater balance.
4.0 - Model Setup and Calibration	From the conceptualization of groundwater flow and budget this section defines the model domain, boundary conditions and grid layout and presents the results of model calibration. Describes steady-state calibration to groundwater conditions from 1980 to 2009.
5.0 - Model Simulations	Presents the results of model simulations using the calibrated model to assess the impacts from Project pumping at the end of 30 years of operation.
6.0 - Sensitivity Analysis	Following the calibrated simulations, this section presents the results of a broad sensitivity analysis of selected model parameters.
7.0 - Conclusions	Presents the conclusions of the numerical groundwater model and the estimate of impacts from Project pumping on surface water recharge to the Mesa Basin.
8.0 - References	References cited in the preparation of this report.

2.0 PREVIOUS STUDIES AND SUMMARY OF AVAILABLE DATA

The SCM which provides the basis for the numerical groundwater model was developed through a review and interpretation of previous investigations, available groundwater, and surface water data through PVID, USBR and USGS, and most recently additional investigations conducted on the Project site. This section describes the significant studies that have been conducted in the Palo Verde Valley, largely the work of Metzger and others (1973) and Owen-Joyce (1984) and Owen-Joyce and Kimsey (1987), and the available information gathered through access to online database information through the USGS and USBR and information provided by the PVID on surface water flow and groundwater levels in the Palo Verde Valley. Lastly, this section describes the recent surface geophysical investigation completed at the Project site to assess subsurface conditions, depth to bedrock and the depth of groundwater and estimate of flow direction below the Project site.

2.1 Summary of Previous Studies

The following are the principal documents that describe subsurface conditions, the water balance in the Palo Verde Valley, and present an estimate of depletion of the Colorado River, and were drawn upon in the development of this numerical groundwater model:

- Metzger, D.G., O.J. Loeltz, and I. Burdge, 1973, Geohydrology of the Parker-Blythe-Cibola Area, Arizona and California, Water Resources of the Lower Colorado River – Salton Sea Area, U.S. Geological Survey Professional Paper 486-G.
- Owen-Joyce, S.J., 1984, A Method for Estimating Ground-Water Return Flow to the Colorado River in the Palo Verde Cibola Area, California and Arizona: U.S. Geological Survey Water -Resources Investigations Report, 84-4236, 48p.
- Owen-Joyce, S.J. and S. L. Kimsey, 1987, Estimates of Consumptive Use and Groundwater Return Flow using Water Budgets in Palo Verde Valley, California: U.S. Geological Survey Water -Resources Investigations Report 87-4070, 50 p.
- Leake, S. A., W. Greer, D. Watt, and P. Weghorst, 2008, Use of Superposition Models to Simulate Possible Depletion of Colorado River Water by Ground-Water Withdrawal - Scientific Investigations Report 2008-5189 (Prepared in Cooperation with the Bureau of Reclamation): U.S. Geological survey, Reston, Virginia, 25p.

A summary of these documents and their application of information and interpretation toward the development of the SCM and the Palo Verde Valley Groundwater Model are provided below:

Metzger and others 1973. The most comprehensive hydrogeologic investigation of the Palo Verde and Cibola Valleys was provided by Metzger and others (1973). In their study of hydrogeologic conditions they provide both hydrostratigraphic data on the distribution of aquifer units, including the Recent- and Quaternary-age Younger and Older Colorado River fluvial deposits, Pliocene-age Bouse Formation and Miocene-age Fanglomerate and their associated

aquifer properties, including estimates of transmissivity and groundwater storage. Lithologic data from the well logs along with cross sections through the Palo Verde Valley were used to define the distribution of aquifer units, estimate distribution of hydraulic conductivity, in the development of the model domain, and the vertical and lateral boundaries of the Colorado River alluvium. Aquifer test data was summarized for the Palo Verde Valley and the data graded average or good by Metzger and other s (1973) were used in the analysis of the spacial distribution of transmissivity within the Colorado River alluvium.

According to Metzger and others (1973), sources of recharge to the Mesa and Valley Basins are the Colorado River, precipitation, and underflow from adjacent areas, including the Parker and Chuckwalla Valleys. They developed a water budget for the Palo Verde Valley, providing estimates of underflow from the Parker area, Chuckwalla Valley and Milpitas Wash, an estimate of the Colorado River depletion over the period of 1957-1966, along with estimates of consumption from irrigated crops, native vegetation and evaporation from surface water. Metzger and others (1973, Table 4) concluded from gauging data of river flows data from 1957-1966, that the Colorado River lost water to the groundwater system at an average of 361,000 afy. This estimate was derived based on a comparison of discharge data at the Palo Verde Dam, including the diversion to PVID, to the discharge data at the Cibola gauging station south of the Palo Verde Valley. The differences between the two flows showed a higher flow at the Palo Verde Dam, inclusive of the diversion by comparison to the Cibola gauge, suggesting loss of water from the river between the stations. From these data, Metzger and others (1973) showed an imbalance in the Palo Verde and Cibola Valleys and an annual loss estimate of 86,000 afy for the Valley, based largely on the imbalance of crop consumption and evapotranspiration (ET) exceeding recharge (or loss) from the River.

Owen-Joyce 1984. The document presents a methodology to estimate groundwater return flows to the Colorado River through the accounting of consumptive use as required under Article V of the decree for the Colorado River. Owen-Joyce indicates in the contrary to Metzger and others (1973) that there is an increase in flow between the gauge below Palo Verde Dam and south of the Cibola Valley that gaining conditions exist along the reach of the river within the Palo Verde Valley largely in the area immediately adjacent to the river. This observation was made without adding the diversion at the Palo Verde Dam, which was included by Metzger and other s (1973). Owen-Joyce (1984) indicated that recharge in the floodplain was largely through canal seepage, underflow from the Mesa Basin and loss from the Colorado River.

In the analysis of gaining and losing conditions along the river, shallow water level data for 1981 largely from PVID wells, was presented that showed a groundwater divide exists in the shallow aquifer about one-half and one mile west of the Colorado River. The groundwater east of the divide discharges to the river and west of the divide groundwater flows away from the river toward the PVID drains. Groundwater west of the divide discharges to the shallow PVID drains aligned generally south parallel with the river. Water from these drains eventually discharges to the river outside of the Palo Verde Valley.

Using measurements of diversion and return flow to the river, along with estimates of inflow from the mesa area, tributary runoff (after Metzger and others, 1973) and seepage and evaporation from canals, consumptive use for the area west of the divide was estimated to be about 452,000 af. This was balanced with a groundwater return flow through the drains west of the drainage divide of 419,500 af. In the water balance west of the divide, Owen-Joyce also used estimates of inflow and out from the Mesa Basin of 9,500 af and 4,700 af respectively, and an assumption of seepage out of the diversion canals of 122,000 af. The canal seepage term was the only value used in the water balance to represent return flows to the groundwater from surface water diversion for irrigation. Owen-Joyce did not provide an estimate of deep percolation of surface water applied for irrigation.

Applying the difference between the surface water diversion and consumptive use plus surface water return to the river, groundwater return to the river east of the divide was measured at 23,000 af for the reach in the Palo Verde Valley and 5,200 af for the Cibola Valley.

Owen-Joyce and Kimsey 1987. This document represents an update of the work performed by Metzger and others (1973) and Owen-Joyce (1984) on the water balance within the Valley Basin or flood plain. Consumptive use by vegetation within the Palo Verde Valley and groundwater return flows to the river were estimated for the period between 1980 and 1984. Consumptive use by vegetation was estimated using difference in diversion less return of water through PVID and less the change in storage. Following this approach:

- Consumptive use ranged between 364,000 and 484,000 afy.
- Groundwater return flows to the Colorado River were estimated at between 2,500 afy and 31,700 afy.

These numbers differ from the values estimated by Metzger and others 1973, who estimated that the Colorado River lost an average of 361,000 afy (1955-1966). However, Owen-Joyce and Kimsey (1987) acknowledge that portions of the river show both gaining and losing conditions relative to the river stage, and note that most reaches of the river gain water when the downstream reservoir requirements are met.

Mapping of average water level data from shallow monitoring wells installed by PVID from 1982 to 1984 confirmed the groundwater drainage divide noted in 1981 (Owen-Joyce 1984) within the shallow aquifer west of the river. Showing historical data between 1982 and 1984, the divide responds moving east and west relative to changes in river stage and amount of water applied for irrigation. Groundwater east of the divide was shown to move back toward the river, and groundwater west of the divide was shown to move west toward the mesa. Water level data for the shallow aquifer for 1983 reveal that the river is losing water to the aquifer generally along the entire length of the river east of the groundwater divide. Changes in water levels for the period between 1982 and 1984 show that changes in groundwater elevation in the Valley Basin vary in accordance to irrigation return and thus applied water and consumptive use west of the groundwater divide and in response to the river stage east of the groundwater divide.

Leake and others 2008. In their analysis of the potential depletion of the Colorado River from groundwater withdrawl, Leake and others (2008) developed a two-dimensional superposition groundwater model using MODFLOW (MacDonald and Harbaugh 2000) inclusive of the Palo Verde and Cibola Valleys and the Chuckwalla Valley. The development of the model included a statistical analysis of aquifer test data from 25 locations along the Colorado River above Yuma and below Parker, which produced a log-normal distribution of transmissivities with a lower bound value (0.05) of 6,300 feet squared per day (ft^2/d) and a mean value (0.50) of 26,000 ft^2/d. The model developed is a simple two-dimensional model, employing a simple vertical geometry and large grid spacing, and a uniform saturated thickness of 500 feet throughout the model domain to evaluate the impacts from groundwater pumping on depletion of the Colorado River.

The Colorado River was simulated using the River Package in MODFLOW-2000 and the river stage was set an elevation of zero throughout the domain with an average river-bed conductance term in the Parker-Palo Verde-Cibola area assumed to be 2.3E5 ft^2/d. Using an assumption of a well pumping for 100 years at 1,200 afy (or twice the Project proposed annual rate), simulations using a transmissivity values of 6,300 ft^2/d and 26,000 ft^2/d, produced river depletion estimates of between 10% to 50%, respectively for wells located on the Project site (Leake and others, 2008, Figures 12 and 13). The results from this assessment are considered very conservative and physically implausible given the nature of the superposition model was to render the water table and river stage flat, and not consider sources of recharge to the model domain other than storage and river return, most specifically mountain front recharge , groundwater underflow and irrigation return from PVID diversion. Without recharge from other sources including agricultural return, pumping would tend to preferentially focus on drawing water from the river.

Information on the aquifer properties of transmissivity and storage from Leake and others (1973) were considered in conjunction with Metzger and others (1973) and from aquifer testing performed as part of Project licensing to develop the conductivity distribution for the numerical groundwater model.

2.2 Summary of Available Information

There are over 500 wells that have been drilled and installed in the Mesa and Valley Basins, though there is little attendant hydrogeologic information, such as well completion interval or yield history, boring logs or pumping test data. In the Mesa Basin, there are a total of 82 wells based on the current USGS NWIS database count and most of these wells have been installed as irrigation or industrial supply wells, while in the Valley Basin most of the wells are shallow drive-point wells (268) that are used to understand the response to surface water diversion and irrigation return or municipal supply wells in the City of Blythe. A significant percentage of wells on the Mesa have been abandoned along with a reduction in agricultural activities beginning in the early 1980s. In the search of available well completion data, and to provide well performance, groundwater quality and current and historic water level information to assess flow with the Mesa and Valley Basins the following database were consulted and information summarized in the following Appendices.

Appendix A Provides a summary of water level and well completion data from the USGS National Water Information System (NWIS) Groundwater Database (USGS 2010a) for wells in the Palo Verde Valley from 1980 to 2010. Additional well completion data was also taken from DWR Bulletin 91-23. . Depth to water and well construction data were available for 245 wells within the Palo Verde Valley. Of the 245 wells, only 30 had depth to water and the screen interval, 140 wells had depth to water and total depth of the boring, but no screen intervals, and the remaining 75 wells had only depth to water readings. All wells had a ground surface elevation, but in the majority of the elevations were from a USGS topographic map. See **Figure 2** for locations of wells where there was available information in the USGS database.

Appendix B Summary of groundwater quality data from the USGS (2010a) NWIS Groundwater Database for wells in the Palo Verde Valley from 1980 to 2010.

Appendix C Surface water elevation and gauging data in the USGS (2010b) Stream Stats Website (http://water.usgs.gov/osw/streamstats/) for the Colorado River as available from 1957 to 2010 for stations along the river including PVID spills and returns and the gauge at the south end of Cibola Valley. See **Figure 3** for the location of stations where there was available data along the Colorado River.

Appendix D Summary of data on depth to groundwater for 268 "well points" used to monitor the water table throughout the valley provide by PVID. The "well points" consist of a 3/4-inch iron pipe driven between 9 and 12 feet into the ground. Depth to water data was available from 1992 to 2010. See **Figure 4** for the location of the "well points".

Appendix E Diversion data for the PVID inclusive of the total diversion, diversion to the Valley and Mesa Basins, spill and drain return and total return to the Colorado River for the period between 1993 and 2009. See **Figure 5** for the location of 253 miles of diversion canals and 153 miles of return drains within the Palo Verde Valley.

In addition to these sources of information, river transect data from the USBR (personal communication John Nickell, August 2010) that provided profiles of the Colorado River from Palo Verde Dam to Cibola Valley were used to provide an accurate representation of the river bottom within the numerical model.

The annual reports provided by the USBR (1993-2009) on the Lower Colorado River Accounting of surface water, which included PVID diversions and return flows, consumption and estimates of ET for non-native vegetation along the river, were used to compare to other estimates and support the analysis of groundwater balance within the Palo Verde Valley. The information in the USBR reports showed that:

- For the period between1993 and 2009 the consumptive use for the Valley Basin ranged from about 325,000 afy to 541,000 afy,
- Between 2003 and 2009, the unmeasured return or groundwater return flow back to the river varied from 45,000 afy to 54,000 afy, and
- The ET for non-native vegetation (2003-2009) along the river reach within PVID averaged about 8,500 afy.

These values are generally within the range estimated by Owen-Joyce (1984) and Owen-Joyce and Kimsey (1987), and were considered in the evaluation of the water balance for the Palo Verde Valley as described in Section 3.0.

2.3 Additional Project Site Investigation

A geophysical investigation was conducted during the final procedural elements of the licensing process for the Project in August 2010 **(Appendix F**). The geophysical program consisted of both seismic refraction and transient electromagnetic (TEM) surveys conducted within the Project ROW to better understand the depth of bedrock and depth of the water table**.** The seismic refraction was used to measure depth of water and comprised an array of 15 100-foot long seismic refraction lines containing 24 geophones and comprised of three-shot locations (i.e., energy source) within the ROW. These locations were supplemented by 24 TEM locations scattered along the lines and within the ROW. TEM uses a pulsed magnetic field to generate a secondary magnetic field within the surface that decays over time. The decay rate is related to the relative resistivity of the formation materials and thus can be used to identify lithology distribution both laterally and vertically and to assess the salinity of the groundwater. The TEM data were calibrated to subsurface geophysical logs gathered as part of the well installation program completed for the licensing phase of the Project (AECOM 2009).

The data from the seismic lines reveal that the water table is at a depth of about 350 feet near the McCoy Mountains on the western portion of the ROW, and about 200 feet near the eastern boundary of the ROW. The data show that the groundwater flows from west to east across the Project site, generally moving from the McCoy Mountains toward the Valley Basin. This direction of flow would lend to the interpretation that mountain front runoff is an important source of water for the Mesa Basin. The TEM survey indicates that the older Colorado River alluvium likely has a higher clay content than the shallow alluvial units and that the total dissolved solids concentration of the groundwater is about 1,500 milligrams per liter (mg/L) or higher. Based on the contrast in resistivity from the TEM survey it is interpreted that the yield from the Colorado River alluvial sediments would be higher on the central and eastern portion of the site and that areas west of Black Creek Road or the west central portion of the site may not be as productive. Depth to bedrock varies across the site, with bedrock being shallow near the McCoy Mountains and getting deeper to the east where it reaches a depth of about 2,000 feet bgs at the eastern boundary.

3.0 HYDROGEOLOGY AND CONCEPTUAL FLOW MODEL FOR PALO VERDE VALLEY

The SCM establishes the framework for the numerical groundwater model, through the definition of aquifer geometry and its characteristics and the horizontal and vertical movement of groundwater. The focus of the SCM are the younger and older Colorado River alluvial sediments, as these units represent the primary source of water supply to the area, are the source of groundwater supply to the Project and are directly influenced by recharge from irrigation return and discharge from the Colorado River. These aquifer units were selected for the analysis as there are available groundwater data from which to develop a SCM, whereas there are no or very limited information on the deeper alluvial deposits below alluvial deposits of the Colorado River in the Palo Verde Valley. To establish the impacts from Project pumping, the framework of the SCM includes the Palo Verde Valley and Palo Verde Mesa geographic areas with the coincident two groundwater sub-basins, the Valley Basin inclusive of the flood plain or valley adjacent to the Colorado river and the Mesa Basin, high lands the west of the flood plain (**Figure 1**).

3.1 Physiography

The Palo Verde Valley (mesa and flood plain) is located in the northwestern Colorado Desert, which is part of the greater Colorado Desert Geomorphic Province. The Colorado Desert Province is characterized by isolated mountain ranges separated by broad alluvium-filled basins of Cenozoic-age sedimentary and volcanic materials overlying older rocks. Much of the Colorado Desert lies at low elevations, with some areas below sea level. The area is characterized by barren mountain ranges and isolated hills with broad alluvial-filled valleys. The Palo Verde Valley is bounded by non-water-bearing rocks of the Big Maria and Little Maria mountains on the north, by the McCoy and Mule Mountains on the west, and by the Palo Verde Mountains to the south (**Figure 1**). The McCoy Mountains and the Big Maria Mountains are the contributing watersheds to the Palo Verde Mesa. McCoy Wash, a tributary of the Colorado River, flows southeast at the northeastern-most part of the site. Surface water drains from the surrounding mountains toward the Colorado River. There are no perennial streams on the mesa.

The mesa has a generally low relief until near the surrounding mountains (McCoy, Big Maria, and Little Maria Mountains). There are two distinct river-cut terraces that form a topographic break westward from the Colorado River. The Project is located on the uppermost of the two terraces. Approximately three miles east of the eastern site boundary, a sharp break in the slope forms the boundary between the mesa and flood plain, which is 80 to 130 feet below the mesa. In this region, the Palo Verde Valley is roughly equivalent to the recent historic floodplain of the Colorado River. The mesa encompasses an area of about 353 square miles or 226,000 acres (DWR 2004a).

The flood plain area of the Palo Verde Valley covers approximately 200 square miles or 128,000 acres (DWR 2004b). The flood plain is that part of the Palo Verde Valley that has been covered by floods of the modern Colorado River prior to the construction of Hoover Dam. The elevation

of the flood plain near Parker, Arizona is approximately 360 feet above sea level (asl) and slopes to approximately 210 feet asl below Cibola. This is a slope of about 150 feet in about 70 miles or about 0.005 feet per mile. The flood plain is wider than the meandering course of the Colorado River and is bounded by terraces on both the western (California) and eastern (Arizona) sides of the plain (Metzger and others 1973). The flood plain is approximately 3 miles wide at the Palo Verde diversion Dam and increases to about 9 miles at the widest point of the valley. The valley narrows to between three and four miles wide at Cibola and then to less than one mile in the bedrock narrows below Cibola (Metzger and others 1973).

3.2 Climate

The climate in the Palo Verde Valley is classified as a "low desert", is characterized by high aridity and low precipitation. The region experiences a wide variation in temperature, with very hot summer months with an average maximum temperature of 108 degrees Fahrenheit (ºF) in July and cold dry winters with an average minimum temperature of 66.7 ºF in December. The Blythe area receives approximately 3.5 inches of rainfall per year (CIMS Reference ETo Zone 18). The majority of the rainfall occurs during the winter months, but rainfall during the late summer is not uncommon. The summer rainfall events tend to be a result of tropical storms that have a short duration and a higher intensity than the winter rains. Annual precipitation ranges from 0.02 to 0.47 inches per month for a total annual precipitation of just under four inches per year. All weather data (1913 to 2008) is from the reporting station at the Blythe Airport, located approximately one mile southeast of the Project site.

3.3 Geology of Palo Verde Valley

The Project is located on the mesa in the alluvial-filled basin of the Palo Verde Valley (**Figure 6**). Regionally, this valley formed as a structural depression or a pull-apart basin and is composed of two broad geologic units, consolidated rocks and unconsolidated alluvium (California Division of Mines and Geology 1967). The consolidated rocks consist of pre-Tertiary age igneous and metamorphic rocks, which form the basement complex, and in some locations, Tertiary-age volcanic rocks that overlie the basement complex. The consolidated rocks are nearly impermeable except for areas where fracturing or weathering has occurred. It is uncertain the extent that these rocks yield water to the alluvium. The flux of groundwater into and out of the bedrock is unknown, and as such has been treated as non-water bearing in the development of the groundwater model.

As part of the modeling effort, a study of the depth to bedrock in the Parker, Palo Verde and Cibola Valleys was conducted (**Appendix G**). This study used gravity data compiled from several USGS projects to render an interpretation on the depth of the bedrock in the Palo Verde Valley. The study indicated bedrock depths were generally deepest under the flood plain (depths range from about 900 to a maximum of 2,400 feet bgs, with an average depth being about 1,400 feet bgs). Under the piedmont areas or below the mesas east and west of the river, depth to bedrock ranges from 300 to 600 feet bgs. The configuration of the bedrock suggests a north-south elongate valley roughly paralleling the river course.

3.3.1 Hydrostratigraphy

The geologic units that are important in an evaluation of the water resources in the Palo Verde Valley are thought to be the Miocene-age fanglomerate, the Bouse Formation, and the fluvial deposits of the Colorado River.

3.3.1.1 Fanglomerate

According to Metzger and others (1973), the Miocene-age fanglomerate is made up chiefly of cemented gravel composed of poorly-sorted pebbles and some fine-grained material with a provenance from a nearby source. The fanglomerate represents composite alluvial fans deposits that built up from local mountains as the fans prograded toward the valley. Because the fanglomerate was deposited on an irregular surface having considerable local relief, it varies widely in thickness. Locally, the fanglomerate may be absent, but at some places (e.g., Milpitas Wash area), it is at least 2,100 feet in thickness. Near Parker, Arizona, wells with specific capacities as much as 15 gallons per minute per foot of drawdown (gpm/ft) have been reported in the fanglomerate. In contrast, well 11S/21E-5F1, installed by the Southern Pacific Company located in Milpitas Wash produced only about 0.01 gpm/ft from a well that is an open hole completed in the fanglomerate from 286 to 752 feet below the ground surface (bgs).

3.3.1.2 Bouse Formation

The Bouse Formation is of Pliocene age and is composed of a basal limestone and tufa overlain by interbedded clay, silt, and sand with minor amounts of gravel. The Bouse sediments were deposited in an embayment of the Gulf of California. The thickness of the formation is relatively uniform throughout the area and was measured at 767 feet in thickness in a well LCRP-27 drilled by the USGS (located in Parker Valley, AZ approximately 10 miles north of the Palo Verde Diversion Dam). Metzger and others (1973) indicated that in general, the Bouse Formation yields very limited quantities of water. The exception is in the upper part of the Bouse Formation, which is composed mostly of sand, where it is reported to yield water at moderate rates. Well LCRP 27 was completed in this sandy zone and had a reported specific capacity of 13 ½ gpm/ft. In Test Well TW-2 located on the mesa and the Project site, encountered the Bouse Formation at a depth of about 480 feet bgs to a depth of about 600 feet where the well boring was terminated (**Figure 7**). The formation consisted of a gravely clay from 480 to 490 feet bgs, underlain by interbedded clay, silt and very fine to fine grained sands to the borings total depth of 600 feet bgs. The test well was not completed in the Bouse Formation, as sediments were observed to be generally very-fine grained and well cemented and did not appear in the core to be saturated.

3.3.1.3 Fluvial Deposits of the Colorado River

Metzger and others (1973) divided the groundwater aquifer in the flood plain into three zones: shallow, primary gravel and deep based on a simplified geologic setting. The shallow zone is generally defined as the younger alluvium, which is underlain by the younger alluvium gravel (hence primary gravel zone), which is underlain by the older alluvium, the Bouse Formation and Fanglomerate. Metzger and others (1973) defining the deep zone to include these three water bearing formations.

Older Alluvium of the Colorado River

The older alluvium is generally comprised of a basal gravel above the Bouse Formation overlain by inter-layered sequences of sand and pebbly sand, with lenses of cobble gravels and silt and clay. In the Blythe area, this sequence has been measured as much as 600 feet in thickness (Metzger and others 1973). The older alluvium forms the mesa above the flood plain and is encountered below the younger alluvium on the flood plain. In the mesa area west of the river, the younger alluvium is absent and the older alluvium consists mostly of finer grained materials (very fine to fine grained sands with interbedded silts and clays). In Test Well TW-2, the bottom of the older alluvium was encountered at 480 feet bgs and the lithology was predominantly fine-grained sand with minor amounts of interbedded silts and clay.

Municipal wells located on the flood plain within the City of Blythe boundaries, are generally completed between 100 and 350 feet bgs with a short (< 100 feet) perforated zone in the older alluvium. These wells generally produce between 250 and 750 gpm (Metzger 1973, DWR 1978). One well, City of Blythe Well 11, is completed between 421 and 505 feet bgs in the Older alluvium and produces 2,000 gpm.

Younger Alluvium of the Colorado River

The younger alluvium occurs below the flood plain and is composed of a basal gravel overlain by sand. The younger alluvium is generally thought to be between about 90 to 125 feet in thickness above its basal gravel, which can be between 5 and 20 feet thick (Metzger and others, 1973). Apart from the limited occurrence of the basal gravel, the contact between the older and younger alluvium is not distinguishable. Owens-Joyce (1984) indicated that the younger and older alluvium is hydraulically connected in the Palo Verde Valley. In well 6S/23E-32E1, located approximately ½-mile west of the City of Blythe, the bottom of the Colorado River fluvial deposits, inclusive of the younger and older alluvium reportedly occurs to a depth of about 506 feet bgs.

Figure 8 is a generalized interpretation of the distribution and thickness of the Colorado River sediments, inclusive of the younger and older alluvium within the Palo Verde Valley. The map was developed from the interpretation of boring logs and the east-west and north-south cross sections contained in Metzger and others (1973) and additional lithologic data gathered from the investigation of the Project site during the licensing phase of the development. The isopach map shows these sediments are an elongate deposit coincident with the north-south axis of the Colorado River and are the deepest along the central axis of the valley, thinning in the direction of the mesa and toward the bedrock outcrops. The older alluvium pinches out slightly north of the Palo Verde Diversion Dam and at the entrance to Cibola Valley where the younger alluvium has been mapped at a thickness of less than 200 feet (Metzger and others 1973, Owens-Joyce 1984). The younger alluvial sediments thin further in a southward direction below the Cibola Valley above the narrows.

3.3.2 Structure

In the Palo Verde Valley there are not significant structural features that are barriers to groundwater flow (**Figure 6a and Figure 6b**). Metzger and others (1973) did not identify significant structural features in the older alluvial sediments and piedmont gravels in the mesa and younger rock units, other than several slump blocks bordering the flood plains. Faulting was only observed in Hart Mine Wash, located southeast of Cibola and outside the Palo Verde Valley. The faults in this area have been interpreted as small normal faults and are concealed by piedmont gravels (Metzger and others 1973). The driller's logs reviewed by Metzger and others (1973) in their development of a north –south cross-section through the flood plain indicate slight down warping of the valley centered in the area of the City of Blythe. This down warping generally follows the interpretation of the thickness of the Colorado River sediments as shown on **Figure 8**.

3.4 Groundwater Occurrence and Flow

Over 500 wells have been completed in the Valley and Mesa Basins, with the significant majority completed in the younger and older Colorado River alluvium (**Figures 2 and 4**). To evaluate the groundwater occurrence and horizontal and vertical movement within the Colorado River alluvium and between the Valley and Mesa Basins, groundwater information provided by PVID and the USGS were compiled and organized into shallow and deep wells based on their completion depth. In general, all shallow well are completed in the younger alluvium and are comprised of the shallow PVID well points. While deep wells are completed below this shallow zone and a depth of about 30 feet in both younger and older alluvium either in the Valley or Mesa Basin above the Bouse Formation

Shallow wells were completed between the water table and a depth of about 30feet bgs. Thirty-nine (39) wells in the USGS database and all of the PVID well points (268) on the floodplain were classified as shallow wells, and all the shallow wells were located in the Valley Basin. The approximate 30 foot depth was chosen as the basal depth in the selection of shallow wells as Metzger and others (1973) indicated the natural groundwater elevation before irrigation was likely between 15 and 25 feet bgs, and wells at this depth are in direct communication with the Colorado River (USBR transects 2010) and drains in the PVID irrigation system responding to seasonality in river flow and irrigation.

One hundred twenty-six (126) wells were classified as deep wells based on their well completion information, which at times only included the total depth of the pilot boring. The majority of deep wells are completed in the vicinity of the City of Blythe and the central portion of the flood plain and in the Mesa Basin above the flood plain.

3.4.1 Groundwater Occurrence

Groundwater in the Valley and Mesa Basins occurs under generally unconfined conditions or water table conditions and within the younger and older alluvium of the Colorado River (Owens-Joyce 1984). Metzger and others (1973) report that wells completed through the Bouse

Formation and into the fanglomerate contain water under artesian conditions. Because there is limited data on deeper water-bearing sediments below the Colorado River sediments, the discussion on groundwater occurrence and flow will focus on the younger and older alluvium in the Valley and Mesa Basins. The Valley Basin contains both the younger and older alluvial deposits west of the river, while in the Mesa Basin, the younger alluvial sediments are absent with only the older alluvial sediments serving as the principal aquifer.

3.4.1.1 Valley Basin

The majority of the groundwater wells installed on the flood plain are for monitoring groundwater levels within the PVID. Wells for domestic water supply (City of Blythe) and industrial purposes are generally located in close proximity to the City of Blythe. For the flood plain area, groundwater level data is available as far back as the late 1940's. A review selected hydrographs of groundwater levels throughout the flood plain (including those measured in Parker Valley, Arizona) revealed that the groundwater levels have generally varied less than about five feet over this time period and most vary less than three feet (**Figure 9**).

The stability of the flood plain groundwater system can be attributed to the irrigation methods used in the flood plain area and the associated drains that manage the shallow groundwater back to the Colorado River. The diversion of Colorado River water is the main source of irrigation water for the flood plain. From the diversion at Palo Verde Dam, water is directed throughout the flood plain via both lined and unlined canals. Water from these canals is applied to the land surface either by opening a weir or pumping water from the canals to flood the land to be irrigated. The canals are generally less than 10 feet deep and are not in contact with underlying shallow groundwater. If water has not been diverted for irrigation it travels through the canals and is returned to the Colorado River via several "spills" along the western bank of the river. A system of drains, generally between 15 and 20 feet deep intersect the water table and return deep percolation from irrigation to the Colorado River at several spill locations, generally at the south end of the Palo Verde Valley and in the northern end of Cibola Valley. The drains serve to regulate and generally stabilize the depth of the groundwater in the flood plain at the current level of approximately 10 feet bgs. This drain system has been expanded several times since the early 1960's to facilitate better drainage of the irrigated lands to achieve the current depth to water (Metzger 1973, PVID 1969, PVID 2009 [PVID references to district acreage maps]).

Groundwater in the Valley Basin is generally encountered at about 270 feet asl in the northern flood plain and 220 feet asl in the south. The depth of groundwater in the shallow wells is about eight feet and 19 feet in the northern and southern parts of the flood plain. The deeper wells show a depth to groundwater ranging from about seven feet to 20 feet bgs by comparison. Where side-by-side comparison can be made there is only about a one foot difference in the water levels in the shallow and deep wells. This minor difference does not suggest a significant vertical gradient and is consistent with the interpretation that the groundwater in the flood plain occurs under generally unconfined or water table conditions in the Colorado River alluvium. The similarity in water level and general similarity in lithology would indicate that the younger and older alluvium should be considered a single aquifer unit.

3.4.1.2 Mesa Basin

The majority of the groundwater wells installed in the Mesa Basin were for irrigation purposes. Wells for domestic and industrial use are generally located near the Blythe Airport and at the Palo Verde Mesa development.

Hydrographs created for selected wells with available groundwater level data in the USGS NWIS database show that groundwater levels in the Mesa Basin have generally remained stable from 1980 through 2007 (**Figure 10 – Hydrographs**). Bulletin 118, for the Palo Verde Mesa Groundwater Basin (DWR 2004a), does not report a significant increase or decrease in water levels for 1980 through 1981. Groundwater on the mesa is generally encountered at 250 feet asl at the eastern edge of the mesa and moving northeastward, up McCoy Wash at about 310 feet asl near the head of the wash based on water level data from isolated wells in that area. There does not appear to be an appreciable difference in water levels in wells completed near the top or at bottom of the older alluvium. There is limited data on aquifer storage in the Mesa Basin, but aquifer testing done on the Project site indicated semi-confined conditions (AECOM 2009).

The Mesa Basin has had moderate to extensive groundwater development in the past. Historically, the first groundwater developed was for use at the Blythe Air Base (now Blythe Airport). By the mid 1960's at least48 large-diameter wells were drilled on the mesa to service the Air Base, nearby housing developments, and irrigation. However, the closing of the Air Base has eliminated the development that had occurred in the McCoy Wash part of the Basin. In 1965 and 1966, new irrigation wells were drilled on the Palo Verde Mesa. At the time, an estimated 200 acres of land were irrigated from pumping (Metzger and other s1973). In the 1970's and early 1980's, agricultural groundwater development on the mesa increased substantially to over 6,500 acres, but the majority of this agricultural effort was economically unproductive by the late 1980's and early 1990's. The decrease of groundwater extraction for irrigation is likely the primary reason for the stability of the water level in the Mesa Basin since the 1980's. The water level data from 1971 show local variations in water level contours in the area due east of the Project, which suggest localized pumping in support of agriculture. In contrast, groundwater level data from 2000, show that the water levels had recovered in the area due east of the Project site, and show a southerly flow of groundwater.

3.4.2 Groundwater Flow

As noted above, water level data in the mesa and flood plain shallow or deep wells have generally been stable with overall changes in water levels generally less than about five feet over the recent history. Where larger differences have been observed, it appears that this was is due to water levels being collected while the well was pumping or influenced by local pumping. Given the stability of the water levels over time within the Valley Basin and Mesa Basin since the mid- to late 1980's, the discussions on groundwater flow for shallow and deep wells in the Valley and Mesa Basin are based on depth to water readings that were averaged for the years 1980 to 2008. In an attempt to develop an assessment of steady state conditions, wells with only one reading and data points that were considered to result from groundwater pumping were excluded from the preparation of water level maps for shallow and deep wells. **Figure 11 and**

12 (shallow and deep zone water level maps) show the groundwater level contours for shallow (i.e., generally 30 feet bgs) and deep wells in the Valley and Mesa Basins.

While the occurrence of groundwater was discussed separately for the Valley and Mesa Basins, groundwater flow will focus on differences between the shallow and deep wells. This was done to understand if there were significant differences in horizontal groundwater flow between the younger and older alluvium in the Valley Basin and to understand groundwater flow in the older alluvium between the Valley and Mesa Basins. As noted above, there is not a significant difference in water levels in the shallow and deep wells in the Valley or Mesa Basins, which is consistent with the interpretation of water table conditions.

3.4.2.1 Groundwater Flow in the Shallow Zone

In the north-easterly portion of the flood plain, groundwater flows into the Palo Verde Valley from Parker Valley at the narrows between Parker and Palo Verde Valley (**Figure 11**). Groundwater movement at the north end of the flood plain of Valley Basin reveals a groundwater divide as water moves in west-southwesterly direction on the western edge of the flood plain, just below the gap, in a manner that wraps around the bedrock of the Big Maria Mountains. It also flows southeast toward the river indicating a gaining condition at the north end portion of the floodplain. The apparent divide appears to be related to movement of water out of the Parker Basin and in response to irrigation or diversion canal leakage just south of the PVID diversion. Most importantly, water moves west-southwestward into the Mesa Basin along the topographic break in slope at the northern portion of the Palo Verde Valley. Owen-Joyce (1984) estimated that about 9,500 afy flows into the Mesa Basin from the southwesterly flow of groundwater in the northern portion of the Palo Verde Valley.

Further to the south, the divide is more prominent as a groundwater mound is present above the City of Blythe that extends south past Interstate-10 (Interstate 10). Water flows east toward the river and west toward the Mesa from this mound or groundwater divide above I-10 in the City of Blythe. South of I-10, groundwater east of the divide flows away from the river indicating losing conditions. Continuing south of I-10, the divide is less evident and shallow groundwater travels in a more south-southwesterly direction largely away from the river. Groundwater contours adjacent to the river would suggest losing conditions as the river discharges to the shallow aquifer in the area below I-10 where it crosses the Colorado River. Continuing further south the contours are generally perpendicular to the river, indicating the river is neither gaining nor losing condition. The groundwater gradient through this section of the valley is approximately 0.0001 feet/foot (ft/ft – feet of vertical change over feet of horizontal distance). In the southern portion of the flood plain above Cibola, where the Colorado River turns sharply to the west, groundwater contours parallel the river, suggesting groundwater moving away from the river and water from the river is discharging too the younger alluvium in this area. Groundwater in the western portion of the floodplain appears to move out of the Mesa Basin south of the gap between the Mule and McCoy Mountains and travels generally southward converging with water moving southwest above Cibola at the southern end of the Palo Verde Valley.

Based on the shallow groundwater data, there appears to be in general gaining conditions in the northern portion of floodplain just south of the diversion and in a few isolated areas south of I-10. The river appears to be discharging to the shallow groundwater along some portions of the reach south of I-10 and certainly in the area of the "ox-bow" bend in the river just north of Cibola.

3.4.2.2 Groundwater Flow in the Deep Zone

Mesa Basin

In the area of the McCoy Wash, groundwater generally flows from the north-northwest to the southeast (**Figure 12**). This flow pattern is a result of the primary recharge mechanism in this area, mountain front runoff from the north end of McCoy wash toward the flood plain. There is also, to a much lesser extent, runoff from the McCoy Mountains located to the west of the Project that flows almost due east through the facility boundary to the flood plain (**Appendix F**). Groundwater flow in the mesa is from the north, southeast through McCoy Wash at a gradient of 0.001 feet/foot (ft/ft), then south-southeast at gradients of between about 0.0003 ft/ft and 0.0008 ft/ft in a direction coincident with the flow of the Colorado River (**Figure 12**). The deep zone contours also show the general westward flow of water into the Mesa Basin as water moves west from the groundwater divide in the northern portion of the flood plain. The divide which is present in the deeper zone data as with the shallow zone, shows that water moves west and mixes with water from McCoy Wash about one-mile west of the topographic break between the valley and the mesa. From the area of mixing in the central portion of the mesa in the McCoy Wash water eventually begins to move south and returns to a southerly directed flow in the flood plain area just east of the gap between the Mule and McCoy Mountains. The mixing zone of two different sources of water is evident in the geochemical data as described in Section 3.5 below.

Another source of groundwater to the Palo Verde Valley is underflow from the Chuckwalla Valley Groundwater Basin. The Chuckwalla Valley underflow occurs at the gap between the McCoy and Mule Mountains. Here groundwater is estimated to flow eastward into the valley at a rate of about 1,000 afy (Worley Parsons, 2010). As with the groundwater movement through McCoy wash, the groundwater flow direction shifts to the south-southeast once it reaches the flood plain and combines with the flood plain groundwater flow (Figure 12). There is small divide in this flow as water flows northeastward in response to local pumping in the area of the Blythe Airport.

Valley Basin

In the flood plain area, groundwater enters through the gap between the Parker and Palo Verde valleys and moves predominantly to the southwest. The groundwater divide present in the shallow zone data is also prominent in this portion of the floodplain as in the northern portion of the valley groundwater moves eastward towards the Colorado River. In general, flow patterns suggest groundwater discharge to the river from the diversion to below I-10.

At the City of Blythe, a cone of depression has developed in the area of the largest concentration of municipal water supply wells for the city. South of the City of Blythe, the groundwater contours generally show flow to the southwest parallel to the river (**Figure 12**). From this point south and within the limits of the data there does not appear to be gaining or losing through this stretch of the flood plain.

In summary,

- Water levels have remained stable in wells completed within the younger and older alluvium. This is a result of flood irrigation and diversion of water to the flood plain for PVID and the network of drains that control the groundwater levels.

- Groundwater occurs under unconfined or water table conditions in the Valley Basin as there is not a significant difference between water levels in shallow and deep wells indicating no or little vertical gradient.

- There is a groundwater mound and divide based on water levels from wells completed both the shallow and deeper zones I the northern portion of the flood plain through the City of Blythe. The groundwater divide corresponds to the divide reported by Owen-Joyce (1984) and Owen-Joyce and Kimsey (1987) and is located between one to four miles west of the river. Groundwater flow east of the divide is toward the river indicating groundwater discharge to the river. Groundwater flow west of the divide is to the west away from the river.

- In general, the divide appears to be further from the river than was mapped by Owen-Joyce (1984) and Owen-Joyce and Kimsey (1987) who showed the divide much closer or coincident with the river from shallow water level data collected in 1981 to 1984. The relative position of the divide is a function of river stage and irrigation practice, as the divide moves closer to the river there is less of a gaining condition and apparently more discharge from irrigation. The divide moving away from the river suggests a higher river stage and more river water discharge to groundwater.

- Groundwater in the older alluvium flows in response to several sources including underflow from the Parker area, flow down McCoy Wash and flow in from Chuckwalla Valley, in addition to influence from irrigation return. Groundwater flow in the flood plain is generally south along with river flow at an approximately similar gradient. Along the Mesa, there is a convergence of flow as water traveling out of McCoy Wash and from the Chuckwalla Valley flowing southeast and east respectively interact with water on the flood plain flowing south.

- The differences in flow direction the older alluvium in the Mesa Basin in contrast to the Valley Basin would suggest different sources of recharge from the McCoy Wash and Chuckwalla Valley along with mixing of groundwater along the divide between the two areas where water from the mesa mixes with water from the flood plain.

- While the Palo Verde Mesa Groundwater Basin (Mesa Basin) and the Palo Verde Valley Groundwater Basin (Valley Basin) have been mapped as separate groundwater sub-basins, water level contours suggest they are in hydraulic communication. Geochemical data does indicated though that the basins have different sources of groundwater in the mesa area and the McCoy Wash, as there is a significant change in Total Dissolved Solids (TDS) concentrations from the floodplain westward to the Project site.

3.5 Groundwater Geochemistry

The following sections discuss the groundwater geochemistry of the Palo Verde Valley. The discussions for the flood plain and mesa areas are handled separately based on the hypothesized primary source of groundwater recharge.

3.5.1 Valley Basin Geochemistry

The shallow zone geochemisty can be characterized as varying widely across the floodplain. TDS concentrations of the shallow groundwater generally range between 600 and 6,000 milligrams per liter (mg/l). By contrast, TDS concentrations in the Colorado River, ranges from 600 to 900 mg/l. Chloride concentrations in the Valley Basin are generally between 100 and 350 mg/l. Sulfate concentrations are generally higher than the chloride concentrations and range from 300 to 800 mg/l. Concentrations of the same constituents in the Colorado River range from 65 to 112 mg/l for chloride and 230 to 370 for sulfate. Metzger and others (1973) theorized that the variability of the geochemistry for the shallow zone was directly related to the time the water had been in the subsurface and the location of the sample relative to canals and diversions. Better quality water would be found the further away from the river or closer to canals or centers of irrigation discharge that may provide river water to the shallow zone through seepage.

Deep zone wells in the Valley Basin are generally centered within two or three miles of the City of Blythe and represent municipal water supply wells (Metzger and others 1973). There are also several wells completed in the deep zone within approximately 10 miles of the city. The deep zone wells generally produce two types of water, one has TDS concentrations ranging from 500 to 700 mg/l, sulfate concentrations generally less than 150 mg/ and chloride concentrations similar to the Colorado River (100 to 350 mg/l). The second type of water produced, has TDS concentrations between 800 to 1,200 mg/l, sulfate concentrations generally above 150 mg/l and chloride concentrations similar to the Colorado River.

Metzger and others (1973) theorized, based on the geochemistry of the groundwater, most flood plain groundwater was at one time surface water of the Colorado River. This water infiltrated into the subsurface as a result of seepage from the river and floods over the last several thousand years or in more recent years from the application of irrigation water to the land surface of the flood plain or seepage from the canal system. An additional, albeit minor source of flood plain groundwater, would be infiltration of flood waters off the mesa.

3.5.2 Mesa Basin Geochemistry

In the Mesa Basin, the best quality water is generally found near the mesa – flood plain boundary. West from that location there is a gradual increase in mineral content westward and northwestward from the flood plain in the direction of McCoy Wash and the McCoy Mountains. Groundwater pumped from depths of between about 150 and 350 feet bgs near the boundary and north of I-10 reportedly have TDS concentrations ranging from 700 to 900 mg/l with chloride concentrations in the range of 150 to 250 mg/l. In contrast, several miles to the west, the TDS concentrations range from 1,000 to 1,500 mg/l.

The TDS and chloride concentration data, along with the groundwater flow patterns, point strongly to the existence of a mixing zone near the eastern boundary of the mesa. Within this zone, high TDS and chloride water, originating as runoff from the McCoy Wash and Mountains combines with the water from the flood plain following the same flow pattern described above and shown on **Figure 12**. A review of boron concentrations (**Figure 13**) further supports the concept of a mixing zone in this area as groundwater samples from the McCoy Wash have boron concentrations ranging from 1,400 to 2,000 mg/l, while groundwater from the flood plain has boron concentrations generally in the below 200 mg/l (**Appendix B**). Consistent with the TDS and chloride distribution, the boron concentration distributions are similar to the groundwater flow patterns moving off the mesa and mixing with water moving westward from the floodplain.

3.6 Palo Verde Valley Aquifer Characteristics

Properties used to define the aquifer characteristics include hydraulic conductivity, transmissivity, and storage coefficient. Hydraulic conductivity is the property of the aquifer material to transmit water, and is expressed in units of feet per day (ft/d). Transmissivity is the hydraulic conductivity multiplied by the thickness of the sediments capable of storing water, and is expressed in units of gallons per day per foot (gpd/ft) or ft^2/d. Storage coefficient refers to the percentage of water that can be released from the aquifer material pore space, and is used for unconfined or water table conditions (Bates and Jackson 1987).

Metzger and others (1973) provide the most comprehensive assessment of aquifer characteristics through an evaluation of pumping tests from 42 wells tested in Parker, Vidal, Palo Verde and Cibola valleys. In the Palo Verde valley, they reported transmissivities in the flood plain ranging from 63,000 gpd/ft (about 8,500 ft^2/d) up to 1.9 million gpd/ft (about 250,000 ft^2/d). However, in their assessment of the results, tended to discount transmisivities over 1 million gpd/ft (130,000 ft^2/d). Metzger and others (1973) showed that in general, transmissivity values are higher in the valley than in the mesa area, though wells located in portions of the mesa near the valley boundary or in the northeastern portion of the mesa near the wash produce large amounts of water suggesting higher transmissivity conditions in these areas.

In their development of a two-dimensional superposition model for the Parker-Palo Verde-Cibola area, which includes the Valley and Mesa Groundwater Basins, Leake and others (2008), evaluated published aquifer testing data and through statistical analysis derived a range of transmissivity values from 25 tests conducted along the river reporting a low value of 6,300 ft^2/d

and an average value of 26,200 ft^2/d. In their model of Colorado River depletion, they selected a storage coefficient of 0.20 to approximate aquifer conditions throughout their model domain.

Groundwater production on the mesa averages 1,650 gpm. The maximum yield reported was 2,750 gpm from well 6S/22E-16A1 located on the mesa. The DWR (1979) indicated that large well yields are common for properly designed and developed wells near the edge of the flood plain. Well yields on the rest of the mesa and further west of the mesa-floodplain break, where sand is the dominant lithology, are lower. The Blythe Energy Project indicated a yield for a well on the mesa due south of the Project site of over 3,000 gpm and a specific capacity of 125 gpm/ft. Yields greater than 1,000 gpm are reported in wells in the McCoy Wash area in the northeastern portion of the wash where it enters the floodplain. A pumping test of Well TW-1 on the Project site in generally fine-grained alluvium yielded a specific capacity of 3 gpm/ft of drawdown and a transmissivity ranging from between 10,000 ft^2/d to 14,000 ft^2/d.

The modified DWR log for well 5S/22E-28C1 (located at the northeast corner of the mesa near the mouth of McCoy Wash) indicates two thin gravel units (three and 16 feet in thickness) were encountered at the base of the alluvium. While Metzger and others (1973) indicated the mesa was generally comprised of finer grained materials, as observed in Well TW-1 on the Project site, the extent of these gravel units is unknown. However it is likely these gravels are reason that some wells in McCoy Wash can produce up to 1,000 gpm.

In the Palo Verde Valley, the gravels and sands from highly permeable beds of the fluvial deposits have the highest hydraulic conductivity (Metzger and others 1973). The USGS study noted wells that tap a sufficient thickness of the gravels had specific capacities greater than 100 gpm/ft of drawdown.

3.7 Water Balance for the Palo Verde Valley

A water balance of the Valley and Mesa Basins was developed for the Palo Verde Valley Groundwater Model using the results from prior investigations (Metzger and others 1973, Owen-Joyce 1984, Owen-Joyce and Kimsey 1987), and stream flow data for the Colorado River (**Appendix C**) and an update using recent PVID diversion and return data (**Appendix E**), and an estimate of discharge from recent groundwater pumping estimates for municipal, industrial and agricultural supply.

The water balance was done for both the Mesa Basin and the Valley Basin together, in contrast to prior investigations where the estimates are largely for the Valley Basin or flood plain (Owen-Joyce 1984; Owen-Joyce and Kimsey 1987).

The groundwater basins were evaluated together, as there is no data to suggest that they are hydraulically separate, and since the purpose of the model is to evaluate pumping from one basin to another, a groundwater balance for the entire valley was constructed. The significant components to the assessment of recharge and discharge within the Palo Verde Valley are the diversion and return of water for the PVID and the gain or loss of water from the Colorado River

(Metzger and others 1973, Owen-Joyce 1984, Owen-Joyce and Kimsey 1987). These water volumes are several orders of magnitude more than mountain front recharge, underflow or discharge from groundwater pumping.

In the development of the water balance significant consideration is given to the relative stability of the groundwater levels since the mid- to late-1980's. This relative stability is a reflection of the management of the diverted water from the Colorado River through its application for irrigation and ultimately return of groundwater through the PVID drains. As water levels have fluctuated only a few feet and locally in response to irrigation, this would indicate a balance between inflow and outflow of groundwater within the Palo Verde Valley. The groundwater balance was evaluated to achieve unity in the difference between the estimates inflow and outflow.

The elements of recharge and discharge within this balance are as follows and are described below:

Recharge

- Mountain Front Recharge
- Underflow from the Parker Valley and Chuckwalla Valley
- Agricultural Return and Canal Seepage
- Loss from the Colorado River

Discharge

- Groundwater Pumping
- Consumptive Use – Non-native Vegetation
- Discharge from the PVID Drains
- Discharge of Groundwater to the Colorado River

The balance of these components that relate directly to the groundwater system in the Palo Verde Valley is presented in **Table 2.** An water balance of 426,600 af is estimated from a balance of the recharge and discharge elements discussed below.

As noted above, the key elements of groundwater balance for recharge are agricultural return and canal seepage and loss from the Colorado River. These elements make up about 97% of the total recharge to the Valley and Mesa Basins, of which irrigation return and canal seepage comprise about 44% (Table 2). The discharge or outflow of groundwater is largely comprised of the measured discharge from the drains, the unmeasured return or groundwater discharge to the river and ET loss from non-native vegetation. These elements make up 97% of the total outflow of which discharge from the drains is about 84%.

3.7.1 Recharge

Groundwater recharge are those components of the water balance for the Palo Verde Valley where water is added through underflow from an adjacent groundwater basin, irrigation return and loss from the Colorado River (i.e., river water discharging to groundwater). In the case of the Palo Verde Valley the most significant component of groundwater recharge is from the diversion of water for irrigation and subsequently irrigation return and through discharge of river water to groundwater. While mountain front recharge is considered, direct precipitation onto the valley floor or mesa is considered negligible. Metzger and others (1973) did not consider precipitation in excess of eight inches to be significant enough to directly recharge groundwater. While precipitation is important to assumptions of consumptive use, it is not considered important as a component of direct recharge to groundwater.

3.7.1.1 Mountain Front Recharge

Mountain front recharge is a component of precipitation which falls onto the bedrock and runs off percolating into the permeable soils in the upper portion of alluvial fans. Recharge from along the mountain front within the Palo Verde Valley was estimated from precipitation data shown on Figure 6 from Hely and Peck (1964) for the western portion of the Valley west of the Colorado River. An estimate of total precipitation was made using an overlay of the annual average isoheytal contours that were overlaid onto the topography of the bedrock. An assumption of 5% was used to estimate the amount of the total that would percolate into the groundwater within each of the bedrock areas. Based on this 5,000 afy was estimated to infiltrate as mountain front recharge. Metzger and others (1973) and Owens-Joyce (1984) estimated that recharge from surface water or tributary runoff through the McCoy Wash was and McCoy and Mule Mountains was about 2,000 afy (**Table 2**).

3.7.1.2 Groundwater Underflow from the Parker Valley and Chuckwalla Valley

Underflow from the two major adjacent groundwater basins is estimated to be 4,500 afy. The value from Parker Valley of 3,500 afy follows what was estimated by Metzger and others (1973) assuming groundwater flow the three-mile gap where the valley narrows adjacent to the Palo Verde Diversion Dam. The underflow from the Chuckwalla Valley has been estimated at 1,000 afy (Worley Parsons 2010), which represents an increase from what was estimated by Metzger and others (1973) of 400 afy. The difference represents more recent information provided by more up-to-date hydrogeologic data on the aquifer characteristics and geophysical surveys conducted to determine the geometry of the bedrock “high”, and subsequently the saturated thickness of the aquifer in the gap between the Chuckwalla and Palo Verde Mesa areas.

Though not relatable to a water balance of the Palo Verde Valley (inclusive of the Mesa and Valley Basins), Owen-Joyce (1984) estimated groundwater inflow from the Valley Basin to the Mesa Basin of 9,500 afy largely from westward flow along the northern portion of the valley (Figure 12). The westward flow of water in this area appears to be through higher transmissivity sediments that extend from the northeastern portion of the wash into the valley.

3.7.1.3 Agricultural Return and Canal Seepage

The largest source of recharge to the Palo Verde Valley inclusive of the Valley Basin and the Mesa Basin, apart from discharge of water from the Colorado River is the deep percolation from water diverted for irrigation by PVID. Between 1993 and 2009, an average of 731,743 af was diverted annually for irrigation in the Valley Basin. An average of 10,616 af was diverted to the Mesa Basin, for a total average diversion of 742,359 af (**Appendix E**). The water is conveyed throughout the flood plain area, via both lined and unlined canals (**Figure 5**). The canals are generally less than 10 feet deep and are not in contact with the groundwater. Water is applied to the land surface from these canals via pumps or opening a weir, and the water that is not consumed (i.e., transpired) or evaporates returns to the groundwater via deep percolation. The PVID drains, dug to depths between 15 and 20 feet bgs, convey the return water not consumed back to the Colorado River.

Recharge from Irrigation Return – Valley Basin

An estimate of the irrigation return is made using the average of water diverted for irrigation on the floodplain less total spill return to the river less consumption, canal seepage and evaporation. The average diversion to the flood plain for irrigation since 1993 is 743,000 afy. Using this measured value and the measured spill return and an estimate of consumption since by the USBR (1993-2009), and an estimate for canal seepage and evaporation (Owen-Joyce 1984) from the canal surface yields the following:

	Quantity (afy)
Diversion to the Valley	743,000
Total Spill Return	(136,000)
Consumption	(420,000)
Canal Seepage	(125,000)
Evaporation	(5,000)
Total	**67,000**

This estimate can be verified using a different approach by removing the consumptive use term and replacing it with a water use or consumed fraction of water by crop values for the Colorado River (PA Number 1004) (Department of Water Resources, 2001). Using the above data, about 487,000 afy is estimated as the volume of water applied for irrigation. Based on the percentage distribution of crops as noted for the period between 2006-2008 in 2008 PVID crop report and an associated water use efficiency of 75%, yields an irrigation return of 120,000 afy.

Recharge from Canal Seepage

As noted above in the estimate of irrigation return, Owen-Joyce (1984) in the development of an estimate of groundwater return to the river using an estimate of canal seepage of 125,000 afy and evaporation loss of 5,000 afy after Bookman-Edmonston (1976). Based on the irrigation return value derived from consumption and the estimate of canal seepage yields a total estimated return to groundwater from the diversion of water to the valley of about 187,000 afy.

Recharge from Irrigation Return – Mesa Basin

There are a total of approximately 2,683 acres of irrigated agricultural, municipal, and domestic land in the Mesa Basin. Of the 2,683 acres, approximately 1,862 acres are irrigated with surface water from the Colorado River through PVID (personal communication Roger Henning PVID 2010). The remaining 724 acres are irrigated with groundwater from the PV Mesa. Return from irrigation of 97 acres at the Blythe Municipal Golf Course is also included in this estimate. Agricultural return was calculated for the total agricultural acreage of 2,683, using the DWR Water Use and Efficiency Estimates for 2001.

To determine agricultural return from irrigation, the water use and consumed fraction of water by crop values for the Colorado River (PA Number 1004) (Department of Water Resources, 2001) were applied to a total of 2,683 acres of irrigated agricultural land on the PV Mesa. Citrus is the primary crop on the PV Mesa, therefore, values for the "sub-crop" category were used for the calculations. The amount of water used per crop was multiplied by the number of agricultural acres on the PV Mesa. The percentage of the total amount of water applied by irrigation that is retained within the root zone and that is available for crop evapotranspiration (consumed fraction) was deducted from the amount of water applied to 2,683 acres, resulting in the amount of water that is recharged to the aquifer. The amount of recharge to the PV Basin on the Mesa from irrigation return is estimated to be 3,561 acre-feet per year.

3.7.1.4 Discharge from the Colorado River

As shown on **Figures 11 and 12**, there are portions of the Colorado River reach through the Palo Verde Valley where the river discharges to the shallow groundwater, largely through high water or river stage conditions. These portions of the reach are largely south of I-10 and concentrated near the southern end of the river above Cibola. An estimate of the river loss was made as the result of the difference between the average measured PVID drain return and unmeasured groundwater return after the USBR for the period between 2003 and 2009, less the estimate of irrigation and canal return. This estimate yielded an estimate of discharge from the Colorado River of about 226,000 afy to the Palo Verde Valley (**Table 2**). This value is closer to though less than what was assumed by Metzger and others (1973) who estimated an average loss along this reach of the Colorado River of 361,000 afy for the period between 1955 and 1961. It is significantly less than the estimate of the loss for the northern reach of the river by Owen-Joyce (1984) of 3,100 af for 1981.

This value is an estimate of measured and unmeasured data, and was made under the assumption that the major components of inflow and outflow from the Palo Verde Valley must in general be in balance as evident by the relative stability of the groundwater levels over time.

3.7.2 Discharge

Groundwater discharge are those components of the water balance for the Palo Verde Valley where water is removed most commonly being through groundwater pumping, underflow out of a basin or through ET loss. In the case of the Palo Verde Valley the most significant component of loss or discharge is through the PVID drains. Underflow out of the Valley would be through

the gap above Cibola, and while there might be some groundwater flow out of the valley it is assumed to be negligible since most of this water would discharge to the river in the Cibola Valley above the narrows. This follows the interpretation of Metzger and others (1973) and Owen-Joyce (1984) who assumed no underflow out of the valley in their estimate of water balance.

3.7.2.1 Groundwater Pumping

Irrigation Use

There are 724 acres of agricultural (predominantly citrus) and municipal land on the mesa that rely on groundwater from private wells for irrigation. To determine agricultural diversions on the PV Mesa, the water requirement ("applied water") for "subtrop" crops in the Colorado River (PA Number 1004) area was multiplied by 724 acres. A total of approximately 3,584 afy are diverted on the PV Mesa by private wells**.**

Municipal, Domestic, and Industrial Groundwater Use

The City of Blythe pumps three wells on the PV Mesa for domestic and municipal use. Mesa Ranch Well #3 is pumped for domestic use and PVC Well #2 is pumped for water use at the Palo Verde College (PVID, 2010). An estimate of 260 afy of diversions from these two wells was provided by the City of Blythe Department of Public Works (2010). A third well (Mesa Ranch Well #2) is pumped for the Blythe Municipal Golf Course. Estimated diversions from this well are approximately 560 acre-feet per year (City of Blythe DPW, 2010).

The County of Riverside operates one well (Airport Well #7) at the Blythe Airport that serves the Mesa Verde Community. Approximately 47 afy of groundwater is pumped from this well (Riverside County – CSA 62, 2010). The Blythe Energy Project I (BEP I) is a 520 mega watt natural gas fired power plant located on the PV Mesa, approximately one mile east of the Blythe Airport. BEP I pumps 3,300 afy of groundwater.

Groundwater discharges attributable to irrigation on the mesa and domestic and municipal pumping in the floodplain largely for the City of Blythe combined account for about 7,500 afy of groundwater discharge.

3.7.2.2 Consumptive Use – Native Vegetation

An estimate of consumptive use of groundwater by non-native vegetation is made annually by the USBR in their estimate of accounting of Colorado River water. Their estimates of ET loss from non-native vegetation includes the areas along the reach through the Palo Verde Valley, including PVID, Cibola National Wildlife Refuge, Colorado River Indian Tribes and other farms east of the river in Arizona. Using the average estimates for areas within the Palo Verde Valley from 2003 to 2009, which would exclude the larger CNWR, yields an estimate of ET loss from non-native vegetation of about 8,500 afy.

3.7.2.3 Discharge from the PVID Drains

As required under the accounting of Colorado River water, the return from the PVID drains to the Colorado River is measured on a daily basis. Based on information provided by PVID, the average return from the drains, inclusive of the Olive Lake and Outfall drains, to the river since 1993 is about 357,000 afy with the range being between about 267,000 afy to 406,000 afy **(Appendix E)**.

3.7.2.4 Groundwater Discharge to Surface Water (Unmeasured Return)

An estimate of unmeasured return or groundwater discharge to the river is made annually by the USBR in their estimate of accounting of Colorado River water. For the period of 2003 to 2009, the average unmeasured return to the Colorado River was about 50,000 afy. This compares to the estimated loss of about 226,000 afy from the river. The unmeasured return values are generally comparable, though higher, than those estimated by Owen-Joyce and Kimsey (1987) who estimated annual return values between 2,500 to 31,700 af.

4.0 MODEL DEVELOPMENT AND CALIBRATION DATA

The numerical groundwater model required under SOIL&WATER-16 was constructed following the SCM and to provide an assessment of the impact from Project pumping on surface water in the Valley Basin and how pumping after a period of 30 years might affect recharge from the Valley Basin to the Mesa Basin where the Project is located. As the key surface water features are the Colorado River and the PVID drains that return groundwater to the Colorado River, the model incorporated the area west of the river to the topographic divide between the adjacent valleys to the west and up to the gap with the Chuckwalla Valley on the west, Parker Valley on the north and gap with the Cibola Valley to the south (**Figure 14**). The model domain extended to the Colorado River did not include portions of the Palo Verde Valley east of the river and across the border with Arizona. The model domain extended to the Colorado River did not include portions of the Palo Verde Valley east of the river and across the border with Arizona. The model domain was limited to the area west of the river since the purpose of the model is to evaluate the effect of Project pumping on surface water sources inclusive of the river and drains west of the river. Excluding areas east of the river is reasonable as there is a general absence of groundwater elevation data east of the river and the younger alluvium limited in areal extent east of the river. As constructed, the model encompasses the key components of recharge and discharge within the Palo Verde Valley and incorporates the majority of the saturated Colorado River alluvium.

The model was calibrated to an average of hydrologic conditions from 1980 to 2009. As discussed in the SCM, water levels within the model domain, both the Valley and Mesa Basins, have been relatively stable not varying more than a few feet during that period. Given the major components of the groundwater system include the PVID diversion and drain and discharge and Colorado River steady state calibration to this period provides an adequate representation of groundwater conditions for the purposes of the model. While there was some pumping in the early to middle part of the 1980's, it had ceased and water levels recovered to provide a reasonable understanding of steady-state conditions within both basins. Transient calibration was not attempted given the relative stability of the water levels over the last 30 years.

The electronic files for the Palo Verde Groundwater Model are provided on CD in **Appendix H**.

4.1 Model Construction

4.1.1 Code Selection

The Palo Verde Valley Groundwater Model was constructed using the MODFLOW2000 model (Harbaugh and others 2000) developed by the USGS. MODFLOW2000 is the latest version of the MODFLOW family of models. MODFLOW is the most popular groundwater flow model used in the United States and has become the standard for groundwater flow modeling in the country.

MODFLOW is capable of simulating steady-state or transient groundwater flow in one, two, or three dimensions. A wide variety of boundary conditions may be simulated, including constant head, constant flux (wells, recharge), and head-dependent flux (ET, drains, rivers, streams, and general head) boundaries. The types of boundaries used in this model will be described below. MODFLOW can simulate aquifer systems that are unconfined, confined, or a combination of confined and unconfined.

MODFLOW was chosen for this study because it has all of the requisite capabilities to simulate flow in the Palo Verde Valley and MODFLOW2000 was chosen in particular because it is one of the newest and most up-to-date versions of MODFLOW and is thoroughly documented (McDonald and Harbaugh, 1988 and Harbaugh and others 2000).

4.1.2 The Model Grid

The flow of groundwater can be described using mathematical equations that form the basis for all computer models used in the field of hydrogeology. Computer models may be subdivided into two broad categories, called numerical and analytical models. Analytical models are exact solutions of the groundwater flow equations, and numerical models are approximate solutions. Given the choice between an exact solution and an approximate one, it seems logical that one would choose an analytical model over a numerical model. However, analytical models are usually limited to ideal aquifers that are homogeneous with simple boundaries. Most real world aquifers are not that simple. Consequently, numerical models are used most often in practice.

Because numerical models are approximate, they typically compute hydraulic head (water levels) at fixed points within the aquifer. These points are called nodes or cells, and are often arranged in a rectangular pattern called a grid. There are many different types of numerical techniques that are used to solve the groundwater flow equations. MODFLOW2000 uses a technique called the finite-difference method.

The finite-difference technique requires that the aquifer system be divided into a set of discrete blocks or cells. These blocks are rectangular in shape and form the model grid. The process of creating the grid is call discretization. Water levels computed for a block represent the average water level over that rectangular region of the aquifer. Thus, adequate discretization is required to resolve features of interest, such as the location of the wells, faults, and basin boundaries in the Palo Verde Valley.

An algebraic equation that describes groundwater flow is written for each block in terms of the surrounding blocks, and the complete set of linear equations is iteratively solved until the change in head between iterations meets a set criterion. An iterative solution is required because the model is an approximate solution to the groundwater flow equations.

The model grid developed for the Palo Verde Valley covers approximately 459.8square miles and includes the Valley and Mesa Basins. The model domain measures approximately 37.2 miles from north to south and 23.7 miles from east to west. The southwest corner of the model grid is located at Easting 6,944,100 feet and Northing 2,062,100 feet. These coordinates are in UTM Zone 11N, NAD 1983, feet.

The model grid spacing varys from 20 feet to 2,000 feet, and tightest around the proposed pumping wells. The model grid was finer in the vicinity of the Project site where the proposed pumping wells are located. The model grid contains 183 rows, 184 columns, and one layer for a total of 33,672 cells of which 24,963 are active. The model simulates only the area up to the mountain blocks. Mountain front recharge was applied at base of the mountain fronts using recharge cells. The model area and grid is shown on **Figure 15**. No-flow cells are those outside the active portion of the model grid and were used to represent the bedrock boundary.

The model was constructed as a single-layer numerical model encompassing both the younger and older alluvium under unconfined conditions. Metzger and others (1973) and Owen-Joyce and Kimsey (1987) indicate that the saturated alluvium in the Palo Verde Valley is present under unconfined conditions. Further, as described in the SCM, unconfined conditions are indicated in the floodplain based on the similarity of water level data between shallow and deeper data.

Multiple layering of the model was not considered appropriate given the absence of lithologic and hydraulic contrast (i.e., absence of a significant vertical gradient) between the younger and older alluvium and the absence of water-bearing sediments in the Bouse Formation and general absence of productive water-bearing sediments in the fanglomerate. Additionally, all of the relevant hydrologic and groundwater data pertains to the younger and older alluvium and there is little to no groundwater data for the Bouse and fanglomerate in the Palo Verde Valley and as the Project proposes to pump groundwater from the base of the older alluvium exclusion of these units from the model is appropriate. The model was constructed with the base of the model following the distribution of Colorado River sediments shown on **Figure 8**. The elevation of the top of the model was interpolated from the USGS digital elevation model (DEM) for the model domain.

4.1.3 Boundary Conditions

Once the aquifer system has been discretized, it is implicitly assumed that groundwater outside the model grid can be ignored. The model, however, must account for areas where groundwater enters or leaves the system. These effects are included in a model using boundary conditions. Ideally, boundary conditions should represent identifiable regional hydrologic features where groundwater flow can reliably be described (Franke and others. 1984). In the case of the Palo Verde Model, the regional hydrologic boundaries for the Palo Verde Valley are the edges of the surrounding mountain blocks or the basin boundaries (**Figure 14**). Groundwater enters and exits the model through the recharge and discharge elements described in the SCM, with water entering via underflow from the Parker and Chuckwalla Valleys, as mountain front recharge, as agricultural return and canal seepage and loss from the Colorado River. It exits via the Palo Verde Drains, ET loss from non-native species and from pumping.

Numerical groundwater models, such as MODFLOW, use three types of boundary conditions to simulate ways in which water may enter or leave the model domain. These include the specified-head, specified-flow, and head-dependent flux boundaries. The specified-flow boundary is used to describe fluxes to surface water bodies, spring flow, underflow, and seepage

to or from bedrock underlying the modeled system (Anderson and others 1992). Specified flow is similar to constant head (which is not available) boundary condition, but with more accurate estimates for inflow and outflow of the system. A specified flow boundary was used to define the inflow from the Chuckwalla Valley and inflow and outflow from the northern and southern gap in the Palo Verde Valley **(Figure 14)**.

Specified flux boundary conditions are implemented in MODFLOW using wells, recharge, or no-flow (i.e., flux equals zero) cells. Constant flux boundary conditions (i.e., recharge) were used in the Palo Verde Valley model to simulate flow of water into the basin from the mountain blocks. The flow rates were determined from the basin water budget presented in the SCM. Recharge from irrigation was applied as uniformly across the valley to approximate the flood irrigation through diversion onto the floodplain. Mountain front recharge was simulated using the same USGS approach (USGS, 2001) as an areal recharge for the recharge cells along portions of the northwestern boundary in the McCoy Wash. The Colorado River was modeled using transects provided by the USBR for select locations along the river reach through the Palo Verde Valley **(Figure 16)**. The river bottom elevation was linearly interpolated from these data for all river cells along the eastern boundary of the model domain. Similarly, the bottom of the PVID drains were set at depth of 20 feet below ground surface and linearly interpolated from DEM data at locations shown on **Figure 17**.

4.1.4 Model Parameters

Model parameters required by MODFLOW2000 for the model include aquifer hydraulic conductivity and storage values for each cell in the model. Hydraulic conductivity determines the ease with which groundwater flows horizontally. This section describes the final distribution of parameters in the model derived during calibration which is described in more detail in Section 4.2.

The usual philosophy in model construction and calibration is to start with a simple distribution of parameters and add complexity (heterogeneity) as required during calibration. In calibrating the Palo Verde Valley model, the hydraulic conductivity distribution was initially homogeneous and additional hydraulic conductivity zones were added as necessary to match the observed water levels and changes in hydraulic gradient in the valley and on the mesa. The final zonation of hydraulic conductivity is shown in **Figure 18.**

The hydraulic conductivity values range from a low of 1.0 ft/d in the northern portion of McCoy Wash in order to match very high water levels and steep gradient in that area. The hydraulic conductivity values for areas adjacent to and west of the river were the highest along with portions of the Project site and areas along the valley mesa boundary. Lower estimates of conductivity were modeled on the western-most areas of the valley and in the area of the gap between the Mule and McCoy Mountains on the west. An area of higher hydraulic conductivity is also indicated in the northernmost portion of the valley to accommodate the westerly directed flow of groundwater from Parker Valley as it appears to wrap around the bedrock knob into the Palo Verde Valley. The storage coefficient in the aquifer was homogeneous for the model and

was assigned a value of 0.20 consistent with what was used in the USGS model of the same area (Leake and others 2008), and with the interpretation that groundwater in the Colorado River alluvium is present under unconfined conditions. The Colorado River conductance was set in the final calibration at about half the USGS (Leake and others 2008) value of 2.3E5 ft^2/d (1.15E5 ft^2/d).

4.2 Model Calibration Concepts

It is important to understand the terms and concepts used in describing the calibration effort. Many of these terms come from the statistical literature and some are unique to groundwater modeling. Calibration is the process of adjusting parameters in the model so that the model-computed water levels match water levels measured in wells. Calibrating a groundwater model is difficult because we have relatively little information on subsurface conditions. Most of the parameters in a model, such as hydraulic conductivity, are only known at a few points where measurements have been taken. Even at those "known" points, the measurement of subsurface properties is an inexact science. Thus, calibration is a necessary part of groundwater modeling where the initial estimates of aquifer properties, entered when the model is first created, are changed so that the model computes more realistic water level elevations.

During the calibration, the model-computed water levels are compared to those water levels measured in wells. These measured water levels are called calibration targets or just targets. The targets represent water levels measured at a particular time during the simulation or they can represent steady-state conditions. In the case of the Palo Verde Valley model, steady-state conditions represent an average of water levels measured from 1980 to 2009. This period follows the period of time where agricultural pumping was significant on the mesa, and as most hydrographs show relatively stable water levels during this time frame varying only a few feet.

Accepted practice in groundwater modeling is to match water level elevations in a steady-state calibration and then water level changes during transient calibration. This was the approach was not taken in the Palo Verde Valley model as there has not be significant variation in water levels over the last 30 years as noted in the SCM and shown on **Figures 9 and 10**. Measured water level elevations in ft above sea level were matched by the model for steady-state conditions for target wells for average conditions between 1980 and 2009.

After each simulation, the target water levels are compared to model-computed water levels. The model-computed water levels are subtracted from the field measurements to produce a residual. Positive residuals represent computed water levels that are lower than those measured in the field. Conversely, negative residuals are those where the model is computing water levels higher than the measured ones.

A statistical analysis is performed on the collection of residuals from all targets used in the model (Konikow, 1978). Simple statistics such as the mean, standard deviation (sometimes called root-mean-square error), and absolute mean are commonly used. The mean residual should be close to zero, indicating that the positive and negative residuals are balanced. The

absolute mean is computed by making all residuals positive and thus represents the average error in the calibration. These statistical measures are used to determine the quality of the calibration. Goals should be established for acceptable values of the mean, standard deviation, and absolute mean.

In addition to statistics computed for residuals, the distribution of residuals should be analyzed during calibration. It is desirable to have positive and negative residuals randomly scattered throughout the model. Clustering of positive or negative residuals over large areas is called spatial bias. One goal of calibration is to reduce spatial bias as much as possible. However, it is virtually impossible, however, to eliminate spatial bias because of the lack of subsurface data.

4.3 Calibration Results

What constitutes an acceptable calibration is very subjective. Woessner and Anderson (1992) suggest that goals should be established before the calibration starts. However, no standards have ever been put forth by American Society of Testing and Materials (ASTM) or in the scientific literature that describe what these goals should be. Goals were established for this model, are based on goals which have undergone peer review from U.S. Environmental Protection Agency (EPA) and many state government agencies. These goals are summarized as follows:

- Residual standard deviation divided by range in head for all targets should be less than 0.10 (10 percent),
- Absolute residual mean divided by range in head for all targets should be less than 0.10 (10 percent),
- Residual mean divided by range in head for all targets should be less than 0.05 (5 percent), and
- There will be limited spatial bias in the distribution of residuals.

As previously discussed, a residual is the difference between a measured water level and the model-computed water level. The residual is calculated as the observed head minus the model-computed head. Thus, a negative residual occurs where the model-computed head is too high and a positive residual is where the model-computed head is too low.

The statistics for the Palo Verde Valley model calibration met the calibration goals described above. The goal for residual mean divided by range in head is 0.9 percent, well below the goal of 5.0 percent. The standard deviation divided by range in head was 4.7 percent, again well below the goal of 10 percent. The absolute residual mean divided by range in head was 3.3 percent, significantly less than the goal of 10 percent. Therefore, all of these statistical measures are substantially better than the established goals.

In addition to statistics, another standard method of judging calibration quality is to plot the measured water levels versus the computed water levels. In a perfect calibration, the points would lie along a straight line at a 45-degree angle indicating that the computed water levels match the observed water levels exactly. In reality, this never happens; however, the spread of data points about the perfect line is an overall indication of spatial bias in the model. **Figure 19** shows that there is no large-scale bias in the calibration with each broad area having the same degree of scatter about the 45-degree line. The higher water levels in the regional model represent the eastern portion of the model domain, while the lower water levels are found in the center of the basin near the river.

Figure 20 shows the calibrated water table for the average condition from 1980 to 2010 represents the steady-state calibration and shows the model-predicted contours overlain onto those provided for the deep zone water level data shown on **Figure 12**. The model-predicted contours match the contours from average water levels between 1980 and 2009 reasonably well as would be expected given the calibration statistics. Model-predicted contours match both the groundwater mounding in the central portion of the floodplain and show the divergent and convergent flows around the river suggestive of gaining and losing conditions. The model-predicted contours also approximate the mixing zone where water moving out of the McCoy Wash mixes with the westward flowing water from the floodplain under the mesa.

Lastly, as another measure of calibration the mass balance of the model inflow and outflow should be nearly equal. As shown on **Table 3**, the difference between the inflow and outflow from the model in less than 0.000001 percent. The flow through the calibrated model is 388,895 afy. This value is less than 10 percent of the water balance estimate of 426,600 afy presented in the SCM (**Table 2**).

Calibration is accomplished by finding a set of parameters, boundary conditions, and stresses that produce simulated heads, flow and fluxes that match field-measured values within a pre-established range of error. In general, the calibration shown the model is capable of producing both field-measured heads and flows which are the calibration targets. No calibration is perfect, and so there will always be mismatches between the model results and water levels measured in the field. The mismatch in the case of the Palo Verde Valley model is primarily due to lack of water level data for areas within the model domain and variability in local irrigation practices and river stages.

5.0 MODEL SIMULATIONS

The calibrated model was used to approximate Project pumping for 30 years following a schedule of 820 afy for both the first and second years, 970 for the 3rd year, 1120 for the 4th year, and 1270 for the 5th year for the period of five years to simulate construction supply and 600 afy for operational supply. This schedule equate to a total of 22,250 af of water used during the course of the Project. Operational supply was phased in beginning in 2013 and the model was run for a period of 30 years to 2043. During this time frame the pumping was equally apportioned through four water supply wells located in each of the four proposed 250-megawatt solar power projects. Groundwater pumping was assumed to occur at each of four water supply wells located on the northern end of the unit power blocks. The wells were assumed to be completed in the lowest portion of the older Colorado River alluvium, above the contact with the Bouse Formation , estimated to be about 500 feet bgs below the Project site. The Project has under condition the option to install 10 water supply wells, but primary water production during operation will come from only one well located in each power block. To assess the influence from Project pumping on surface water in the Valley Basin, the model was run to:

- Determine the radius of influence from Project pumping after 30 years, and,
- Assess the change in mass balance between the calibrated model non-pumping and pumping condition after 30 years to determine if there were changes in mass flux in either the PVID drains or the Colorado River.

The radius of influence from Project pumping at the end of 30 years as predicted using the calibrated model is shown on **Figure 21** and a vector plot showing direction of groundwater flow and magnitude from the pumping is shown on **Figure 22**.

As shown on **Figure 21**, the predicted influence from pumping at the end of 30 years shows that the drawdown contour of 0.1 foot does not extend off the mesa and does not extend across the floodplain to the Colorado River. This suggests that groundwater derived for pumping is coming largely from the mesa area. Further, the cone of depression would likely never reach the Colorado River, given the volume of water from irrigation recharge and the groundwater divide central to the floodplain east of the Project. The cone of depression as predicted by the model would probably never extend off the mesa boundary into the floodplain, given the large volume of water recharging the Colorado River alluvium on an annual basis by comparison to the annual Project pumping requirements and the available storage below the mesa.

The vector plot (**Figure 22**), which maps the direction and magnitude of groundwater flow vectors shows that the majority of water to support pumping comes from the area of the McCoy Wash and mesa and from the westerly directed groundwater flow from the drainage divide at the northern-most portion of the valley. This is the flow direction estimated by Owen-Joyce (1984) to contribute about 9,500 afy to the mesa from inflow from the valley. The groundwater flow

vectors are not deflected from Project pumping east of the mesa boundary and in the area of the PVID drains and Colorado River. This is consistent with groundwater flow in the northern portion of the valley west of the groundwater divide. As shown on **Figures 11 and 12**, groundwater flows westerly as it enters the valley from Parker and is directed westerly from the groundwater mound developed in this area, largely following a zone of apparently higher transmissivity sediments in this area.

As another measure of influence from Project pumping, the model mass balance between the non-pumping and pumping condition for the base or calibrated condition were compared to assess changes in surface water flow for the PVID drain and Colorado River. As shown on **Table 3**, the balance between inflow and outflow for the non-pumping and pumping condition is near unity and there is no change between the mass balance for the Colorado River between the non-pumping and pumping condition after 30 years. This indicates that the pumping does not affect the Colorado River recharge to the model over the duration of 30 years of Project pumping.

Table 3 does show that there is a very small change in the PVID drain mass balance between the non-pumping and pumping condition at the end of construction of 20 af and a total change of 1,785 af at the end of the operation period of a30 years. The total change represents variance of 0.014% of the modeled throughput of the PVID drain over 30 years. It is important to note that this change could not be reliably measured and thus the model prediction could not be verified. The mass balance for the pumping condition does show that the majority of water from pumping on an annual basis comes from changes in storage in the mesa area. The amount of the total change in drain discharge (1,785 af) represents eight percent of the total amount of water (22,250 af) being pumped for the Project indicating most of the water for Project pumping is coming from outside of the floodplain, and from changes in storage in the Mesa Basin.

6.0 SENSITIVITY ANALYSES

A series of simulations were conducted to test the model response to changes in parameters, boundary conditions, and other assumptions. The purpose of a calibration sensitivity analysis is to document the relative importance of model parameters on calibration statistics. This provides the user and the CEC with additional information about which parameters are most important to the calibration process. The most sensitive parameters are those that are usually best estimated in the calibration. The following simulations were included in the sensitivity analysis:

- Hydraulic conductivity was increased by a factor of 2.0.
- Hydraulic conductivity was decreased by a factor of 0.5.
- PVID Drain conductance was increased by 50 %.
- PVID Drain conductance was decrease by 50 %.

The model was run for these changes and the mass balance was compared to the non-pumping and the calibrated condition as shown on **Table 3**. As shown on **Table 3** (drain conductance) and **Table 4** (hydraulic conductivity), the most sensitive variable is hydraulic conductivity. With these changes there is no change in the mass balance between the pumping and non-pumping condition for the Colorado River. The total change in the PVID drain mass flux from the hydraulic conductivity sensitivity analysis varies from 1,077 af to 3,315 af above and below the calibrated value (1,785 af) after 30 years. The total change in the PVID drain mass flux from the variance in the drain conductance varies from 1,684 af to 2,111 af above and below the calibrated value (1,785 af) after 30 years. The largest change in PVID drain discharge were predicted when both the hydraulic conductivity and drain conductance were twice their calibrated value.

For comparison to the calibrated drain flow of 387,932 afy, both the sensitivity runs that double the hydraulic conductivity and drain conductance predict drain flow 17% to 20% above the calibrated value and 100,000 afy above the measured average of 357,000 afy. By comparison these predictions appear to be overly conservative, and beyond a reasonable predictive estimate of impacts from Project pumping. The model prediction from the calibrated model appears to be a better representation of potential impacts from Project pumping.

7.0 CONCLUSIONS

A numerical groundwater model was developed as required under CEC final licensing condition SOIL&WATER-16 to estimate the increase in discharge from surface water to groundwater that affects recharge from the Valley Basin to the Mesa Basin from Project pumping after 30 years.

The model was constructed to include both the floodplain of the Colorado River (Valley Basin) and the Palo Verde Mesa (Mesa Basin). An SCM of the Palo Verde Valley was constructed showing that groundwater levels in the Valley and Mesa Basin for wells completed in the younger and older alluvium have remained relatively stable since the mid-1980s. As water levels have fluctuated only a few feet locally in response to irrigation, this indicates a balance between inflow and outflow of groundwater within the Palo Verde Valley. Key elements in the groundwater balance are recharge elements that include agricultural return and canal seepage and discharge (loss) from the Colorado River. Conversely, the discharge elements are comprised of the measured discharge from the drains, the unmeasured return or groundwater discharge to the Colorado River and ET loss from non-native vegetation. The relative stability of the water levels in the floodplain and mesa suggest that these volumes are nearly equal.

The numerical model was developed in consideration of the water balance for the Palo Verde Valley, and as such was constructed as a single-layer numerical model encompassing both the younger and older alluvium of the Colorado River under unconfined conditions. The model was calibrated to assumed steady-state conditions from 1980 to 2009. Transient calibration was not attempted given the relative stability of the water levels over the last 30 years.

The model calibration was within acceptable tolerances and the model was used to evaluate the affect from Project pumping on surface water discharge in the floodplain including the PVID drains and the Colorado River. From the modeling the following conclusions are offered:

- The influence to a predicted drawdown of 0.1 foot is within the mesa and does not extend into the floodplain. Groundwater flow vectors after 30 years of pumping show that groundwater flows to the pumping wells largely from areas on the mesa and the McCoy Wash and from westerly flow to the mesa in the northern portion of the floodplain. These results suggest little to no significant influence on the surface water in the PVID drains and no influence on the Colorado River as the cone of depression does not reach these features.

- A comparison of the mass balance between the calibrated model pumping and non-pumping condition shows that there is no change in flux of water from the Colorado River to the groundwater, indicating that the Project pumping does not affect a change in the river discharge. This is expected given the distance from the pumping center, recharge of water from irrigation return, and the location of a groundwater divide in the central portion of the floodplain between the pumping wells and the Colorado River.

- A comparison of the mass balance to the PVID drains shows that there is a small change in the mass balance of about 20 af at the end of construction and 1,785 af total after 30 years of pumping. This change represents about 0.014% of the total flow through the drains in the model over 30 years. A value of this magnitude is insignificant and could not be verified by measurement given the average annual drain flow over the last 10 years is about 353,000 afy and the total drain flow in the model is 12,800,000 af. The amount of change in the drain flow is about 8% of the total groundwater pumped during 30 years for the Project. This suggests that most of the water is from storage in the mesa and represents a small change in recharge from the Valley Basin to the Mesa Basin.

- The predictive sensitivity analysis shows that hydraulic conductivity is the most sensitive variable. Modeling a range of values around the calibrated variable yields changes in the PVID drain discharge of between 1,077 and 3,315 af after 30 years of pumping. The largest changes in PVID drain discharge were predicted when both the hydraulic conductivity and drain conductance were twice their calibrated value. These model scenarios may be overly conservative and beyond a reasonable predictive estimate of impacts from Project pumping, as the drain flow is 100,000 afy more than the measured average in the PVID drain since 1993. The model prediction from the calibrated model appears to be a better representation of potential impacts from Project pumping through the operational life of 30 years.

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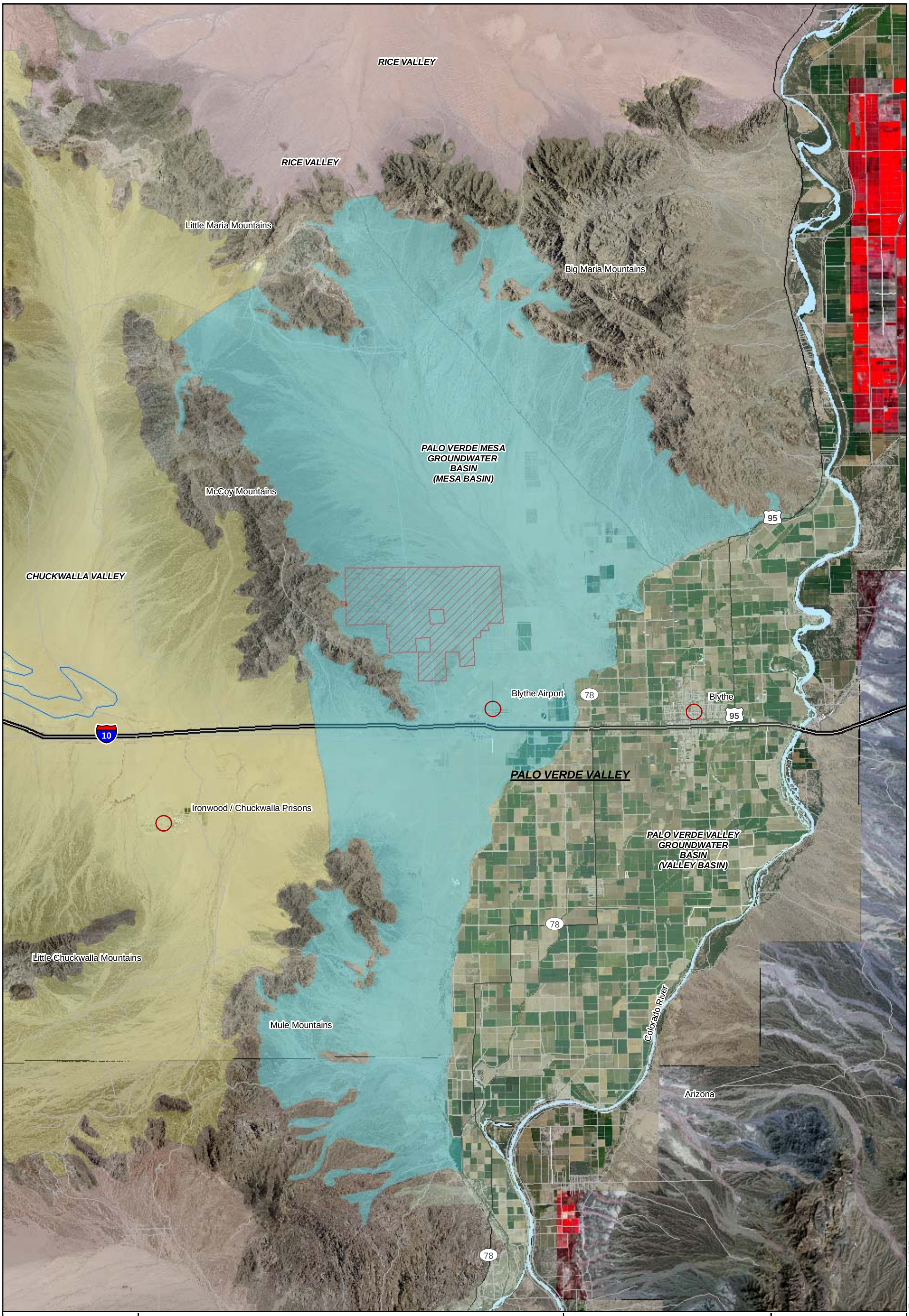
Figures



Map Location

Legend

- Project Right-of-Way
- Geographic/Cultural Area of Interest
- Freeway
- Highway / Major Road
- Palo Verde Mesa Groundwater Basin (Mesa Basin)
- Palo Verde Valley Groundwater Basin (Valley Basin)

1:200,000

0 10,000 20,000 Feet

N W E S

Source:

Blythe Solar Power Project

Figure 1
Regional Groundwater Basins

Palo Verde I, LLC

AECOM

Project: 60157720
Date: October 2010

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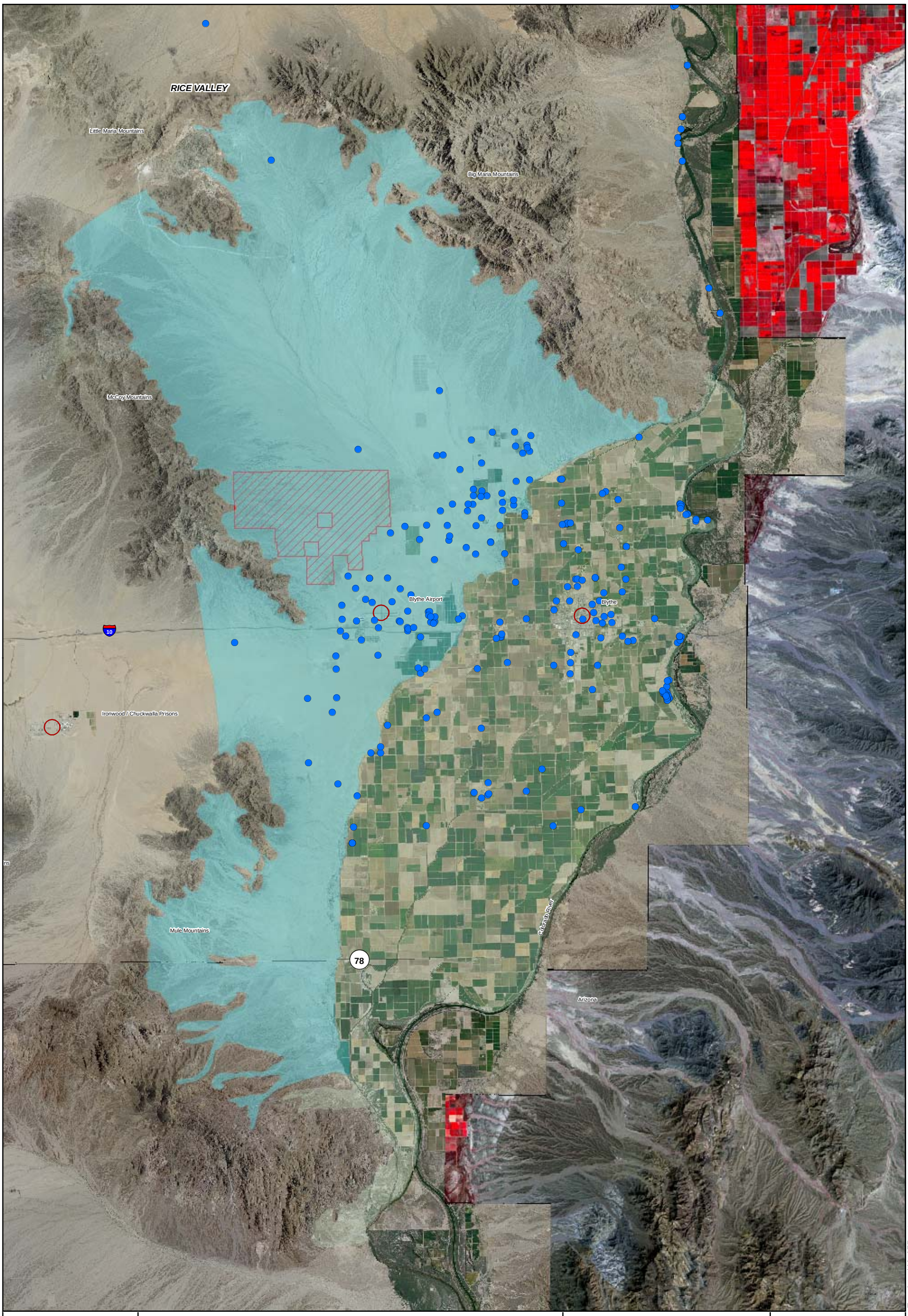

Map Location

Legend

- Well in USGS NWIS Database
- Project Right-of-Way
- Geographic/Cultural Area of Interest
- Freeway
- Highway / Major Road
- Palo Verde Mesa Groundwater Basin (Mesa Basin)
- Palo Verde Valley Groundwater Basin (Valley Basin)

1:200,000 0 10,000 20,000 Feet

N W E S

Blythe Solar Power Project

Figure 2
Wells in USGS NWIS Database

Source:

Palo Verde I, LLC

AECOM

Project: 60157720
Date: October 2010

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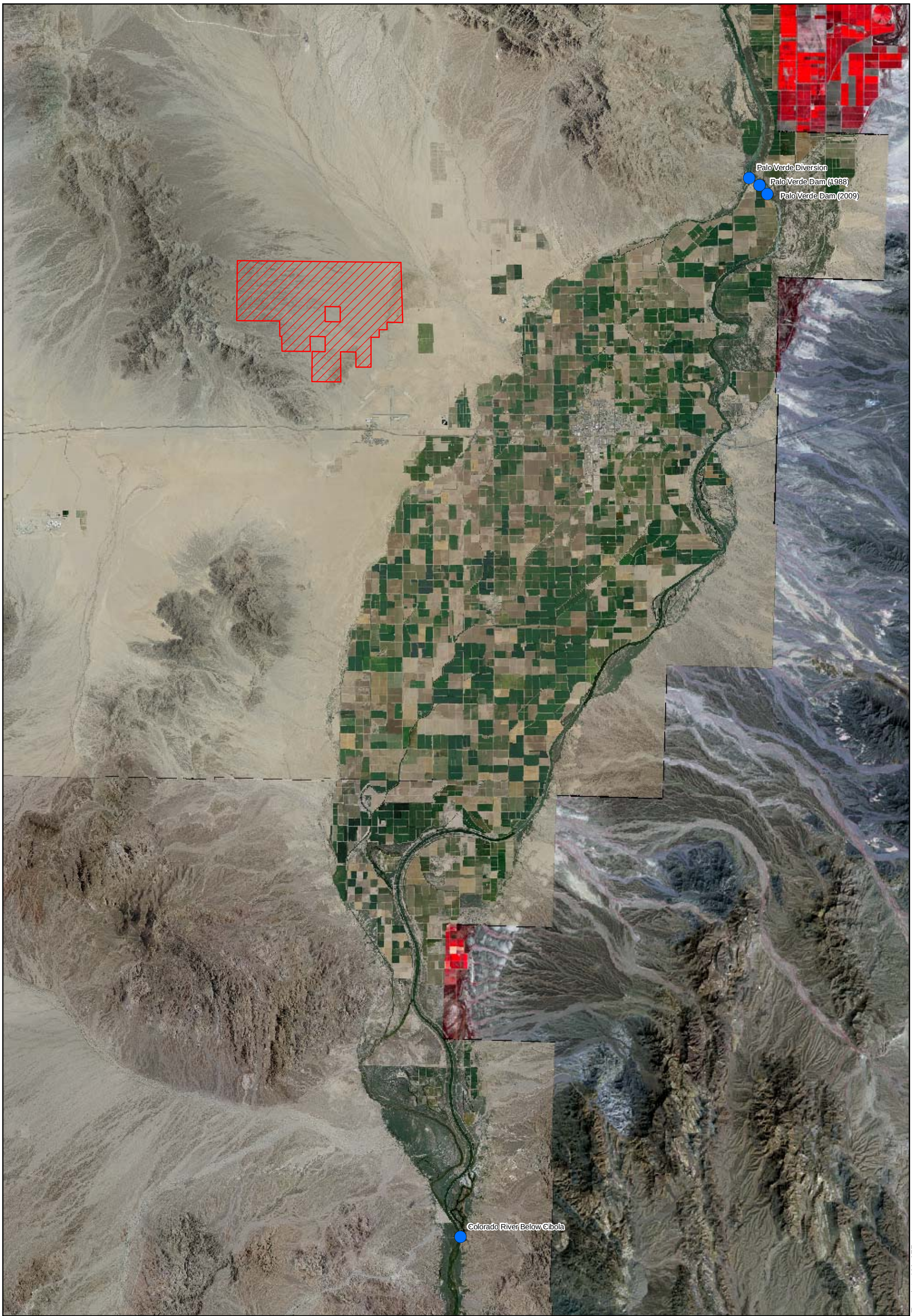

Map Location

Legend

Gauging Station Location

Project Right-of-Way

1 in = 3 miles

0 3 6 Miles

N W E S

Blythe Solar Power Project

Figure 3
Surface Water Gauging Stations Along the Colorado River

Source:

Palo Verde I, LLC

AECOM

Project: 60157720
Date: October 2010

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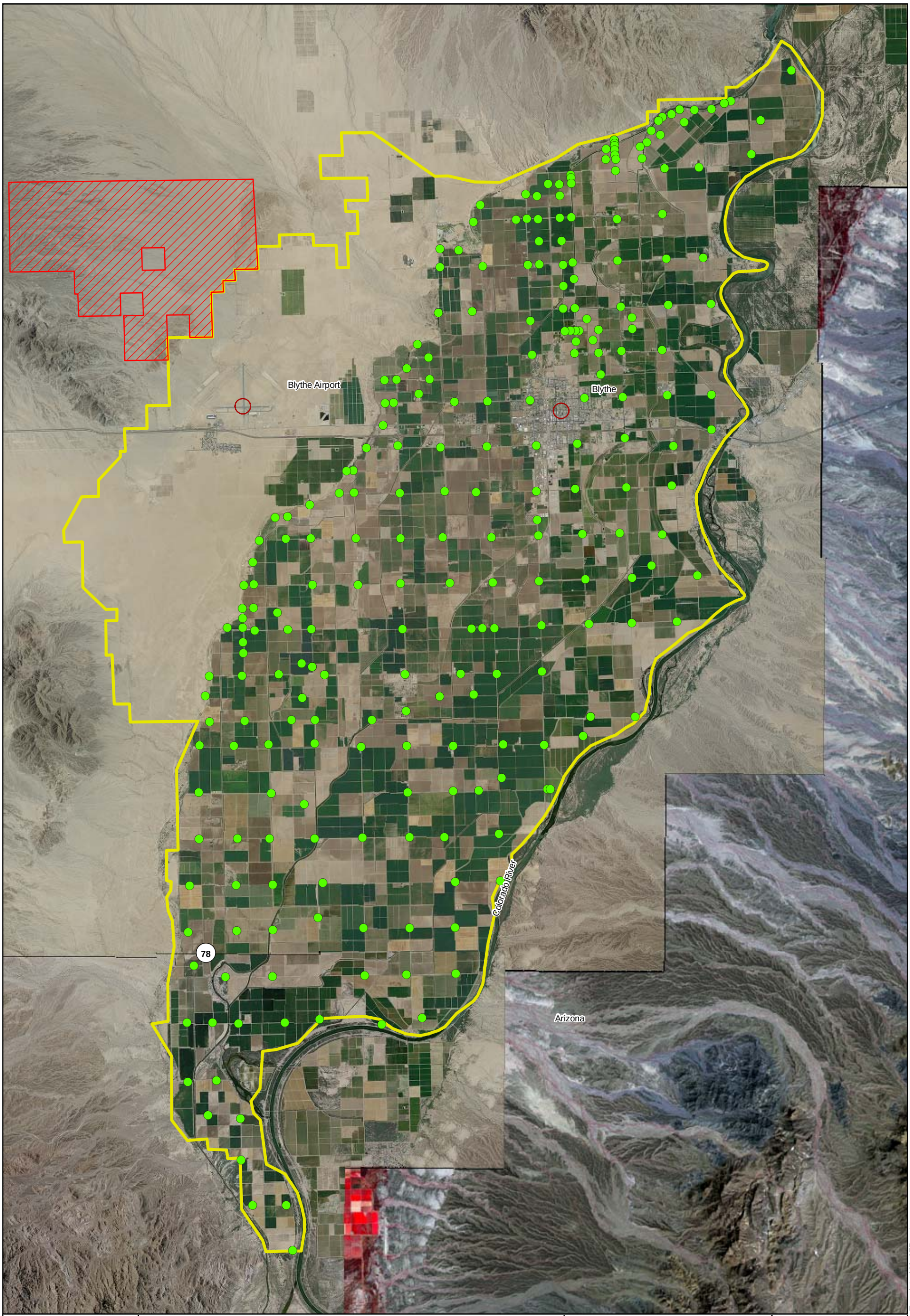

Map Location

Legend

- PVID Well Point Location
- Project Right-of-Way
- Geographic/Cultural Area of Interest
- Freeway
- Highway / Major Road
- Palo Verde Irrigation District Boundary

1 in = 2 miles

0 2 4 Miles

N W E S

Source:

Blythe Solar Power Project

Figure 4
PVID Well Point Locations

Palo Verde I, LLC

AECOM

Project: 60157720
Date: October 2010

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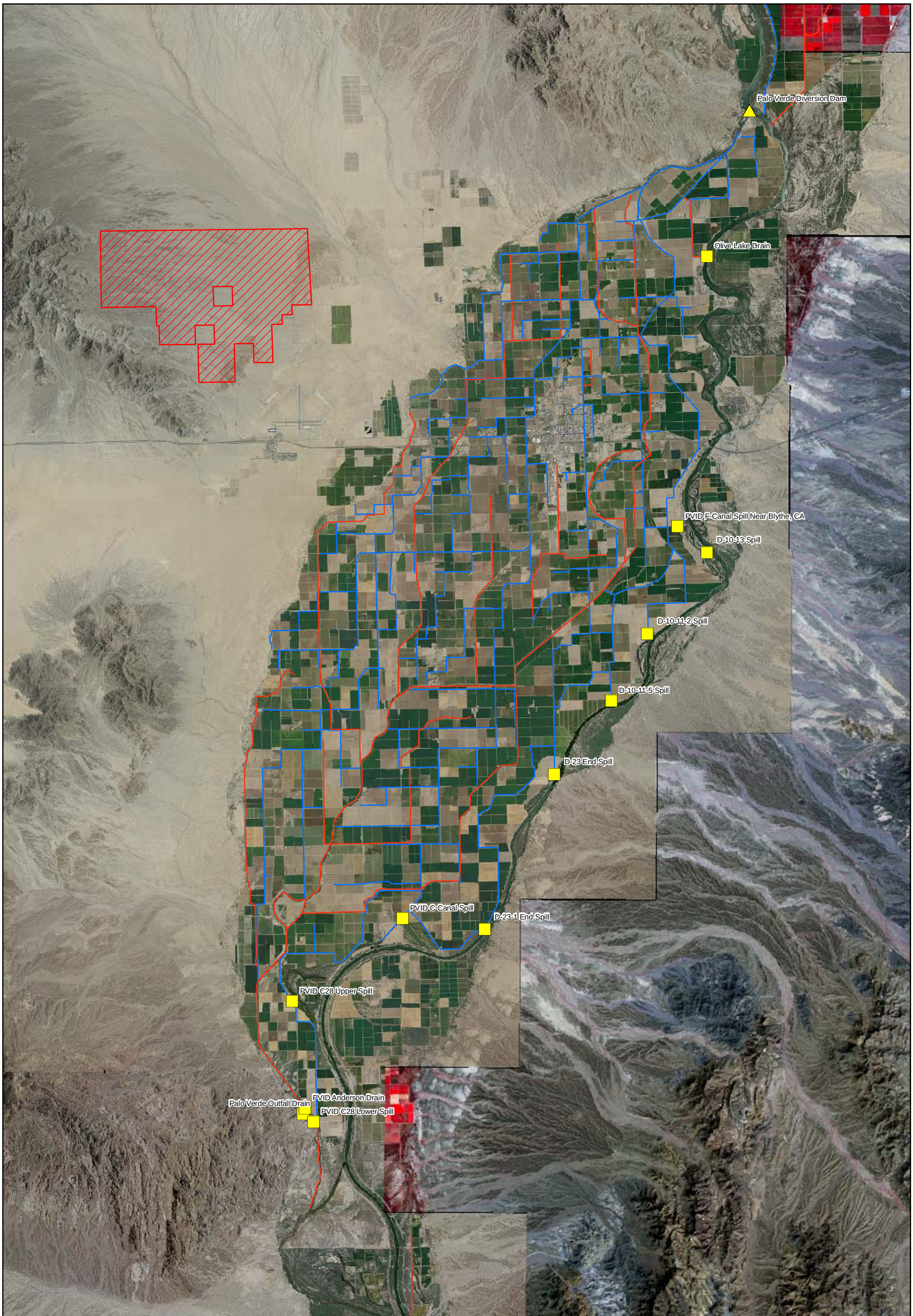

Map Location

Legend

- Surface Water Diversion
- Spills/Returns
- PVID Drains
- PVID Canals
- Project Right-of-Way

1:150,000

0 10,000 20,000 Feet

N W E S

Source:

Blythe Solar Power Project

Figure 5
Palo Verde Irrigation District Diversions, Spills and Returns

Palo Verde I, LLC

AECOM

Project: 60157720
Date: October 2010

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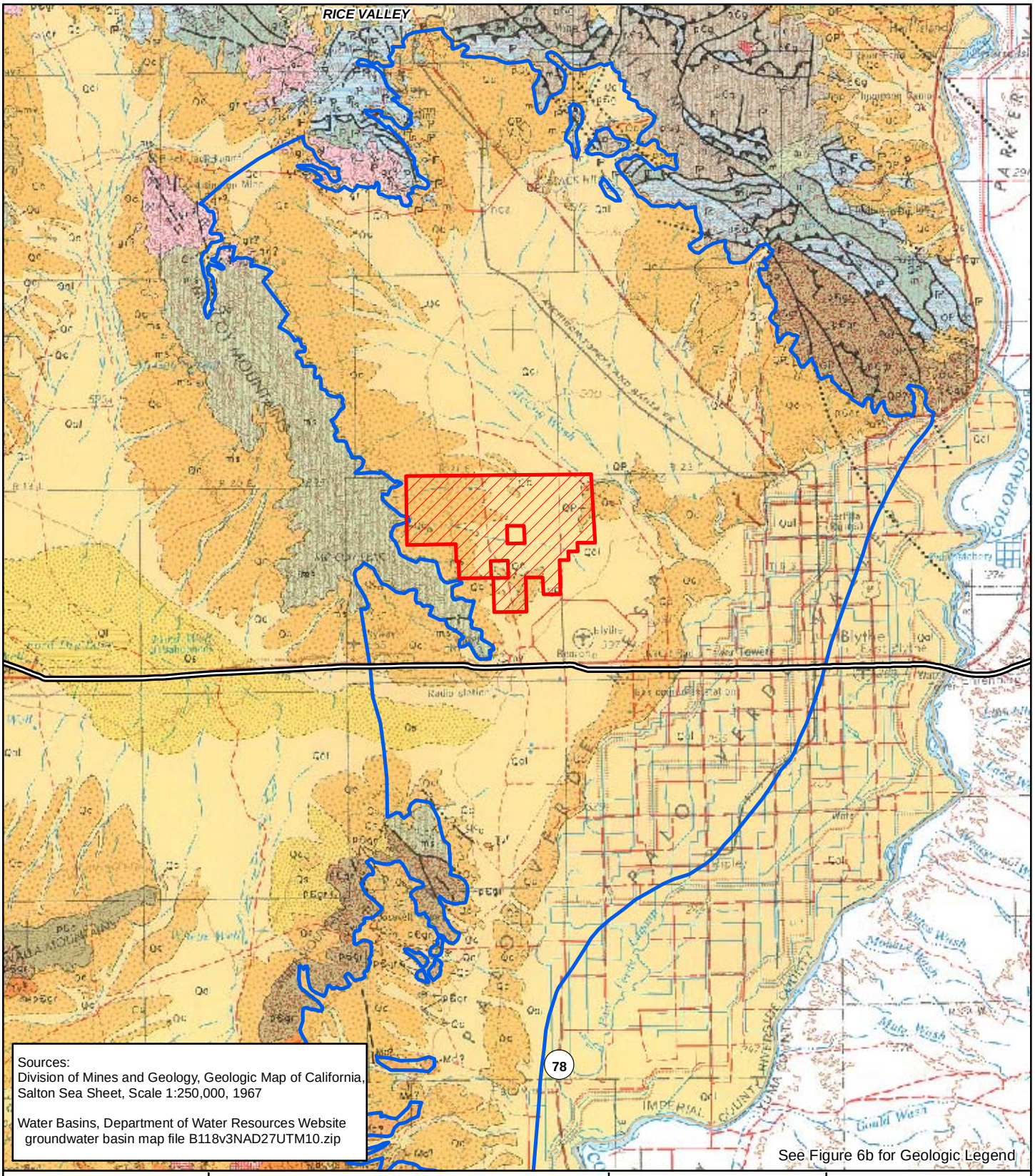

Map Location

Legend

- Project Right-of-Way
- Freeway
- Palo Verde Mesa Groundwater Basin Boundary

0 4 8 Miles

N W E S

Blythe Solar Power Project

Figure 6a Regional Geologic Map

Palo Verde I, LLC

AECOM

Project: 60157720
Date: October 2010

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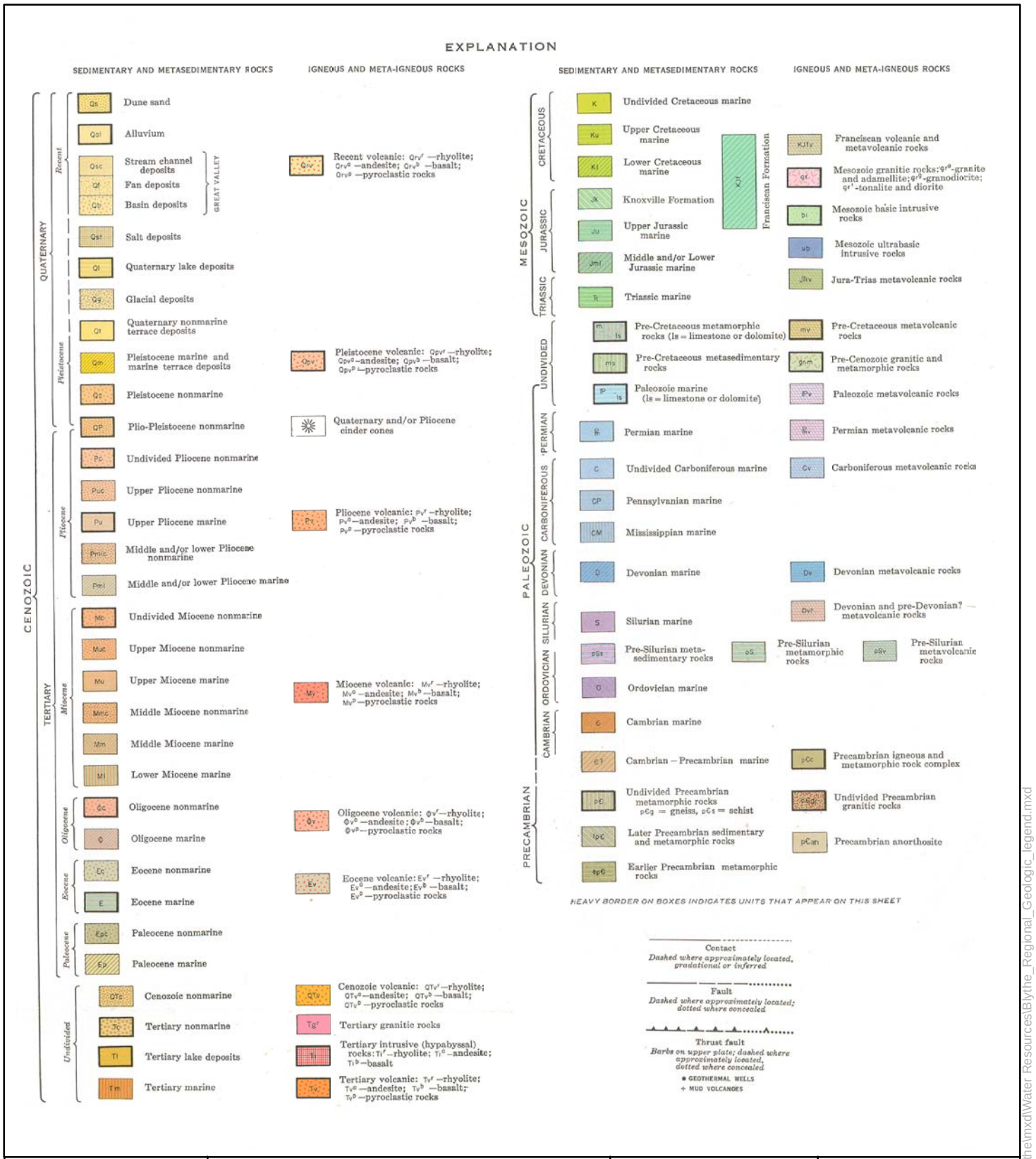

Map Location

Legend

Source: Geologic Map of California, Salton Sea Sheet, 1967

Blythe Solar Power Project

Figure 6b Regional Geologic Map Legend

Palo Verde I, LLC

AECOM

Project: 60157720
Date: October 2010

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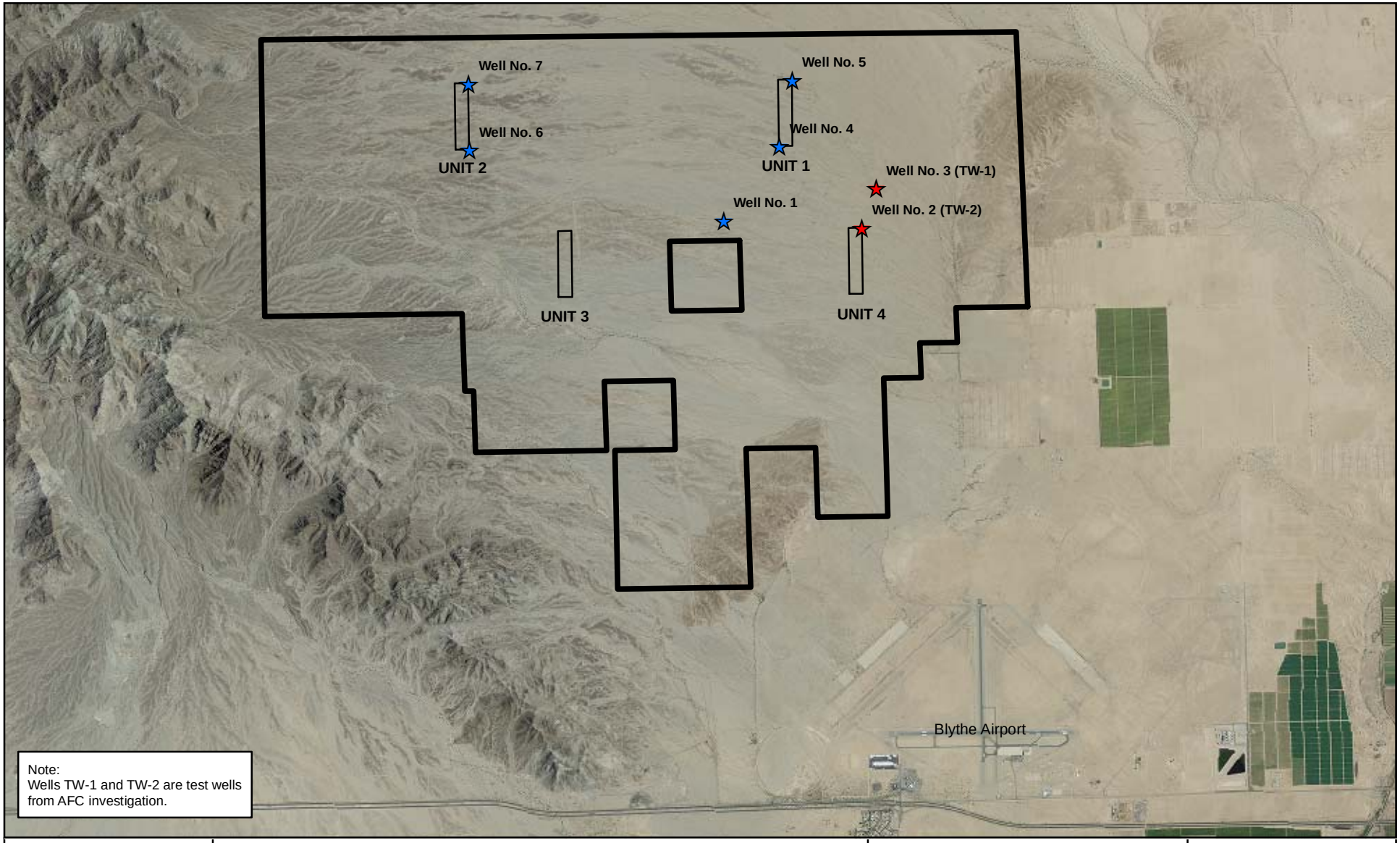

Note:
Wells TW-1 and TW-2 are test wells from AFC investigation.

Map Location

Legend

- Proposed Water Supply Well
- Existing Water Supply Well
- Project Right-of-Way

1 in = 1 miles

0 1 2 Miles

N W E S

Source:

Blythe Solar Power Project

Figure 7
Site Map Showing Test Wells and Planned Operational Wells

Palo Verde I, LLC

AECOM

Project: 60157720
Date: October 2010

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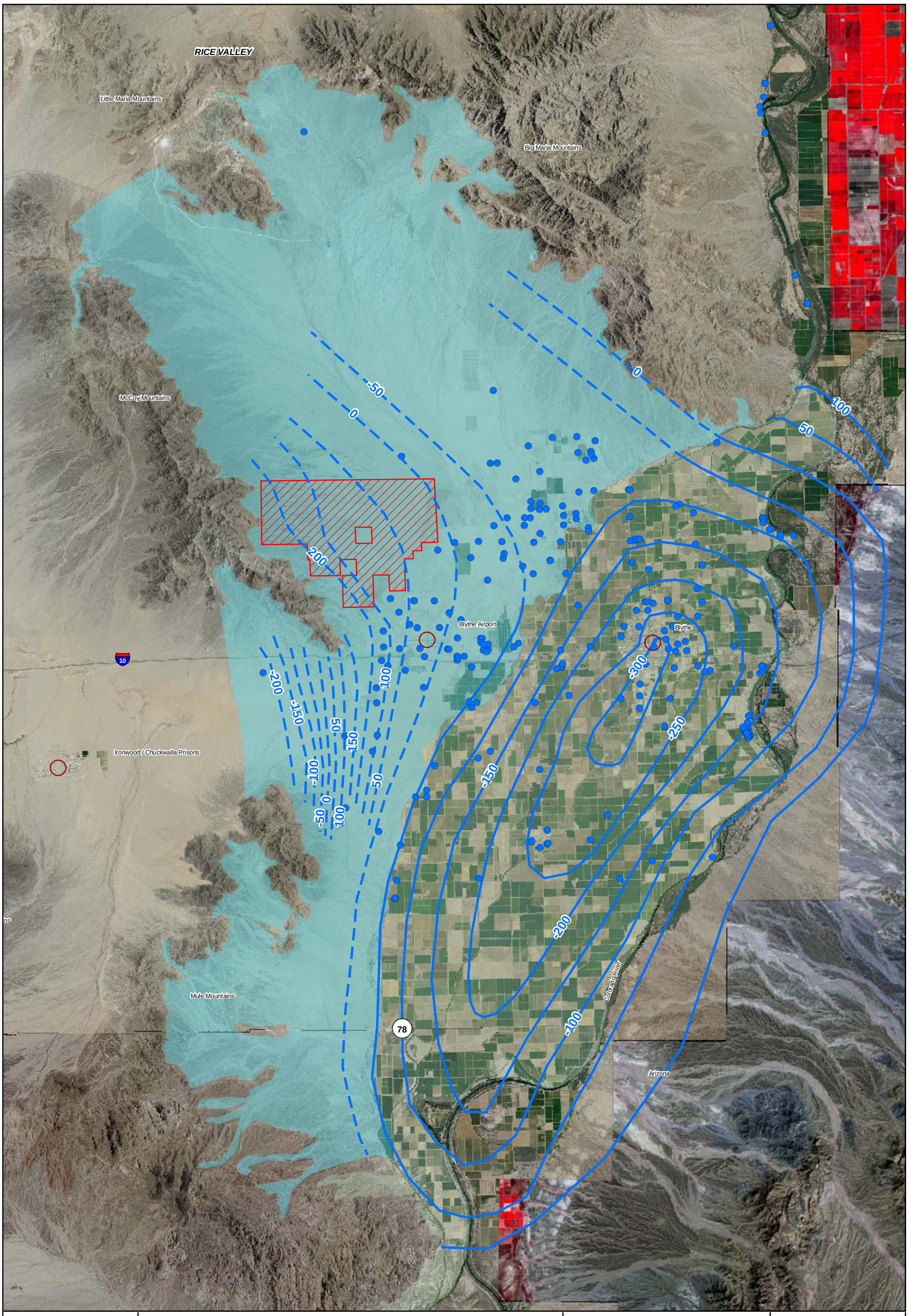


Map Location

Legend

- Bottom Elevation of CRA (feet msl)
- Well in USGS NWIS Database
- Project Right-of-Way
- Geographic/Cultural Area of Interest
- Palo Verde Mesa Groundwater Basin (Mesa Basin)
- Palo Verde Valley Groundwater Basin (Valley Basin)

1 in = 3 miles

0 3 6 Miles

N W E S

Blythe Solar Power Project

Figure 8
Isopach Map of the Colorado River Alluvium

Source:

Palo Verde I, LLC

AECOM

Project: 60157720
Date: October 2010

J:\GIS\Projects\SolarMillinneum\Blythe\mxd\6200-gw-model\figure 8 Bottom of CRA.mxd

Data Sources:
Air Photo, California Spatial Information Library, NAIP, 2005 Riverside County

Water Basins, Department of Water Resources Website groundwater basin map file B118v3NAD27UTM10.zip

Groundwater elevation data is included in Appendix J

4/21-9B1

5/22-21H1

5/22-31E1

6/22-24D1

6/23-35E1

6/22-32R1

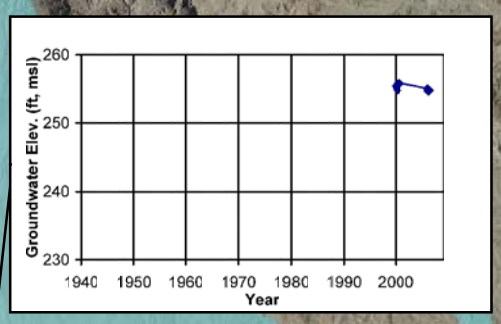
6/22-35R2

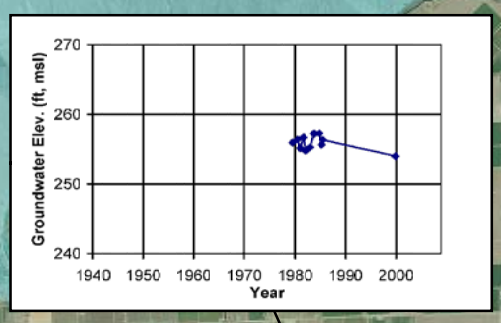
7/21-5C2

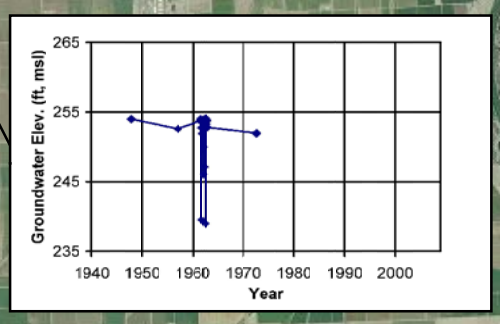
7/21-15A1

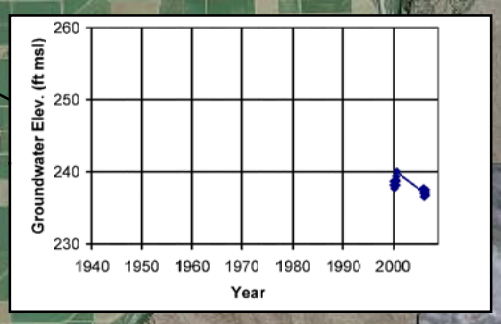
7/21-14B1

7/22-19K1









Map Location

Legend

- Groundwater Well Location
- Palo Verde Mesa Groundwater Basin
- Palo Verde Valley Groundwater Basin
- Project Right-of-Way

1 in = 2 miles

0 6,000 12,000 Feet

N W E S

Source:

Blythe Solar Power Project

Figure 9 Hydrographs - Valley Basin

Palo Verde I, LLC

AECOM

Project: 60157720
Date: October 2010

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Data Sources:
Air Photo, California Spatial Information Library, NAIP, 2005 Riverside County

Water Basins, Department of Water Resources Website groundwater basin map file B118v3NAD27UTM10.zip

Groundwater elevation data is included in Appendix J

4/21-9B1

5/22-21H1

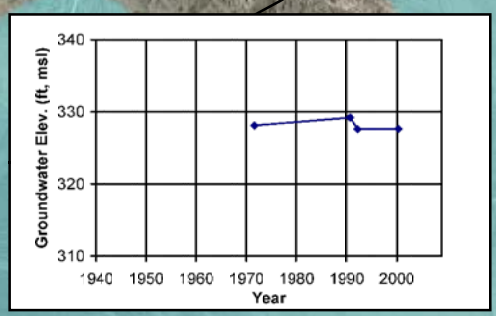
5/22-31E1

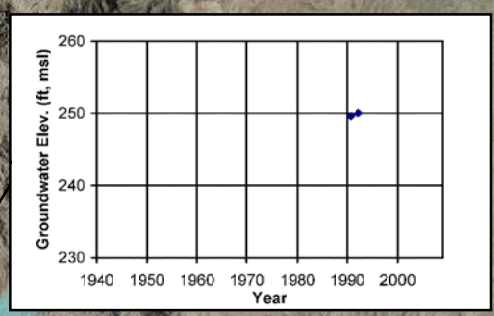
6/22-32R1

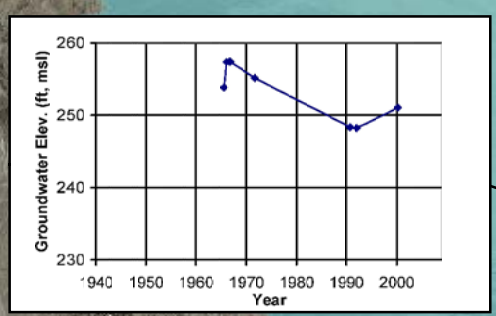
7/21-5C2

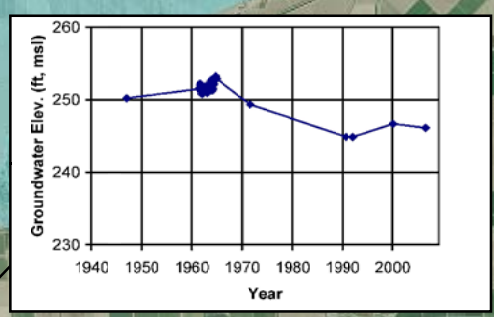
7/21-15A1

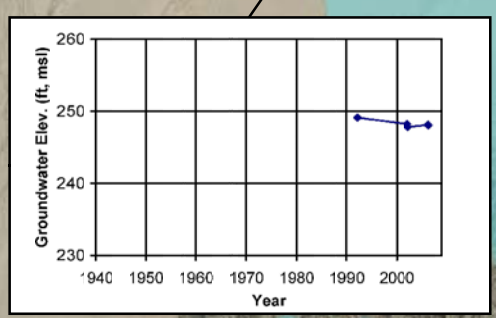
7/21-14B1

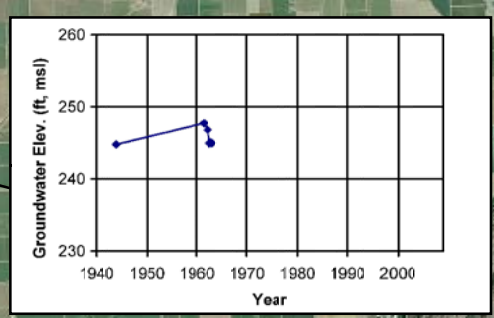


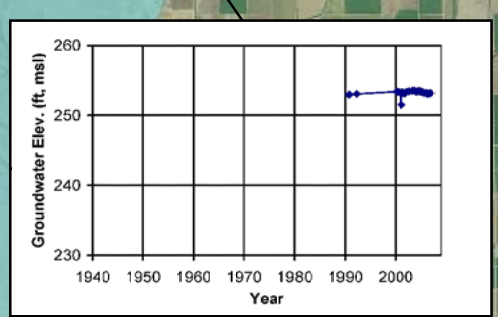












Map Location

Legend

- Groundwater Well Location
- Palo Verde Mesa Groundwater Basin
- Palo Verde Valley Groundwater Basin
- Project Right-of-Way

1 in = 2 miles

0 2 4 Miles

N W E S

Source:

Blythe Solar Power Project

Figure 10 Hydrographs - Mesa Basin

Palo Verde I, LLC

AECOM

Project: 60157720
Date: October 2010

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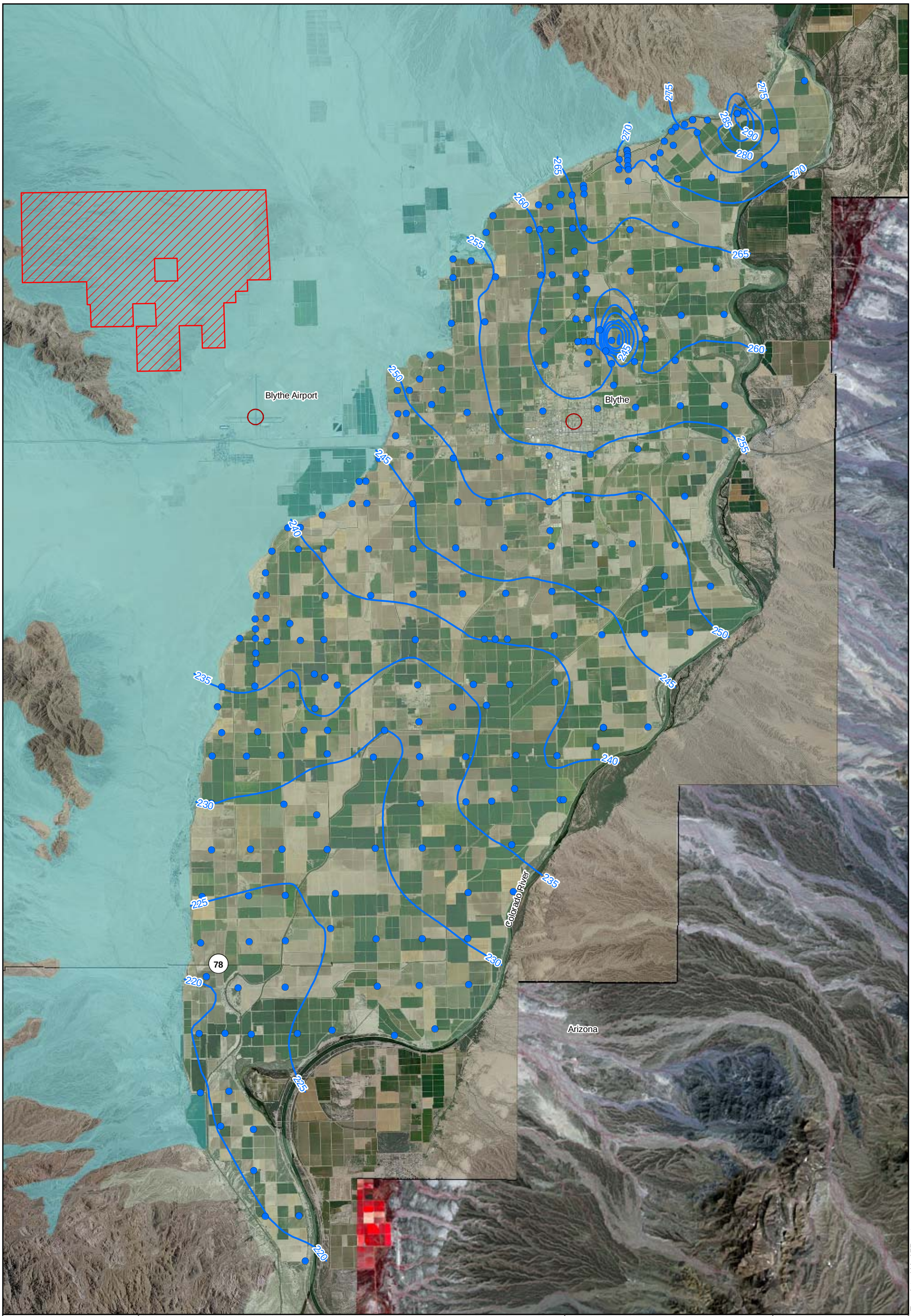

Map Location

Legend

- Contour of Groudwater Elevation
- PVID Well Point Location
- Project Right-of-Way
- Geographic/Cultural Area of Interest
- Palo Verde Mesa Groundwater Basin (Mesa Basin)
- Palo Verde Valley Groundwater Basin (Valley Basin)

1 in = 2 miles

0 2 4 Miles

N W E S

Source:

Blythe Solar Power Project

Figure 11 Shallow Zone Water Level

Palo Verde I, LLC

AECOM

Project: 60157720
Date: October 2010

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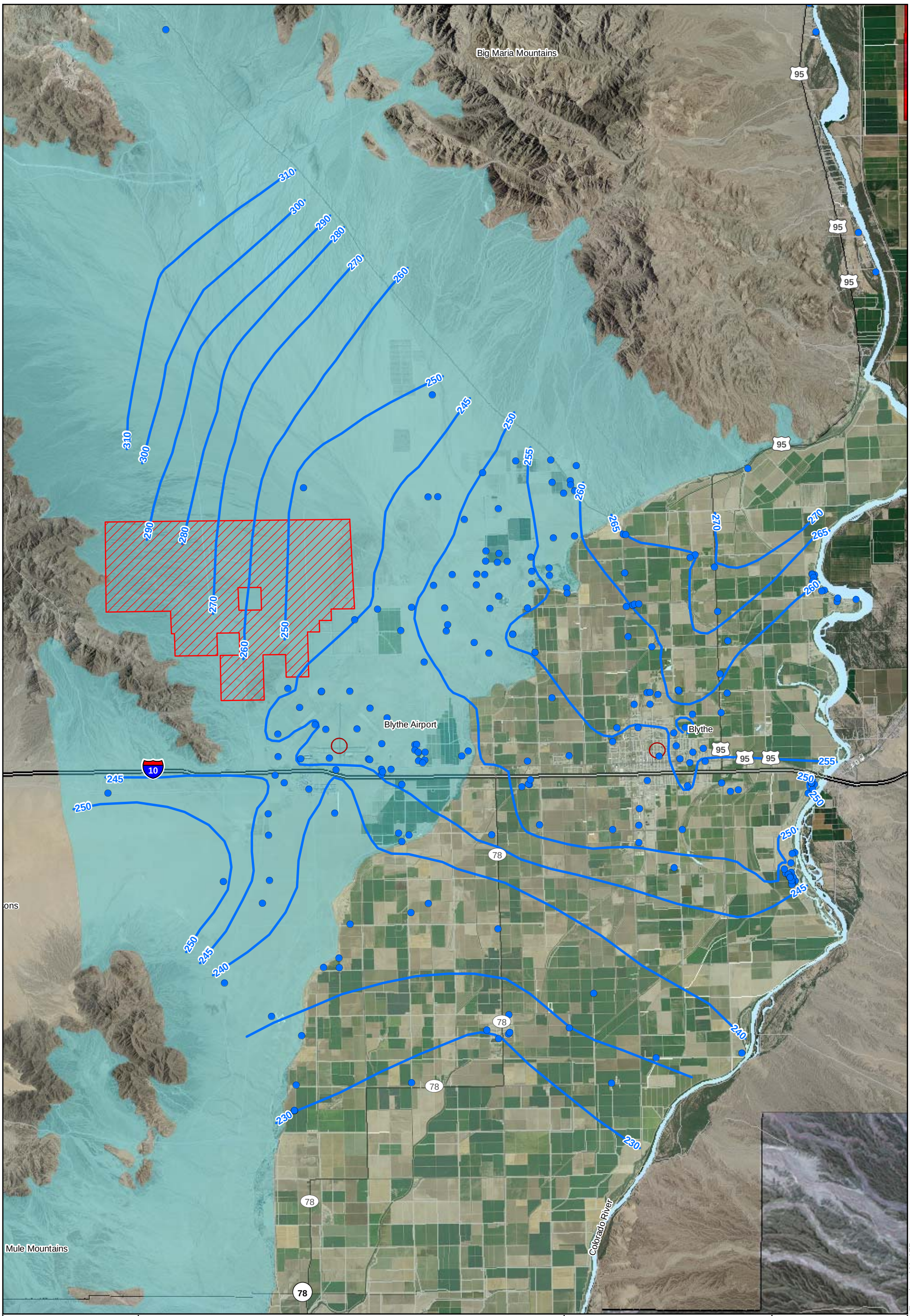

Map Location

Legend

- Contour of Groundwater Elevation (ft, msl)
- Well in USGS NWIS Database
- Project Right-of-Way
- Geographic/Cultural Area of Interest
- Freeway
- Highway / Major Road
- Palo Verde Mesa Groundwater Basin (Mesa Basin)
- Palo Verde Valley Groundwater Basin (Valley Basin)

1 in = 2 miles

0 2 4 Miles

N W E S

Source:

Blythe Solar Power Project

Figure 12
Deep Zone Water Level

Palo Verde I, LLC

AECOM

Project: 60157720
Date: October 2010

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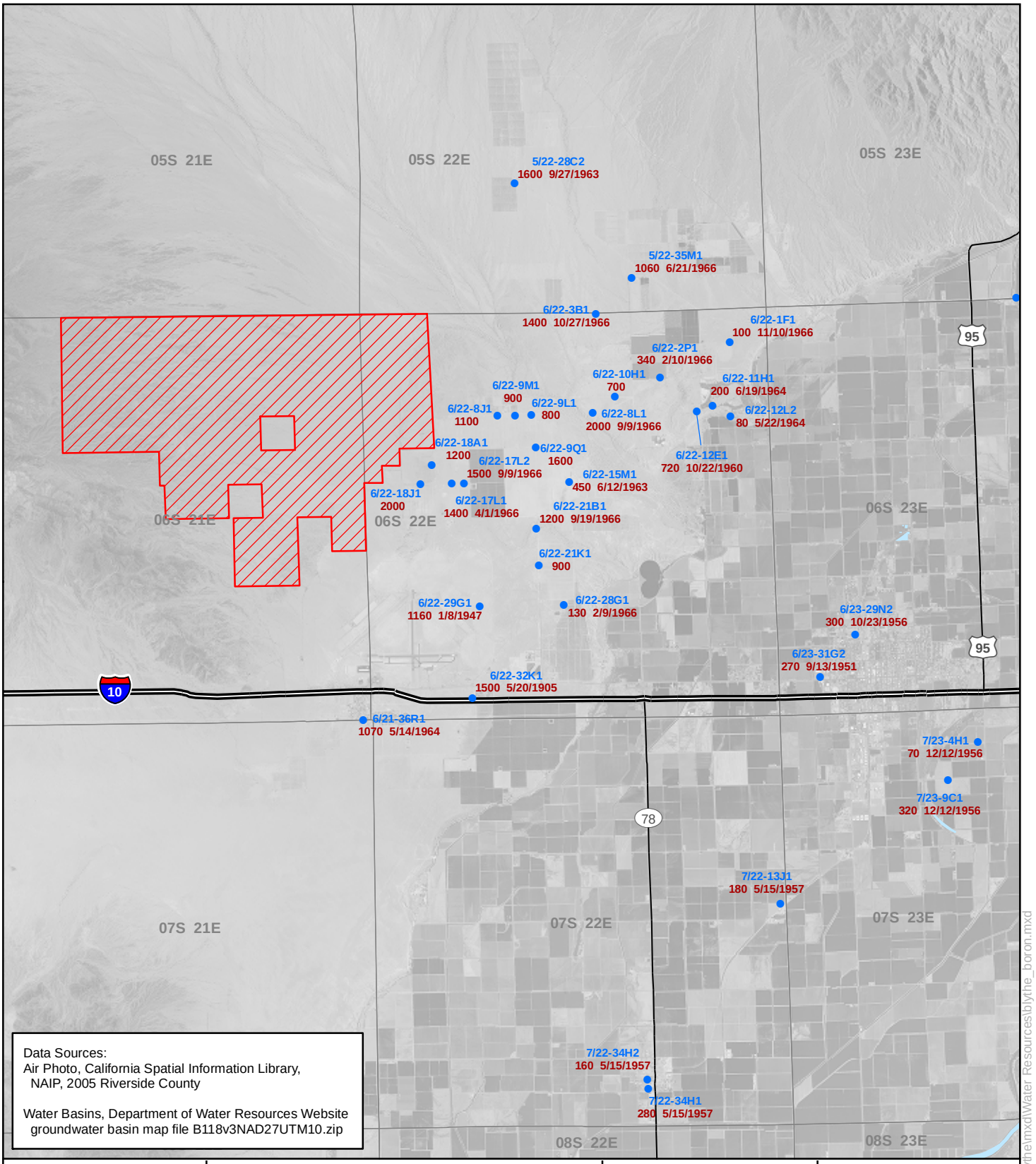

Data Sources:
Air Photo, California Spatial Information Library, NAIP, 2005 Riverside County

Water Basins, Department of Water Resources Website groundwater basin map file B118v3NAD27UTM10.zip

Map Location

Legend

Project Right-of-Way

Freeway

Highway / Major Road

Groundwater Well

7/22-34H2
0.6 5/15/1957
State Well Number and Boron Concentration (in mg/L) and Sample Date

1 in = 2 miles

0 1 2 Miles

N W E S

Blythe Solar Power Project

Figure 13
Boron Concentrations in Groundwater
Palo Verde Mesa Groundwater Basin

Palo Verde I, LLC

AECOM

Project: 60157720
Date: October 2010

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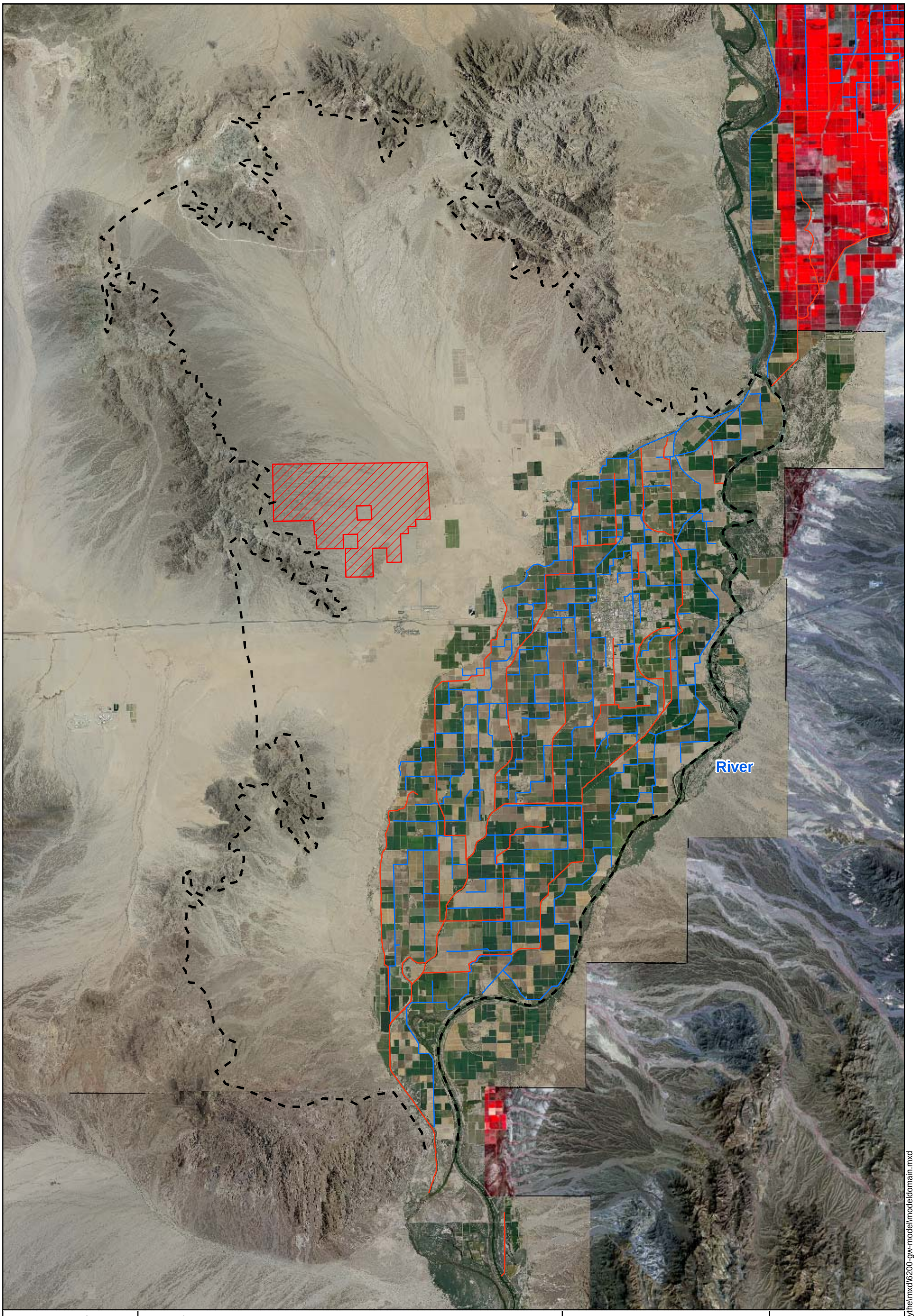

Map Location

Legend

- Groundwater Model Domain
- PVID Drains
- PVID Canals
- Project Right-of-Way

1:200,000

0 10,000 20,000 Feet

N W E S

Source:

Blythe Solar Power Project

Figure 14
Model Domain

Palo Verde I, LLC

AECOM

Project: 60157720
Date: October 2010

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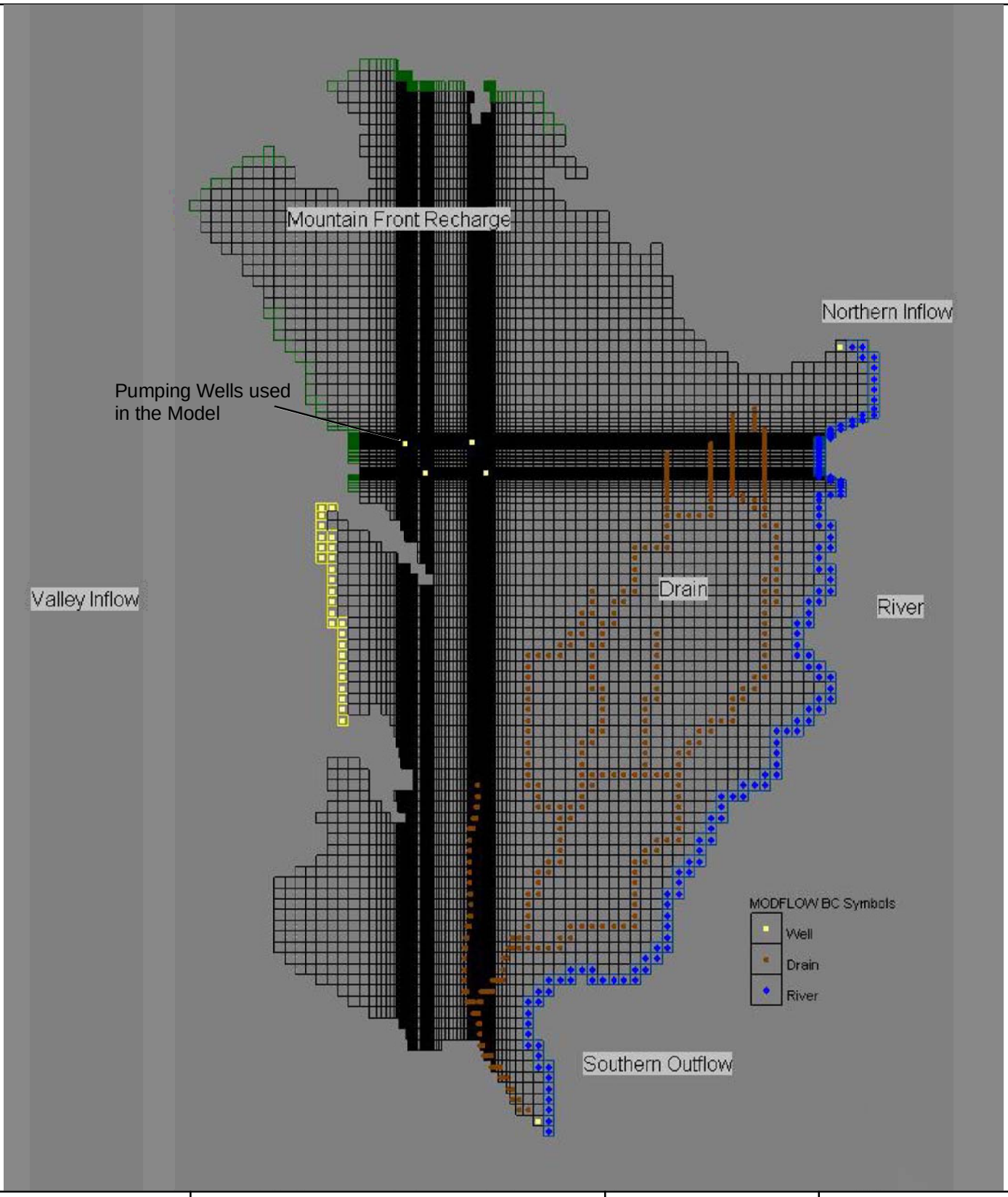

Map Location

Legend

- Model Grid
- River Cell
- Specified Flow Boundary

Not to Scale

Blythe Solar Power Project

Figure 15
Model Grid

Palo Verde I, LLC

AECOM

Project: 60157720
Date: October 2010

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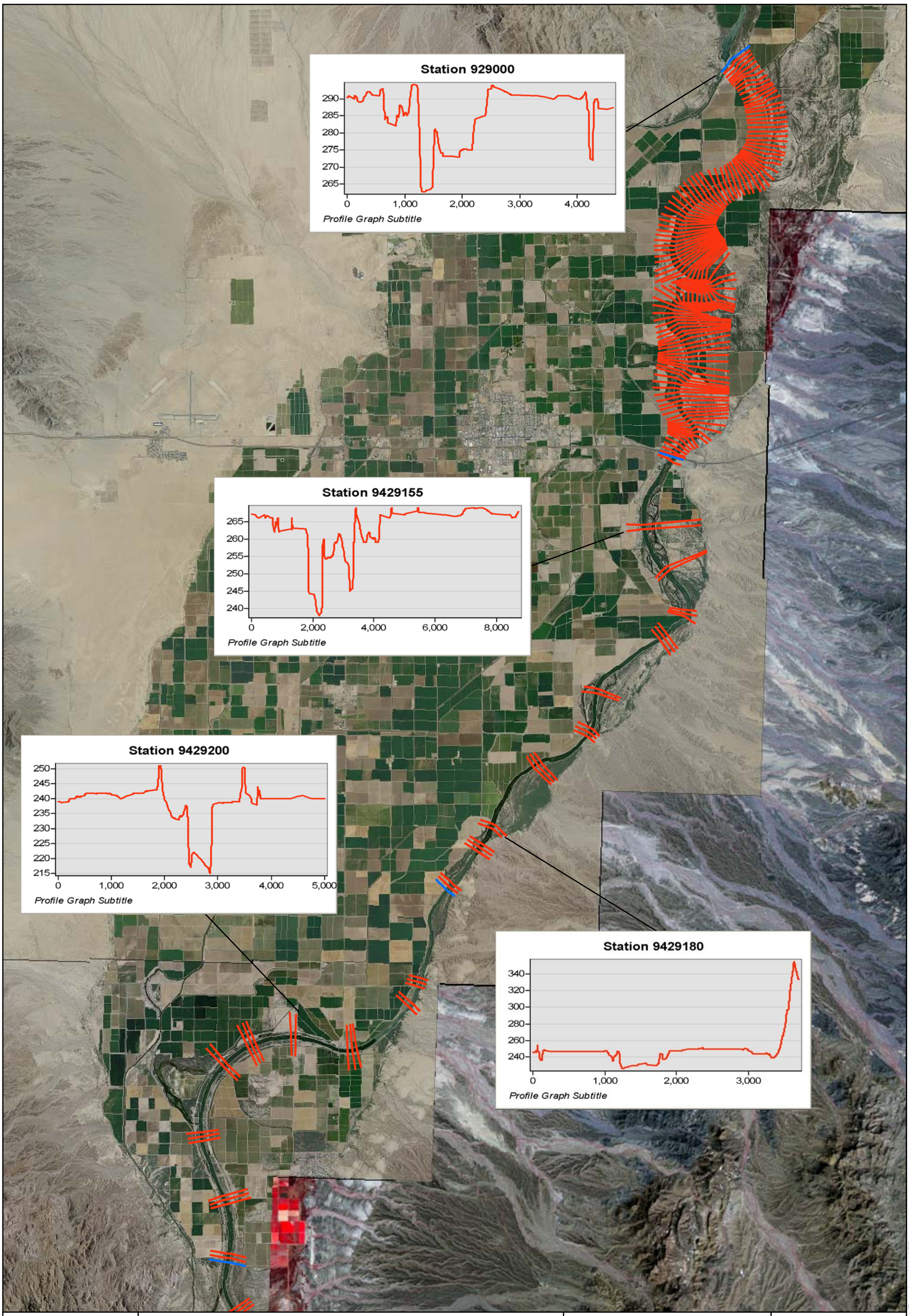

Map Location

Legend

River Transects

Transects Used in Palo Verde Valley Groundwater Model

Source:
River transects from U.S. Bureau of Reclamation, Lower Colorado Region, Yuma Area Office, August 31, 2010

1 in = 2 miles

0 2 4 Miles

N W E S

Blythe Solar Power Project

Figure 16
Colorado River Transects (USBR)

Palo Verde I, LLC

AECOM

Project: 60157720
Date: October 2010

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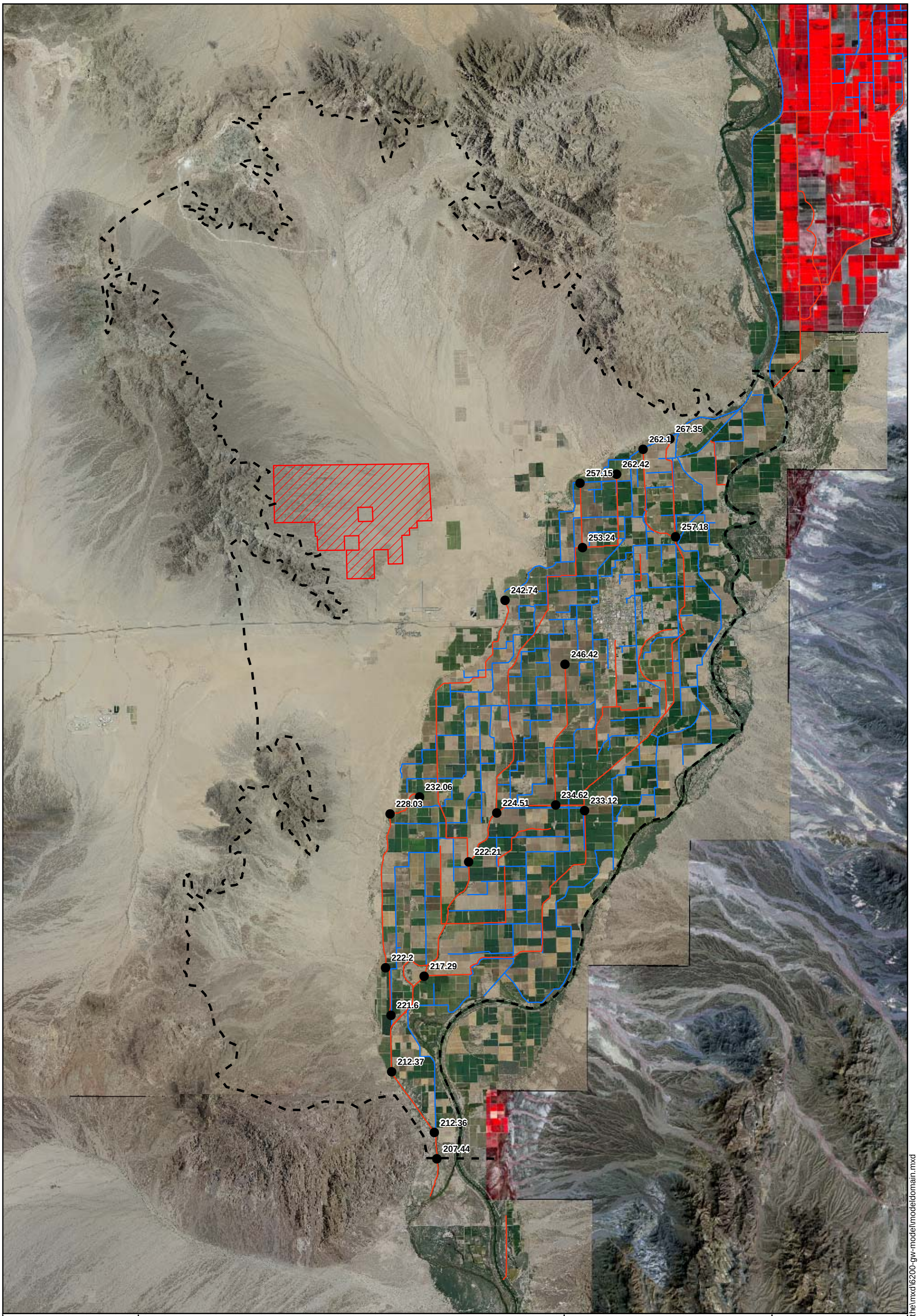

Map Location

Legend

- Drainage Points with Bottom of Drainage Elevation
- PVID Drains
- PVID Canals
- Groundwater Model Domain
- Project Right-of-Way

1:200,000 0 10,000 20,000 Feet

N W E S

Blythe Solar Power Project

Figure 17
PVID Drains and DEM Locations

Palo Verde I, LLC

AECOM

Project: 60157720
Date: October 2010

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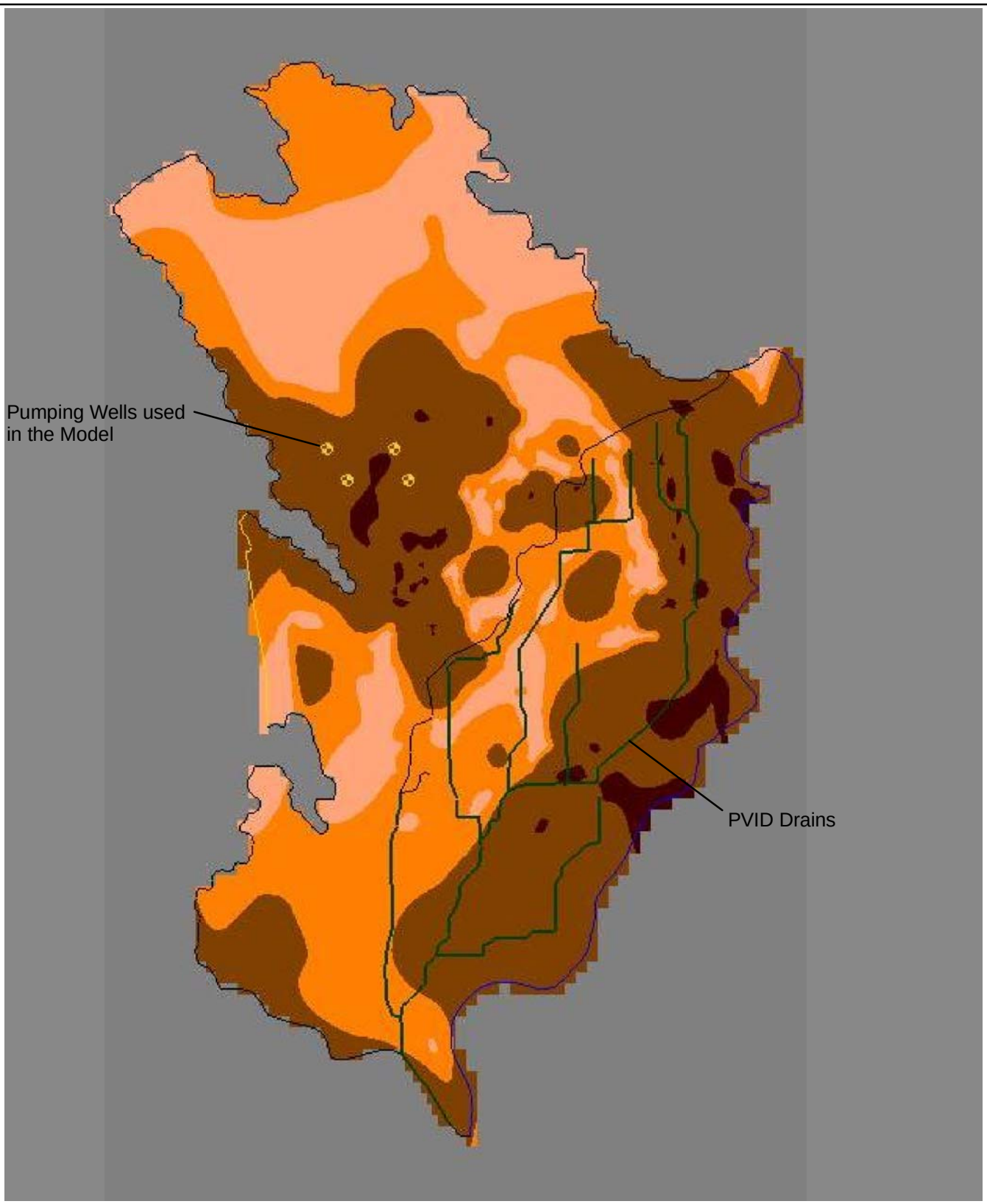

Map Location

- 1 foot per day
- 10 feet per day
- 100 feet per day
- 1000 feet per day

N
W
E
S

Blythe Solar Power Project

Figure 18
Hydraulic Conductivity Zonation

Palo Verde I, LLC

AECOM

Project: 60157720
Date: October 2010

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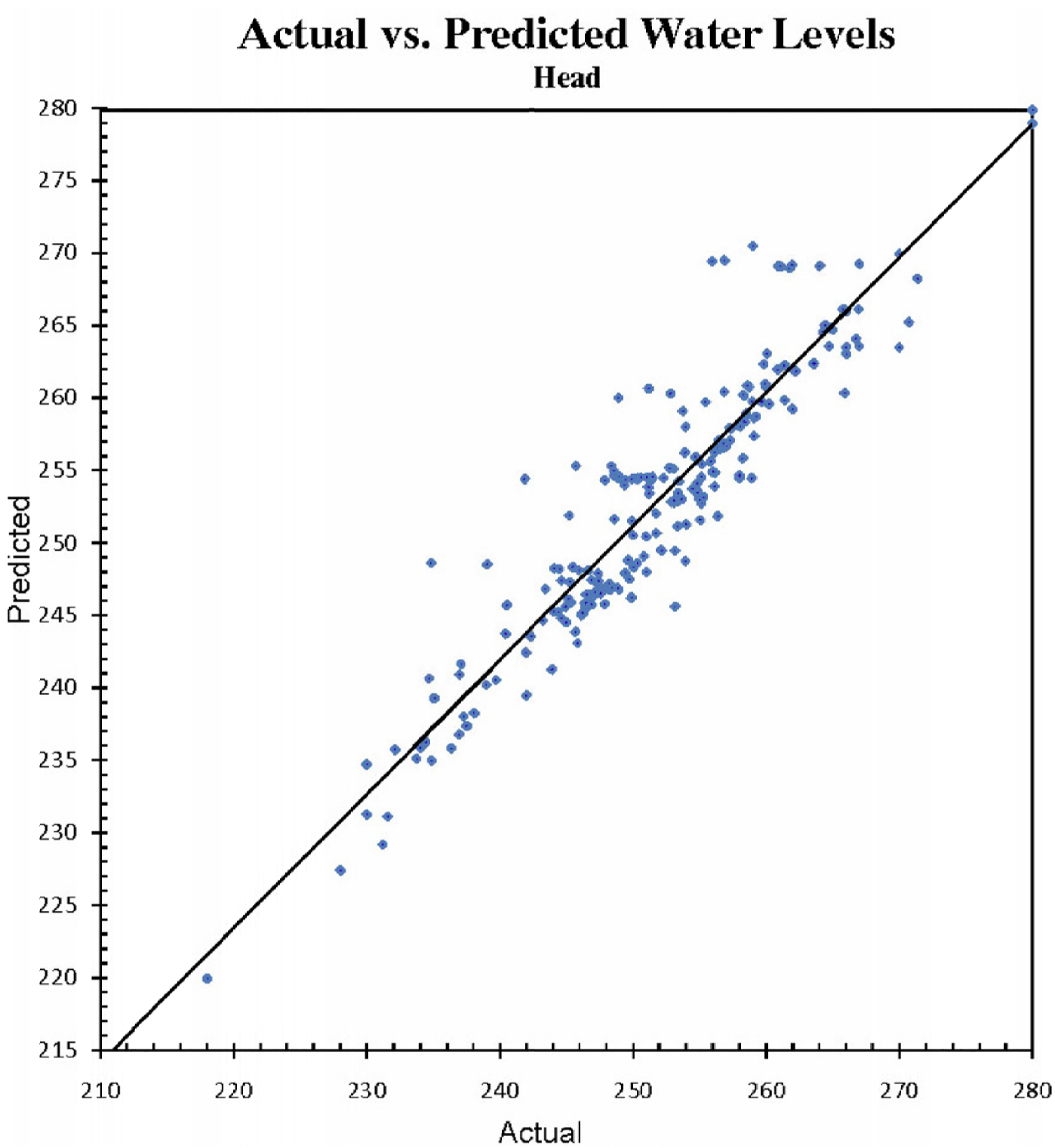


Map Location

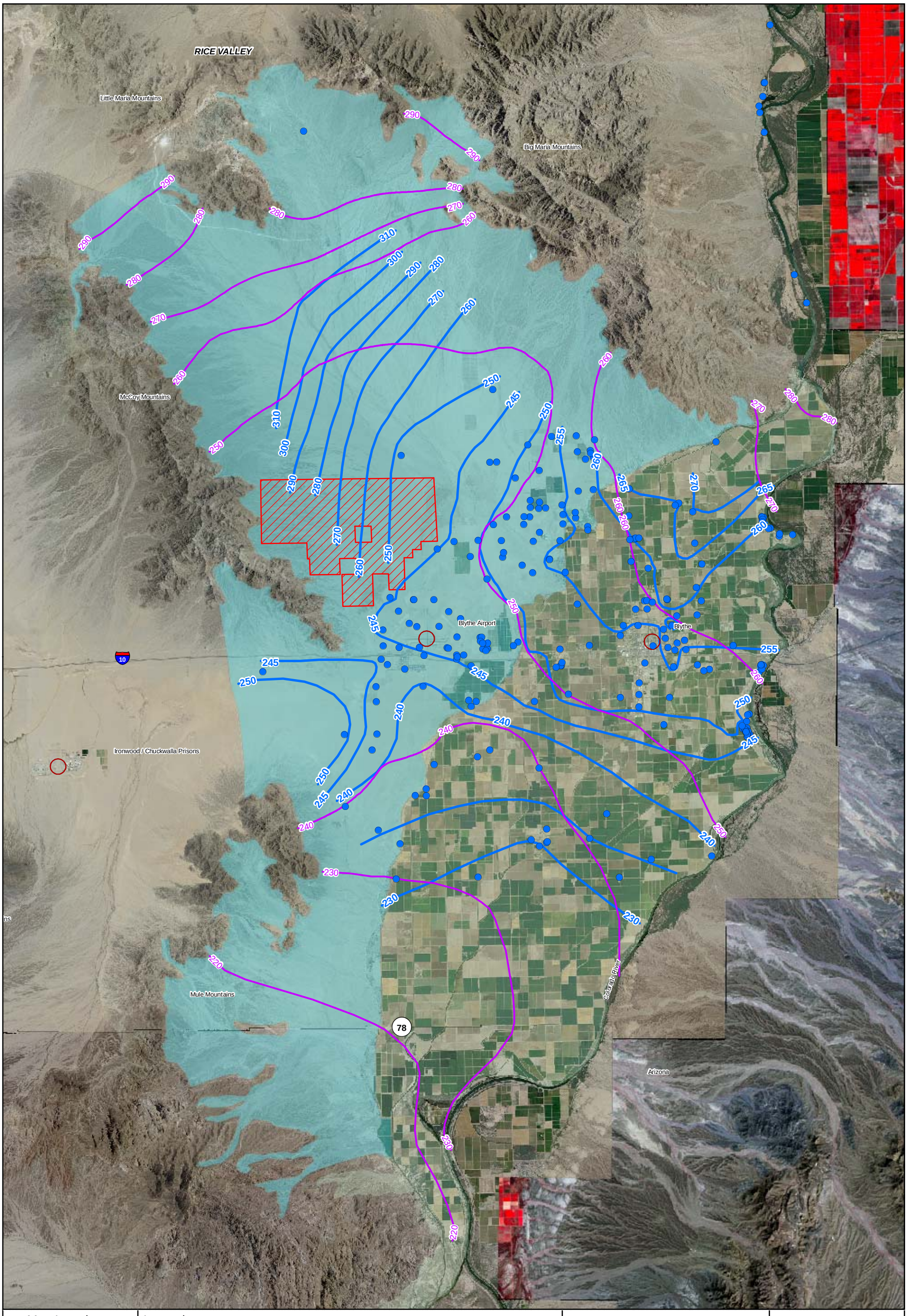
Blythe Solar Power Project

Figure 19 Calibration - Actual vs. Predicted Water Levels

Palo Verde I, LLC

AECOM

Project: 60157720
Date: October 2010



Map Location

Legend

- Model Predicted Water Levels (ft, msl)
- Contour of Groundwater Elevation (ft, msl)
- Well in USGS NWIS Database
- Project Right-of-Way
- Geographic/Cultural Area of Interest
- Palo Verde Mesa Groundwater Basin (Mesa Basin)
- Palo Verde Valley Groundwater Basin (Valley Basin)

1 in = 3 miles

0 3 6 Miles

N W E S

Blythe Solar Power Project

Figure 20
Model Predicted Water Levels

Source:

Palo Verde I, LLC

AECOM

Project: 60157720
Date: October 2010

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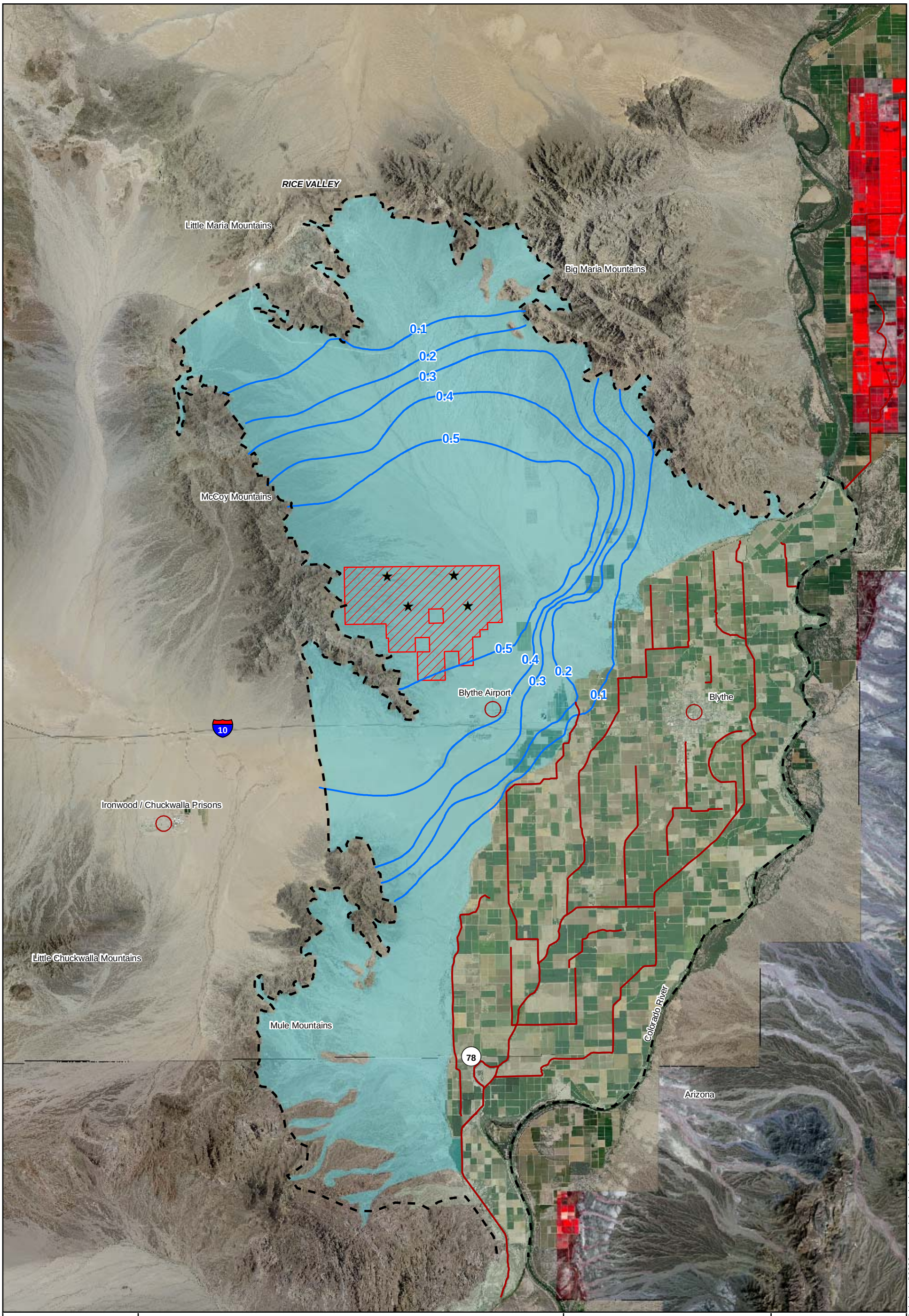


Map Location

Legend

- ★ Pumping Wells used in the Model
- Model Predicting Drawdown (30 years) 0.1 foot contour interval
- Groundwater Model Domain
- PVID Drain
- Geographic/Cultural Area of Interest
- Palo Verde Mesa Groundwater Basin (Mesa Basin)
- Palo Verde Valley Groundwater Basin (Valley Basin)
- Project Right-of-Way

1:200,000

0 10,000 20,000 Feet

N W E S

Blythe Solar Power Project

Figure 21
Model Predicted Zone of Influence
30 Years of Operation

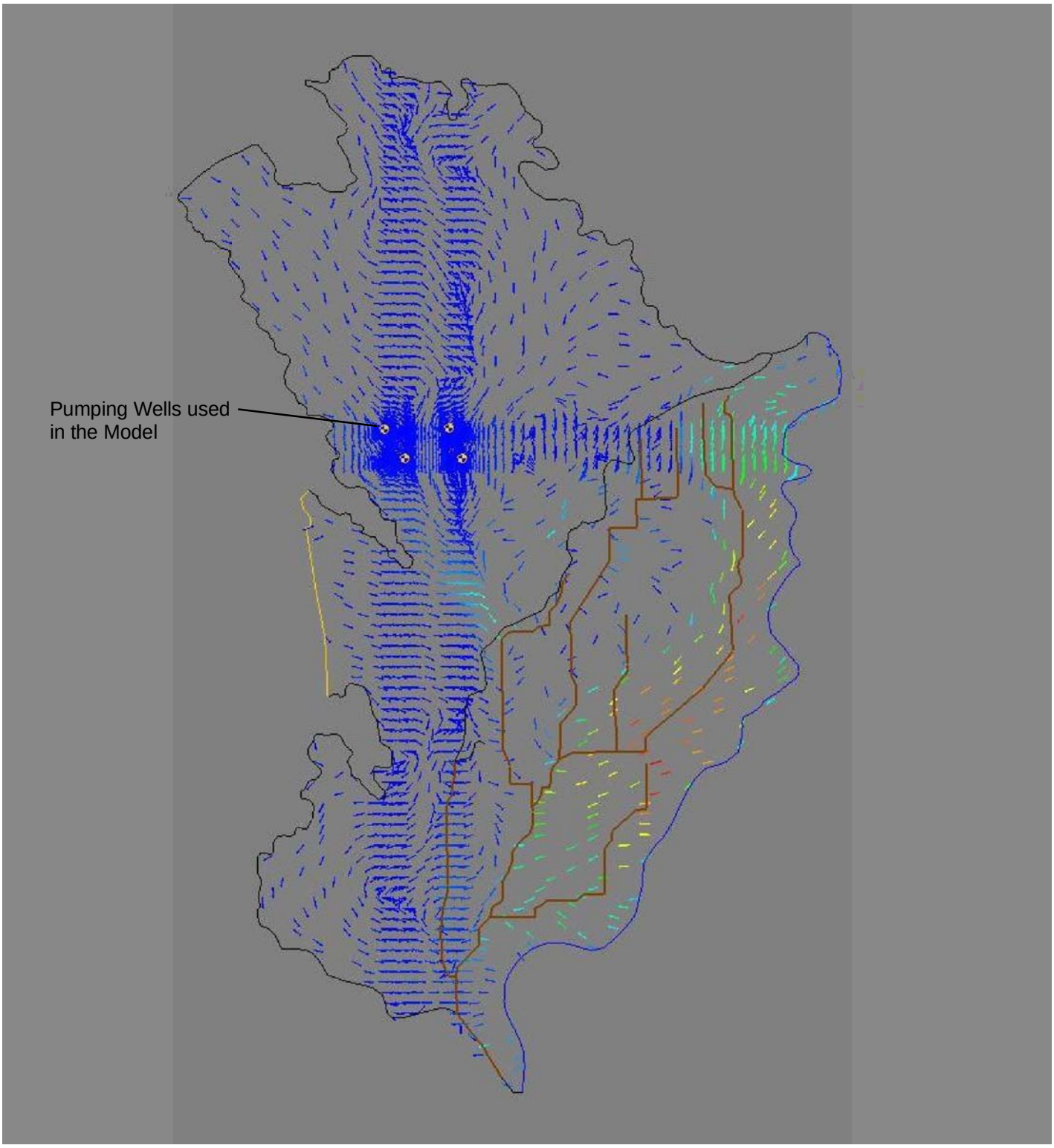
Source:

Palo Verde I, LLC

AECOM

Project: 60157720
Date: October 2010

J:\GIS\Projects\SolarMillinneum\Blythe\mxd\6200-gw-model\model-drawdown30yrs.mxd



Map Location

Groundwater Flow Vector

Low
High
Magnitude

Not to Scale

Blythe Solar Power Project

Figure 22
Model Predicted Flow Vectors and Magnitude

Palo Verde I, LLC

AECOM

Project: 60157720
Date: October 2010

Y:\Projects\Solar_Millennium\Figure_Templates\85x11P.mxt

Tables

Table-1 Forecasted Construction Phasing Summary

Phase	Area of Site	Total Area (acres)
Phase 1a	Black Rock Road, Shared Facilities, Construction Power, Utilities Corridor including the main access road, Water Wells and initial portion of Unit #1	772.68
Phase 1b	Remainder of Unit #1, Unit #2 and Gen-tie line	3,024
Phase 2	Unit #3 and Unit #4	3,227.82
	Total	7,024.5

TABLE 2
WATER BALANCE
PALO VERDE MESA GROUNDWATER BASIN (VALLEY and MESA BASINS)
PALO VERDE VALLEY GRONDWATER MODEL
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORINA

RECHARGE AND DISCHARGE			BASIS FOR ESTIMATE	WATER BALANCE ESTIMATES REPORTED BY OTHERS (acre-feet per year)			
				Metzger, and others, 1973 USGS Professional Paper 486-G[1]	Owen-Joyce, 1984 USGS 84-4236[2]	Owen-Joyce, 1987 USGS 87-4078[2]	WorleyParsons 2010
RECHARGE (INFLOW)		**acre-feet per year**					
UNDERFLOW from the CHUCKWALLA		**1,000**	Estimate after WorleyParsons (2010), "Response to Cure, Water Resources Data Request 1-9, Application for Certification - Genesis Solar Power Project (09-AFC-8), April 2010.	**400**	**400**	**--**	**988**
UNDERFLOW from PARKER VALLEY		**3,500**	Underflow calculated using transmissivity of 26,000 ft^2/d (from Leake, 2008), gradient of 0.0003 ft/ft, a 19,000-foot width, and 600-foot depth (from Metzger et.al.,1973) for the saturated section.	**3,000**	**--**	**--**	**--**
PERCOLATION[3]							
	AGRICULTURE RETURN - MESA	**3,500**	There are a total of approximately 2,683 acres of irrigated agricultural land on the Mesa (PVID February 2010). Of the 2,683 acres, approximately 1,862 acres are irrigated with surface water from PVID and the remaining 724 acres are irrigated with groundwater. Agricultural return on the Mesa was calculated for the 2,683 acres using the DWR Water Use Estimates (2001) for water use (4.5-5.85 acre-feet/acre) and crop efficiency (70%-75%). The return was the difference between the total applied water less the consumptive use as derived by the efficiency estimates.	**--**	**9,500**	**9,500**	**--**
	AGRICULTURE RETURN - VALLEY	**67,000**	The estimate is based on the average of PVID diversions to the Valley (1993-2008) (743,000 acre-feet) less the average total spill return (136,000 acre-feet) over the same period,less the seepage (125,000) and evaporation loss (5,000) and less average consumptive use estimates for the PVID (420,000) since 1993.	**0**	**0**	**0**	**--**
	POTW RETURN	**750**	Estimate of return from the Blythe POTW based on inflormation provided on the daily flow to evaporation/percolration ponds (City of Blythe website), an assumption that the total pond area is aobut 120 acres (estimate dervied from photo review) and an annual evaporation rate of 71 inches.	**--**	**--**	**--**	**--**
	MOUNTAIN FRONT	**5,000**	Estimate derived using the average annual isoheytal contours shown on Figure 6 from Hely and Peck (1964), wherein the average annual precipitation was overlayed onto the topography of the Palo Verde Valley to provide an estimate of total precipitation in acre-feet for the Basin under an assumption that 5% of the total estimate from precipitation would return as deep percolation to the groundwater basin.	**2,000**	**2,000**		**--**
	IRRIGATION CANAL LEAKAGE (LESS EVAPORATION)	**120,000**	After Bookman Edmondson (1976) and Owen-Joyce (1984), 125,000 afy (Canal Leakage) - 5,000 (Evaporation).	**--**	**120,000**	**120,000**	**--**
RIVER DISCHARGE TO GROUNDWATER (LOSING CONDITION)		**225,850**	Estimate based on the difference between the measured values of total discharge less the estimate of agricultural return and canal leakage (inflow). The estimate was made under the assumption that groundwater levels have not changed significantly and as such there must be a balance between inflow and outflow in the Palo Verde Valley.	**361,000**	**3,100**		**--**
BEDROCK		**0**	Although recharge from the bedrock is possible there is insufficient well data to determine flux into the Valley or Mesa Groundwawer Basins.	**--**	**--**	**--**	**--**
	TOTAL (INFLOW)	**426,600**		**366,400**	**135,000**	**129,500**	**--**
DISCHARGE (OUTFLOW)		**acre-feet per year**					
UNDERFLOW OUT of the PALO VERDE and CIBOLA VALLEY AQUIFER		**0**	After Metzger et al (1973).	**0**	**0**	**--**	**--**
GROUNDWATER PUMPING							
	AGRICULTURE - MESA	**3,600**	To determine agricultural diversions on the PV Mesa, the "Estimated Water Use" values from DWR (2001) were applied to a total of 724 acres of agricultural land that uses groundwater for irrigation. There are approximately 364 acres of agricultural land inside the PVID boundary that use private wells and approximately 360 acres of agricultural land outside of the PVID boundaries that use groundwater for irrigation.	**--**	**--**	**--**	**--**
	MUNICIPAL and DOMESTIC	**7,500**	Within the City Limits as per the Department of Public Works Department, the City of Blythe pumps the Mesa Ranch Well #3 for domestic use (230 afy) and PVC Well #2 for municipal use at the Palo Verde College (260 AFY), Main System (3700 AFY) and Mesa Well #2 for the Golf Course (560 AFY). The County of Riverside operates one well (Airport Well #7) at the Blythe Airport that serves the Mesa Verde Community (47 afy). This estimate also includes pumping for the Blythe Energy Plant I (3,300 afy). It does not include pumping for BEP II as this well is not yet in operation. Information after City of Blythe Department of Public Works, Kevin Nelson, February 2010.	**--**	**2,000 (1981)**	**--**	**--**
UNMEASURED RETURN (GAINING CONDITION)		**50,000**	Average unmeasured return after the USBR, Lower Colorado River Accounting and Water Use Report - Arizona, California, and Nevada - Calendar Year 2003-2009.		**23,900**	**2,500-31,700**	**--**
CONSUMPTIVE USE - NATIVE VEGETATION		**8,500**	Estimate derived from distrubution of riparian vegetation within the PVID area (Figure 3-5 "Land Cover Types in Reach 4", Lower Colorado River Multi-Species Conservation Plan: CDFG 2081-2005-008-06), and the estimate of consumptive use and evaporation loss as provided for these areas and summarized in Table-1 "Agricultural and Riparian Vegetation ET, and Evaporation by Water User, Lower Colorado River, Hoover Dam ot Mexico", Lower Colorado River Accounting System, Evapotranspiration Calculations, 2003-2009.	**136,000**	**--**	**--**	**--**
GROUNDWATER DISCHARGE		**357,000**	Average Outfall Drain Return for 1993-2008. See Appendix E.	**--**	**419,500**	**--**	**--**
	TOTAL (OUTFLOW)	**426,600**		**-86,000**	**--**	**--**	**--**
NOTES	**WATER BALANCE**	**0**					

1	The consumptive use non-native vegetation estimate provided by Metzger and others includes areas outside the Palo Verde Valley.
2	Owen-Joyce (1984) estimated the inflow to the Palo Verde Mesa (Mesa Basin) at 9,500 afy and correspondingly estimated the outflow to the Palo Verde Valley (Valley Basin) at 4,700 afy.
3	Precipitation recharge onto the Palo Verde Mesa floor assumed to be negligible. It is assumed that all water transpires or evaporates as it falls onto the valley floor. There is no return to the groundwater from direct precipitation.

TABLE 3
MASS BALANCE - CALIBRATED (BASE) MODEL
PALO VERDE VALLEY GROUNDWATER MODEL
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

MASS BALANCE - BASE CONDITION AND SENSITIVITY ANALYSIS FOR CHANGES IN DRAIN CONDUCTANCE

WATER BALANCE		NO PUMPING						PUMPING						PUMPING					
		BASE		drain 50%		drain 20%		drain 50%		BASE		drain 20%		drain 50%		BASE		drain 20%	
		No Pumping						CUMULATIVE AT THE END OF 2015						CUMULATIVE AT THE END OF 2043					
		ft^3	AF	ft^3	AF	ft^3	AF	ft^3	AF	ft^3	AF	ft^3	AF	ft^3	AF	ft^3	AF	ft^3	AF
Recharge (into the system)	Storage							216,536,720	4,971	216,827,568	4,978	216,983,744	4,981.3	832,166,848	19,104	845,266,944	19,405	850,215,040	19,518
	Inflow	68,757,608	1,578	68,757,608	1,578	68,757,608	1,578	412,545,632	9,471	412,545,632	9,471	412,545,632	9,471	2,269,001,472	52,089	2,269,001,472	52,089	2,269,001,472	52,089
	River	8,337,349,632	191,399	11,328,987,136	260,078	7,282,492,416	167,183	67,973,939,200	1,560,467	50,024,108,032	1,148,396	43,694,968,832	1,003,098	373,856,927,744	8,582,574	275,132,710,912	6,316,178	240,322,592,768	5,517,048
	Recharge	8,538,060,800	196,007	8,538,060,800	196,007	8,538,060,800	196,007	51,228,368,896	1,176,042	51,228,368,896	1,176,042	51,228,368,896	1,176,042	281,756,041,216	6,468,229	281,756,041,216	6,468,229	281,756,041,216	6,468,229
	sub-total	16,944,168,040	388,985	19,935,805,544	457,663	15,889,310,824	364,768	119,831,390,448	2,750,950.2	101,881,850,128	2,338,885	95,552,867,104	2,193,592.0	658,714,137,280	15,121,995.8	560,003,020,544	12,855,900	525,197,850,496	12,056,883.6
Dishcarge (out of the system)	Storage							50,105	1.2	66,260	1.5	55,791	1.3	2,513,108	57.7	2,517,769	57.8	2,501,310	57.4
	Outflow	45,867,360	1,053	45,867,360	1,053	45,867,360	1,053	492,928,096	11,316	492,928,096	11,316	492,928,096	11,316	2,434,993,408	55,900	2,434,993,408	55,900	2,434,993,408	55,900
	Drain	16,898,304,000	387,932	19,889,987,584	456,611	15843448832	363,716	119,338,606,592	2,739,637	101,388,959,744	2,327,570	95,059,886,080	2,182,275	656,277,635,072	15,066,061	557,566,263,296	12,799,960	522,760,454,144	12,000,929
	River						0												
	sub-total	16,944,171,360	388,985	19,935,854,944	457,664	15,889,316,192	364,769	119,831,584,793	2,750,955	101,881,954,100	2,338,888	95,552,869,967	2,193,592	658,715,141,588	15,122,019	560,003,774,473	12,855,918	525,197,948,862	12,056,886
Mass Balance	% discrepany	-2.0E-07	-2.0E-07	-2.5E-06	-2.5E-06	-3.4E-07	-3.4E-07	-1.6E-06	-1.6E-06	-1.0E-06	-1.0E-06	-3.0E-08	-3.0E-08	-1.5E-06	-1.5E-06	-1.3E-06	-1.3E-06	-1.9E-07	-1.9E-07

CUMULATIVE CHANGE IN DRAIN FLOW - BASE CONDITION

Cumulative Difference: Non-Pumping and Base Model			
condition	ft^3	af	cumulative difference, af
no pumping	16,898,304,000	387,932	0
2015	101,388,959,744	2,327,570	**-20**
2043	557,566,263,296	12,799,960	**-1,785**

SENSITIVITY ANALYSIS - 50% AND 20% SENSITIVITY SCENARIOS

Cumulative Difference Non-Pumping and Drain Conductance @50%			
condition	ft^3	af	cumulative difference, af
no pumping	19,889,987,584	456,611	0
2015	119,338,606,592	2,739,637	**-30**
2043	656,277,635,072	15,066,061	**-2,111**

Cumulative Difference Non-Pumping and Drain Conductance @20%			
condition	ft^3	af	cumulative difference, af
no pumping	15,843,448,832	363,716	0
2015	95,059,886,080	2,182,275	**-19**
2043	522,760,454,144	12,000,929	**-1,684**

NOTES

1	**Base model or calibrated model. This model run assumed that the drain conductance was 25% of the USGS value for the Colorado River (Leake and others 2008)**
2	**50% drain model. This model run is a sensitivity analysis that assumed drain conductance was 50% of the USGS value for the Colorado River (Leake and others 2008)**
3	**20% drain model. This model run is a sensitivity analysis that assumed drain conductance was 20% of the USGS value for the Colorado River (Leake and others 2008)**

AFY	**acre-feet per year**
ft^3/day	**cubic feet per day**

TABLE 4
MODEL MASS BALANCE - PREDICTIVE SENSITIVY ANALYSIS
HYDRAULIC CONDUCTIVITY
PALO VERDE VALLEY GROUNDWATER MODEL
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

SENSITIVITY ANALYSIS - 1/2 THE CALIBRATED HYDRAULIC CONDUCTIVITY

WATER BALANCE		HYDRAULIC CONDUCTIVITY 1/2 THE BASE (CALIBRATED) MODEL[1]					
		no pumping		2015		2043	
		ft^3	AF	ft^3	AF	ft^3	AF
Recharge (into the system)	Storage	0	0	217,470,400	4,992	876,782,464	20,128
	Inflow	68,757,608	1,578	412,545,632	9,471	2,269,001,472	52,089
	River	5,782,189,568	132,741	34,693,156,864	796,445	190,812,356,608	4,380,449
	Recharge	8,538,060,800	196,007	51,228,368,896	1,176,042	281,756,041,216	6,468,229
	sub-total	14,389,007,976	330,326	86,551,541,792	1,986,950	475,714,181,760	10,920,895
Dishcarge (out of the system)	Storage	0	0	96,607	2	2,946,825	68
	Outflow	45,867,360	1,053	492,928,096	11,316	2,434,993,408	55,900
	Drain	14,313,170,944	328,585	85,878,775,808	1,971,505	472,287,739,904	10,842,235
	River	29,973,384	688	179,838,576	4,129	989,110,784	22,707
	sub-total	14,389,011,688	330,326	86,551,639,087	1,986,952	475,714,790,921	10,920,909
Mass Balance	% discrepany	-2.6E-07	-2.6E-07	-1.1E-06	-1.1E-06	-1.3E-06	-1.3E-06

Cumulative Discharge of Drain

condition	ft^3	af	cumulative difference, af
no pumping	14,313,170,944	328,585	0
2015	85,878,775,808	1,971,505	-5.7
2043	472,287,739,904	10,842,235	**-1,077**

Notes:
1. cumulative difference is compared to no pumping cumulative
2. run i.d. rc50dc25k1000mfr5000_K l

SENSITIVITY ANALYSIS - 2X THE CALIBRATED HYDRAULIC CONDUCTIVITY

WATER BALANCE		HYDRAULIC CONDUCTIVITY TWO TIMES THE BASE (CALIBRATED) MODEL[2]					
		no pumping		2015		2043	
		ft^3	AF	ft^3	AF	ft^3	AF
Recharge (into the system)	Storage			214,903,104	4,933	775,617,216	17,806
	Inflow	68,757,608	1,578	412,545,632	9,471	2,269,001,472	52,089
	River	11,842,115,584	271,858	71,052,697,600	1,631,145	390,792,085,504	8,971,352
	Recharge	8,538,060,800	196,007	51,228,368,896	1,176,042	281,756,041,216	6,468,229
	sub-total	20,448,933,992	469,443	122,908,515,232	2,821,591	675,592,745,408	15,509,475
Dishcarge (out of the system)	Storage			52,143	1	1,614,692	37
	Outflow	45,867,360	1,053	492,928,096	11,316	2,434,993,408	55,900
	Drain	20,386,525,184	468,010	122,316,390,400	2,807,998	672,610,910,208	15,441,022
	River	16,544,364	380	99,265,864	2,279	545,958,400	12,533
	sub-total	20,448,936,908	469,443	122,908,636,503	2,821,594	675,593,476,708	15,509,492
Mass Balance	% discrepany	-1.4E-07	-1.4E-07	-9.9E-07	-9.9E-07	-1.1E-06	-1.1E-06

Cumulative Discharge of Drain

condition	ft^3	af	cumulative difference, af
no pumping	20,386,525,184	468,010	0
2015	122,316,390,400	2,807,998	-63.4
2043	672,610,910,208	15,441,022	**-3,315**

Notes:
1. cumulative difference is compared to no pumping cumulative
2. run i.d. rc50dc25k1000mfr5000_K c

NOTES

1	The model was run changing the hydraulic conductivity by one half the calibrated value
2	The model was run changing the hydraulic conductivity by two times the calibrated value
AFY	acre-feet per year
ft^3/day	cubic feet per day

APPENDIX A

GROUNDWATER WELLS AND WATER LEVEL DATABASE (USGS)

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
02S/20E-16P01S	002S020E16P001S	33.995293	-114.886915	879	304					10/1/1917	297	582.00	582.000
02S/20E-28H01S	002S020E28H001S	33.971585	-114.876192	903.6						3/20/1992	308.92	594.68	590.960
02S/20E-28H01S	002S020E28H001S	33.971585	-114.876192	903.6						3/9/2001	316.36	587.24	590.960
02S/20E-36F02S	002S020E36F002S	33.957238	-114.835524	817						3/16/1992	203.01	613.99	613.990
02S/23E-36H02S	002S023E36H002S	33.962323	-114.512985	315	72					5/4/1995	10.76	304.24	304.240
02S/24E-31C01S	002S024E31C001S	33.963823	-114.500873	320						1/13/1995	17.54	302.46	302.460
02S/24E-31C02S	002S024E31C002S	33.961295	-114.502735	320	72					5/4/1995	12.23	307.77	307.770
02S/24E-31D01S	002S024E31D001S	33.963823	-114.505568	320	72					5/4/1995	11.34	308.66	308.660
03S/20E-13J01S	003S020E13J001S	33.909739	-114.828023	882	585					3/28/1905	355	527.00	527.000
03S/21E-18D01S	003S021E18D001S	33.917517	-114.818023	885						3/29/1962	284.99	600.01	599.476
03S/21E-18D01S	003S021E18D001S	33.917517	-114.818023	885						4/24/1979	285.63	599.37	599.476
03S/21E-18D01S	003S021E18D001S	33.917517	-114.818023	885						7/27/1979	285.53	599.47	599.476
03S/21E-18D01S	003S021E18D001S	33.917517	-114.818023	885						7/24/1980	285.63	599.37	599.476
03S/21E-18D01S	003S021E18D001S	33.917517	-114.818023	885						1/22/1981	285.75	599.25	599.476
03S/21E-18D01S	003S021E18D001S	33.917517	-114.818023	885						8/28/1981	285.53	599.47	599.476
03S/21E-18D01S	003S021E18D001S	33.917517	-114.818023	885						3/4/1982	285.52	599.48	599.476
03S/21E-18D01S	003S021E18D001S	33.917517	-114.818023	885						12/9/1982	285.46	599.54	599.476
03S/21E-18D01S	003S021E18D001S	33.917517	-114.818023	885						10/20/1983	285.65	599.35	599.476
03S/21E-18D01S	003S021E18D001S	33.917517	-114.818023	885						4/18/1984	285.55	599.45	599.476
03S/23E-14B01S	003S023E14B001S	33.922907	-114.533430	320	160					5/4/1995	16.36	303.64	303.640
03S/23E-14B02S	003S023E14B002S	33.923379	-114.532041	315	200					5/4/1995	15.68	299.32	299.320
03S/23E-25D12S	003S023E25D012S	33.892630	-114.525485	318	64.3					2/8/1996	15.15	302.85	302.850
03S/23E-35R01S	003S023E35R001S	33.866491	-114.529207	310						1/11/1995	24.25	285.75	285.750
03S/23E-35R03S	003S023E35R003S	33.866574	-114.528985	305						1/11/1995	18.49	286.51	286.510
04S/21E-09B01S	004S021E09B001S	33.847832	-114.779446	874.7	1088					7/29/1971	546.6	328.10	328.133
04S/21E-09B01S	004S021E09B001S	33.847832	-114.779446	874.7	1088					9/25/1990	545.5	329.20	328.133
04S/21E-09B01S	004S021E09B001S	33.847832	-114.779446	874.7	1088					3/10/1992	547.1	327.60	328.133
04S/21E-09B01S	004S021E09B001S	33.847832	-114.779446	874.7	1088					4/24/2000	547.07	327.63	328.133
04S/23E-02H01S	004S023E02H001S	33.860380	-114.530040	310						1/11/1995	25.5	284.50	284.500
04S/23E-02K01S	004S023E02K001S	33.856102	-114.532179	310	43.2					2/7/1996	28.34	281.66	281.660
04S/23E-02Q01S	004S023E02Q001S	33.853075	-114.531902	325						5/5/1995	16.82	308.18	308.180

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
04S/23E-11H01S	004S023E11H001S	33.843964	-114.529568	300						5/5/1995	12.9	287.10	287.100
04S/23E-36Q03S	004S023E36Q003S	33.779298	-114.514567	295	60					5/4/1995	10.5	284.50	284.500
05S/22E-21H01S	005S022E21H001S	33.729188	-114.679127	515.55						9/18/1990	265.96	249.59	249.805
05S/22E-21H01S	005S022E21H001S	33.729188	-114.679127	515.55						3/21/1992	265.53	250.02	249.805
05S/22E-25L01S	005S022E25L001S	33.707689	-114.634120	455						3/22/1992	197.44	257.56	257.720
05S/22E-25L01S	005S022E25L001S	33.707689	-114.634120	455						5/12/1993	198.5	256.50	257.720
05S/22E-25L01S	005S022E25L001S	33.707689	-114.634120	455						12/9/1999	195.9	259.10	257.720
05S/22E-26Q01S	005S022E26Q001S	33.707636	-114.647512	449.6						6/13/1992	199.67	249.93	249.930
05S/22E-27R01S	005S022E27R001S	33.703952	-114.660385	442.3						9/17/1990	207.46	234.84	234.840
05S/22E-28Q01S	005S022E28Q001S	33.704466	-114.682738	455	300					2/13/1962	195.35	259.65	258.136
05S/22E-28Q01S	005S022E28Q001S	33.704466	-114.682738	455	300					5/24/1962	196.53	258.47	258.136
05S/22E-28Q01S	005S022E28Q001S	33.704466	-114.682738	455	300					6/20/1962	196.66	258.34	258.136
05S/22E-28Q01S	005S022E28Q001S	33.704466	-114.682738	455	300					7/19/1962	196.77	258.23	258.136
05S/22E-28Q01S	005S022E28Q001S	33.704466	-114.682738	455	300					8/16/1962	197.16	257.84	258.136
05S/22E-28Q01S	005S022E28Q001S	33.704466	-114.682738	455	300					9/13/1962	196.98	258.02	258.136
05S/22E-28Q01S	005S022E28Q001S	33.704466	-114.682738	455	300					10/11/1962	197.15	257.85	258.136
05S/22E-28Q01S	005S022E28Q001S	33.704466	-114.682738	455	300					11/8/1962	197.18	257.82	258.136
05S/22E-28Q01S	005S022E28Q001S	33.704466	-114.682738	455	300					12/13/1962	197.06	257.94	258.136
05S/22E-28Q01S	005S022E28Q001S	33.704466	-114.682738	455	300					1/9/1963	197.19	257.81	258.136
05S/22E-28Q01S	005S022E28Q001S	33.704466	-114.682738	455	300					10/19/1966	197.47	257.53	258.136
05S/22E-31E01S	005S022E31E001S	33.700025	-114.729109	475.83	484	291	184.83	467	8.83	7/26/1965	222	253.83	253.043
05S/22E-31E01S	005S022E31E001S	33.700025	-114.729109	475.83	484	291	184.83	467	8.83	2/8/1966	218.5	257.33	253.043
05S/22E-31E01S	005S022E31E001S	33.700025	-114.729109	475.83	484	291	184.83	467	8.83	10/19/1966	218.42	257.41	253.043
05S/22E-31E01S	005S022E31E001S	33.700025	-114.729109	475.83	484	291	184.83	467	8.83	8/4/1971	220.69	255.14	253.043
05S/22E-31E01S	005S022E31E001S	33.700025	-114.729109	475.83	484	291	184.83	467	8.83	9/26/1990	227.5	248.33	253.043
05S/22E-31E01S	005S022E31E001S	33.700025	-114.729109	475.83	484	291	184.83	467	8.83	2/14/1992	227.62	248.21	253.043
05S/22E-31E01S	005S022E31E001S	33.700025	-114.729109	475.83	484	291	184.83	467	8.83	3/30/2000	224.78	251.05	253.043
05S/22E-33J02S	005S022E33J002S	33.696411	-114.681349	437.19	300					3/1/1968	183	254.19	246.324
05S/22E-33J02S	005S022E33J002S	33.696411	-114.681349	437.19	300					9/8/1971	190.15	247.04	246.324
05S/22E-33J02S	005S022E33J002S	33.696411	-114.681349	437.19	300					9/9/1971	189.35	247.84	246.324
05S/22E-33J02S	005S022E33J002S	33.696411	-114.681349	437.19	300					9/15/1990	199.09	238.10	246.324

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
05S/22E-33J02S	005S022E33J002S	33.696411	-114.681349	437.19	300					3/21/1992	192.74	244.45	246.324
05S/22E-33J04S	005S022E33J004S	33.696439	-114.677591	438.7						9/15/1990	194.62	244.08	244.080
05S/22E-34P01S	005S022E34P001S	33.689220	-114.668235	418.79						9/15/1990	172.56	246.23	247.560
05S/22E-34P01S	005S022E34P001S	33.689220	-114.668235	418.79						3/21/1992	169.9	248.89	247.560
05S/22E-35D01S	005S022E35D001S	33.704189	-114.655793	440	293					9/1/1971	183	257.00	257.000
05S/22E-35P01S	005S022E35P001S	33.692292	-114.654498	415.1	410					5/28/1985	168	247.10	251.127
05S/22E-35P01S	005S022E35P001S	33.692292	-114.654498	415.1	410					9/15/1990	165.18	249.92	251.127
05S/22E-35P01S	005S022E35P001S	33.692292	-114.654498	415.1	410					3/28/2006	158.74	256.36	251.127
05S/22E-36A01S	005S022E36A001S	33.700914	-114.626725	432.4	209.5					3/12/1992	174	258.40	259.278
05S/22E-36A01S	005S022E36A001S	33.700914	-114.626725	432.4	209.5					3/25/1993	173.78	258.62	259.278
05S/22E-36A01S	005S022E36A001S	33.700914	-114.626725	432.4	209.5					4/25/1993	173.72	258.68	259.278
05S/22E-36A01S	005S022E36A001S	33.700914	-114.626725	432.4	209.5					6/13/2000	170.99	261.41	259.278
05S/22E-36G01S	005S022E36G001S	33.700578	-114.633014	425	360					9/1/1971	174	251.00	251.000
05S/22E-36G02S	005S022E36G002S	33.700539	-114.633709	428.2						12/9/1999	170.14	258.06	258.060
05S/22E-36G03S	005S022E36G003S	33.696989	-114.629336	416.6	193					2/16/1992	158	258.60	258.467
05S/22E-36G03S	005S022E36G003S	33.696989	-114.629336	416.6	193					11/8/1995	158.32	258.28	258.467
05S/22E-36G03S	005S022E36G003S	33.696989	-114.629336	416.6	193					6/13/2000	158.08	258.52	258.467
05S/22E-36H02S	005S022E36H002S	33.697739	-114.625145	418.7						3/29/2006	159.04	259.66	259.660
05S/22E-36H03S	005S022E36H003S	33.699672	-114.626578	425.2						12/9/1999	166.24	258.96	258.960
05S/23E-25K01S	005S023E25K001S	33.712800	-114.527456	286						6/1/1971	4	282.00	282.000
05S/23E-25L01S	005S023E25L001S	33.711689	-114.530234	285						6/1/1971	4	281.00	281.000
05S/23E-25M01S	005S023E25M001S	33.710300	-114.535512	284						6/1/1971	4	280.00	280.000
05S/23E-26J01S	005S023E26J001S	33.710022	-114.538567	284						6/1/1971	4	280.00	280.000
05S/23E-26J02S	005S023E26J002S	33.710300	-114.542178	285						6/1/1971	7	278.00	278.000
05S/23E-26L01S	005S023E26L001S	33.710300	-114.547179	283						6/1/1971	4	279.00	279.000
05S/23E-26N01S	005S023E26N001S	33.707522	-114.554401	282						6/1/1971	6	276.00	276.000
05S/23E-26P01S	005S023E26P001S	33.709189	-114.551068	282						7/1/1971	5	277.00	277.000
05S/23E-26Q01S	005S023E26Q001S	33.705855	-114.546067	284						6/1/1971	3	281.00	281.000
05S/23E-27R01S	005S023E27R001S	33.706411	-114.555790	282						6/1/1971	6	276.00	276.000
05S/23E-31D01S	005S023E31D001S	33.705764	-114.624256	437.5	207					10/31/1987	188.5	249.00	255.603
05S/23E-31D01S	005S023E31D001S	33.705764	-114.624256	437.5	207					11/3/1987	180.3	257.20	255.603

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
05S/23E-31D01S	005S023E31D001S	33.705764	-114.624256	437.5	207					3/22/1992	179.88	257.62	255.603
05S/23E-31D01S	005S023E31D001S	33.705764	-114.624256	437.5	207					6/13/2000	178.91	258.59	255.603
05S/23E-33J01S	005S023E33J001S	33.697522	-114.575790	277						6/1/1971	5	272.00	272.000
05S/23E-33R01S	005S023E33R001S	33.694189	-114.575513	278						6/1/1971	7	271.00	271.000
05S/23E-34A01S	005S023E34A001S	33.702800	-114.557734	280						6/1/1971	6	274.00	274.000
05S/23E-34A02S	005S023E34A002S	33.703633	-114.558290	279						6/1/1971	6	273.00	273.000
05S/23E-34A03S	005S023E34A003S	33.704022	-114.558457	280						6/13/1997	8.62	271.38	271.380
05S/23E-34C01S	005S023E34C001S	33.701967	-114.565235	281						6/1/1971	8	273.00	273.000
05S/23E-34E01S	005S023E34E001S	33.698633	-114.572457	278						6/1/1971	5	273.00	273.000
05S/23E-34E02S	005S023E34E002S	33.699744	-114.572457	278						6/1/1971	5	273.00	273.000
05S/23E-34E03S	005S023E34E003S	33.700578	-114.572457	279						6/1/1971	7	272.00	272.000
05S/23E-34H01S	005S023E34H001S	33.701967	-114.559679	278						6/1/1971	4	274.00	274.000
05S/23E-34J01S	005S023E34J001S	33.696411	-114.556901	280						6/1/1971	5	275.00	275.000
05S/23E-34K01S	005S023E34K001S	33.698356	-114.562734	279						6/1/1971	4	275.00	275.000
05S/23E-34M01S	005S023E34M001S	33.694467	-114.572179	278						6/1/1971	6	272.00	272.000
05S/23E-34M02S	005S023E34M002S	33.695856	-114.572179	278						6/1/1971	5	273.00	273.000
05S/23E-34M03S	005S023E34M003S	33.697244	-114.572179	278						6/1/1971	6	272.00	272.000
05S/23E-34N01S	005S023E34N001S	33.691134	-114.572179	278						6/1/1971	4	274.00	274.000
05S/23E-34Q03S	005S023E34Q003S	33.694467	-114.562734	279						6/1/1971	6	273.00	273.000
05S/23E-35A01S	005S023E35A001S	33.705300	-114.538845	283.96	12					1/23/1948	3.5	280.46	276.403
05S/23E-35A01S	005S023E35A001S	33.705300	-114.538845	283.96	12					9/3/1948	6.03	277.93	276.403
05S/23E-35A01S	005S023E35A001S	33.705300	-114.538845	283.96	12					1/3/1949	5.91	278.05	276.403
05S/23E-35A01S	005S023E35A001S	33.705300	-114.538845	283.96	12					5/23/1950	7.31	276.65	276.403
05S/23E-35A01S	005S023E35A001S	33.705300	-114.538845	283.96	12					8/3/1950	7.31	276.65	276.403
05S/23E-35A01S	005S023E35A001S	33.705300	-114.538845	283.96	12					1/22/1951	7.9	276.06	276.403
05S/23E-35A01S	005S023E35A001S	33.705300	-114.538845	283.96	12					9/10/1951	8	275.96	276.403
05S/23E-35A01S	005S023E35A001S	33.705300	-114.538845	283.96	12					1/22/1952	7.97	275.99	276.403
05S/23E-35A01S	005S023E35A001S	33.705300	-114.538845	283.96	12					1/28/1953	8.22	275.74	276.403
05S/23E-35A01S	005S023E35A001S	33.705300	-114.538845	283.96	12					10/29/1953	9.02	274.94	276.403
05S/23E-35A01S	005S023E35A001S	33.705300	-114.538845	283.96	12					3/26/1954	8.52	275.44	276.403
05S/23E-35A01S	005S023E35A001S	33.705300	-114.538845	283.96	12					9/27/1954	7.92	276.04	276.403

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
05S/23E-35A01S	005S023E35A001S	33.705300	-114.538845	283.96	12					2/21/1955	7.52	276.44	276.403
05S/23E-35A01S	005S023E35A001S	33.705300	-114.538845	283.96	12					9/26/1955	8.12	275.84	276.403
05S/23E-35A01S	005S023E35A001S	33.705300	-114.538845	283.96	12					2/24/1956	8.82	275.14	276.403
05S/23E-35A01S	005S023E35A001S	33.705300	-114.538845	283.96	12					10/2/1956	7.62	276.34	276.403
05S/23E-35A01S	005S023E35A001S	33.705300	-114.538845	283.96	12					1/4/1957	8.42	275.54	276.403
05S/23E-35A01S	005S023E35A001S	33.705300	-114.538845	283.96	12					9/17/1957	7.42	276.54	276.403
05S/23E-35A01S	005S023E35A001S	33.705300	-114.538845	283.96	12					1/22/1958	7.47	276.49	276.403
05S/23E-35A01S	005S023E35A001S	33.705300	-114.538845	283.96	12					9/24/1958	7.75	276.21	276.403
05S/23E-35A01S	005S023E35A001S	33.705300	-114.538845	283.96	12					1/3/1959	7.95	276.01	276.403
05S/23E-35A02S	005S023E35A002S	33.702800	-114.541901	284.97	8					1/23/1948	6.63	278.34	278.180
05S/23E-35A02S	005S023E35A002S	33.702800	-114.541901	284.97	8					9/3/1948	6.95	278.02	278.180
05S/23E-35N01S	005S023E35N001S	33.691411	-114.554123	282						6/1/1971	7	275.00	275.000
05S/23E-35R01S	005S023E35R001S	33.691411	-114.540512	281						6/1/1971	6	275.00	275.000
05S/24E-06Q02S	005S024E06Q002S	33.766465	-114.508095	290	22.7					5/25/1995	9.02	280.98	280.980
05S/24E-30D01S	005S024E30D001S	33.717244	-114.517178	290						7/1/1971	3	287.00	287.000
05S/24E-31D01S	005S024E31D001S	33.706133	-114.516344	284						6/1/1971	5	279.00	279.000
05S/24E-31M01S	005S024E31M001S	33.695300	-114.519955	286						6/1/1971	9	277.00	277.000
06S/21E-24K01S	006S021E24K001S	33.635604	-114.736281	410.5						9/26/1990	165.6	244.90	245.223
06S/21E-24K01S	006S021E24K001S	33.635604	-114.736281	410.5						3/7/1997	163.18	247.32	245.223
06S/21E-24K01S	006S021E24K001S	33.635604	-114.736281	410.5						9/16/1999	167.05	243.45	245.223
06S/21E-25A02S	006S021E25A002S	33.629460	-114.731847	397.1	317					3/6/1980	146	251.10	247.588
06S/21E-25A02S	006S021E25A002S	33.629460	-114.731847	397.1	317					9/26/1990	152.3	244.80	247.588
06S/21E-25A02S	006S021E25A002S	33.629460	-114.731847	397.1	317					3/7/1997	149.79	247.31	247.588
06S/21E-25A02S	006S021E25A002S	33.629460	-114.731847	397.1	317					9/16/1999	149.96	247.14	247.588
06S/21E-25F01S	006S021E25F001S	33.628252	-114.740403	411.7						9/26/1990	167.05	244.65	246.427
06S/21E-25F01S	006S021E25F001S	33.628252	-114.740403	411.7						3/7/1997	164.83	246.87	246.427
06S/21E-25F01S	006S021E25F001S	33.628252	-114.740403	411.7						9/16/1999	163.94	247.76	246.427
06S/21E-25L01S	006S021E25L001S	33.620980	-114.740417	400.2						9/21/1990	148.24	251.96	246.080
06S/21E-25L01S	006S021E25L001S	33.620980	-114.740417	400.2						3/7/1997	161.07	239.13	246.080
06S/21E-25L01S	006S021E25L001S	33.620980	-114.740417	400.2						9/16/1999	153.72	246.48	246.080
06S/21E-25L01S	006S021E25L001S	33.620980	-114.740417	400.2						3/30/2006	153.45	246.75	246.080

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
06S/21E-36F01S	006S021E36F001S	33.613735	-114.740403	391.7	319					3/30/1979	147	244.70	242.633
06S/21E-36F01S	006S021E36F001S	33.613735	-114.740403	391.7	319					9/21/1990	155.98	235.72	242.633
06S/21E-36F01S	006S021E36F001S	33.613735	-114.740403	391.7	319					3/7/1997	146.77	244.93	242.633
06S/21E-36F01S	006S021E36F001S	33.613735	-114.740403	391.7	319					9/16/1999	146.52	245.18	242.633
06S/21E-36G01S	006S021E36G001S	33.612944	-114.731686	391.6						9/24/1990	147.95	243.65	245.040
06S/21E-36G01S	006S021E36G001S	33.612944	-114.731686	391.6						3/30/2006	145.17	246.43	245.040
06S/21E-36M01S	006S021E36M001S	33.609469	-114.744406	393	186					10/24/1927	133	260.00	260.000
06S/21E-36M03S	006S021E36M003S	33.607802	-114.741628	392						9/28/1990	146.68	245.32	245.320
06S/22E-01R01S	006S022E01R001S	33.675578	-114.624681	269						6/1/1971	10	259.00	259.000
06S/22E-02J01S	006S022E02J001S	33.679011	-114.646137	404.72	452					5/14/1951	144.5	260.22	253.149
06S/22E-02J01S	006S022E02J001S	33.679011	-114.646137	404.72	452					10/19/1966	143.35	261.37	253.149
06S/22E-02J01S	006S022E02J001S	33.679011	-114.646137	404.72	452					7/1/1971	147	257.72	253.149
06S/22E-02J01S	006S022E02J001S	33.679011	-114.646137	404.72	452					7/21/1971	147.13	257.59	253.149
06S/22E-02N01S	006S022E02N001S	33.675059	-114.655156	404.5						9/14/1990	156.04	248.46	251.890
06S/22E-02N01S	006S022E02N001S	33.675059	-114.655156	404.5						3/19/2002	149.18	255.32	251.890
06S/22E-02P02S	006S022E02P002S	33.677961	-114.654593	405.92	350					8/20/1968	149	256.92	255.094
06S/22E-02P02S	006S022E02P002S	33.677961	-114.654593	405.92	350					8/1/1971	150	255.92	255.094
06S/22E-02P02S	006S022E02P002S	33.677961	-114.654593	405.92	350					8/19/1971	148.27	257.65	255.094
06S/22E-02P02S	006S022E02P002S	33.677961	-114.654593	405.92	350					9/14/1990	154.6	251.32	255.094
06S/22E-02P02S	006S022E02P002S	33.677961	-114.654593	405.92	350					3/23/1992	152.26	253.66	255.094
06S/22E-03B01S	006S022E03B001S	33.689033	-114.667613	420	414					1/20/1964	161	259.00	250.829
06S/22E-03B01S	006S022E03B001S	33.689033	-114.667613	420	414					8/18/1971	165	254.86	250.829
06S/22E-03B01S	006S022E03B001S	33.689033	-114.667613	420	414					7/24/1980	170	249.56	250.829
06S/22E-03B01S	006S022E03B001S	33.689033	-114.667613	420	414					1/23/1981	170	249.84	250.829
06S/22E-03B01S	006S022E03B001S	33.689033	-114.667613	420	414					8/28/1981	171	249.09	250.829
06S/22E-03B01S	006S022E03B001S	33.689033	-114.667613	420	414					3/4/1982	170	249.90	250.829
06S/22E-03B01S	006S022E03B001S	33.689033	-114.667613	420	414					12/10/1982	171	248.87	250.829
06S/22E-03B01S	006S022E03B001S	33.689033	-114.667613	420	414					9/20/1983	171	248.84	250.829
06S/22E-03B01S	006S022E03B001S	33.689033	-114.667613	420	414					9/18/1984	172	248.30	250.829
06S/22E-03B01S	006S022E03B001S	33.689033	-114.667613	420	414					2/28/1985	171	249.22	250.829
06S/22E-03B01S	006S022E03B001S	33.689033	-114.667613	420	414					6/12/1985	171	248.52	250.829

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
06S/22E-03B01S	**006S022E03B001S**	**33.689033**	**-114.667613**	420	414					4/5/2000	166	253.95	250.829
06S/22E-03J01S	**006S022E03J001S**	**33.680300**	**-114.660237**	406	83					7/22/1971	68	337.90	337.900
06S/22E-03P01S	**006S022E03P001S**	**33.675300**	**-114.668293**	401	400					5/5/1905	134	267.00	267.000
06S/22E-09G01S	**006S022E09G001S**	33.668073	-114.679782	380.3						9/22/1990	137	243.72	248.535
06S/22E-09G01S	**006S022E09G001S**	33.668073	-114.679782	380.3						3/30/2006	127	253.35	248.535
06S/22E-10E01S	**006S022E10E001S**	33.671481	-114.672626	400.6	362					2/8/1980	152	248.60	248.600
06S/22E-10H02S	**006S022E10H002S**	33.667920	-114.663429	404.4	358					2/15/1980	142	262.40	256.593
06S/22E-10H02S	**006S022E10H002S**	33.667920	-114.663429	404.4	358					2/16/2000	150	254.47	256.593
06S/22E-10H02S	**006S022E10H002S**	33.667920	-114.663429	404.4	358					3/28/2006	150	254.64	256.593
06S/22E-10H02S	**006S022E10H002S**	33.667920	-114.663429	404.4	358					3/30/2006	150	254.86	256.593
06S/22E-10H03S	**006S022E10H003S**	33.671273	-114.660157	403.9	297					4/30/1997	150	253.90	254.445
06S/22E-10H03S	**006S022E10H003S**	33.671273	-114.660157	403.9	297					3/30/2006	149	254.99	254.445
06S/22E-11H01S	**006S022E11H001S**	33.668006	-114.642137	407.97	235					9/30/1955	147	260.97	255.038
06S/22E-11H03S	**006S022E11H003S**	33.672106	-114.642012	408.4						9/14/1990	156	252.75	252.750
06S/22E-11N01S	**006S022E11N001S**	33.664231	-114.654870	404.2	480					8/1/1971	150	254.20	252.953
06S/22E-11N01S	**006S022E11N001S**	33.664231	-114.654870	404.2	480					8/18/1971	148	255.93	252.953
06S/22E-11N01S	**006S022E11N001S**	33.664231	-114.654870	404.2	480					9/15/1990	154	250.50	252.953
06S/22E-11N01S	**006S022E11N001S**	33.664231	-114.654870	404.2	480					3/28/1992	153	251.18	252.953
06S/22E-12A01S	**006S022E12A001S**	33.675023	-114.627458	269						6/1/1971	10	259.00	259.000
06S/22E-12C01S	**006S022E12C001S**	33.672981	-114.635325	408.62	476					5/29/1969	145	263.62	259.085
06S/22E-12C01S	**006S022E12C001S**	33.672981	-114.635325	408.62	476					8/19/1971	150	258.98	259.085
06S/22E-12C01S	**006S022E12C001S**	33.672981	-114.635325	408.62	476					9/15/1990	152	256.42	259.085
06S/22E-12C01S	**006S022E12C001S**	33.672981	-114.635325	408.62	476					11/18/1999	151	257.32	259.085
06S/22E-12E01S	**006S022E12E001S**	33.669167	-114.638106	410.54	230					10/19/1944	150	260.54	249.955
06S/22E-12E01S	**006S022E12E001S**	33.669167	-114.638106	410.54	230					8/19/1971	170	240.24	249.955
06S/22E-12F01S	**006S022E12F001S**	33.670553	-114.635250	409.64	252					2/9/1962	136	273.64	264.890
06S/22E-12F01S	**006S022E12F001S**	33.670553	-114.635250	409.64	252					9/15/1990	154	256.14	264.890
06S/22E-12J01S	**006S022E12J001S**	33.666503	-114.628686	294.9	60					5/31/1905	34	260.90	258.965
06S/22E-12J01S	**006S022E12J001S**	33.666503	-114.628686	294.9	60					3/30/2006	38	257.03	258.965
06S/22E-12J02S	**006S022E12J002S**	33.664920	-114.628664	271.1	60					6/5/2000	14	256.96	256.740
06S/22E-12J02S	**006S022E12J002S**	33.664920	-114.628664	271.1	60					3/30/2006	15	256.52	256.740
06S/22E-12L01S	**006S022E12L001S**	33.666134	-114.633292	270						7/1/1971	12	258.00	258.000

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
06S/22E-12L02S	**006S022E12L002S**	33.666734	-114.633575	279.57	442					1/22/1961	18	261.57	261.570
06S/22E-12M01S	**006S022E12M001S**	33.666412	-114.640514	268						7/1/1971	11	257.00	257.000
06S/22E-12N01S	**006S022E12N001S**	**33.660856**	**-114.641348**	275						7/1/1971	17	258.00	258.000
06S/22E-13N01S	**006S022E13N001S**	**33.646412**	**-114.640792**	276						7/1/1971	19	257.00	257.000
06S/22E-13Q01S	**006S022E13Q001S**	**33.596414**	**-114.632180**	268	116					3/23/1967	8	260.04	207.648
06S/22E-13Q01S	**006S022E13Q001S**	**33.596414**	**-114.632180**	268	116					7/1/1971	8	260.00	207.648
06S/22E-13Q02S	**006S022E13Q002S**	**33.646412**	**-114.632180**	268	22					3/23/1967	8	260.28	255.546
06S/22E-13Q02S	**006S022E13Q002S**	**33.646412**	**-114.632180**	268	22					7/1/1971	8	260.00	255.546
06S/22E-13Q03S	**006S022E13Q003S**	**33.646412**	**-114.629403**	266						7/1/1971	8	258.00	258.000
06S/22E-14A02S	**006S022E14A002S**	**33.660379**	**-114.643856**	281.7	400					4/6/2006	27	255.15	255.140
06S/22E-14A02S	**006S022E14A002S**	**33.660379**	**-114.643856**	281.7	400					4/7/2006	27	255.13	255.140
06S/22E-14D01S	**006S022E14D001S**	**33.660295**	**-114.658356**	400.6						9/15/1990	149	251.94	253.210
06S/22E-14D01S	**006S022E14D001S**	**33.660295**	**-114.658356**	400.6						3/14/2000	146	254.48	253.210
06S/22E-15E01S	**006S022E15E001S**	**33.655359**	**-114.674546**	394.89						6/28/1967	140	254.89	253.985
06S/22E-15E01S	**006S022E15E001S**	**33.655359**	**-114.674546**	394.89						1/27/2000	142	253.08	253.985
06S/22E-15Q01S	**006S022E15Q001S**	**33.649496**	**-114.664590**	372.54	585					9/12/1963	113	259.54	247.797
06S/22E-15Q01S	**006S022E15Q001S**	**33.649496**	**-114.664590**	372.54	585					9/17/1963	115	257.29	247.797
06S/22E-15Q01S	**006S022E15Q001S**	**33.649496**	**-114.664590**	372.54	585					6/28/1967	132	240.54	247.797
06S/22E-15Q01S	**006S022E15Q001S**	**33.649496**	**-114.664590**	372.54	585					7/23/1971	142	230.92	247.797
06S/22E-15Q01S	**006S022E15Q001S**	**33.649496**	**-114.664590**	372.54	585					9/22/1990	121	251.29	247.797
06S/22E-15Q01S	**006S022E15Q001S**	**33.649496**	**-114.664590**	372.54	585					2/19/1992	121	251.23	247.797
06S/22E-16A01S	**006S022E16A001S**	**33.660698**	**-114.675624**	366.67	364					3/29/1966	124	242.67	204.308
06S/22E-16A01S	**006S022E16A001S**	**33.660698**	**-114.675624**	366.67	364					4/4/1966	124	242.67	204.308
06S/22E-16A01S	**006S022E16A001S**	**33.660698**	**-114.675624**	366.67	364					7/22/1971	181	185.71	204.308
06S/22E-16A01S	**006S022E16A001S**	**33.660698**	**-114.675624**	366.67	364					9/22/1990	119	247.70	204.308
06S/22E-16A01S	**006S022E16A001S**	**33.660698**	**-114.675624**	366.67	364					2/15/1992	118	248.75	204.308
06S/22E-16A01S	**006S022E16A001S**	**33.660698**	**-114.675624**	366.67	364					1/27/2000	114	252.89	204.308
06S/22E-16E01S	**006S022E16E001S**	**33.653737**	**-114.692552**	396	345					10/11/1968	145	251.00	236.030
06S/22E-16E01S	**006S022E16E001S**	**33.653737**	**-114.692552**	396	345					7/28/1971	184	211.60	236.030
06S/22E-16E01S	**006S022E16E001S**	**33.653737**	**-114.692552**	396	345					9/19/1990	151	245.49	236.030
06S/22E-16G01S	**006S022E16G001S**	**33.653634**	**-114.681904**	400						7/1/1971	156	244.00	244.000

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
06S/22E-16P01S	006S022E16P001S	33.646451	-114.684182	389.71	306					10/11/1968	131	258.71	244.140
06S/22E-16P01S	006S022E16P001S	33.646451	-114.684182	389.71	306					7/23/1971	160	229.57	244.140
06S/22E-17B01S	006S022E17B001S	33.660631	-114.701360	399.64	302					5/26/1966	149	250.64	249.954
06S/22E-17B01S	006S022E17B001S	33.660631	-114.701360	399.64	302					8/22/1966	149	250.64	249.954
06S/22E-17B01S	006S022E17B001S	33.660631	-114.701360	399.64	302					9/20/1990	153	247.00	249.954
06S/22E-17B01S	006S022E17B001S	33.660631	-114.701360	399.64	302					2/15/1992	153	246.88	249.954
06S/22E-17L02S	006S022E17L002S	33.653357	-114.702183	397	323					7/1/1971	156	241.00	241.000
06S/22E-18A01S	006S022E18A001S	33.657412	-114.710236	406.88	298					6/2/1966	155	251.88	248.016
06S/22E-18A01S	006S022E18A001S	33.657412	-114.710236	406.88	298					7/1/1971	163	243.88	248.016
06S/22E-18A01S	006S022E18A001S	33.657412	-114.710236	406.88	298					7/28/1971	163	244.10	248.016
06S/22E-18A01S	006S022E18A001S	33.657412	-114.710236	406.88	298					9/20/1990	162	245.27	248.016
06S/22E-19N02S	006S022E19N002S	33.634485	-114.723475	397	300					8/26/1977	150	247.00	247.640
06S/22E-19N02S	006S022E19N002S	33.634485	-114.723475	397	300					9/15/1999	149	248.28	247.640
06S/22E-19N03S	006S022E19N003S	33.634518	-114.723389	397.2	394					2/29/1980	147	250.20	248.445
06S/22E-19N03S	006S022E19N003S	33.634518	-114.723389	397.2	394					9/23/1990	152	245.65	248.445
06S/22E-19N03S	006S022E19N003S	33.634518	-114.723389	397.2	394					3/7/1997	149	248.23	248.445
06S/22E-19N03S	006S022E19N003S	33.634518	-114.723389	397.2	394					9/15/1999	148	248.74	248.445
06S/22E-19N03S	006S022E19N003S	33.634518	-114.723389	397.2	394					4/4/2006	148	248.92	248.445
06S/22E-19N03S	006S022E19N003S	33.634518	-114.723389	397.2	394					4/5/2006	148	248.93	248.445
06S/22E-19R01S	006S022E19R001S	33.634440	-114.712455	395.6	300					9/17/1977	150	245.60	247.778
06S/22E-19R01S	006S022E19R001S	33.634440	-114.712455	395.6	300					9/23/1990	150	245.81	247.778
06S/22E-19R01S	006S022E19R001S	33.634440	-114.712455	395.6	300					3/7/1997	147	248.54	247.778
06S/22E-19R01S	006S022E19R001S	33.634440	-114.712455	395.6	300					9/15/1999	147	248.92	247.778
06S/22E-19R01S	006S022E19R001S	33.634440	-114.712455	395.6	300					4/4/2006	147	248.95	247.778
06S/22E-19R01S	006S022E19R001S	33.634440	-114.712455	395.6	300					4/5/2006	147	248.85	247.778
06S/22E-20A01S	006S022E20A001S	33.646134	-114.693016	395.79	250					7/1/1971	148	247.79	247.790
06S/22E-21B01S	006S022E21B001S	33.643432	-114.683765	373.9	378					4/28/1966	117	256.90	213.277
06S/22E-21B01S	006S022E21B001S	33.643432	-114.683765	373.9	378					8/23/1966	121	253.20	213.277
06S/22E-21B01S	006S022E21B001S	33.643432	-114.683765	373.9	378					1/25/2000	122	251.78	213.277
06S/22E-21K01S	006S022E21K001S	33.635526	-114.683226	375.3	323					5/11/1966	126	249.30	249.695
06S/22E-21K01S	006S022E21K001S	33.635526	-114.683226	375.3	323					8/24/1966	121	254.00	249.695

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
06S/22E-21K01S	006S022E21K001S	33.635526	-114.683226	375.3	323					7/28/1971	160	215.66	249.695
06S/22E-22A01S	006S022E22A001S	33.646032	-114.658962	364.9	305					12/5/1972	109	255.90	253.916
06S/22E-22A01S	006S022E22A001S	33.646032	-114.658962	364.9	305					9/22/1990	111	253.51	253.916
06S/22E-22A01S	006S022E22A001S	33.646032	-114.658962	364.9	305					2/19/1992	112	252.80	253.916
06S/22E-22A01S	006S022E22A001S	33.646032	-114.658962	364.9	305					1/27/2000	111	253.97	253.916
06S/22E-22A01S	006S022E22A001S	33.646032	-114.658962	364.9	305					3/30/2006	112	253.40	253.916
06S/22E-23L01S	006S022E23L001S	33.635579	-114.649681	268						7/1/1971	15	253.00	253.000
06S/22E-24D01S	006S022E24D001S	33.645987	-114.641261	277.6	25.31					5/11/2000	22	255.76	255.229
06S/22E-24D01S	006S022E24D001S	33.645987	-114.641261	277.6	25.31					2000-01	22	255.40	255.229
06S/22E-24D01S	006S022E24D001S	33.645987	-114.641261	277.6	25.31					2000-03	22	255.12	255.229
06S/22E-24D01S	006S022E24D001S	33.645987	-114.641261	277.6	25.31					2000-04	22	255.32	255.229
06S/22E-24D01S	006S022E24D001S	33.645987	-114.641261	277.6	25.31					2000-05	23	254.78	255.229
06S/22E-24D01S	006S022E24D001S	33.645987	-114.641261	277.6	25.31					2000-06	22	255.67	255.229
06S/22E-24D01S	006S022E24D001S	33.645987	-114.641261	277.6	25.31					2000-08	22	255.65	255.229
06S/22E-24D01S	006S022E24D001S	33.645987	-114.641261	277.6	25.31					2000-09	22	255.70	255.229
06S/22E-24D01S	006S022E24D001S	33.645987	-114.641261	277.6	25.31					2000-10	22	255.87	255.229
06S/22E-24D01S	006S022E24D001S	33.645987	-114.641261	277.6	25.31					2006-01	23	255.05	255.229
06S/22E-24D01S	006S022E24D001S	33.645987	-114.641261	277.6	25.31					2006-02	23	254.74	255.229
06S/22E-24D01S	006S022E24D001S	33.645987	-114.641261	277.6	25.31					2006-03	23	254.65	255.229
06S/22E-24D01S	006S022E24D001S	33.645987	-114.641261	277.6	25.31					2006-04	23	254.67	255.229
06S/22E-24D01S	006S022E24D001S	33.645987	-114.641261	277.6	25.31					2006-05	23	254.83	255.229
06S/22E-25C01S	006S022E25C001S	33.631329	-114.635014	265	62					4/16/1998	14	251.00	251.000
06S/22E-26B01S	006S022E26B001S	33.628357	-114.645514	262						7/1/1971	10	252.00	252.000
06S/22E-26B02S	006S022E26B002S	33.631690	-114.645514	263						7/1/1971	8	255.00	255.000
06S/22E-26E01S	006S022E26E001S	33.626691	-114.657736	270	64					3/28/1967	16	254.42	200.390
06S/22E-26E01S	006S022E26E001S	33.626691	-114.657736	270	64					7/1/1971	18	252.00	200.390
06S/22E-26E02S	006S022E26E002S	33.626691	-114.657736	270	21					3/28/1967	15	254.80	205.288
06S/22E-26E02S	006S022E26E002S	33.626691	-114.657736	270	21					7/1/1971	17	253.00	205.288
06S/22E-26E03S	006S022E26E003S	33.624746	-114.657736	262						7/1/1971	10	252.00	252.000
06S/22E-26G01S	006S022E26G001S	33.624746	-114.644681	260	79					3/28/1967	9	250.97	254.798
06S/22E-26G01S	006S022E26G001S	33.624746	-114.644681	260	79					7/1/1971	9	251.00	254.798

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FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
06S/22E-26G02S	006S022E26G002S	33.624746	-114.644681	260	21					3/28/1967	9	251.50	255.122
06S/22E-26G02S	006S022E26G002S	33.624746	-114.644681	260	21					7/1/1971	9	251.00	255.122
06S/22E-26G03S	006S022E26G003S	33.624746	-114.644681	263						7/1/1971	10	253.00	253.000
06S/22E-26Q01S	006S022E26Q001S	33.619746	-114.649403	261						7/1/1971	8	253.00	253.000
06S/22E-27H01S	006S022E27H001S	33.624746	-114.662181	264						7/1/1971	12	252.00	252.000
06S/22E-27R01S	006S022E27R001S	33.617524	-114.659681	257						7/1/1971	7	250.00	250.000
06S/22E-27R02S	006S022E27R002S	33.617524	-114.661903	259						7/1/1971	9	250.00	250.000
06S/22E-28H01S	006S022E28H001S	33.626968	-114.680237	355	300					9/1/1971	107	248.00	248.000
06S/22E-29C01S	006S022E29C001S	33.628868	-114.704857	393.6						9/24/1990	148	245.79	247.403
06S/22E-29C01S	006S022E29C001S	33.628868	-114.704857	393.6						2/15/1992	147	246.61	247.403
06S/22E-29C01S	006S022E29C001S	33.628868	-114.704857	393.6						9/15/1999	145	248.85	247.403
06S/22E-29C01S	006S022E29C001S	33.628868	-114.704857	393.6						4/5/2006	145	248.36	247.403
06S/22E-29D01S	006S022E29D001S	33.631413	-114.705516	394.2	193					7/1/1971	145	249.20	184.855
06S/22E-29D01S	006S022E29D001S	33.631413	-114.705516	394.2	193					7/15/1971	145	249.02	184.855
06S/22E-29G02S	006S022E29G002S	33.625693	-114.698279	391.9						9/23/1990	145	246.94	248.345
06S/22E-29G02S	006S022E29G002S	33.625693	-114.698279	391.9						9/15/1999	142	249.75	248.345
06S/22E-29J01S	006S022E29J001S	33.623080	-114.695238	390	243					8/1/1943	138	252.50	254.175
06S/22E-29J01S	006S022E29J001S	33.623080	-114.695238	390	243					6/9/1961	135	255.04	254.175
06S/22E-29J01S	006S022E29J001S	33.623080	-114.695238	390	243					11/16/1966	133	256.98	254.175
06S/22E-29J01S	006S022E29J001S	33.623080	-114.695238	390	243					7/14/1971	138	252.18	254.175
06S/22E-29M01S	006S022E29M001S	33.622307	-114.709957	393.6	304					3/23/1979	144	249.60	247.593
06S/22E-29M01S	006S022E29M001S	33.622307	-114.709957	393.6	304					9/24/1990	148	245.27	247.593
06S/22E-29M01S	006S022E29M001S	33.622307	-114.709957	393.6	304					3/7/1997	146	247.42	247.593
06S/22E-29M01S	006S022E29M001S	33.622307	-114.709957	393.6	304					9/15/1999	146	247.95	247.593
06S/22E-29M01S	006S022E29M001S	33.622307	-114.709957	393.6	304					4/4/2006	146	247.74	247.593
06S/22E-29M01S	006S022E29M001S	33.622307	-114.709957	393.6	304					4/5/2006	146	247.58	247.593
06S/22E-29Q01S	006S022E29Q001S	33.617449	-114.700490	390.6	306					3/19/1979	141	249.60	247.637
06S/22E-29Q01S	006S022E29Q001S	33.617449	-114.700490	390.6	306					9/23/1990	144	246.32	247.637
06S/22E-29Q01S	006S022E29Q001S	33.617449	-114.700490	390.6	306					2/15/1992	145	246.06	247.637
06S/22E-29Q01S	006S022E29Q001S	33.617449	-114.700490	390.6	306					3/7/1997	143	247.98	247.637
06S/22E-29Q01S	006S022E29Q001S	33.617449	-114.700490	390.6	306					9/14/1999	142	248.49	247.637

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
06S/22E-29Q01S	006S022E29Q001S	33.617449	-114.700490	390.6	306					4/4/2006	143	247.57	247.637
06S/22E-29Q01S	006S022E29Q001S	33.617449	-114.700490	390.6	306					4/5/2006	143	247.44	247.637
06S/22E-30L01S	006S022E30L001S	33.622288	-114.722005	394.5						3/7/1997	148	246.42	246.745
06S/22E-30L01S	006S022E30L001S	33.622288	-114.722005	394.5						9/16/1999	147	247.07	246.745
06S/22E-30M01S	006S022E30M001S	33.623829	-114.725944	394.7						9/26/1990	150	244.70	245.728
06S/22E-30M01S	006S022E30M001S	33.623829	-114.725944	394.7						3/7/1997	148	246.95	245.728
06S/22E-30M01S	006S022E30M001S	33.623829	-114.725944	394.7						9/16/1999	150	244.26	245.728
06S/22E-30M01S	006S022E30M001S	33.623829	-114.725944	394.7						3/30/2006	148	247.00	245.728
06S/22E-31F01S	006S022E31F001S	33.613055	-114.720699	389.3						9/24/1990	155	233.99	240.945
06S/22E-31F01S	006S022E31F001S	33.613055	-114.720699	389.3						8/27/1999	141	247.90	240.945
06S/22E-31K01S	006S022E31K001S	33.609191	-114.718294	387.7						7/1/1971	140	247.70	246.040
06S/22E-31K01S	006S022E31K001S	33.609191	-114.718294	387.7						7/15/1971	140	248.14	246.040
06S/22E-31K01S	006S022E31K001S	33.609191	-114.718294	387.7						9/21/1990	144	243.75	246.040
06S/22E-31K01S	006S022E31K001S	33.609191	-114.718294	387.7						3/28/1992	143	244.36	246.040
06S/22E-31K01S	006S022E31K001S	33.609191	-114.718294	387.7						2/15/2000	141	246.25	246.040
06S/22E-32F01S	006S022E32F001S	33.613080	-114.704682	388.5	230					7/1/1971	139	249.50	249.500
06S/22E-32F02S	006S022E32F002S	33.612585	-114.705674	388.6	300					12/28/1973	137	251.60	248.463
06S/22E-32F02S	006S022E32F002S	33.612585	-114.705674	388.6	300					11/19/1999	141	247.32	248.463
06S/22E-32F02S	006S022E32F002S	33.612585	-114.705674	388.6	300					3/29/2006	142	246.47	248.463
06S/22E-32F03S	006S022E32F003S	33.612308	-114.705190	387.5	500					3/25/2002	147	240.50	240.500
06S/22E-32K01S	006S022E32K001S	33.607524	-114.700793	362.8	464					10/27/1953	112	250.80	254.475
06S/22E-32K01S	006S022E32K001S	33.607524	-114.700793	362.8	464					5/23/1961	117	245.80	254.475
06S/22E-32K01S	006S022E32K001S	33.607524	-114.700793	362.8	464					9/21/1990	118	244.34	254.475
06S/22E-32K02S	006S022E32K002S	33.609191	-114.700793	371.8						4/12/1971	124	247.80	246.373
06S/22E-32K02S	006S022E32K002S	33.609191	-114.700793	371.8						8/1/1972	126	246.00	246.373
06S/22E-32K02S	006S022E32K002S	33.609191	-114.700793	371.8						9/21/1990	127	244.78	246.373
06S/22E-32K02S	006S022E32K002S	33.609191	-114.700793	371.8						1/26/2000	125	246.91	246.373
06S/22E-32K03S	006S022E32K003S	33.608463	-114.700365	365.5						9/21/1990	121	244.43	245.510
06S/22E-32K03S	006S022E32K003S	33.608463	-114.700365	365.5						3/30/2006	119	246.59	245.510
06S/22E-32K04S	006S022E32K004S	33.609113	-114.697046	329.7						9/22/1990	85	244.78	246.076
06S/22E-32K04S	006S022E32K004S	33.609113	-114.697046	329.7						9/23/1990	85	244.88	246.076

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
06S/22E-32K04S	006S022E32K004S	33.609113	-114.697046	329.7						1/24/2000	83	247.14	246.076
06S/22E-32K04S	006S022E32K004S	33.609113	-114.697046	329.7						1/26/2000	83	247.07	246.076
06S/22E-32K04S	006S022E32K004S	33.609113	-114.697046	329.7						3/30/2006	83	246.51	246.076
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					4/30/1905	84	250.20	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					5/23/1961	83	251.50	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					8/24/1961	82	252.03	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					9/21/1961	82	252.24	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					10/18/1961	82	252.04	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					11/21/1961	83	251.53	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					12/20/1961	83	251.16	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					1/22/1962	83	250.80	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					2/19/1962	83	250.85	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					3/26/1962	83	251.05	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					4/24/1962	83	251.35	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					5/24/1962	83	251.47	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					6/20/1962	83	251.64	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					7/19/1962	83	251.63	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					8/16/1962	83	251.58	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					9/17/1962	82	251.85	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					10/11/1962	83	251.68	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					11/8/1962	83	251.49	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					12/13/1962	83	251.20	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					1/10/1963	83	251.14	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					2/4/1963	83	250.91	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					3/4/1963	83	250.96	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					4/1/1963	83	251.26	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					5/6/1963	83	251.66	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					6/3/1963	82	252.05	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					7/11/1963	82	252.20	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					8/6/1963	82	252.35	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					9/9/1963	82	252.62	250.839

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					10/29/1963	81	252.74	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					11/27/1963	82	252.42	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					12/31/1963	82	251.73	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					2/7/1964	83	251.29	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					3/10/1964	83	251.54	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					4/15/1964	82	252.05	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					5/12/1964	82	252.23	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					6/18/1964	81	252.84	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					7/21/1964	81	252.90	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					8/19/1964	81	253.16	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					9/17/1964	81	253.27	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					10/21/1964	81	252.99	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					12/2/1964	81	252.91	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					7/15/1971	85	249.35	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					9/22/1990	89	244.88	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					2/15/1992	89	244.86	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					2/15/2000	88	246.69	250.839
06S/22E-32R01S	006S022E32R001S	33.604236	-114.692959	334.2	560					3/31/2006	88	246.12	250.839
06S/22E-33C01S	006S022E33C001S	33.615280	-114.687851	335.4						5/28/2003	86	249.42	249.420
06S/22E-33C03S	006S022E33C003S	33.614488	-114.683920	335.7	117.1					5/28/2003	86	249.39	249.390
06S/22E-33C04S	006S022E33C004S	33.616955	-114.687871	338.2	108.4					3/29/2006	90	248.30	247.130
06S/22E-33C04S	006S022E33C004S	33.616955	-114.687871	338.2	108.4					5/16/2006	92	245.96	247.130
06S/22E-33C05S	006S022E33C005S	33.617016	-114.687157	337.1	124.5					3/29/2006	89	248.29	247.465
06S/22E-33C05S	006S022E33C005S	33.617016	-114.687157	337.1	124.5					5/16/2006	90	246.64	247.465
06S/22E-33C06S	006S022E33C006S	33.614549	-114.686598	337.8						3/29/2006	90	247.98	247.680
06S/22E-33C06S	006S022E33C006S	33.614549	-114.686598	337.8						5/16/2006	90	247.38	247.680
06S/22E-33F01S	006S022E33F001S	33.611122	-114.684857	334.9						9/26/1990	89	246.38	246.980
06S/22E-33F01S	006S022E33F001S	33.611122	-114.684857	334.9						3/28/1992	89	246.34	246.980
06S/22E-33F01S	006S022E33F001S	33.611122	-114.684857	334.9						1/26/2000	87	248.22	246.980
06S/22E-33F02S	006S022E33F002S	33.611749	-114.686579	336.9	110					5/28/2003	91	245.91	246.655
06S/22E-33F02S	006S022E33F002S	33.611749	-114.686579	336.9	110					3/29/2006	90	247.40	246.655

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
06S/22E-33F03S	006S022E33F003S	33.611910	-114.684126	336.2	110					5/28/2003	87	249.37	248.320
06S/22E-33F03S	006S022E33F003S	33.611910	-114.684126	336.2	110					3/29/2006	89	247.27	248.320
06S/22E-34C01S	006S022E34C001S	33.614646	-114.667517	338	122					9/24/1990	89	248.74	249.180
06S/22E-34C01S	006S022E34C001S	33.614646	-114.667517	338	122					1/24/2000	88	249.62	249.180
06S/22E-34F01S	006S022E34F001S	33.613080	-114.669959	336						9/24/1990	91	245.00	244.810
06S/22E-34F01S	006S022E34F001S	33.613080	-114.669959	336						3/29/1992	91	244.62	244.810
06S/22E-34G01S	006S022E34G001S	33.610302	-114.664681	258.15	14					7/13/1971	10	248.25	248.250
06S/22E-34L01S	006S022E34L001S	33.608358	-114.667737	330	360					8/1/1972	93	237.00	237.000
06S/22E-34N01S	006S022E34N001S	33.602802	-114.671348	255						7/1/1971	7	248.00	248.000
06S/22E-34R02S	006S022E34R002S	33.603636	-114.657736	257						7/1/1971	9	248.00	248.000
06S/22E-35H02S	006S022E35H002S	33.611108	-114.644736	263	265					8/8/1984	10	252.67	252.920
06S/22E-35H02S	006S022E35H002S	33.611108	-114.644736	263	265					1/26/2000	10	253.17	252.920
06S/22E-35M01S	006S022E35M001S	33.609191	-114.653569	260	310					2/7/1962	7	253.00	253.000
06S/22E-35Q07S	006S022E35Q007S	33.602913	-114.647097	260	24.86					10/4/2000	10	249.89	249.890
06S/22E-35R01S	006S022E35R001S	33.604052	-114.644236	257	326					10/31/1947	6	251.00	252.760
06S/22E-35R01S	006S022E35R001S	33.604052	-114.644236	257	326					5/25/1961	7	250.04	252.760
06S/22E-35R01S	006S022E35R001S	33.604052	-114.644236	257	326					7/6/1961	6	250.81	252.760
06S/22E-35R01S	006S022E35R001S	33.604052	-114.644236	257	326					7/28/1961	6	250.70	252.760
06S/22E-35R01S	006S022E35R001S	33.604052	-114.644236	257	326					8/24/1961	7	249.73	252.760
06S/22E-35R01S	006S022E35R001S	33.604052	-114.644236	257	326					9/25/1961	7	249.84	252.760
06S/22E-35R01S	006S022E35R001S	33.604052	-114.644236	257	326					10/18/1961	7	249.70	252.760
06S/22E-35R01S	006S022E35R001S	33.604052	-114.644236	257	326					11/21/1961	7	249.76	252.760
06S/22E-35R01S	006S022E35R001S	33.604052	-114.644236	257	326					12/20/1961	7	249.58	252.760
06S/22E-35R01S	006S022E35R001S	33.604052	-114.644236	257	326					1/22/1962	8	249.04	252.760
06S/22E-35R01S	006S022E35R001S	33.604052	-114.644236	257	326					2/15/1962	18	239.14	252.760
06S/22E-35R01S	006S022E35R001S	33.604052	-114.644236	257	326					3/26/1962	7	250.19	252.760
06S/22E-35R01S	006S022E35R001S	33.604052	-114.644236	257	326					4/23/1962	8	249.15	252.760
06S/22E-35R01S	006S022E35R001S	33.604052	-114.644236	257	326					5/24/1962	7	250.38	252.760
06S/22E-35R01S	006S022E35R001S	33.604052	-114.644236	257	326					6/21/1962	7	250.50	252.760
06S/22E-35R01S	006S022E35R001S	33.604052	-114.644236	257	326					7/19/1962	8	249.10	252.760
06S/22E-35R01S	006S022E35R001S	33.604052	-114.644236	257	326					8/16/1962	7	249.63	252.760

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
06S/22E-35R01S	006S022E35R001S	33.604052	-114.644236	257	326					9/20/1962	7	250.34	252.760
06S/22E-35R01S	006S022E35R001S	33.604052	-114.644236	257	326					10/11/1962	7	250.20	252.760
06S/22E-35R01S	006S022E35R001S	33.604052	-114.644236	257	326					11/8/1962	7	250.03	252.760
06S/22E-35R01S	006S022E35R001S	33.604052	-114.644236	257	326					12/13/1962	7	250.07	252.760
06S/22E-35R01S	006S022E35R001S	33.604052	-114.644236	257	326					1/11/1963	8	249.18	252.760
06S/22E-35R01S	006S022E35R001S	33.604052	-114.644236	257	326					8/2/1972	9	247.80	252.760
06S/22E-35R02S	006S022E35R002S	33.602941	-114.644264	260	328					11/18/1947	6	254.00	251.040
06S/22E-35R02S	006S022E35R002S	33.602941	-114.644264	260	328					2/8/1957	7	252.58	251.040
06S/22E-35R02S	006S022E35R002S	33.602941	-114.644264	260	328					5/25/1961	6	253.75	251.040
06S/22E-35R02S	006S022E35R002S	33.602941	-114.644264	260	328					7/6/1961	6	254.02	251.040
06S/22E-35R02S	006S022E35R002S	33.602941	-114.644264	260	328					7/28/1961	6	254.00	251.040
06S/22E-35R02S	006S022E35R002S	33.602941	-114.644264	260	328					8/24/1961	7	252.76	251.040
06S/22E-35R02S	006S022E35R002S	33.602941	-114.644264	260	328					9/25/1961	20	239.54	251.040
06S/22E-35R02S	006S022E35R002S	33.602941	-114.644264	260	328					10/18/1961	8	251.93	251.040
06S/22E-35R02S	006S022E35R002S	33.602941	-114.644264	260	328					11/21/1961	6	253.62	251.040
06S/22E-35R02S	006S022E35R002S	33.602941	-114.644264	260	328					12/20/1961	7	253.35	251.040
06S/22E-35R02S	006S022E35R002S	33.602941	-114.644264	260	328					1/22/1962	7	252.75	251.040
06S/22E-35R02S	006S022E35R002S	33.602941	-114.644264	260	328					2/19/1962	8	252.40	251.040
06S/22E-35R02S	006S022E35R002S	33.602941	-114.644264	260	328					3/26/1962	14	246.06	251.040
06S/22E-35R02S	006S022E35R002S	33.602941	-114.644264	260	328					4/23/1962	10	250.02	251.040
06S/22E-35R02S	006S022E35R002S	33.602941	-114.644264	260	328					5/25/1962	6	254.06	251.040
06S/22E-35R02S	006S022E35R002S	33.602941	-114.644264	260	328					6/21/1962	13	247.11	251.040
06S/22E-35R02S	006S022E35R002S	33.602941	-114.644264	260	328					7/19/1962	7	253.24	251.040
06S/22E-35R02S	006S022E35R002S	33.602941	-114.644264	260	328					8/16/1962	21	239.00	251.040
06S/22E-35R02S	006S022E35R002S	33.602941	-114.644264	260	328					9/20/1962	6	254.09	251.040
06S/22E-35R02S	006S022E35R002S	33.602941	-114.644264	260	328					10/11/1962	6	253.98	251.040
06S/22E-35R02S	006S022E35R002S	33.602941	-114.644264	260	328					10/23/1962	7	253.30	251.040
06S/22E-35R02S	006S022E35R002S	33.602941	-114.644264	260	328					11/8/1962	6	253.74	251.040
06S/22E-35R02S	006S022E35R002S	33.602941	-114.644264	260	328					12/13/1962	6	253.77	251.040
06S/22E-35R02S	006S022E35R002S	33.602941	-114.644264	260	328					1/11/1963	7	252.80	251.040
06S/22E-35R02S	006S022E35R002S	33.602941	-114.644264	260	328					8/1/1972	8	252.00	251.040

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
06S/22E-35R02S	006S022E35R002S	33.602941	-114.644264	260	328					8/2/1972	8	251.90	251.040
06S/22E-35R05S	006S022E35R005S	33.605052	-114.643791	260	22.9					10/4/2000	9	250.85	250.850
06S/22E-35R06S	006S022E35R006S	33.603552	-114.644208	260	19.17					10/4/2000	10	250.31	250.310
06S/22E-35R07S	006S022E35R007S	33.603719	-114.644541	260	19.38					10/4/2000	10	250.05	250.050
06S/22E-36G18S	006S022E36G018S	33.612608	-114.628763	264						3/23/2004	11	253.31	253.310
06S/22E-36R01S	006S022E36R001S	33.602802	-114.623846	260.9	9					7/20/1971	6	255.24	255.240
06S/23E-03R01S	006S023E03R001S	33.676689	-114.554956	274						6/1/1971	6	268.00	268.000
06S/23E-04D01S	006S023E04D001S	33.690300	-114.588846	278						6/1/1971	8	270.00	270.000
06S/23E-04N01S	006S023E04N001S	33.676134	-114.588568	276						6/1/1971	6	270.00	270.000
06S/23E-04Q05S	006S023E04Q005S	33.676523	-114.579235	275						1/13/2005	11	264.43	264.430
06S/23E-05A01S	006S023E05A001S	33.688634	-114.589680	277						6/1/1971	7	270.00	270.000
06S/23E-05E01S	006S023E05E001S	33.686689	-114.606902	282						6/1/1971	16	266.00	266.000
06S/23E-05E03S	006S023E05E003S	33.683384	-114.605763	278						2/23/2000	11	266.94	266.940
06S/23E-05E04S	006S023E05E004S	33.683411	-114.606680	278	62					4/19/1998	12	266.00	265.885
06S/23E-05E04S	006S023E05E004S	33.683411	-114.606680	278	62					2/23/2000	12	265.77	265.885
06S/23E-05H01S	006S023E05H001S	33.686689	-114.589957	276						6/1/1971	5	271.00	271.000
06S/23E-05H02S	006S023E05H002S	33.686689	-114.593846	274						6/1/1971	7	267.00	267.000
06S/23E-05K01S	006S023E05K001S	33.682800	-114.593846	274						6/1/1971	7	267.00	267.000
06S/23E-05M01S	006S023E05M001S	33.682800	-114.603291	272						6/1/1971	8	264.00	264.000
06S/23E-05N01S	006S023E05N001S	33.675856	-114.606902	270						6/1/1971	6	264.00	264.000
06S/23E-05P01S	006S023E05P001S	33.675856	-114.602735	271						7/1/1971	8	263.00	263.000
06S/23E-06M01S	006S023E06M001S	33.681134	-114.624403	269						6/1/1971	9	260.00	260.000
06S/23E-08B01S	006S023E08B001S	33.675856	-114.593846	273						7/1/1971	8	265.00	265.000
06S/23E-08E03S	006S023E08E003S	33.671106	-114.606319	273	61					4/28/1998	12	261.00	262.620
06S/23E-08E03S	006S023E08E003S	33.671106	-114.606319	273	61					2/24/2000	9	264.24	262.620
06S/23E-08H01S	006S023E08H001S	33.668912	-114.593291	275						6/1/1971	11	264.00	264.000
06S/23E-08L01S	006S023E08L001S	33.668356	-114.602180	271						7/1/1971	9	262.00	262.000
06S/23E-08R01S	006S023E08R001S	33.661690	-114.589679	271						6/1/1971	9	262.00	262.000
06S/23E-09A01S	006S023E09A001S	33.675856	-114.572179	277						6/1/1971	8	269.00	269.000
06S/23E-09C01S	006S023E09C001S	33.675637	-114.581290	276						2/17/2005	11	264.80	264.800
06S/23E-10E01S	006S023E10E001S	33.672523	-114.571873	281						4/14/2004	10	270.75	270.750

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
06S/23E-10N01S	006S023E10N001S	33.662245	-114.571345	274						6/1/1971	10	264.00	264.000
06S/23E-11N01S	006S023E11N001S	33.662245	-114.553289	277						6/1/1971	10	267.00	267.000
06S/23E-11R01S	006S023E11R001S	33.662523	-114.539122	274						6/1/1971	6	268.00	268.000
06S/23E-12M01S	006S023E12M001S	33.669634	-114.534344	280						2/1/2000	19	261.06	261.060
06S/23E-12M07S	006S023E12M007S	33.668606	-114.533928	280						2/1/2000	19	260.95	260.950
06S/23E-12M10S	006S023E12M010S	33.668106	-114.533844	280	62					4/21/1998	17	263.00	262.110
06S/23E-12M10S	006S023E12M010S	33.668106	-114.533844	280	62					2/2/2000	19	261.22	262.110
06S/23E-12M12S	006S023E12M012S	33.667412	-114.534261	280						2/4/2000	18	261.79	261.790
06S/23E-12M27S	006S023E12M027S	33.669467	-114.533567	280	47					5/25/2000	18	261.98	261.980
06S/23E-12M32S	006S023E12M032S	33.669801	-114.534511	280	220					3/30/2000	19	260.89	260.890
06S/23E-12P14S	006S023E12P014S	33.664273	-114.530900	278	62					5/19/1999	14	264.00	264.000
06S/23E-12P41S	006S023E12P041S	33.664412	-114.529844	277	25					6/2/1997	10	267.00	267.000
06S/23E-13B01S	006S023E13B001S	33.661829	-114.524816	275						11/18/1999	18	256.89	256.890
06S/23E-13B02S	006S023E13B002S	33.660829	-114.525066	275	492					2/5/1997	17	258.00	256.970
06S/23E-13B02S	006S023E13B002S	33.660829	-114.525066	275	492					11/18/1999	19	255.94	256.970
06S/23E-14R01S	006S023E14R001S	33.648079	-114.536622	272						7/1/1971	6	266.00	266.000
06S/23E-15D02S	006S023E15D002S	33.658190	-114.571012	277						4/28/2004	10	266.75	266.750
06S/23E-15N01S	006S023E15N001S	33.647246	-114.571067	274						7/1/1971	9	265.00	265.000
06S/23E-15N03S	006S023E15N003S	33.648690	-114.567234	275						1/25/2005	10	264.70	264.700
06S/23E-16E01S	006S023E16E001S	33.657245	-114.588568	273	390					6/10/1966	8	265.00	265.000
06S/23E-17C02S	006S023E17C002S	33.661023	-114.601013	272	63					4/22/1998	5	267.00	267.000
06S/23E-17D02S	006S023E17D002S	33.660718	-114.603485	271	25.15					3/7/2000	11	260.06	260.060
06S/23E-17D03S	006S023E17D003S	33.660634	-114.603458	271	62					4/10/1998	5	266.00	266.000
06S/23E-17D04S	006S023E17D004S	33.660995	-114.602763	271	62					4/8/1998	5	266.00	266.000
06S/23E-17D05S	006S023E17D005S	33.660245	-114.605902	271	62					4/11/1998	10	261.00	260.925
06S/23E-17D05S	006S023E17D005S	33.660245	-114.605902	271	62					1/25/2000	10	260.85	260.925
06S/23E-17H01S	006S023E17H001S	33.654468	-114.593290	271						7/1/1971	7	264.00	264.000
06S/23E-17M01S	006S023E17M001S	33.650523	-114.605402	270						11/3/2004	10	260.20	260.200
06S/23E-17Q04S	006S023E17Q004S	33.647273	-114.596485	270	100					4/27/2000	10	259.94	259.940
06S/23E-17R01S	006S023E17R001S	33.647246	-114.589124	273						7/1/1971	9	264.00	264.000
06S/23E-18A01S	006S023E18A001S	33.660856	-114.606902	271						8/1/1971	9	262.00	262.000

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FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
06S/23E-18D01S	006S023E18D001S	33.660579	-114.624125	267						8/1/1971	8	259.00	259.000
06S/23E-19P01S	006S023E19P001S	33.631968	-114.619124	268						7/1/1971	8	260.00	260.000
06S/23E-20D01S	006S023E20D001S	33.643357	-114.606068	268						7/1/1971	8	260.00	260.000
06S/23E-20J01S	006S023E20J001S	33.639468	-114.588846	272						7/1/1971	7	265.00	265.000
06S/23E-20J02S	006S023E20J002S	33.639468	-114.590790	272						7/1/1971	7	265.00	265.000
06S/23E-20J03S	006S023E20J003S	33.639468	-114.593012	269						7/1/1971	6	263.00	263.000
06S/23E-20N01S	006S023E20N001S	33.632246	-114.605791	271						7/1/1971	8	263.00	263.000
06S/23E-20P01S	006S023E20P001S	33.632552	-114.597485	270	28.25					3/20/1995	10	260.00	260.000
06S/23E-20P08S	006S023E20P008S	33.632468	-114.598485	273	25.2					11/16/2004	7	265.88	265.880
06S/23E-20R01S	006S023E20R001S	33.631968	-114.588846	271						7/1/1971	4	267.00	267.000
06S/23E-20R02S	006S023E20R002S	33.619191	-114.588845	273						7/1/1971	7	266.00	266.000
06S/23E-20R03S	006S023E20R003S	33.619191	-114.593012	273						7/1/1971	8	265.00	265.000
06S/23E-21C01S	006S023E21C001S	33.644468	-114.584401	272						7/1/1971	7	265.00	265.000
06S/23E-21G01S	006S023E21G001S	33.639746	-114.579679	271						7/1/1971	3	268.00	268.000
06S/23E-21L01S	006S023E21L001S	33.636413	-114.582179	270						7/1/1971	6	264.00	264.000
06S/23E-21N01S	006S023E21N001S	33.632802	-114.586290	270						5/12/2004	10	259.80	261.680
06S/23E-21N01S	006S023E21N002S	33.633135	-114.586568	270						5/12/2004	6	263.56	261.680
06S/23E-21N02S	006S023E22A001S	33.646968	-114.554678	268						7/1/1971	3	265.00	265.000
06S/23E-22A01S	006S023E22M006S	33.638135	-114.570484	269.6						4/14/2004	8	261.41	261.410
06S/23E-22M06S	006S023E22R001S	33.632802	-114.555789	268						7/1/1971	6	262.00	262.000
06S/23E-22R01S	006S023E25D001S	33.631691	-114.535233	269						7/1/1971	7	262.00	262.000
06S/23E-25D01S	006S023E26R001S	33.619191	-114.537177	270						7/1/1971	9	261.00	261.000
06S/23E-26R01S	006S023E27C001S	33.632524	-114.562734	272						6/1/1971	9	263.00	263.000
06S/23E-27C01S	006S023E27D001S	33.631968	-114.567901	270	62					4/27/1998	12	258.00	258.000
06S/23E-27D01S	006S023E27D001S	33.631968	-114.567901	270	62					1/27/2000	12	258.29	258.690
06S/23E-27D01S	006S023E27E004S	33.625685	-114.570273	270.9						4/13/2004	12	259.09	258.690
06S/23E-27E04S	006S023E27R001S	33.618635	-114.554400	266						7/1/1971	7	259.00	259.000
06S/23E-27R01S	006S023E28A001S	33.632246	-114.572734	268						7/1/1971	5	263.00	263.000
06S/23E-28A01S	006S023E28F002S	33.625357	-114.581318	270						12/16/2004	12	258.34	258.340
06S/23E-28F02S	006S023E28N001S	33.618080	-114.586068	271						7/1/1971	9	262.00	262.000
06S/23E-28N01S	006S023E28N002S	33.621163	-114.584123	270	592					12/20/1975	10	260.00	260.000

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
06S/23E-28N02S	006S023E28N002S	33.621163	-114.584123	270	592					1/27/1997	15	254.80	257.960
06S/23E-28N02S	006S023E28N002S	33.621163	-114.584123	270	592					11/18/1999	13	256.86	257.960
06S/23E-28N02S	006S023E29B007S	33.631857	-114.594401	271						11/16/2004	9	262.22	257.960
06S/23E-29B07S	006S023E29C004S	33.628746	-114.597457	271						5/19/2004	12	258.72	258.720
06S/23E-29C04S	006S023E29E002S	33.628718	-114.603485	270	158					8/20/1963	8	262.00	262.000
06S/23E-29E02S	006S023E29E002S	33.628718	-114.603485	270	158					1/11/2000	13	257.27	258.635
06S/23E-29E02S	006S023E29N001S	33.621135	-114.600235	270	266					8/1/1972	10	260.00	258.635
06S/23E-29N01S	006S023E29N003S	33.621302	-114.602207	270	682					9/12/1973	14	256.00	256.000
06S/23E-29N03S	006S023E29N003S	33.621302	-114.602207	270	682					1/28/1997	21	249.00	254.690
06S/23E-29N03S	006S023E29N003S	33.621302	-114.602207	270	682					9/2/1999	16	253.80	254.690
06S/23E-29N03S	006S023E29N003S	33.621302	-114.602207	270	682					11/18/1999	13	257.36	254.690
06S/23E-29N03S	006S023E29R001S	33.619469	-114.588568	270	382					2/7/1961	11	258.60	254.690
06S/23E-29R01S	006S023E29R001S	33.619469	-114.588568	270	382					8/3/1971	38	232.15	245.575
06S/23E-29R01S	006S023E30K001S	33.621413	-114.610235	269	690					10/4/1977	10	259.00	245.575
06S/23E-30K01S	006S023E30K001S	33.621413	-114.610235	269	690					6/27/1979	9	259.55	258.828
06S/23E-30K01S	006S023E30K001S	33.621413	-114.610235	269	690					7/26/1979	9	259.55	258.828
06S/23E-30K01S	006S023E30K001S	33.621413	-114.610235	269	690					7/23/1980	10	259.47	258.828
06S/23E-30K01S	006S023E30K001S	33.621413	-114.610235	269	690					1/23/1981	11	258.38	258.828
06S/23E-30K01S	006S023E30K001S	33.621413	-114.610235	269	690					9/23/1981	9	259.63	258.828
06S/23E-30K01S	006S023E30K001S	33.621413	-114.610235	269	690					2/3/1982	11	258.38	258.828
06S/23E-30K01S	006S023E30K001S	33.621413	-114.610235	269	690					12/9/1982	10	259.19	258.828
06S/23E-30K01S	006S023E30K001S	33.621413	-114.610235	269	690					9/20/1983	10	259.23	258.828
06S/23E-30K01S	006S023E30K001S	33.621413	-114.610235	269	690					9/18/1984	10	259.08	258.828
06S/23E-30K01S	006S023E30K001S	33.621413	-114.610235	269	690					2/27/1985	11	258.22	258.828
06S/23E-30K01S	006S023E30K001S	33.621413	-114.610235	269	690					6/12/1985	11	258.25	258.828
06S/23E-30K01S	006S023E30N001S	33.617524	-114.622735	264						7/1/1971	7	257.00	258.828
06S/23E-30N01S	006S023E31A001S	33.617246	-114.606068	267						7/1/1971	8	259.00	259.000
06S/23E-31A01S	006S023E31B001S	33.616969	-114.611902	267	554					10/11/1972	6	261.00	261.000
06S/23E-31B01S	006S023E31B001S	33.616969	-114.611902	267	554					9/2/1999	12	254.80	257.150
06S/23E-31B01S	006S023E31B001S	33.616969	-114.611902	267	554					11/18/1999	12	255.15	257.150
06S/23E-31B01S	006S023E31J001S	33.609108	-114.608235	266	390					2/6/1962	5	261.50	257.150

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
06S/23E-31J01S	006S023E32C002S	33.616052	-114.597179	269	602					3/21/1973	14	255.00	255.000
06S/23E-32C02S	006S023E32D001S	33.617246	-114.605235	268	316					7/30/1953	5	263.00	263.000
06S/23E-32D01S	006S023E32D001S	33.617246	-114.605235	268	316					2/7/1961	9	259.00	259.500
06S/23E-32D01S	006S023E32E001S	33.612802	-114.603290	267	660					2/1/1966	7	260.00	259.500
06S/23E-32E01S	006S023E32F001S	33.613080	-114.597735	268	188					4/20/1905	11	257.00	257.000
06S/23E-32F01S	006S023E32F001S	33.613080	-114.597735	268	188					5/24/1962	9	259.28	258.594
06S/23E-32F01S	006S023E32F001S	33.613080	-114.597735	268	188					6/20/1962	9	259.40	258.594
06S/23E-32F01S	006S023E32F001S	33.613080	-114.597735	268	188					7/20/1962	9	258.92	258.594
06S/23E-32F01S	006S023E32F001S	33.613080	-114.597735	268	188					8/16/1962	9	258.86	258.594
06S/23E-32F01S	006S023E32F001S	33.613080	-114.597735	268	188					10/10/1962	8	259.69	258.594
06S/23E-32F01S	006S023E32F001S	33.613080	-114.597735	268	188					11/8/1962	8	259.97	258.594
06S/23E-32F01S	006S023E32F001S	33.613080	-114.597735	268	188					12/13/1962	8	260.00	258.594
06S/23E-32F01S	006S023E32F001S	33.613080	-114.597735	268	188					1/10/1963	9	259.09	258.594
06S/23E-32F01S	006S023E32F001S	33.613080	-114.597735	268	188					8/1/1971	11	257.00	258.594
06S/23E-32F01S	006S023E32F001S	33.613080	-114.597735	268	188					8/3/1971	11	257.32	258.594
06S/23E-32F01S	006S023E32F002S	33.612802	-114.600790	267	252					4/20/1905	12	255.00	258.594
06S/23E-32F02S	006S023E32F002S	33.612802	-114.600790	267	252					8/3/1971	21	245.85	254.325
06S/23E-32F02S	006S023E32G001S	33.611969	-114.594401	270	190					12/15/1961	7	262.80	254.325
06S/23E-32G01S	006S023E32G001S	33.611969	-114.594401	270	190					1961-10	8	262.00	261.955
06S/23E-32G01S	006S023E32G002S	33.613302	-114.594929	270	590					12/15/1961	8	261.91	261.955
06S/23E-32G02S	006S023E32G002S	33.613302	-114.594929	270	590					12/21/1961	8	262.00	260.000
06S/23E-32G02S	006S023E32G003S	33.612802	-114.594957	268	123.5					10/4/1949	10	258.00	260.000
06S/23E-32G03S	006S023E32L001S	33.606969	-114.598846	265	176					2/7/1961	9	256.50	256.500
06S/23E-32L01S	006S023E32L002S	33.609469	-114.598568	267						7/1/1971	11	256.00	256.000
06S/23E-32L02S	006S023E32L003S	33.609469	-114.599123	267	127					8/1/1972	11	256.00	256.000
06S/23E-32L03S	006S023E32M001S	33.609747	-114.602179	267	300					2/7/1961	7	259.70	259.700
06S/23E-32M01S	006S023E32P001S	33.604219	-114.598846	265	430					8/3/1971	21	244.25	244.250
06S/23E-32P01S	006S023E32P001S	33.604219	-114.598846	265	430					11/4/1999	11	253.90	257.633
06S/23E-32P01S	006S023E33A001S	33.617802	-114.571345	267						7/1/1971	7	260.00	257.633
06S/23E-32P01S	006S023E33D001S	33.615274	-114.587762	270	568					6/21/1974	11	259.00	257.633
06S/23E-33A01S	006S023E33D001S	33.615274	-114.587762	270	568					11/17/1999	15	255.43	255.430

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
06S/23E-33D01S	006S023E33E001S	33.611136	-114.586345	270	368					8/2/1947	11	259.30	246.565
06S/23E-33D01S	006S023E33E001S	33.611136	-114.586345	270	368					8/3/1971	36	233.83	246.565
06S/23E-33E01S	006S023E33F001S	33.613163	-114.581373	270	464					5/31/1966	8	262.00	258.750
06S/23E-33E01S	006S023E33F001S	33.613163	-114.581373	270	464					7/26/1972	15	255.50	258.750
06S/23E-33F01S	006S023E33F001S	33.613163	-114.581373	270	464					11/19/1999	14	256.45	259.783
06S/23E-33F01S	006S023E33G001S	33.614249	-114.577290	270.2	600					4/30/1959	9	261.70	259.783
06S/23E-33F01S	006S023E33G001S	33.614249	-114.577290	270.2	600					2/7/1962	9	261.20	259.783
06S/23E-33G01S	006S023E33G001S	33.614249	-114.577290	270.2	600					11/19/1999	13	257.44	257.315
06S/23E-33G01S	006S023E33G001S	33.614249	-114.577290	270.2	600					4/18/2002	13	256.82	257.315
06S/23E-33G01S	006S023E33K001S	33.610080	-114.576678	267	408					6/22/1960	7	260.00	257.315
06S/23E-33G01S	006S023E33K001S	33.610080	-114.576678	267	408					7/1/1972	12	255.00	257.315
06S/23E-33K01S	006S023E33K001S	33.610080	-114.576678	267	408					7/20/1972	12	255.20	255.668
06S/23E-33K01S	006S023E33K001S	33.610080	-114.576678	267	408					11/19/1999	12	254.69	255.668
06S/23E-33K01S	006S023E33M001S	33.609830	-114.582567	270	100					11/19/1999	14	256.42	255.668
06S/23E-33K01S	006S023E33M001S	33.609830	-114.582567	270	100					11/19/1999	14	256.36	255.668
06S/23E-33M01S	006S023E33M001S	33.609830	-114.582567	270	100					1949-01	8	262.00	259.303
06S/23E-33M01S	006S023E33N001S	33.603358	-114.587179	265.84	10.9					7/20/1971	10	255.41	259.303
06S/23E-33M01S	006S023E34M001S	33.609330	-114.568067	265	478					9/23/1966	5	260.50	259.303
06S/23E-33N01S	006S023E34N001S	33.604191	-114.570511	263						7/1/1971	7	256.00	256.000
06S/23E-34M01S	006S023E35E001S	33.611691	-114.551066	265	365.5					7/26/1979	9	255.96	255.960
06S/23E-34N01S	006S023E35E001S	33.611691	-114.551066	265	365.5					7/23/1980	9	256.41	256.410
06S/23E-35E01S	006S023E35E001S	33.611691	-114.551066	265	365.5					1/22/1981	10	255.15	255.939
06S/23E-35E01S	006S023E35E001S	33.611691	-114.551066	265	365.5					8/27/1981	8	256.70	255.939
06S/23E-35E01S	006S023E35E001S	33.611691	-114.551066	265	365.5					2/3/1982	10	254.76	255.939
06S/23E-35E01S	006S023E35E001S	33.611691	-114.551066	265	365.5					12/10/1982	10	255.27	255.939
06S/23E-35E01S	006S023E35E001S	33.611691	-114.551066	265	365.5					9/20/1983	8	257.24	255.939
06S/23E-35E01S	006S023E35E001S	33.611691	-114.551066	265	365.5					9/18/1984	8	257.28	255.939
06S/23E-35E01S	006S023E35E001S	33.611691	-114.551066	265	365.5					2/27/1985	9	255.64	255.939
06S/23E-35E01S	006S023E35E001S	33.611691	-114.551066	265	365.5					6/12/1985	9	256.34	255.939
06S/23E-35E01S	006S023E35E001S	33.611691	-114.551066	265	365.5					11/19/1999	11	253.95	255.939
06S/23E-35E01S	006S023E35N001S	33.604747	-114.551066	267						7/1/1971	12	255.00	255.939

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
06S/23E-35E01S	006S023E35R002S	33.606414	-114.536344	271						7/1/1971	13	258.00	255.939
06S/23E-35N01S	006S023E36N001S	33.605858	-114.533566	270	248					2/6/1962	16	253.77	253.770
06S/23E-35R02S	006S023E36N001S	33.605858	-114.533566	270	248					7/1/1972	14	256.00	256.000
06S/23E-36N01S	006S024E18D001S	33.661357	-114.517927	275	57					5/18/1993	16	259.00	251.205
06S/23E-36N01S	007S021E01C001S	33.605305	-114.738250	389						11/17/1992	146	243.41	251.205
06S/24E-18D01S	007S021E01C001S	33.605305	-114.738250	389						2/16/2000	144	244.61	244.610
07S/21E-01C01S	007S021E01C001S	33.605305	-114.738250	389						3/30/2006	144	244.76	243.333
07S/21E-01C01S	007S021E01C001S	33.605305	-114.738250	389						3/31/2006	144	244.93	243.333
07S/21E-01C01S	007S021E02J001S	33.595389	-114.744525	388.8						9/24/1990	149	239.55	243.333
07S/21E-01C01S	007S021E02J001S	33.595389	-114.744525	388.8						3/29/2006	145	244.09	243.333
07S/21E-02J01S	007S021E02J001S	33.595389	-114.744525	388.8						3/30/2006	145	244.02	242.923
07S/21E-02J01S	007S021E02R001S	33.588555	-114.744514	387.7						9/24/1990	146	241.48	242.923
07S/21E-02J01S	007S021E02R001S	33.588555	-114.744514	387.7						2/15/2000	144	243.27	242.923
07S/21E-02R01S	007S021E05C002S	33.602827	-114.805707	504.4						2/10/1992	255	249.12	248.670
07S/21E-02R01S	007S021E05C002S	33.602827	-114.805707	504.4						2/5/2002	256	248.22	248.670
07S/21E-05C02S	007S021E05C002S	33.602827	-114.805707	504.4						3/19/2002	257	247.81	250.000
07S/21E-05C02S	007S021E05C002S	33.602827	-114.805707	504.4						3/29/2006	256	248.12	250.000
07S/21E-05C02S	007S021E05C002S	33.602827	-114.805707	504.4						3/30/2006	256	248.06	250.000
07S/21E-05C02S	007S021E12D001S	33.588350	-114.744277	387.58	390					9/3/1965	130	257.58	250.000
07S/21E-05C02S	007S021E12D001S	33.588350	-114.744277	387.58	390					1/28/1966	139	248.43	250.000
07S/21E-12D01S	007S021E12D001S	33.588350	-114.744277	387.58	390					10/20/1966	139	248.12	244.598
07S/21E-12D01S	007S021E12D001S	33.588350	-114.744277	387.58	390					8/1/1972	141	246.58	244.598
07S/21E-12D01S	007S021E12N001S	33.574014	-114.744411	385.85						9/22/1990	145	240.82	244.598
07S/21E-12D01S	007S021E12N001S	33.574014	-114.744411	385.85						2/16/2000	143	242.87	244.598
07S/21E-12N01S	007S021E12N001S	33.574014	-114.744411	385.85						1944-12	140	245.85	246.903
07S/21E-12N01S	007S021E14A001S	33.573847	-114.744652	386.86						6/9/1961	140	247.20	246.903
07S/21E-12N01S	007S021E14A001S	33.573847	-114.744652	386.86						2/15/1962	139	247.66	246.903
07S/21E-14A01S	007S021E14A001S	33.573847	-114.744652	386.86						10/20/1966	139	247.66	246.515
07S/21E-14A01S	007S021E14A001S	33.573847	-114.744652	386.86						7/1/1971	141	245.86	246.515
07S/21E-14A01S	007S021E14B001S	33.573922	-114.749289	384.8						4/27/1905	140	244.80	246.515
07S/21E-14A01S	007S021E14B001S	33.573922	-114.749289	384.8						6/9/1961	137	247.74	246.515

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
07S/21E-14B01S	007S021E14B001S	33.573922	-114.749289	384.8						2/15/1962	138	246.80	245.657
07S/21E-14B01S	007S021E14B001S	33.573922	-114.749289	384.8						5/24/1962	140	245.00	245.657
07S/21E-14B01S	007S021E14B001S	33.573922	-114.749289	384.8						6/20/1962	140	244.90	245.657
07S/21E-14B01S	007S021E14B001S	33.573922	-114.749289	384.8						7/19/1962	140	244.99	245.657
07S/21E-14B01S	007S021E14B001S	33.573922	-114.749289	384.8						8/16/1962	140	245.05	245.657
07S/21E-14B01S	007S021E14B001S	33.573922	-114.749289	384.8						9/17/1962	140	245.10	245.657
07S/21E-14B01S	007S021E14B001S	33.573922	-114.749289	384.8						10/11/1962	140	244.98	245.657
07S/21E-14B01S	007S021E14B001S	33.573922	-114.749289	384.8						11/8/1962	140	244.98	245.657
07S/21E-14B01S	007S021E14B001S	33.573922	-114.749289	384.8						12/13/1962	140	244.96	245.657
07S/21E-14B01S	007S021E14B001S	33.573922	-114.749289	384.8						1/9/1963	140	244.98	245.657
07S/21E-14B01S	007S021E14H001S	33.566709	-114.747241	379.52	900					3/1/1966	130	249.52	245.657
07S/21E-14B01S	007S021E14H001S	33.566709	-114.747241	379.52	900					10/20/1966	133	246.62	245.657
07S/21E-14H01S	007S021E14H001S	33.566709	-114.747241	379.52	900					8/1/1972	134	245.52	253.334
07S/21E-14H01S	007S021E14H001S	33.566709	-114.747241	379.52	900					9/22/1990	138	241.92	253.334
07S/21E-14H01S	007S021E15A001S	33.573864	-114.761956	390.8						9/23/1990	138	252.99	253.334
07S/21E-14H01S	007S021E15A001S	33.573864	-114.761956	390.8						3/23/1992	138	253.07	253.334
07S/21E-15A01S	007S021E15A001S	33.573864	-114.761956	390.8						3/29/2000	137	253.40	252.098
07S/21E-15A01S	007S021E15A001S	33.573864	-114.761956	390.8						10/4/2000	137	253.34	252.098
07S/21E-15A01S	007S021E15A001S	33.573864	-114.761956	390.8						12/14/2000	138	253.20	252.098
07S/21E-15A01S	007S021E15A001S	33.573864	-114.761956	390.8						2/25/2001	139	251.53	252.098
07S/21E-15A01S	007S021E15A001S	33.573864	-114.761956	390.8						4/17/2001	138	253.30	252.098
07S/21E-15A01S	007S021E15A001S	33.573864	-114.761956	390.8						7/11/2001	138	253.27	252.098
07S/21E-15A01S	007S021E15A001S	33.573864	-114.761956	390.8						11/7/2001	138	253.17	252.098
07S/21E-15A01S	007S021E15A001S	33.573864	-114.761956	390.8						4/3/2002	137	253.41	252.098
07S/21E-15A01S	007S021E15A001S	33.573864	-114.761956	390.8						10/2/2002	137	253.47	252.098
07S/21E-15A01S	007S021E15A001S	33.573864	-114.761956	390.8						6/3/2003	137	253.52	252.098
07S/21E-15A01S	007S021E15A001S	33.573864	-114.761956	390.8						11/5/2003	137	253.55	252.098
07S/21E-15A01S	007S021E15A001S	33.573864	-114.761956	390.8						3/2/2004	137	253.39	252.098
07S/21E-15A01S	007S021E15A001S	33.573864	-114.761956	390.8						8/4/2004	137	253.48	252.098
07S/21E-15A01S	007S021E15A001S	33.573864	-114.761956	390.8						12/8/2004	137	253.44	252.098
07S/21E-15A01S	007S021E15A001S	33.573864	-114.761956	390.8						4/15/2005	137	253.38	252.098

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
07S/21E-15A01S	007S021E15A001S	33.573864	-114.761956	390.8						8/31/2005	138	253.23	252.098
07S/21E-15A01S	007S021E15A001S	33.573864	-114.761956	390.8						1/27/2006	138	253.19	252.098
07S/21E-15A01S	007S021E15A001S	33.573864	-114.761956	390.8						3/30/2006	138	253.17	252.098
07S/21E-15A01S	007S021E15A001S	33.573864	-114.761956	390.8						3/31/2006	138	253.17	252.098
07S/21E-15A01S	007S021E15A001S	33.573864	-114.761956	390.8						5/5/2006	138	253.11	252.098
07S/21E-15A01S	007S021E15A001S	33.573864	-114.761956	390.8						8/10/2006	138	253.16	252.098
07S/21E-15A01S	007S021E15A001S	33.573864	-114.761956	390.8						12/8/2006	138	253.19	252.098
07S/21E-15A01S	007S021E27H001S	33.541237	-114.762102	374.7						9/23/1990	135	239.58	252.098
07S/21E-15A01S	007S021E27H001S	33.541237	-114.762102	374.7						3/23/1992	135	239.69	252.098
07S/21E-27H01S	007S021E36D001S	33.530293	-114.744404	370.1						9/23/1990	133	236.76	236.545
07S/21E-27H01S	007S021E36D001S	33.530293	-114.744404	370.1						3/23/1992	134	236.33	236.545
07S/21E-36D01S	007S021E36G001S	33.524010	-114.732854	247.4	16.47					5/18/2006	13	234.55	234.695
07S/21E-36D01S	007S021E36G001S	33.524010	-114.732854	247.4	16.47					5/19/2006	13	234.84	234.695
07S/21E-36G01S	007S021E36G001S	33.524010	-114.732854	247.4	16.47					2000-01	12	235.89	236.633
07S/21E-36G01S	007S021E36G001S	33.524010	-114.732854	247.4	16.47					2000-03	12	235.73	236.633
07S/21E-36G01S	007S021E36G001S	33.524010	-114.732854	247.4	16.47					2000-04	11	236.10	236.633
07S/21E-36G01S	007S021E36G001S	33.524010	-114.732854	247.4	16.47					2000-05	11	236.87	236.633
07S/21E-36G01S	007S021E36G001S	33.524010	-114.732854	247.4	16.47					2000-06	11	236.04	236.633
07S/21E-36G01S	007S021E36G001S	33.524010	-114.732854	247.4	16.47					2000-07	11	236.55	236.633
07S/21E-36G01S	007S021E36G001S	33.524010	-114.732854	247.4	16.47					2000-08	11	236.85	236.633
07S/21E-36G01S	007S021E36G001S	33.524010	-114.732854	247.4	16.47					2000-09	11	236.48	236.633
07S/21E-36G01S	007S021E36G001S	33.524010	-114.732854	247.4	16.47					2000-10	11	236.02	236.633
07S/21E-36G01S	007S021E36G001S	33.524010	-114.732854	247.4	16.47					2006-01	13	234.82	236.633
07S/21E-36G01S	007S021E36G001S	33.524010	-114.732854	247.4	16.47					2006-02	13	234.69	236.633
07S/21E-36G01S	007S021E36G001S	33.524010	-114.732854	247.4	16.47					2006-03	13	234.60	236.633
07S/21E-36G01S	007S021E36G001S	33.524010	-114.732854	247.4	16.47					2006-04	13	234.86	236.633
07S/21E-36G01S	007S021E36R001S	33.516138	-114.730793	239						8/1/1971	6	233.00	236.633
07S/21E-36G01S	007S022E01D001S	33.601691	-114.639958	261						7/1/1971	10	251.00	236.633
07S/21E-36R01S	007S022E02R001S	33.588358	-114.640513	257						7/1/1971	8	249.00	249.000
07S/22E-01D01S	007S022E02R005S	33.590580	-114.640541	261						5/20/2004	8	253.46	253.460
07S/22E-02R01S	007S022E03D001S	33.602525	-114.671070	260	49					3/30/1967	5	254.59	254.590

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
07S/22E-02R05S	007S022E03D001S	33.602525	-114.671070	260	49					6/1/1967	5	255.10	255.100
07S/22E-03D01S	007S022E03D001S	33.602525	-114.671070	260	49					6/10/1968	7	252.77	256.359
07S/22E-03D01S	007S022E03D001S	33.602525	-114.671070	260	49					8/2/1972	7	253.10	256.359
07S/22E-03D01S	007S022E03D002S	33.602525	-114.671070	260	20					3/30/1967	5	254.87	256.359
07S/22E-03D01S	007S022E03D002S	33.602525	-114.671070	260	20					6/1/1967	5	255.44	256.359
07S/22E-03D02S	007S022E03D002S	33.602525	-114.671070	260	20					6/10/1968	7	253.13	248.620
07S/22E-03D02S	007S022E03D002S	33.602525	-114.671070	260	20					8/2/1972	11	249.00	248.620
07S/22E-03D02S	007S022E03H001S	33.595580	-114.657736	255	118					3/30/1967	9	245.80	248.620
07S/22E-03D02S	007S022E03H001S	33.595580	-114.657736	255	118					6/1/1967	9	245.87	248.620
07S/22E-03H01S	007S022E03H001S	33.595580	-114.657736	255	118					6/10/1968	11	243.65	251.039
07S/22E-03H01S	007S022E03H001S	33.595580	-114.657736	255	118					8/2/1972	11	244.50	251.039
07S/22E-03H01S	007S022E03H002S	33.595580	-114.657736	255	22					3/30/1967	10	245.20	251.039
07S/22E-03H01S	007S022E03H002S	33.595580	-114.657736	255	22					6/1/1967	10	245.31	251.039
07S/22E-03H02S	007S022E03H002S	33.595580	-114.657736	255	22					6/10/1968	12	242.95	252.244
07S/22E-03H02S	007S022E03H002S	33.595580	-114.657736	255	22					8/2/1972	11	244.00	252.244
07S/22E-03H02S	007S022E03L001S	33.595580	-114.670514	257						7/1/1971	10	247.00	252.244
07S/22E-03H02S	007S022E03N001S	33.588636	-114.674403	254						7/1/1971	9	245.00	252.244
07S/22E-03L01S	007S022E04H001S	33.595580	-114.675237	256						7/1/1971	11	245.00	245.000
07S/22E-03N01S	007S022E04H002S	33.595858	-114.677181	256						7/1/1971	10	246.00	246.000
07S/22E-04H01S	007S022E04P001S	33.589469	-114.684403	310	156					9/25/1961	59	251.43	251.430
07S/22E-04H02S	007S022E04P001S	33.589469	-114.684403	310	156					10/18/1961	59	251.47	251.470
07S/22E-04P01S	007S022E04P001S	33.589469	-114.684403	310	156					11/21/1961	58	252.45	248.568
07S/22E-04P01S	007S022E04P001S	33.589469	-114.684403	310	156					12/20/1961	58	252.10	248.568
07S/22E-04P01S	007S022E04P001S	33.589469	-114.684403	310	156					1/22/1962	59	250.78	248.568
07S/22E-04P01S	007S022E04P001S	33.589469	-114.684403	310	156					2/19/1962	60	250.25	248.568
07S/22E-04P01S	007S022E04P001S	33.589469	-114.684403	310	156					3/26/1962	59	250.58	248.568
07S/22E-04P01S	007S022E04P001S	33.589469	-114.684403	310	156					4/23/1962	60	250.13	248.568
07S/22E-04P01S	007S022E04P001S	33.589469	-114.684403	310	156					5/25/1962	60	250.12	248.568
07S/22E-04P01S	007S022E04P001S	33.589469	-114.684403	310	156					6/21/1962	60	250.00	248.568
07S/22E-04P01S	007S022E04P001S	33.589469	-114.684403	310	156					7/19/1962	60	250.35	248.568
07S/22E-04P01S	007S022E04P001S	33.589469	-114.684403	310	156					8/16/1962	60	250.47	248.568

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
07S/22E-04P01S	007S022E04P001S	33.589469	-114.684403	310	156					9/17/1962	59	250.59	248.568
07S/22E-04P01S	007S022E04P001S	33.589469	-114.684403	310	156					10/11/1962	60	250.14	248.568
07S/22E-04P01S	007S022E04P001S	33.589469	-114.684403	310	156					11/8/1962	60	249.98	248.568
07S/22E-04P01S	007S022E04P001S	33.589469	-114.684403	310	156					12/13/1962	60	249.97	248.568
07S/22E-04P01S	007S022E04P001S	33.589469	-114.684403	310	156					1/9/1963	59	251.39	248.568
07S/22E-04P01S	007S022E04Q001S	33.588914	-114.683015	275						5/1/1961	22	253.00	248.568
07S/22E-04P01S	007S022E04Q001S	33.588914	-114.683015	275						5/25/1961	22	252.56	248.568
07S/22E-04Q01S	007S022E04Q001S	33.588914	-114.683015	275						7/6/1961	23	252.32	251.407
07S/22E-04Q01S	007S022E04Q001S	33.588914	-114.683015	275						7/28/1961	23	252.35	251.407
07S/22E-04Q01S	007S022E04Q001S	33.588914	-114.683015	275						8/24/1961	23	252.37	251.407
07S/22E-04Q01S	007S022E04Q001S	33.588914	-114.683015	275						9/25/1961	22	253.24	251.407
07S/22E-04Q01S	007S022E04Q001S	33.588914	-114.683015	275						10/18/1961	23	251.74	251.407
07S/22E-04Q01S	007S022E04Q001S	33.588914	-114.683015	275						11/21/1961	22	252.88	251.407
07S/22E-04Q01S	007S022E04Q001S	33.588914	-114.683015	275						12/20/1961	22	252.55	251.407
07S/22E-04Q01S	007S022E04Q001S	33.588914	-114.683015	275						1/22/1962	23	252.32	251.407
07S/22E-04Q01S	007S022E04Q001S	33.588914	-114.683015	275						2/19/1962	23	252.46	251.407
07S/22E-04Q01S	007S022E04Q001S	33.588914	-114.683015	275						3/26/1962	22	252.68	251.407
07S/22E-04Q01S	007S022E04Q001S	33.588914	-114.683015	275						4/23/1962	23	251.91	251.407
07S/22E-04Q01S	007S022E04Q001S	33.588914	-114.683015	275						5/25/1962	23	251.97	251.407
07S/22E-04Q01S	007S022E04Q001S	33.588914	-114.683015	275						6/21/1962	23	252.40	251.407
07S/22E-04Q01S	007S022E04Q001S	33.588914	-114.683015	275						7/19/1962	23	252.22	251.407
07S/22E-04Q01S	007S022E04Q001S	33.588914	-114.683015	275						8/16/1962	23	252.34	251.407
07S/22E-04Q01S	007S022E04Q001S	33.588914	-114.683015	275						9/17/1962	23	252.38	251.407
07S/22E-04Q01S	007S022E04Q002S	33.588914	-114.748016	255						7/1/1971	10	245.00	251.407
07S/22E-04Q01S	007S022E05R002S	33.588608	-114.694620	330.2	600					5/20/1996	88	242.20	251.407
07S/22E-04Q02S	007S022E05R002S	33.588608	-114.694620	330.2	600					2/15/2000	86	243.92	243.920
07S/22E-05R02S	007S022E06L001S	33.595339	-114.718974	389.9						9/23/1990	148	242.33	238.500
07S/22E-05R02S	007S022E08A01S	33.585858	-114.693293	323						9/22/1990	88	234.67	238.500
07S/22E-06L01S	007S022E08K001S	33.581136	-114.700515	250						7/1/1971	8	242.00	242.000
07S/22E-08A01S	007S022E08M001S	33.581136	-114.705237	254						7/1/1971	12	242.00	242.000
07S/22E-08K01S	007S022E09D001S	33.584747	-114.691626	254						7/1/1971	10	244.00	244.000

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
07S/22E-08M01S	007S022E09D002S	33.587992	-114.690618	332.2						9/24/1990	95	236.95	236.950
07S/22E-09D01S	007S022E09N001S	33.574192	-114.691348	252						7/1/1971	9	243.00	243.000
07S/22E-09D02S	007S022E10A001S	33.587664	-114.658986	255	25					4/6/1995	10	245.00	245.000
07S/22E-09N01S	007S022E10R001S	33.574192	-114.657458	254						7/1/1971	7	247.00	247.000
07S/22E-10A01S	007S022E11D001S	33.588081	-114.656903	256						7/1/1971	10	246.00	246.000
07S/22E-10R01S	007S022E11Q001S	33.574470	-114.648013	256	460					2/14/1961	8	248.28	248.280
07S/22E-11D01S	007S022E11Q001S	33.574470	-114.648013	256	460					2/14/1962	8	248.28	248.280
07S/22E-11Q01S	007S022E12R001S	33.573636	-114.622735	256						7/1/1971	5	251.00	250.000
07S/22E-11Q01S	007S022E13E001S	33.570025	-114.635513	256						7/1/1971	7	249.00	250.000
07S/22E-12R01S	007S022E13E002S	33.568637	-114.639124	253						7/1/1971	5	248.00	248.000
07S/22E-13E01S	007S022E13E003S	33.566692	-114.639957	256						7/1/1971	7	249.00	249.000
07S/22E-13E02S	007S022E13F001S	33.566692	-114.635235	257						7/1/1971	8	249.00	249.000
07S/22E-13E03S	007S022E13G001S	33.566970	-114.630235	256						7/1/1971	9	247.00	247.000
07S/22E-13F01S	007S022E13H001S	33.566692	-114.626902	259						7/1/1971	10	249.00	249.000
07S/22E-13G01S	007S022E13H002S	33.570025	-114.626902	259						7/1/1971	10	249.00	249.000
07S/22E-13H01S	007S022E13J002S	33.564470	-114.626346	259						8/1/1971	9	250.00	250.000
07S/22E-13H02S	007S022E13J003S	33.563081	-114.626068	259						8/1/1971	9	250.00	250.000
07S/22E-13J02S	007S022E13J004S	33.564470	-114.622179	255						7/1/1971	11	244.00	244.000
07S/22E-13J03S	007S022E13K001S	33.564748	-114.630235	257						8/1/1971	10	247.00	247.000
07S/22E-13J04S	007S022E13L001S	33.564748	-114.634957	257						8/1/1971	10	247.00	247.000
07S/22E-13K01S	007S022E13M001S	33.564748	-114.639957	255						7/1/1971	8	247.00	247.000
07S/22E-13L01S	007S022E13P001S	33.563081	-114.634957	257						8/1/1971	10	247.00	247.000
07S/22E-13M01S	007S022E13R001S	33.561220	-114.622651	255	183					6/30/1978	5	250.00	250.000
07S/22E-13P01S	007S022E14A001S	33.573636	-114.640235	257						7/1/1971	7	250.00	250.000
07S/22E-13R01S	007S022E14E001S	33.566970	-114.656625	255						7/1/1971	10	245.00	245.000
07S/22E-14A01S	007S022E14E002S	33.568359	-114.657180	253						8/1/1971	6	247.00	247.000
07S/22E-14E01S	007S022E14F001S	33.566970	-114.652458	253						7/1/1971	8	245.00	245.000
07S/22E-14E02S	007S022E14G001S	33.566970	-114.648013	256						7/1/1971	12	244.00	244.000
07S/22E-14F01S	007S022E14G002S	33.568081	-114.648013	256						8/1/1971	9	247.00	247.000
07S/22E-14G01S	007S022E14H001S	33.566970	-114.644124	256						7/1/1971	7	249.00	249.000
07S/22E-14G02S	007S022E14H002S	33.569192	-114.643846	254						8/1/1971	6	248.00	248.000

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
07S/22E-14H01S	007S022E14H003S	33.568081	-114.643846	254						8/1/1971	7	247.00	247.000
07S/22E-14H02S	007S022E14J001S	33.564748	-114.644124	255						8/1/1971	8	247.00	247.000
07S/22E-14H03S	007S022E14K001S	33.564748	-114.648569	252						8/1/1971	12	240.00	240.000
07S/22E-14J01S	007S022E14M001S	33.565303	-114.656625	253						7/1/1971	8	245.00	245.000
07S/22E-14K01S	007S022E14N001S	33.560581	-114.656625	252						7/1/1971	6	246.00	246.000
07S/22E-14M01S	007S022E14P001S	33.563081	-114.652458	254						8/1/1971	9	245.00	245.000
07S/22E-14N01S	007S022E14P002S	33.563081	-114.649402	253						8/1/1971	8	245.00	245.000
07S/22E-14P01S	007S022E14P003S	33.563081	-114.650513	253						8/1/1971	9	244.00	244.000
07S/22E-14P02S	007S022E14Q001S	33.562803	-114.645235	255						8/1/1971	10	245.00	245.000
07S/22E-14P03S	007S022E14Q002S	33.562803	-114.646624	255						8/1/1971	10	245.00	245.000
07S/22E-14Q01S	007S022E14Q003S	33.562803	-114.647735	255						8/1/1971	11	244.00	244.000
07S/22E-14Q02S	007S022E14Q004S	33.563081	-114.648569	254						8/1/1971	9	245.00	245.000
07S/22E-14Q03S	007S022E14R001S	33.562803	-114.644124	255						8/1/1971	10	245.00	245.000
07S/22E-14Q04S	007S022E15B001S	33.570303	-114.661903	254						8/1/1971	10	244.00	244.000
07S/22E-14R01S	007S022E15D001S	33.573914	-114.674125	252						7/1/1971	8	244.00	244.000
07S/22E-15B01S	007S022E15E001S	33.566970	-114.674681	253						8/1/1971	10	243.00	243.000
07S/22E-15D01S	007S022E15E002S	33.568637	-114.674681	252						8/1/1971	9	243.00	243.000
07S/22E-15E01S	007S022E15F001S	33.566970	-114.666069	253						8/1/1971	12	241.00	241.000
07S/22E-15E02S	007S022E15F002S	33.568359	-114.666069	254						8/1/1971	14	240.00	240.000
07S/22E-15F01S	007S022E15H001S	33.566970	-114.661347	255						8/1/1971	11	244.00	244.000
07S/22E-15F02S	007S022E15H002S	33.568359	-114.661069	254						8/1/1971	11	243.00	243.000
07S/22E-15H01S	007S022E15J001S	33.563081	-114.661069	255						8/1/1971	11	244.00	244.000
07S/22E-15H02S	007S022E15J002S	33.564470	-114.661069	253						8/1/1971	9	244.00	244.000
07S/22E-15J01S	007S022E15M002S	33.564470	-114.671069	252						8/1/1971	10	242.00	242.000
07S/22E-15J02S	007S022E15N001S	33.559748	-114.671069	252						8/1/1971	10	242.00	242.000
07S/22E-15M02S	007S022E15N002S	33.564470	-114.670792	251						8/1/1971	10	241.00	241.000
07S/22E-15N01S	007S022E16G001S	33.566970	-114.679125	255						8/1/1971	10	245.00	245.000
07S/22E-15N02S	007S022E16G002S	33.566970	-114.682736	254						8/1/1971	11	243.00	243.000
07S/22E-16G01S	007S022E16G003S	33.568359	-114.683014	255						8/1/1971	11	244.00	244.000
07S/22E-16G02S	007S022E16H001S	33.568637	-114.678570	254						8/1/1971	10	244.00	244.000
07S/22E-16G03S	007S022E16J001S	33.565026	-114.675514	250						8/1/1971	10	240.00	240.000

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
07S/22E-16H01S	007S022E16J002S	33.562803	-114.679125	254						8/1/1971	10	244.00	244.000
07S/22E-16J01S	007S022E16J003S	33.564470	-114.679125	253						8/1/1971	10	243.00	243.000
07S/22E-16J02S	007S022E16K001S	33.564470	-114.682736	253						8/1/1971	10	243.00	243.000
07S/22E-16J03S	007S022E16L001S	33.565803	-114.683542	257	24.35					3/8/2001	11	245.69	245.690
07S/22E-16K01S	007S022E16M001S	33.562998	-114.690264	250	24.56					3/6/2001	11	238.96	238.960
07S/22E-16L01S	007S022E17C001S	33.573636	-114.701070	252						7/1/1971	10	242.00	242.000
07S/22E-16M01S	007S022E17P001S	33.559748	-114.704404	250						1/24/1961	7	243.15	243.150
07S/22E-17C01S	007S022E17P001S	33.559748	-114.704404	250						8/1/1972	8	242.00	242.000
07S/22E-17P01S	007S022E18A001S	33.573636	-114.711071	251						7/1/1971	9	242.00	241.500
07S/22E-17P01S	007S022E18J001S	33.566414	-114.713571	251						7/1/1971	10	241.00	241.500
07S/22E-18A01S	007S022E18K001S	33.563359	-114.713848	249						7/1/1971	8	241.00	241.000
07S/22E-18J01S	007S022E18Q001S	33.559470	-114.716904	248						7/1/1971	7	241.00	241.000
07S/22E-18K01S	007S022E18R001S	33.559667	-114.713701	251.5	17.81					4/26/2000	14	237.93	237.930
07S/22E-18Q01S	007S022E18R001S	33.559667	-114.713701	251.5	17.81					2000-01	13	238.50	238.500
07S/22E-18R01S	007S022E18R001S	33.559667	-114.713701	251.5	17.81					2000-03	14	237.67	237.971
07S/22E-18R01S	007S022E18R001S	33.559667	-114.713701	251.5	17.81					2000-04	14	237.20	237.971
07S/22E-18R01S	007S022E18R001S	33.559667	-114.713701	251.5	17.81					2000-05	14	237.80	237.971
07S/22E-18R01S	007S022E18R001S	33.559667	-114.713701	251.5	17.81					2000-06	13	238.20	237.971
07S/22E-18R01S	007S022E18R001S	33.559667	-114.713701	251.5	17.81					2000-07	13	238.05	237.971
07S/22E-18R01S	007S022E18R001S	33.559667	-114.713701	251.5	17.81					2000-08	13	238.71	237.971
07S/22E-18R01S	007S022E18R001S	33.559667	-114.713701	251.5	17.81					2000-09	13	238.32	237.971
07S/22E-18R01S	007S022E18R001S	33.559667	-114.713701	251.5	17.81					2006-02	15	236.98	237.971
07S/22E-18R01S	007S022E18R001S	33.559667	-114.713701	251.5	17.81					2006-03	15	236.98	237.971
07S/22E-18R01S	007S022E18R001S	33.559667	-114.713701	251.5	17.81					2006-04	15	236.93	237.971
07S/22E-18R01S	007S022E18R001S	33.559667	-114.713701	251.5	17.81					2006-05	14	237.28	237.971
07S/22E-18R01S	007S022E19A001S	33.545304	-114.713848	248						7/1/1971	7	241.00	237.971
07S/22E-18R01S	007S022E19K001S	33.548759	-114.718146	247.7	14.35					5/9/2000	9	238.50	237.971
07S/22E-19A01S	007S022E19K001S	33.548759	-114.718146	247.7	14.35					5/9/2000	8	238.61	238.610
07S/22E-19K01S	007S022E19K001S	33.548759	-114.718146	247.7	14.35					2000-01	10	238.18	238.124
07S/22E-19K01S	007S022E19K001S	33.548759	-114.718146	247.7	14.35					2000-01	8	238.67	238.124
07S/22E-19K01S	007S022E19K001S	33.548759	-114.718146	247.7	14.35					2000-03	10	237.70	238.124

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
07S/22E-19K01S	007S022E19K001S	33.548759	-114.718146	247.7	14.35					2000-03	9	238.04	238.124
07S/22E-19K01S	007S022E19K001S	33.548759	-114.718146	247.7	14.35					2000-04	10	237.70	238.124
07S/22E-19K01S	007S022E19K001S	33.548759	-114.718146	247.7	14.35					2000-04	9	237.98	238.124
07S/22E-19K01S	007S022E19K001S	33.548759	-114.718146	247.7	14.35					2000-05	9	238.26	238.124
07S/22E-19K01S	007S022E19K001S	33.548759	-114.718146	247.7	14.35					2000-05	8	238.51	238.124
07S/22E-19K01S	007S022E19K001S	33.548759	-114.718146	247.7	14.35					2000-06	9	238.70	238.124
07S/22E-19K01S	007S022E19K001S	33.548759	-114.718146	247.7	14.35					2000-06	8	238.88	238.124
07S/22E-19K01S	007S022E19K001S	33.548759	-114.718146	247.7	14.35					2000-07	9	238.97	238.124
07S/22E-19K01S	007S022E19K001S	33.548759	-114.718146	247.7	14.35					2000-07	7	239.44	238.124
07S/22E-19K01S	007S022E19K001S	33.548759	-114.718146	247.7	14.35					2000-08	9	238.88	238.124
07S/22E-19K01S	007S022E19K001S	33.548759	-114.718146	247.7	14.35					2000-08	7	239.34	238.124
07S/22E-19K01S	007S022E19K001S	33.548759	-114.718146	247.7	14.35					2000-09	10	238.14	238.124
07S/22E-19K01S	007S022E19K001S	33.548759	-114.718146	247.7	14.35					2000-09	8	238.69	238.124
07S/22E-19K01S	007S022E19K001S	33.548759	-114.718146	247.7	14.35					2000-10	7	240.07	238.124
07S/22E-19K01S	007S022E19K001S	33.548759	-114.718146	247.7	14.35					2006-01	11	237.05	238.124
07S/22E-19K01S	007S022E19K001S	33.548759	-114.718146	247.7	14.35					2006-01	9	237.76	238.124
07S/22E-19K01S	007S022E19K001S	33.548759	-114.718146	247.7	14.35					2006-02	11	236.56	238.124
07S/22E-19K01S	007S022E19K001S	33.548759	-114.718146	247.7	14.35					2006-02	10	237.14	238.124
07S/22E-19K01S	007S022E19K001S	33.548759	-114.718146	247.7	14.35					2006-04	11	236.69	238.124
07S/22E-19K01S	007S022E19K001S	33.548759	-114.718146	247.7	14.35					2006-04	10	237.17	238.124
07S/22E-19K01S	007S022E19K001S	33.548759	-114.718146	247.7	14.35					2006-05	11	236.87	238.124
07S/22E-19K01S	007S022E19K001S	33.548759	-114.718146	247.7	14.35					2006-05	9	237.51	238.124
07S/22E-19K01S	007S022E19N001S	33.545790	-114.724074	253.5	22.58					5/18/2006	15	238.18	238.124
07S/22E-19K01S	007S022E19N001S	33.545790	-114.724074	253.5	22.58					5/19/2006	15	238.20	238.124
07S/22E-19K01S	007S022E19N001S	33.545790	-114.724074	253.5	22.58					2006-01	15	238.20	238.124
07S/22E-19N01S	007S022E19N001S	33.545790	-114.724074	253.5	22.58					2006-02	16	237.78	237.951
07S/22E-19N01S	007S022E19N001S	33.545790	-114.724074	253.5	22.58					2006-04	16	237.81	237.951
07S/22E-19N01S	007S022E19N001S	33.545790	-114.724074	253.5	22.58					2006-05	15	238.04	237.951
07S/22E-19N01S	007S022E19Q001S	33.545648	-114.718137	248.9	11.45					4/26/2000	11	238.13	237.951
07S/22E-19N01S	007S022E19Q001S	33.545648	-114.718137	248.9	11.45					4/26/2000	11	238.12	237.951
07S/22E-19N01S	007S022E19Q001S	33.545648	-114.718137	248.9	11.45					2000-01	11	238.15	237.951

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
07S/22E-19N01S	007S022E19Q001S	33.545648	-114.718137	248.9	11.45					2000-03	11	237.88	237.951
07S/22E-19N01S	007S022E19Q001S	33.545648	-114.718137	248.9	11.45					2000-04	11	237.70	237.951
07S/22E-19Q01S	007S022E19Q001S	33.545648	-114.718137	248.9	11.45					2000-06	10	238.56	239.067
07S/22E-19Q01S	007S022E19Q001S	33.545648	-114.718137	248.9	11.45					2000-07	10	239.00	239.067
07S/22E-19Q01S	007S022E19Q001S	33.545648	-114.718137	248.9	11.45					2000-08	10	238.62	239.067
07S/22E-19Q01S	007S022E19Q001S	33.545648	-114.718137	248.9	11.45					2000-09	11	238.06	239.067
07S/22E-19Q01S	007S022E19Q001S	33.545648	-114.718137	248.9	11.45					2006-01	12	236.98	239.067
07S/22E-19Q01S	007S022E19Q001S	33.545648	-114.718137	248.9	11.45					2006-02	12	236.60	239.067
07S/22E-19Q01S	007S022E19Q001S	33.545648	-114.718137	248.9	11.45					2006-03	12	236.48	239.067
07S/22E-19Q01S	007S022E19Q001S	33.545648	-114.718137	248.9	11.45					2006-04	12	236.71	239.067
07S/22E-19Q01S	007S022E19Q001S	33.545648	-114.718137	248.9	11.45					2006-05	12	236.93	239.067
07S/22E-19Q01S	007S022E19R001S	33.559470	-114.713571	250						8/1/1971	9	241.00	239.067
07S/22E-19Q01S	007S022E20Q001S	33.545026	-114.700514	249						8/1/1971	9	240.00	239.067
07S/22E-19Q01S	007S022E21B001S	33.559192	-114.678847	252						8/1/1971	8	244.00	239.067
07S/22E-19Q01S	007S022E21D001S	33.558915	-114.691348	250						7/1/1971	9	241.00	239.067
07S/22E-19Q01S	007S022E21J001S	33.551415	-114.677181	253						8/1/1971	10	243.00	239.067
07S/22E-19R01S	007S022E21P003S	33.547804	-114.682736	253						9/1/1971	11	242.00	242.000
07S/22E-20Q01S	007S022E21P004S	33.545026	-114.686347	248						8/1/1971	5	243.00	243.000
07S/22E-21B01S	007S022E21R001S	33.548082	-114.678292	251						8/1/1971	10	241.00	241.000
07S/22E-21D01S	007S022E22M001S	33.551970	-114.674125	250						8/1/1971	9	241.00	241.000
07S/22E-21J01S	007S022E22N001S	33.545026	-114.674125	251						8/1/1971	11	240.00	240.000
07S/22E-21P03S	007S022E22P001S	33.548359	-114.670236	249						8/1/1971	9	240.00	240.000
07S/22E-21P04S	007S022E23D005S	33.557415	-114.657097	253	19.29					4/22/2003	11	241.95	241.950
07S/22E-21R01S	007S022E24D001S	33.559192	-114.639124	252						7/1/1971	6	246.00	246.000
07S/22E-22M01S	007S022E25A001S	33.544193	-114.621901	252						9/1/1971	7	245.00	245.000
07S/22E-22N01S	007S022E27B001S	33.544748	-114.656902	251						8/1/1971	15	236.00	236.000
07S/22E-22P01S	007S022E27C001S	33.544748	-114.669680	250						8/1/1971	12	238.00	238.000
07S/22E-23D05S	007S022E27L001S	33.537526	-114.669680	246						8/1/1971	12	234.00	234.000
07S/22E-24D01S	007S022E27L002S	33.537526	-114.668013	245						8/1/1971	11	234.00	234.000
07S/22E-25A01S	007S022E28D001S	33.544471	-114.691070	248						8/1/1971	6	242.00	242.000
07S/22E-27B01S	007S022E29H001S	33.540026	-114.693848	249						8/1/1971	11	238.00	238.000

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
07S/22E-27C01S	007S022E29R001S	33.530582	-114.695514	246						8/1/1971	6	240.00	240.000
07S/22E-27L01S	007S022E30B001S	33.541415	-114.717737	249						8/1/1971	10	239.00	239.000
07S/22E-27L02S	007S022E30G001S	33.538082	-114.717737	248						8/1/1971	7	241.00	241.000
07S/22E-28D01S	007S022E30P001S	33.530582	-114.718848	245						8/1/1971	8	237.00	237.000
07S/22E-29H01S	007S022E31Q001S	33.515860	-114.717459	244						8/1/1971	8	236.00	236.000
07S/22E-29R01S	007S022E33D001S	33.530026	-114.691903	248						8/1/1971	7	241.00	241.000
07S/22E-30B01S	007S022E33N001S	33.516138	-114.691069	246						8/1/1971	10	236.00	236.000
07S/22E-30G01S	007S022E34C001S	33.530026	-114.669680	243						8/1/1971	12	231.00	231.000
07S/22E-30P01S	007S022E34H002S	33.525304	-114.657457	245	101					8/1/1972	10	235.00	235.000
07S/22E-31Q01S	007S022E34H003S	33.524888	-114.661985	243	1000					2/3/2000	13	230.00	230.000
07S/22E-33D01S	007S022E34P001S	33.515582	-114.669124	244						8/1/1971	16	228.00	228.000
07S/22E-33N01S	007S022E35D001S	33.530304	-114.656069	245						8/1/1971	11	234.00	234.000
07S/22E-34C01S	007S022E35D003S	33.529721	-114.653402	247	23.04					6/7/2002	13	234.44	234.440
07S/22E-34H02S	007S022E35E010S	33.523527	-114.653680	246	21.41					6/4/2002	14	232.09	232.090
07S/22E-34H03S	007S022E35F001S	33.524027	-114.653180	247	700					2/3/2000	13	234.00	234.000
07S/22E-34P01S	007S022E35J001S	33.522527	-114.643290	247						8/1/1971	12	235.00	235.000
07S/22E-35D01S	007S022E35M003S	33.522054	-114.657485	246	23.7					6/6/2002	12	233.72	233.720
07S/22E-35D03S	007S022E36A001S	33.530304	-114.621623	253						9/1/1971	12	241.00	239.500
07S/22E-35D03S	007S022E36D002S	33.530026	-114.635235	249						8/1/1971	11	238.00	239.500
07S/22E-35E10S	007S022E36F001S	33.522804	-114.630790	250						8/1/1971	11	239.00	239.000
07S/22E-35F01S	007S022E36F002S	33.525221	-114.630262	249						4/17/2003	14	235.06	235.060
07S/22E-35J01S	007S023E01D001S	33.602219	-114.534871	272.2	32.9					9/19/1996	21	251.20	251.200
07S/22E-35M03S	007S023E01D004S	33.602580	-114.536094	274	33.2					9/19/1996	20	254.21	253.495
07S/22E-35M03S	007S023E01D005S	33.602580	-114.536094	272.5	87.2					9/19/1996	20	252.78	253.495
07S/22E-36A01S	007S023E01D006S	33.602580	-114.536094	272.3	136.2					9/19/1996	19	252.84	252.840
07S/22E-36D02S	007S023E01D007S	33.600691	-114.535649	270	60					3/21/2002	21	248.91	248.910
07S/22E-36F01S	007S023E02H001S	33.599358	-114.537371	275	53					5/24/1993	16	259.00	259.000
07S/22E-36F02S	007S023E02H001S	33.599358	-114.537371	275	53					9/13/2000	21	253.82	253.800
07S/22E-36F02S	007S023E02H001S	33.599358	-114.537371	275	53					9/13/2000	21	253.78	253.800
07S/23E-01D01S	007S023E02H001S	33.599358	-114.537371	275	53					9/13/2000	21	253.74	253.740
07S/23E-01D04S	007S023E03C001S	33.600858	-114.564122	265	24					4/12/1990	7	258.00	258.000

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
07S/23E-01D05S	007S023E03D001S	33.603080	-114.570511	260	24					4/12/1990	4	256.00	256.000
07S/23E-01D06S	007S023E03D002S	33.600303	-114.567178	265	24					4/12/1990	7	258.00	258.000
07S/23E-01D07S	007S023E03N001S	33.589192	-114.570233	262						7/1/1971	8	254.00	255.000
07S/23E-01D07S	007S023E03R001S	33.589192	-114.555233	267						7/1/1971	11	256.00	255.000
07S/23E-02H01S	007S023E04D001S	33.602414	-114.583678	268	500					5/9/1973	13	255.00	255.458
07S/23E-02H01S	007S023E04D001S	33.602414	-114.583678	268	500					7/26/1979	12	256.50	255.458
07S/23E-02H01S	007S023E04D001S	33.602414	-114.583678	268	500					7/23/1980	12	255.76	255.458
07S/23E-02H01S	007S023E04D001S	33.602414	-114.583678	268	500					1/22/1981	13	254.57	255.458
07S/23E-03C01S	007S023E04D001S	33.602414	-114.583678	268	500					8/27/1981	11	256.66	256.660
07S/23E-03D01S	007S023E04D001S	33.602414	-114.583678	268	500					2/3/1982	13	255.01	255.010
07S/23E-03D02S	007S023E04D001S	33.602414	-114.583678	268	500					12/10/1982	13	255.48	255.480
07S/23E-03N01S	007S023E04D001S	33.602414	-114.583678	268	500					9/20/1983	13	255.46	255.460
07S/23E-03R01S	007S023E04D001S	33.602414	-114.583678	268	500					9/18/1984	12	256.21	256.210
07S/23E-04D01S	007S023E04D001S	33.602414	-114.583678	268	500					2/27/1985	12	255.61	255.522
07S/23E-04D01S	007S023E04D001S	33.602414	-114.583678	268	500					6/12/1985	12	255.84	255.522
07S/23E-04D01S	007S023E05C001S	33.600719	-114.599123	265	340					11/9/1978	12	253.00	255.522
07S/23E-04D01S	007S023E05D001S	33.600025	-114.601901	265	200					3/16/1955	8	257.00	255.522
07S/23E-04D01S	007S023E05D001S	33.600025	-114.601901	265	200					7/1/1972	8	257.00	255.522
07S/23E-04D01S	007S023E05D001S	33.600025	-114.601901	265	200					7/25/1972	8	257.20	255.522
07S/23E-04D01S	007S023E05D002S	33.600025	-114.601901	265	142					2/7/1962	8	257.00	255.522
07S/23E-04D01S	007S023E05E001S	33.595025	-114.602179	265						2/15/1962	14	251.00	255.522
07S/23E-04D01S	007S023E05F001S	33.598636	-114.599679	267	109					6/13/1951	7	260.00	255.522
07S/23E-04D01S	007S023E05M003S	33.595247	-114.602096	265						10/19/2000	12	253.09	255.522
07S/23E-04D01S	007S023E05N002S	33.589942	-114.602373	265	60					5/28/1993	11	254.00	255.522
07S/23E-05C01S	007S023E05N002S	33.589942	-114.602373	265	60					9/12/2000	10	254.92	254.920
07S/23E-05D01S	007S023E05R001S	33.588914	-114.588012	262	11.9					7/16/1971	9	252.55	253.030
07S/23E-05D01S	007S023E06A001S	33.602802	-114.605790	262						7/1/1971	8	254.00	253.030
07S/23E-05D01S	007S023E06N001S	33.588358	-114.622457	259.36	8.3					7/16/1971	7	252.54	253.030
07S/23E-05D02S	007S023E06Q005S	33.588719	-114.612540	263	10.47					5/26/2004	4	258.94	258.930
07S/23E-05D02S	007S023E06Q005S	33.588719	-114.612540	263	10.47					5/26/2004	4	258.92	258.930
07S/23E-05E01S	007S023E06R001S	33.588636	-114.605512	258						7/1/1971	8	250.00	251.000

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
07S/23E-05E01S	007S023E08C001S	33.586553	-114.596540	262	194					4/7/1977	10	252.00	251.000
07S/23E-05F01S	007S023E08E001S	33.584414	-114.602540	265	140					3/26/1993	11	254.00	254.000
07S/23E-05M03S	007S023E08R001S	33.574470	-114.587456	257.62	9					7/9/1971	9	248.97	249.485
07S/23E-05M03S	007S023E08R003S	33.576164	-114.589262	260	53					10/15/1992	10	250.00	249.485
07S/23E-05N02S	007S023E09D001S	33.588386	-114.585928	260	10.31					5/25/2004	8	251.76	251.750
07S/23E-05N02S	007S023E09D001S	33.588386	-114.585928	260	10.31					5/25/2004	8	251.75	251.750
07S/23E-05N02S	007S023E09D001S	33.588386	-114.585928	260	10.31					5/25/2004	8	251.74	251.750
07S/23E-05R01S	007S023E11K002S	33.580359	-114.542871	260	32.2					6/11/2002	12	248.39	248.390
07S/23E-06A01S	007S023E11K003S	33.580053	-114.543927	259	36.15					6/11/2002	13	245.75	245.750
07S/23E-06N01S	007S023E11P001S	33.577109	-114.544399	260	33.7					5/14/2002	11	248.57	248.570
07S/23E-06Q05S	007S023E11P002S	33.575081	-114.546927	265	43.72					5/14/2002	15	250.33	249.948
07S/23E-06Q05S	007S023E14B003S	33.572525	-114.543621	260	28.61					4/17/2002	11	248.98	249.948
07S/23E-06Q05S	007S023E14C004S	33.571359	-114.544232	265	85					4/17/2002	16	248.92	249.948
07S/23E-06Q05S	007S023E14C007S	33.572387	-114.544844	264	21.85					4/17/2002	12	251.56	249.948
07S/23E-06R01S	007S023E14C008S	33.572387	-114.544844	264						4/17/2002	12	252.28	252.280
07S/23E-08C01S	007S023E14C011S	33.572553	-114.544871	263	35.65					4/17/2002	12	251.28	251.280
07S/23E-08E01S	007S023E14C012S	33.572553	-114.544871	263	25.63					4/17/2002	12	251.38	251.380
07S/23E-08R01S	007S023E14C014S	33.574053	-114.544316	261	23.97					4/18/2002	12	248.58	248.580
07S/23E-08R03S	007S023E14C016S	33.572998	-114.544871	263	35.05					4/18/2002	12	251.04	251.040
07S/23E-09D01S	007S023E14C019S	33.573331	-114.545038	263	24.54					4/18/2002	12	250.63	250.913
07S/23E-09D01S	007S023E14C019S	33.573331	-114.545038	263	24.54					4/18/2002	12	250.62	250.913
07S/23E-09D01S	007S023E14C021S	33.573387	-114.545455	263	25.75					4/18/2002	12	251.14	250.913
07S/23E-09D01S	007S023E14C022S	33.573387	-114.545455	263	35.1					4/18/2002	12	251.26	250.913
07S/23E-11K02S	007S023E14C028S	33.573748	-114.546371	265	24.7					5/14/2002	14	251.45	249.680
07S/23E-11K02S	007S023E14F003S	33.570109	-114.544149	264	43.1					4/16/2002	16	247.91	249.680
07S/23E-11K03S	007S023E14F005S	33.570331	-114.544121	265	35.17					4/16/2002	16	249.43	249.870
07S/23E-11K03S	007S023E14F008S	33.570553	-114.544094	266	34.17					4/16/2002	16	250.31	249.870
07S/23E-11P01S	007S023E14F010S	33.570776	-114.544038	266	35.3					4/6/2002	24	241.84	244.775
07S/23E-11P01S	007S023E14F011S	33.570942	-114.544121	266	24.15					4/16/2002	18	247.71	244.775
07S/23E-11P02S	007S023E14F012S	33.570942	-114.544121	266	38.15					4/16/2002	16	249.95	250.525
07S/23E-11P02S	007S023E14G008S	33.571220	-114.542871	261	22.68					5/13/2002	10	251.10	250.525

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
07S/23E-14B03S	007S023E14G010S	33.571220	-114.542871	261	24.49					5/13/2002	10	251.48	251.940
07S/23E-14B03S	007S023E15A001S	33.574470	-114.555788	264.75	13.3					7/9/1971	12	252.40	251.940
07S/23E-14C04S	007S023E15N001S	33.560026	-114.569400	258.24	11.6					7/20/1971	11	247.42	248.615
07S/23E-14C04S	007S023E16A001S	33.574192	-114.573011	258.93	11					7/9/1971	9	249.81	248.615
07S/23E-14C07S	007S023E16C001S	33.573553	-114.579234	260	120					9/12/1973	5	255.00	251.500
07S/23E-14C07S	007S023E17D001S	33.571637	-114.604429	255	176					8/20/1951	7	248.00	251.500
07S/23E-14C08S	007S023E17D002S	33.573914	-114.604679	256						7/1/1971	8	248.00	248.000
07S/23E-14C08S	007S023E17N001S	33.559748	-114.604123	255						7/1/1971	7	248.00	248.000
07S/23E-14C11S	007S023E17R001S	33.560026	-114.587178	256						7/1/1971	9	247.00	248.500
07S/23E-14C11S	007S023E18E001S	33.567803	-114.621901	254						7/1/1971	4	250.00	248.500
07S/23E-14C12S	007S023E18F001S	33.566970	-114.617179	256						7/1/1971	7	249.00	249.000
07S/23E-14C14S	007S023E18M001S	33.566137	-114.621901	260						7/1/1971	10	250.00	249.000
07S/23E-14C14S	007S023E18N001S	33.560859	-114.621901	253						9/1/1971	5	248.00	249.000
07S/23E-14C16S	007S023E21H001S	33.551970	-114.570511	260	400					2/15/1962	12	248.00	247.240
07S/23E-14C16S	007S023E21N001S	33.545582	-114.582456	259.8	16.3					9/1/1971	13	246.48	247.240
07S/23E-14C19S	007S023E22N001S	33.545582	-114.569122	260						9/1/1971	7	253.00	252.000
07S/23E-14C19S	007S023E27A001S	33.545582	-114.552177	264						9/1/1971	13	251.00	252.000
07S/23E-14C21S	007S023E27N001S	33.531138	-114.568844	257						9/1/1971	7	250.00	247.500
07S/23E-14C21S	007S023E29D001S	33.544748	-114.603567	255	353					5/25/1961	10	245.00	247.500
07S/23E-14C22S	007S023E29N001S	33.530582	-114.603289	255.42	16.8					9/1/1971	15	240.72	242.860
07S/23E-14C22S	007S023E30A001S	33.544748	-114.604123	255						9/1/1971	10	245.00	242.860
07S/23E-14C28S	007S023E30M001S	33.536193	-114.620734	252						4/16/2003	15	237.08	237.540
07S/23E-14C28S	007S023E31N001S	33.515582	-114.616623	253						9/1/1971	15	238.00	237.540
07S/23E-14F03S	007S023E33D001S	33.530582	-114.582178	259						9/1/1971	11	248.00	243.510
07S/23E-14F03S	007S023E34P001S	33.516332	-114.564399	256	438					9/27/1990	17	239.02	243.510
07S/23E-14F05S	007S023E34P001S	33.516332	-114.564399	256	438					3/30/2000	17	239.00	235.000
07S/23E-14F05S	008S021E01Q001S	33.507805	-114.734682	244						8/1/1971	13	231.00	235.000
07S/23E-14F08S	008S021E01Q002S	33.508099	-114.735251	244.3	16.73					5/18/2006	13	231.67	231.760
07S/23E-14F08S	008S021E01Q002S	33.508099	-114.735251	244.3	16.73					5/19/2006	12	231.85	231.760
07S/23E-14F10S	008S021E01Q002S	33.508099	-114.735251	244.3	16.73					2006-01	13	231.63	231.385
07S/23E-14F10S	008S021E01Q002S	33.508099	-114.735251	244.3	16.73					2006-02	13	231.14	231.385

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
07S/23E-14F11S	008S021E01Q002S	33.508099	-114.735251	244.3	16.73					2006-03	13	231.09	231.125
07S/23E-14F11S	008S021E01Q002S	33.508099	-114.735251	244.3	16.73					2006-04	13	231.16	231.125
07S/23E-14F12S	008S021E01Q002S	33.508099	-114.735251	244.3	16.73					2006-05	13	231.53	230.715
07S/23E-14F12S	008S021E12E001S	33.500027	-114.736071	241.44	15					11/25/1980	12	229.90	230.715
07S/23E-14G08S	008S021E12E001S	33.500027	-114.736071	241.44	15					12/19/1980	11	230.45	230.445
07S/23E-14G08S	008S021E12E001S	33.500027	-114.736071	241.44	15					1/5/1981	11	230.44	230.445
07S/23E-14G10S	008S021E12E001S	33.500027	-114.736071	241.44	15					1/12/1981	11	230.35	230.045
07S/23E-14G10S	008S021E12E001S	33.500027	-114.736071	241.44	15					2/2/1981	12	229.74	230.045
07S/23E-15A01S	008S021E12E001S	33.500027	-114.736071	241.44	15					2/4/1981	12	229.92	229.920
07S/23E-15N01S	008S021E12E001S	33.500027	-114.736071	241.44	15					2/11/1981	12	229.59	229.590
07S/23E-16A01S	008S021E12E001S	33.500027	-114.736071	241.44	15					2/13/1981	12	229.64	229.640
07S/23E-16C01S	008S021E12E001S	33.500027	-114.736071	241.44	15					2/18/1981	11	230.24	230.240
07S/23E-17D01S	008S021E12E001S	33.500027	-114.736071	241.44	15					2/25/1981	10	231.12	231.120
07S/23E-17D02S	008S021E12E001S	33.500027	-114.736071	241.44	15					3/31/1981	10	231.41	231.410
07S/23E-17N01S	008S021E12E001S	33.500027	-114.736071	241.44	15					5/21/1981	10	231.16	231.160
07S/23E-17R01S	008S021E12E002S	33.500027	-114.736071	241.69	25					11/25/1980	12	229.92	229.920
07S/23E-18E01S	008S021E12E002S	33.500027	-114.736071	241.69	25					12/19/1980	11	230.45	230.450
07S/23E-18F01S	008S021E12E002S	33.500027	-114.736071	241.69	25					1/5/1981	12	229.69	229.690
07S/23E-18M01S	008S021E12E002S	33.500027	-114.736071	241.69	25					1/12/1981	11	230.35	230.350
07S/23E-18N01S	008S021E12E002S	33.500027	-114.736071	241.69	25					2/2/1981	11	230.44	230.440
07S/23E-21H01S	008S021E12E002S	33.500027	-114.736071	241.69	25					2/4/1981	12	229.91	229.910
07S/23E-21N01S	008S021E12E002S	33.500027	-114.736071	241.69	25					2/11/1981	12	229.54	229.540
07S/23E-22N01S	008S021E12E002S	33.500027	-114.736071	241.69	25					2/13/1981	12	229.54	229.540
07S/23E-27A01S	008S021E12E002S	33.500027	-114.736071	241.69	25					2/18/1981	12	230.19	230.190
07S/23E-27N01S	008S021E12E002S	33.500027	-114.736071	241.69	25					2/25/1981	11	231.07	231.070
07S/23E-29D01S	008S021E12E002S	33.500027	-114.736071	241.69	25					3/31/1981	10	231.35	231.350
07S/23E-29N01S	008S021E12E002S	33.500027	-114.736071	241.69	25					5/21/1981	11	230.72	230.720
07S/23E-30A01S	008S021E12E003S	33.500027	-114.736071	241.92	40					11/25/1980	12	230.19	230.190
07S/23E-30M01S	008S021E12E003S	33.500027	-114.736071	241.92	40					12/19/1980	11	230.44	230.430
07S/23E-30M01S	008S021E12E003S	33.500027	-114.736071	241.92	40					1/5/1981	12	230.42	230.430
07S/23E-31N01S	008S021E12E003S	33.500027	-114.736071	241.92	40					1/12/1981	12	230.35	230.350

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
07S/23E-33D01S	008S021E12E003S	33.500027	-114.736071	241.92	40					2/2/1981	12	229.72	229.720
07S/23E-34P01S	008S021E12E003S	33.500027	-114.736071	241.92	40					2/4/1981	12	229.89	229.660
07S/23E-34P01S	008S021E12E003S	33.500027	-114.736071	241.92	40					2/11/1981	12	229.52	229.660
07S/23E-34P01S	008S021E12E003S	33.500027	-114.736071	241.92	40					2/13/1981	12	229.57	229.660
08S/21E-01Q01S	008S021E12E003S	33.500027	-114.736071	241.92	40					2/18/1981	12	230.22	230.220
08S/21E-01Q02S	008S021E12E003S	33.500027	-114.736071	241.92	40					2/25/1981	11	231.07	230.421
08S/21E-01Q02S	008S021E12E003S	33.500027	-114.736071	241.92	40					3/31/1981	11	231.34	230.421
08S/21E-01Q02S	008S021E12E003S	33.500027	-114.736071	241.92	40					5/21/1981	11	230.71	230.421
08S/21E-01Q02S	008S021E12E004S	33.500027	-114.736071	241.41	100					11/25/1980	12	229.87	230.421
08S/21E-01Q02S	008S021E12E004S	33.500027	-114.736071	241.41	100					12/19/1980	11	230.59	230.421
08S/21E-01Q02S	008S021E12E004S	33.500027	-114.736071	241.41	100					1/5/1981	11	230.46	230.421
08S/21E-01Q02S	008S021E12E004S	33.500027	-114.736071	241.41	100					1/12/1981	11	230.19	230.421
08S/21E-01Q02S	008S021E12E004S	33.500027	-114.736071	241.41	100					2/2/1981	12	229.66	230.421
08S/21E-01Q02S	008S021E12E004S	33.500027	-114.736071	241.41	100					2/4/1981	12	229.90	230.421
08S/21E-12E01S	008S021E12E004S	33.500027	-114.736071	241.41	100					2/11/1981	12	229.71	232.248
08S/21E-12E01S	008S021E12E004S	33.500027	-114.736071	241.41	100					2/13/1981	12	229.71	232.248
08S/21E-12E01S	008S021E12E004S	33.500027	-114.736071	241.41	100					2/18/1981	12	229.91	232.248
08S/21E-12E01S	008S021E12E004S	33.500027	-114.736071	241.41	100					2/25/1981	11	230.59	232.248
08S/21E-12E01S	008S021E12E004S	33.500027	-114.736071	241.41	100					3/31/1981	11	230.67	232.248
08S/21E-12E01S	008S021E12E004S	33.500027	-114.736071	241.41	100					5/21/1981	11	230.62	232.248
08S/21E-12E01S	008S022E04E001S	33.515305	-114.691069	246						9/1/1971	8	238.00	232.248
08S/21E-12E01S	008S022E04M001S	33.513638	-114.691069	244						9/1/1971	10	234.00	232.248
08S/21E-12E01S	008S022E04N001S	33.510583	-114.691069	242						9/1/1971	10	232.00	232.248
08S/21E-12E01S	008S022E04N002S	33.508360	-114.691069	242	13.6					10/5/1923	8	234.29	232.248
08S/21E-12E01S	008S022E04N002S	33.508360	-114.691069	242	13.6					11/20/1923	8	234.19	232.248
08S/21E-12E01S	008S022E04N002S	33.508360	-114.691069	242	13.6					1/29/1924	9	233.29	232.248
08S/21E-12E02S	008S022E04N002S	33.508360	-114.691069	242	13.6					9/5/1924	8	233.79	233.995
08S/21E-12E02S	008S022E04N002S	33.508360	-114.691069	242	13.6					3/3/1925	8	233.69	233.995
08S/21E-12E02S	008S022E04N002S	33.508360	-114.691069	242	13.6					10/23/1925	9	233.39	233.995
08S/21E-12E02S	008S022E04N002S	33.508360	-114.691069	242	13.6					1/13/1926	9	233.29	233.995
08S/21E-12E02S	008S022E04N002S	33.508360	-114.691069	242	13.6					2/28/1926	9	233.09	233.995

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
08S/21E-12E02S	008S022E04N002S	33.508360	-114.691069	242	13.6					11/20/1936	9	232.96	233.995
08S/21E-12E02S	008S022E04N002S	33.508360	-114.691069	242	13.6					1/4/1937	9	233.16	233.995
08S/21E-12E02S	008S022E04N002S	33.508360	-114.691069	242	13.6					9/12/1937	8	233.91	233.995
08S/21E-12E02S	008S022E04N002S	33.508360	-114.691069	242	13.6					1/12/1948	7	234.97	233.995
08S/21E-12E02S	008S022E04N002S	33.508360	-114.691069	242	13.6					9/8/1948	6	235.62	233.995
08S/21E-12E02S	008S022E04N002S	33.508360	-114.691069	242	13.6					1/5/1949	8	234.42	233.995
08S/21E-12E02S	008S022E04N002S	33.508360	-114.691069	242	13.6					9/9/1949	6	235.65	233.995
08S/21E-12E03S	008S022E04N002S	33.508360	-114.691069	242	13.6					1/5/1950	7	235.41	235.833
08S/21E-12E03S	008S022E04N002S	33.508360	-114.691069	242	13.6					9/13/1950	6	236.28	235.833
08S/21E-12E03S	008S022E04N002S	33.508360	-114.691069	242	13.6					1/24/1951	7	235.13	235.833
08S/21E-12E03S	008S022E04N002S	33.508360	-114.691069	242	13.6					9/12/1951	6	235.78	235.833
08S/21E-12E03S	008S022E04N002S	33.508360	-114.691069	242	13.6					1/31/1952	8	234.35	235.833
08S/21E-12E03S	008S022E04N002S	33.508360	-114.691069	242	13.6					10/2/1952	6	236.45	235.833
08S/21E-12E03S	008S022E04N002S	33.508360	-114.691069	242	13.6					1/7/1953	7	234.75	235.833
08S/21E-12E03S	008S022E04N002S	33.508360	-114.691069	242	13.6					9/28/1953	5	237.35	235.833
08S/21E-12E03S	008S022E04N002S	33.508360	-114.691069	242	13.6					1/15/1954	7	234.75	235.833
08S/21E-12E03S	008S022E04N002S	33.508360	-114.691069	242	13.6					10/1/1954	5	237.35	235.833
08S/21E-12E03S	008S022E04N002S	33.508360	-114.691069	242	13.6					1/2/1955	6	235.65	235.833
08S/21E-12E03S	008S022E04N002S	33.508360	-114.691069	242	13.6					9/29/1955	5	236.75	235.833
08S/21E-12E04S	008S022E04N002S	33.508360	-114.691069	242	13.6					1/28/1956	5	236.85	236.327
08S/21E-12E04S	008S022E04N002S	33.508360	-114.691069	242	13.6					10/2/1956	5	237.05	236.327
08S/21E-12E04S	008S022E04N002S	33.508360	-114.691069	242	13.6					1/9/1957	6	235.82	236.327
08S/21E-12E04S	008S022E04N002S	33.508360	-114.691069	242	13.6					9/10/1957	5	237.36	236.327
08S/21E-12E04S	008S022E04N002S	33.508360	-114.691069	242	13.6					1/14/1958	6	235.51	236.327
08S/21E-12E04S	008S022E04N002S	33.508360	-114.691069	242	13.6					9/18/1958	4	237.59	236.327
08S/21E-12E04S	008S022E04N002S	33.508360	-114.691069	242	13.6					1/8/1959	7	234.99	236.327
08S/21E-12E04S	008S022E04N002S	33.508360	-114.691069	242	13.6					9/10/1959	4	237.89	236.327
08S/21E-12E04S	008S022E04N002S	33.508360	-114.691069	242	13.6					1/6/1960	8	234.49	236.327
08S/21E-12E04S	008S022E04N002S	33.508360	-114.691069	242	13.6					9/15/1960	6	235.79	236.327
08S/21E-12E04S	008S022E04N002S	33.508360	-114.691069	242	13.6					1/4/1961	6	236.39	236.327
08S/21E-12E04S	008S022E04N002S	33.508360	-114.691069	242	13.6					9/9/1961	6	236.19	236.327

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FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
08S/22E-04E01S	008S022E04N002S	33.508360	-114.691069	242	13.6					1/18/1962	6	236.29	236.290
08S/22E-04M01S	008S022E04N002S	33.508360	-114.691069	242	13.6					9/20/1962	6	236.19	236.190
08S/22E-04N01S	008S022E04N002S	33.508360	-114.691069	242	13.6					1/19/1963	6	235.79	235.790
08S/22E-04N02S	008S022E04N002S	33.508360	-114.691069	242	13.6					9/20/1963	6	236.39	240.628
08S/22E-04N02S	008S022E04N002S	33.508360	-114.691069	242	13.6					1/10/1964	6	236.49	240.628
08S/22E-04N02S	008S022E04N002S	33.508360	-114.691069	242	13.6					9/10/1964	4	237.54	240.628
08S/22E-04N02S	008S022E04N002S	33.508360	-114.691069	242	13.6					1/11/1965	7	234.59	240.628
08S/22E-04N02S	008S022E04N002S	33.508360	-114.691069	242	13.6					9/11/1965	5	237.24	240.628
08S/22E-04N02S	008S022E04N002S	33.508360	-114.691069	242	13.6					1/13/1966	8	234.19	240.628
08S/22E-04N02S	008S022E04N002S	33.508360	-114.691069	242	13.6					9/16/1966	7	234.69	240.628
08S/22E-04N02S	008S022E04N002S	33.508360	-114.691069	242	13.6					1/14/1967	10	231.89	240.628
08S/22E-04N02S	008S022E04N002S	33.508360	-114.691069	242	13.6					9/19/1967	10	232.39	240.628
08S/22E-04N02S	008S022E04N002S	33.508360	-114.691069	242	13.6					9/17/1968	9	232.85	240.628
08S/22E-04N02S	008S022E04N002S	33.508360	-114.691069	242	13.6					1/21/1969	12	229.85	240.628
08S/22E-04N02S	008S022E04N002S	33.508360	-114.691069	242	13.6					9/20/1969	8	234.00	240.628
08S/22E-04N02S	008S022E04N002S	33.508360	-114.691069	242	13.6					1/21/1970	13	229.25	240.628
08S/22E-04N02S	008S022E04N002S	33.508360	-114.691069	242	13.6					1/19/1971	13	229.35	240.628
08S/22E-04N02S	008S022E04N002S	33.508360	-114.691069	242	13.6					8/31/1971	9	233.17	240.628
08S/22E-04N02S	008S022E04N002S	33.508360	-114.691069	242	13.6					4/24/1979	11	230.65	240.628
08S/22E-04N02S	008S022E04N002S	33.508360	-114.691069	242	13.6					7/23/1980	10	231.60	240.628
08S/22E-04N02S	008S022E04N002S	33.508360	-114.691069	242	13.6					1/22/1981	13	229.38	240.628
08S/22E-04N02S	008S022E04N002S	33.508360	-114.691069	242	13.6					8/27/1981	10	231.89	240.628
08S/22E-04N02S	008S022E04N002S	33.508360	-114.691069	242	13.6					2/3/1982	13	229.18	240.628
08S/22E-04N02S	008S022E04N002S	33.508360	-114.691069	242	13.6					12/10/1982	11	230.51	240.628
08S/22E-04N02S	008S022E04N002S	33.508360	-114.691069	242	13.6					9/20/1983	11	230.72	240.628
08S/22E-04N02S	008S022E04N002S	33.508360	-114.691069	242	13.6					9/18/1984	11	231.44	240.628
08S/22E-04N02S	008S022E04N002S	33.508360	-114.691069	242	13.6					2/28/1985	12	229.60	240.628
08S/22E-04N02S	008S022E04N002S	33.508360	-114.691069	242	13.6					6/13/1985	12	230.00	240.628
08S/22E-04N02S	008S022E04P001S	33.510583	-114.686903	244						9/1/1971	11	233.00	240.628
08S/22E-04N02S	008S022E05G001S	33.515582	-114.699681	245						8/1/1971	10	235.00	240.628
08S/22E-04N02S	008S022E06N001S	33.507805	-114.721904	243						8/1/1971	9	234.00	240.628

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
08S/22E-04N02S	008S022E08D002S	33.506694	-114.708292	244						8/1/1971	11	233.00	240.628
08S/22E-04N02S	008S022E10B001S	33.506972	-114.664680	242						8/1/1971	13	229.00	240.628
08S/22E-04N02S	008S022E10D001S	33.506972	-114.673569	242						8/1/1971	13	229.00	240.628
08S/22E-04N02S	008S022E11D001S	33.506972	-114.655791	242						8/1/1971	12	230.00	240.628
08S/22E-04N02S	008S022E12D001S	33.506694	-114.638568	247						8/1/1971	12	235.00	240.628
08S/22E-04N02S	008S023E03E001S	33.515305	-114.568566	257.71	16.5					9/1/1971	13	244.70	240.628
08S/22E-04N02S	008S023E04E001S	33.515305	-114.586066	256	9.7					9/3/1971	7	248.59	240.628
08S/22E-04N02S	008S023E05C001S	33.515194	-114.597344	255	21.9					5/6/2004	15	240.41	240.628
08S/22E-04N02S	008S023E05E001S	33.515305	-114.601067	256	13.5					9/3/1971	11	245.12	240.628
08S/22E-04N02S	008S023E06P001S	33.507249	-114.614456	253	390					2/8/1962	10	242.68	240.628
08S/22E-04N02S	008S023E06P001S	33.507249	-114.614456	253	390					8/1/1972	12	241.20	240.628
08S/22E-04N02S	008S023E07B001S	33.505860	-114.611900	254	390					2/13/1962	15	239.00	240.628
08S/22E-04N02S	008S023E07D001S	33.506694	-114.619401	251.37	16.9					8/31/1971	14	237.01	240.628
08S/22E-04N02S	008S023E08D001S	33.506972	-114.603011	256.75	18					8/31/1971	13	243.42	240.628
08S/22E-04N02S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	6/12/1968	146.15	253.49	240.628
08S/22E-04N02S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	7/1/1971	155	244.64	240.628
08S/22E-04N02S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	7/28/1971	154.93	244.71	240.628
08S/22E-04N02S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	3/29/1984	157.76	241.88	240.628
08S/22E-04N02S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	9/21/1990	154.01	245.63	240.628
08S/22E-04N02S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	2/14/1992	151.03	248.61	240.628
08S/22E-04N02S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	2/15/2000	147.6	252.04	240.628
08S/22E-04N02S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	12/14/2000	147.59	252.05	240.628
08S/22E-04N02S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	11/6/2001	147.57	252.07	240.628
08S/22E-04N02S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	4/16/2002	147.4	252.24	240.628
08S/22E-04N02S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	10/2/2002	147.97	251.67	240.628
08S/22E-04N02S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	6/3/2003	147.17	252.47	240.628
08S/22E-04N02S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	11/4/2003	147.22	252.42	240.628
08S/22E-04N02S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	3/2/2004	147.02	252.62	240.628
08S/22E-04N02S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	3/2/2004	147.03	252.61	240.628
08S/22E-04N02S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	8/4/2004	146.99	252.65	240.628
08S/22E-04N02S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	12/8/2004	147.2	252.44	240.628

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
08S/22E-04N02S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	4/15/2005	147.18	252.46	240.628
08S/22E-04N02S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	8/31/2005	147.26	252.38	240.628
08S/22E-04N02S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	1/27/2006	147.36	252.28	240.628
08S/22E-04N02S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	3/30/2006	146.64	253.00	240.628
08S/22E-04N02S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	5/5/2006	147.44	252.20	240.628
08S/22E-04N02S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	8/10/2006	147.41	252.23	240.628
08S/22E-04N02S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	8/10/2006	147.42	252.22	240.628
08S/22E-04N02S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	12/8/2006	147.53	252.11	240.628
08S/22E-04P01S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	2/7/2007	147.52	252.12	252.120
08S/22E-05G01S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	2/7/2007	147.53	252.11	252.110
08S/22E-06N01S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	5/17/2007	147.52	252.12	252.120
08S/22E-08D02S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	5/17/2007	147.53	252.11	252.110
08S/22E-10B01S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	9/5/2007	147.44	252.20	252.200
08S/22E-10D01S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	12/13/2007	147.5	252.14	252.140
08S/22E-11D01S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	3/18/2008	147.48	252.16	252.160
08S/22E-12D01S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	6/25/2008	147.43	252.21	252.210
08S/23E-03E01S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	6/25/2008	147.45	252.19	252.190
08S/23E-04E01S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	9/23/2008	147.39	252.25	252.250
08S/23E-05C01S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	9/23/2008	147.41	252.23	252.190
08S/23E-05C01S	006S022E09P001S	33.661090	-114.688300	399.64	252	230	169.64	250	149.64	1/13/2009	147.49	252.15	252.190
08S/23E-05E01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	1/1/1947	84	250.20	250.200
08S/23E-06P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	5/23/1961	82.7	251.50	251.765
08S/23E-06P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	8/24/1961	82.17	252.03	251.765
08S/23E-07B01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	9/21/1961	81.96	252.24	252.240
08S/23E-07D01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	10/18/1961	82.16	252.04	252.040
08S/23E-08D01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	11/21/1961	82.67	251.53	251.530
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	12/20/1961	83.04	251.16	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	1/22/1962	83.4	250.80	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	2/19/1962	83.35	250.85	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	3/26/1962	83.15	251.05	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	4/24/1962	82.85	251.35	251.239

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	5/24/1962	82.73	251.47	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	6/20/1962	82.56	251.64	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	7/19/1962	82.57	251.63	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	8/16/1962	82.62	251.58	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	9/17/1962	82.35	251.85	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	10/11/1962	82.52	251.68	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	11/8/1962	82.71	251.49	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	12/13/1962	83	251.20	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	1/10/1963	83.06	251.14	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	2/4/1963	83.29	250.91	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	3/4/1963	83.24	250.96	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	4/1/1963	82.94	251.26	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	5/6/1963	82.54	251.66	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	6/3/1963	82.15	252.05	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	7/11/1963	82	252.20	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	8/6/1963	81.85	252.35	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	9/9/1963	81.58	252.62	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	10/29/1963	81.46	252.74	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	11/27/1963	81.78	252.42	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	12/31/1963	82.47	251.73	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	2/7/1964	82.91	251.29	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	3/10/1964	82.66	251.54	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	4/15/1964	82.15	252.05	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	5/12/1964	81.97	252.23	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	6/18/1964	81.36	252.84	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	7/21/1964	81.3	252.90	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	8/19/1964	81.04	253.16	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	9/17/1964	80.93	253.27	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	10/21/1964	81.21	252.99	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	12/2/1964	81.29	252.91	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	7/15/1971	84.85	249.35	251.239

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	9/22/1990	89.32	244.88	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	2/15/1992	89.34	244.86	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	2/15/2000	87.51	246.69	251.239
06S/22E-09P01S	006S022E32R001S	33.604240	-114.692960	334.2	560	120	214.2	488	-153.8	3/31/2006	88.08	246.12	251.239
06S/22E-09P01S	006S022E35R002S	33.602940	-114.644260	260	328	302	-42	326	-66	11/18/1947	6	254.00	251.239
06S/22E-09P01S	006S022E35R002S	33.602940	-114.644260	260	328	302	-42	326	-66	2/8/1957	7.42	252.58	251.239
06S/22E-09P01S	006S022E35R002S	33.602940	-114.644260	260	328	302	-42	326	-66	5/25/1961	6.25	253.75	251.239
06S/22E-09P01S	006S022E35R002S	33.602940	-114.644260	260	328	302	-42	326	-66	7/6/1961	5.98	254.02	251.239
06S/22E-09P01S	006S022E35R002S	33.602940	-114.644260	260	328	302	-42	326	-66	7/28/1961	6	254.00	251.239
06S/22E-09P01S	006S022E35R002S	33.602940	-114.644260	260	328	302	-42	326	-66	8/24/1961	7.24	252.76	251.239
06S/22E-09P01S	006S022E35R002S	33.602940	-114.644260	260	328	302	-42	326	-66	9/25/1961	20.46	239.54	251.239
06S/22E-09P01S	006S022E35R002S	33.602940	-114.644260	260	328	302	-42	326	-66	10/18/1961	8.07	251.93	251.239
06S/22E-32R01S	006S022E35R002S	33.602940	-114.644260	260	328	302	-42	326	-66	11/21/1961	6.38	253.62	250.839
06S/22E-32R01S	006S022E35R002S	33.602940	-114.644260	260	328	302	-42	326	-66	12/20/1961	6.65	253.35	250.839
06S/22E-32R01S	006S022E35R002S	33.602940	-114.644260	260	328	302	-42	326	-66	1/22/1962	7.25	252.75	250.839
06S/22E-32R01S	006S022E35R002S	33.602940	-114.644260	260	328	302	-42	326	-66	2/19/1962	7.6	252.40	250.839
06S/22E-32R01S	006S022E35R002S	33.602940	-114.644260	260	328	302	-42	326	-66	3/26/1962	13.94	246.06	250.839
06S/22E-32R01S	006S022E35R002S	33.602940	-114.644260	260	328	302	-42	326	-66	4/23/1962	9.98	250.02	250.839
06S/22E-32R01S	006S022E35R002S	33.602940	-114.644260	260	328	302	-42	326	-66	5/25/1962	5.94	254.06	250.839
06S/22E-32R01S	006S022E35R002S	33.602940	-114.644260	260	328	302	-42	326	-66	6/21/1962	12.89	247.11	250.839
06S/22E-32R01S	006S022E35R002S	33.602940	-114.644260	260	328	302	-42	326	-66	7/19/1962	6.76	253.24	250.839
06S/22E-32R01S	006S022E35R002S	33.602940	-114.644260	260	328	302	-42	326	-66	8/16/1962	21	239.00	250.839
06S/22E-32R01S	006S022E35R002S	33.602940	-114.644260	260	328	302	-42	326	-66	9/20/1962	5.91	254.09	250.839
06S/22E-32R01S	006S022E35R002S	33.602940	-114.644260	260	328	302	-42	326	-66	10/11/1962	6.02	253.98	250.839
06S/22E-32R01S	006S022E35R002S	33.602940	-114.644260	260	328	302	-42	326	-66	10/23/1962	6.7	253.30	250.839
06S/22E-32R01S	006S022E35R002S	33.602940	-114.644260	260	328	302	-42	326	-66	11/8/1962	6.26	253.74	250.839
06S/22E-32R01S	006S022E35R002S	33.602940	-114.644260	260	328	302	-42	326	-66	12/13/1962	6.23	253.77	250.839
06S/22E-32R01S	006S022E35R002S	33.602940	-114.644260	260	328	302	-42	326	-66	1/11/1963	7.2	252.80	250.839
06S/22E-32R01S	006S022E35R002S	33.602940	-114.644260	260	328	302	-42	326	-66	8/1/1972	8	252.00	250.839
06S/22E-32R01S	006S022E35R002S	33.602940	-114.644260	260	328	302	-42	326	-66	8/2/1972	8.1	251.90	250.839
06S/22E-32R01S	006S022E35R001S	33.604050	-114.644240	257	326	302	-45	326	-69	10/31/1947	6	251.00	250.839

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
06S/22E-32R01S	006S022E35R001S	33.604050	-114.644240	257	326	302	-45	326	-69	5/25/1961	6.96	250.04	250.839
06S/22E-32R01S	006S022E35R001S	33.604050	-114.644240	257	326	302	-45	326	-69	7/6/1961	6.19	250.81	250.839
06S/22E-32R01S	006S022E35R001S	33.604050	-114.644240	257	326	302	-45	326	-69	7/28/1961	6.3	250.70	250.839
06S/22E-32R01S	006S022E35R001S	33.604050	-114.644240	257	326	302	-45	326	-69	8/24/1961	7.27	249.73	250.839
06S/22E-32R01S	006S022E35R001S	33.604050	-114.644240	257	326	302	-45	326	-69	9/25/1961	7.16	249.84	250.839
06S/22E-32R01S	006S022E35R001S	33.604050	-114.644240	257	326	302	-45	326	-69	10/18/1961	7.3	249.70	250.839
06S/22E-32R01S	006S022E35R001S	33.604050	-114.644240	257	326	302	-45	326	-69	11/21/1961	7.24	249.76	250.839
06S/22E-32R01S	006S022E35R001S	33.604050	-114.644240	257	326	302	-45	326	-69	12/20/1961	7.42	249.58	250.839
06S/22E-32R01S	006S022E35R001S	33.604050	-114.644240	257	326	302	-45	326	-69	1/22/1962	7.96	249.04	250.839
06S/22E-32R01S	006S022E35R001S	33.604050	-114.644240	257	326	302	-45	326	-69	2/15/1962	17.86	239.14	250.839
06S/22E-32R01S	006S022E35R001S	33.604050	-114.644240	257	326	302	-45	326	-69	3/26/1962	6.81	250.19	250.839
06S/22E-32R01S	006S022E35R001S	33.604050	-114.644240	257	326	302	-45	326	-69	4/23/1962	7.85	249.15	250.839
06S/22E-32R01S	006S022E35R001S	33.604050	-114.644240	257	326	302	-45	326	-69	5/24/1962	6.62	250.38	250.839
06S/22E-32R01S	006S022E35R001S	33.604050	-114.644240	257	326	302	-45	326	-69	6/21/1962	6.5	250.50	250.839
06S/22E-32R01S	006S022E35R001S	33.604050	-114.644240	257	326	302	-45	326	-69	7/19/1962	7.9	249.10	250.839
06S/22E-32R01S	006S022E35R001S	33.604050	-114.644240	257	326	302	-45	326	-69	8/16/1962	7.37	249.63	250.839
06S/22E-32R01S	006S022E35R001S	33.604050	-114.644240	257	326	302	-45	326	-69	9/20/1962	6.66	250.34	250.839
06S/22E-32R01S	006S022E35R001S	33.604050	-114.644240	257	326	302	-45	326	-69	10/11/1962	6.8	250.20	250.839
06S/22E-32R01S	006S022E35R001S	33.604050	-114.644240	257	326	302	-45	326	-69	11/8/1962	6.97	250.03	250.839
06S/22E-32R01S	006S022E35R001S	33.604050	-114.644240	257	326	302	-45	326	-69	12/13/1962	6.93	250.07	250.839
06S/22E-32R01S	006S022E35R001S	33.604050	-114.644240	257	326	302	-45	326	-69	1/11/1963	7.82	249.18	250.839
06S/22E-32R01S	006S022E35R001S	33.604050	-114.644240	257	326	302	-45	326	-69	8/2/1972	9.2	247.80	250.839
06S/22E-32R01S	007S022E04P001S	33.589470	-114.684400	310	156	118	192	136	174	9/25/1961	58.57	251.43	250.839
06S/22E-32R01S	007S022E04P001S	33.589470	-114.684400	310	156	118	192	136	174	10/18/1961	58.53	251.47	250.839
06S/22E-32R01S	007S022E04P001S	33.589470	-114.684400	310	156	118	192	136	174	11/21/1961	57.55	252.45	250.839
06S/22E-32R01S	007S022E04P001S	33.589470	-114.684400	310	156	118	192	136	174	12/20/1961	57.9	252.10	250.839
06S/22E-32R01S	007S022E04P001S	33.589470	-114.684400	310	156	118	192	136	174	1/22/1962	59.22	250.78	250.839
06S/22E-32R01S	007S022E04P001S	33.589470	-114.684400	310	156	118	192	136	174	2/19/1962	59.75	250.25	250.839
06S/22E-35R02S	007S022E04P001S	33.589470	-114.684400	310	156	118	192	136	174	3/26/1962	59.42	250.58	251.040
06S/22E-35R02S	007S022E04P001S	33.589470	-114.684400	310	156	118	192	136	174	4/23/1962	59.87	250.13	251.040
06S/22E-35R02S	007S022E04P001S	33.589470	-114.684400	310	156	118	192	136	174	5/25/1962	59.88	250.12	251.040

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
06S/22E-35R02S	007S022E04P001S	33.589470	-114.684400	310	156	118	192	136	174	6/21/1962	60	250.00	251.040
06S/22E-35R02S	007S022E04P001S	33.589470	-114.684400	310	156	118	192	136	174	7/19/1962	59.65	250.35	251.040
06S/22E-35R02S	007S022E04P001S	33.589470	-114.684400	310	156	118	192	136	174	8/16/1962	59.53	250.47	251.040
06S/22E-35R02S	007S022E04P001S	33.589470	-114.684400	310	156	118	192	136	174	9/17/1962	59.41	250.59	251.040
06S/22E-35R02S	007S022E04P001S	33.589470	-114.684400	310	156	118	192	136	174	10/11/1962	59.86	250.14	251.040
06S/22E-35R02S	007S022E04P001S	33.589470	-114.684400	310	156	118	192	136	174	11/8/1962	60.02	249.98	251.040
06S/22E-35R02S	007S022E04P001S	33.589470	-114.684400	310	156	118	192	136	174	12/13/1962	60.03	249.97	251.040
06S/22E-35R02S	007S022E04P001S	33.589470	-114.684400	310	156	118	192	136	174	1/9/1963	58.61	251.39	251.040
06S/22E-35R02S	006S022E03R002S	33.678820	-114.659560	406.76	350	170	236.76	350	56.76	5/17/1966	143	263.76	251.040
06S/22E-35R02S	006S022E03R002S	33.678820	-114.659560	406.76	350	170	236.76	350	56.76	10/6/1966	146.9	259.86	251.040
06S/22E-35R02S	006S022E03R002S	33.678820	-114.659560	406.76	350	170	236.76	350	56.76	8/18/1971	171.56	235.20	251.040
06S/22E-35R02S	006S022E03R002S	33.678820	-114.659560	406.76	350	170	236.76	350	56.76	7/24/1980	158.69	248.07	251.040
06S/22E-35R02S	006S022E03R002S	33.678820	-114.659560	406.76	350	170	236.76	350	56.76	1/23/1981	156.39	250.37	251.040
06S/22E-35R02S	006S022E03R002S	33.678820	-114.659560	406.76	350	170	236.76	350	56.76	8/28/1981	167.4	239.36	251.040
06S/22E-35R02S	006S022E03R002S	33.678820	-114.659560	406.76	350	170	236.76	350	56.76	3/4/1982	157.36	249.40	251.040
06S/22E-35R02S	006S022E03R002S	33.678820	-114.659560	406.76	350	170	236.76	350	56.76	12/10/1982	157.48	249.28	251.040
06S/22E-35R02S	006S022E03R002S	33.678820	-114.659560	406.76	350	170	236.76	350	56.76	9/20/1983	158.56	248.20	251.040
06S/22E-35R02S	006S022E03R002S	33.678820	-114.659560	406.76	350	170	236.76	350	56.76	9/18/1984	158.98	247.78	251.040
06S/22E-35R02S	006S022E03R002S	33.678820	-114.659560	406.76	350	170	236.76	350	56.76	6/12/1985	157.82	248.94	251.040
06S/22E-35R02S	006S022E03R002S	33.678820	-114.659560	406.76	350	170	236.76	350	56.76	1/15/2002	151.68	255.08	251.040
06S/22E-35R02S	006S022E03R002S	33.678820	-114.659560	406.76	350	170	236.76	350	56.76	1/15/2002	151.71	255.05	251.040
06S/22E-35R02S	007S022E03D002S	33.602520	-114.671070	260	20	18	242	20	240	3/30/1967	5.13	254.87	251.040
06S/22E-35R02S	007S022E03D002S	33.602520	-114.671070	260	20	18	242	20	240	6/1/1967	4.65	255.35	251.040
06S/22E-35R01S	007S022E03D002S	33.602520	-114.671070	260	20	18	242	20	240	6/10/1968	6.87	253.13	252.760
06S/22E-35R01S	007S022E03D002S	33.602520	-114.671070	260	20	18	242	20	240	8/2/1972	11	249.00	252.760
06S/22E-35R01S	006S022E14L001S	33.651890	-114.649710	292.6	94	90	202.6	94	198.6	3/31/1967	32.92	259.68	252.760
06S/22E-35R01S	006S022E14L001S	33.651890	-114.649710	292.6	94	90	202.6	94	198.6	6/1/1967	32.85	259.75	252.760
06S/22E-35R01S	006S022E14L001S	33.651890	-114.649710	292.6	94	90	202.6	94	198.6	6/10/1968	33.18	259.42	252.760
06S/22E-35R01S	006S022E14L001S	33.651890	-114.649710	292.6	94	90	202.6	94	198.6	8/1/1971	35	257.60	252.760
06S/22E-35R01S	006S022E14L001S	33.651890	-114.649710	292.6	94	90	202.6	94	198.6	8/4/1971	35	257.60	252.760
06S/22E-35R01S	006S022E14L001S	33.651890	-114.649710	292.6	94	90	202.6	94	198.6	5/11/2000	36.48	256.12	252.760

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
06S/22E-35R01S	006S022E15M001S	33.653280	-114.675080	396.6	315	171	225.6	315	81.6	2/15/1955	136	260.60	252.760
06S/22E-35R01S	006S022E15M001S	33.653280	-114.675080	396.6	315	171	225.6	315	81.6	2/6/1962	139.13	257.47	252.760
06S/22E-35R01S	006S022E15M001S	33.653280	-114.675080	396.6	315	171	225.6	315	81.6	6/10/1963	139.8	256.80	252.760
06S/22E-35R01S	006S022E15M001S	33.653280	-114.675080	396.6	315	171	225.6	315	81.6	6/11/1963	139.74	256.86	252.760
06S/22E-35R01S	006S022E15M001S	33.653280	-114.675080	396.6	315	171	225.6	315	81.6	6/12/1963	140.24	256.36	252.760
06S/22E-35R01S	006S022E15M001S	33.653280	-114.675080	396.6	315	171	225.6	315	81.6	4/3/2000	143.49	253.11	252.760
06S/22E-35R01S	006S022E15M001S	33.653280	-114.675080	396.6	315	171	225.6	315	81.6	4/3/2000	143.5	253.10	252.760
06S/22E-35R01S	006S022E01F001S	33.682610	-114.633530	406.54	350	150	256.54	350	56.54	10/6/1966	145	261.54	252.760
06S/22E-35R01S	006S022E01F001S	33.682610	-114.633530	406.54	350	150	256.54	350	56.54	7/1/1971	157	249.54	252.760
06S/22E-35R01S	006S022E01F001S	33.682610	-114.633530	406.54	350	150	256.54	350	56.54	7/22/1971	157.91	248.63	252.760
06S/22E-35R01S	006S022E01F001S	33.682610	-114.633530	406.54	350	150	256.54	350	56.54	3/27/1984	149.64	256.90	252.760
06S/22E-35R01S	006S022E01F001S	33.682610	-114.633530	406.54	350	150	256.54	350	56.54	9/17/1990	149.09	257.45	252.760
06S/22E-35R01S	006S022E01F001S	33.682610	-114.633530	406.54	350	150	256.54	350	56.54	3/23/1992	148.77	257.77	252.760
06S/22E-35R01S	006S022E01F001S	33.682610	-114.633530	406.54	350	150	256.54	350	56.54	2/17/2000	148.15	258.39	252.760
06S/22E-35R01S	006S022E10H001S	33.671460	-114.663110	404.21	304	174	230.21	304	100.21	8/1/1971	150	254.21	252.760
07S/22E-04P01S	006S022E10H001S	33.671460	-114.663110	404.21	304	174	230.21	304	100.21	9/15/1990	154.9	249.31	248.568
07S/22E-04P01S	006S022E10H001S	33.671460	-114.663110	404.21	304	174	230.21	304	100.21	2/16/2000	149.7	254.51	248.568
07S/22E-04P01S	006S022E10H001S	33.671460	-114.663110	404.21	304	174	230.21	304	100.21	2/16/2000	149.73	254.48	248.568
07S/22E-04P01S	006S022E10H001S	33.671460	-114.663110	404.21	304	174	230.21	304	100.21	1/15/2002	149.08	255.13	248.568
07S/22E-04P01S	006S022E15Q001S	33.649500	-114.664590	372.54	585	346	26.54	572	-199.46	9/12/1963	113	259.54	248.568
07S/22E-04P01S	006S022E15Q001S	33.649500	-114.664590	372.54	585	346	26.54	572	-199.46	9/17/1963	115.25	257.29	248.568
07S/22E-04P01S	006S022E15Q001S	33.649500	-114.664590	372.54	585	346	26.54	572	-199.46	6/28/1967	132	240.54	248.568
07S/22E-04P01S	006S022E15Q001S	33.649500	-114.664590	372.54	585	346	26.54	572	-199.46	7/23/1971	141.62	230.92	248.568
07S/22E-04P01S	006S022E15Q001S	33.649500	-114.664590	372.54	585	346	26.54	572	-199.46	9/22/1990	121.25	251.29	248.568
07S/22E-04P01S	006S022E15Q001S	33.649500	-114.664590	372.54	585	346	26.54	572	-199.46	2/19/1992	121.31	251.23	248.568
07S/22E-04P01S	006S022E16A001S	33.660700	-114.675620	366.67	364	170	196.67	359	7.67	3/29/1966	124	242.67	248.568
07S/22E-04P01S	006S022E16A001S	33.660700	-114.675620	366.67	364	170	196.67	359	7.67	4/4/1966	124	242.67	248.568
07S/22E-04P01S	006S022E16A001S	33.660700	-114.675620	366.67	364	170	196.67	359	7.67	7/22/1971	180.96	185.71	248.568
07S/22E-04P01S	006S022E16A001S	33.660700	-114.675620	366.67	364	170	196.67	359	7.67	9/22/1990	118.97	247.70	248.568
07S/22E-04P01S	006S022E16A001S	33.660700	-114.675620	366.67	364	170	196.67	359	7.67	2/15/1992	117.92	248.75	248.568
07S/22E-04P01S	006S022E16A001S	33.660700	-114.675620	366.67	364	170	196.67	359	7.67	1/27/2000	113.78	252.89	248.568

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
07S/22E-04P01S	006S022E02R001S	33.676590	-114.642370	404.26	514	406	-1.74	514	-109.74	2/10/1966	142.45	261.81	248.568
06S/22E-03R02S	006S022E02R001S	33.676590	-114.642370	404.26	514	406	-1.74	514	-109.74	8/1/1971	146	258.26	253.175
06S/22E-03R02S	006S022E02R001S	33.676590	-114.642370	404.26	514	406	-1.74	514	-109.74	8/19/1971	145.51	258.75	253.175
06S/22E-03R02S	006S022E02R001S	33.676590	-114.642370	404.26	514	406	-1.74	514	-109.74	9/17/1990	150.02	254.24	253.175
06S/22E-03R02S	006S022E02R001S	33.676590	-114.642370	404.26	514	406	-1.74	514	-109.74	3/23/1992	148.96	255.30	253.175
06S/22E-03R02S	006S022E02R001S	33.676590	-114.642370	404.26	514	406	-1.74	514	-109.74	3/14/2000	147.48	256.78	253.175
06S/22E-03R02S	006S021E36R001S	33.603180	-114.728800	389.09	636	520	-130.91	620	-230.91	5/1/1946	138	251.09	253.175
06S/22E-03R02S	006S021E36R001S	33.603180	-114.728800	389.09	636	520	-130.91	620	-230.91	9/27/1990	146.64	242.45	253.175
06S/22E-03R02S	006S021E36R001S	33.603180	-114.728800	389.09	636	520	-130.91	620	-230.91	2/23/2000	144.62	244.47	253.175
06S/22E-03R02S	006S021E36R001S	33.603180	-114.728800	389.09	636	520	-130.91	620	-230.91	3/29/2000	144.47	244.62	253.175
06S/22E-03R02S	006S022E11H001S	33.668010	-114.642140	407.97	235	165	242.97	235	172.97	9/30/1955	147	260.97	253.175
06S/22E-03R02S	006S022E11H001S	33.668010	-114.642140	407.97	235	165	242.97	235	172.97	3/28/1984	155.1	252.87	253.175
06S/22E-03R02S	006S022E11H001S	33.668010	-114.642140	407.97	235	165	242.97	235	172.97	3/23/1992	152.66	255.31	253.175
06S/22E-03R02S	006S022E11H001S	33.668010	-114.642140	407.97	235	165	242.97	235	172.97	4/4/2000	151.81	256.16	253.175
07S/22E-03D02S	006S022E17B001S	33.660630	-114.701360	399.64	302	181	218.64	302	97.64	5/26/1966	149	250.64	248.620
07S/22E-03D02S	006S022E17B001S	33.660630	-114.701360	399.64	302	181	218.64	302	97.64	8/22/1966	149	250.64	248.620
07S/22E-03D02S	006S022E17B001S	33.660630	-114.701360	399.64	302	181	218.64	302	97.64	9/20/1990	152.64	247.00	248.620
07S/22E-03D02S	006S022E17B001S	33.660630	-114.701360	399.64	302	181	218.64	302	97.64	2/15/1992	152.76	246.88	248.620
06S/22E-14L01S	006S022E18A001S	33.657410	-114.710240	406.88	298	168	238.88	298	108.88	6/2/1966	155	251.88	252.591
06S/22E-14L01S	006S022E18A001S	33.657410	-114.710240	406.88	298	168	238.88	298	108.88	7/1/1971	163	243.88	252.591
06S/22E-14L01S	006S022E18A001S	33.657410	-114.710240	406.88	298	168	238.88	298	108.88	7/28/1971	162.78	244.10	252.591
06S/22E-14L01S	006S022E18A001S	33.657410	-114.710240	406.88	298	168	238.88	298	108.88	9/20/1990	161.61	245.27	252.591
06S/22E-14L01S	006S022E01H001S	33.683220	-114.625380	404.16	320	180	224.16	320	84.16	3/25/1959	141.67	262.49	252.591
06S/22E-14L01S	006S022E01H001S	33.683220	-114.625380	404.16	320	180	224.16	320	84.16	2/13/1962	142.43	261.73	252.591
06S/22E-14L01S	006S022E01H001S	33.683220	-114.625380	404.16	320	180	224.16	320	84.16	3/23/1992	145.37	258.79	252.591
06S/22E-15M01S	006S022E01H001S	33.683220	-114.625380	404.16	320	180	224.16	320	84.16	2/17/2000	144.92	259.24	259.191
06S/22E-15M01S	006S022E02J001S	33.679010	-114.646140	404.72	452	406	-1.28	514	-109.28	5/14/1951	144.5	260.22	259.191
06S/22E-15M01S	006S022E02J001S	33.679010	-114.646140	404.72	452	406	-1.28	514	-109.28	10/19/1966	143.35	261.37	259.191
06S/22E-15M01S	006S022E02J001S	33.679010	-114.646140	404.72	452	406	-1.28	514	-109.28	7/1/1971	147	257.72	259.191
06S/22E-15M01S	006S022E02J001S	33.679010	-114.646140	404.72	452	406	-1.28	514	-109.28	7/21/1971	147.13	257.59	259.191
06S/22E-15M01S	006S022E02P001S	33.675340	-114.651380	400.85	250	150	250.85	250	150.85	2/6/1964	137.5	263.35	259.191

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
06S/22E-15M01S	006S022E02P001S	33.675340	-114.651380	400.85	250	150	250.85	250	150.85	8/1/1971	146	254.85	259.191
06S/22E-01F01S	006S022E02P001S	33.675340	-114.651380	400.85	250	150	250.85	250	150.85	8/19/1971	146.2	254.65	248.886
06S/22E-01F01S	006S022E02P001S	33.675340	-114.651380	400.85	250	150	250.85	250	150.85	9/14/1990	151.47	249.38	248.886
06S/22E-01F01S	007S021E14H001S	33.566710	-114.747240	379.52	900	700	-320.48	900	-520.48	3/1/1966	130	249.52	248.886
06S/22E-01F01S	007S021E14H001S	33.566710	-114.747240	379.52	900	700	-320.48	900	-520.48	10/20/1966	132.9	246.62	248.886
06S/22E-01F01S	007S021E14H001S	33.566710	-114.747240	379.52	900	700	-320.48	900	-520.48	8/1/1972	134	245.52	248.886
06S/22E-01F01S	007S021E14H001S	33.566710	-114.747240	379.52	900	700	-320.48	900	-520.48	9/22/1990	137.6	241.92	248.886
06S/22E-01F01S	007S022E03D001S	33.602520	-114.671070	260	49	45	215	49	211	3/30/1967	5.41	254.59	248.886
06S/22E-10H01S	007S022E03D001S	33.602520	-114.671070	260	49	45	215	49	211	6/1/1967	4.9	255.10	249.382
06S/22E-10H01S	007S022E03D001S	33.602520	-114.671070	260	49	45	215	49	211	6/10/1968	7.23	252.77	249.382
06S/22E-10H01S	007S022E03D001S	33.602520	-114.671070	260	49	45	215	49	211	8/2/1972	6.9	253.10	249.382
06S/22E-10H01S	007S022E03H001S	33.595580	-114.657740	255	118	114	141	118	137	3/30/1967	9.2	245.80	249.382
06S/22E-10H01S	007S022E03H001S	33.595580	-114.657740	255	118	114	141	118	137	6/1/1967	9.13	245.87	249.382
06S/22E-10H01S	007S022E03H001S	33.595580	-114.657740	255	118	114	141	118	137	6/10/1968	11.35	243.65	249.382
06S/22E-15Q01S	007S022E03H001S	33.595580	-114.657740	255	118	114	141	118	137	8/2/1972	10.5	244.50	247.797
06S/22E-15Q01S	007S022E03H002S	33.595580	-114.657740	255	22	20	235	22	233	3/30/1967	9.8	245.20	247.797
06S/22E-15Q01S	007S022E03H002S	33.595580	-114.657740	255	22	20	235	22	233	6/1/1967	9.69	245.31	247.797
06S/22E-15Q01S	007S022E03H002S	33.595580	-114.657740	255	22	20	235	22	233	6/10/1968	12.05	242.95	247.797
06S/22E-15Q01S	007S022E03H002S	33.595580	-114.657740	255	22	20	235	22	233	8/2/1972	11	244.00	247.797
06S/22E-15Q01S	006S022E14L002S	33.651968	-114.649681	293	34	30	263	34	259	6/1/1967	32.21	260.79	247.797
06S/22E-16A01S	006S022E14L002S	33.651968	-114.649681	293	34	30	263	34	259	3/31/1967	32.24	260.76	204.308
06S/22E-16A01S	006S022E14L002S	33.651968	-114.649681	293	34	30	263	34	259	6/10/1968	32.55	260.45	204.308
06S/22E-16A01S	006S022E14L002S	33.651968	-114.649681	293	34	30	263	34	259	5/11/2000		0.00	204.308
06S/22E-16A01S	006S022E14L002S	33.651968	-114.649681	293	34	30	263	34	259	8/4/1971		0.00	204.308
06S/22E-16A01S	006S022E21B001S	33.643430	-114.683770	373.9	378	192	181.9	372	1.9	4/28/1966	117	256.90	204.308
06S/22E-16A01S	006S022E21B001S	33.643430	-114.683770	373.9	378	192	181.9	372	1.9	8/23/1966	120.7	253.20	204.308
06S/22E-02R01S	006S022E21B001S	33.643430	-114.683770	373.9	378	192	181.9	372	1.9	1/25/2000	122.12	251.78	244.557
06S/22E-02R01S	006S022E21K001S	33.635530	-114.683230	375.3	323	182	193.3	323	52.3	5/11/1966	126	249.30	244.557
06S/22E-02R01S	006S022E21K001S	33.635530	-114.683230	375.3	323	182	193.3	323	52.3	8/24/1966	121.3	254.00	244.557
06S/22E-02R01S	006S022E21K001S	33.635530	-114.683230	375.3	323	182	193.3	323	52.3	7/28/1971	159.64	215.66	244.557
06S/22E-02R01S	006S022E32K001S	33.607520	-114.700790	362.8	464	112	250.8	464	-101.2	10/27/1953	112	250.80	244.557

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GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
06S/22E-02R01S	006S022E32K001S	33.607520	-114.700790	362.8	464	112	250.8	464	-101.2	5/23/1961	117	245.80	244.557
06S/21E-36R01S	006S022E32K001S	33.607520	-114.700790	362.8	464	112	250.8	464	-101.2	9/21/1990	118.46	244.34	256.932
06S/21E-36R01S	006S022E13Q001S	33.596410	-114.632180	268	116	114	154	116	152	3/23/1967	7.96	260.04	256.932
06S/21E-36R01S	006S022E13Q001S	33.596410	-114.632180	268	116	114	154	116	152	7/1/1971	8	260.00	256.932
06S/21E-36R01S	006S022E13Q002S	33.646410	-114.632180	268	22	20	248	22	246	3/23/1967	7.72	260.28	256.932
06S/21E-36R01S	006S022E13Q002S	33.646410	-114.632180	268	22	20	248	22	246	7/1/1971	8	260.00	256.932
06S/22E-11H01S	006S022E26E001S	33.626690	-114.657740	270	64	62	208	64	206	3/28/1967	15.58	254.42	255.038
06S/22E-11H01S	006S022E26E001S	33.626690	-114.657740	270	64	62	208	64	206	7/1/1971	18	252.00	255.038
06S/22E-11H01S	006S022E26E002S	33.626690	-114.657740	270	21	19	251	21	249	3/28/1967	15.2	254.80	255.038
06S/22E-11H01S	006S022E26E002S	33.626690	-114.657740	270	21	19	251	21	249	7/1/1971	17	253.00	255.038
06S/22E-17B01S	006S022E26G001S	33.624750	-114.644680	260	79	77	183	79	181	3/28/1967	9.03	250.97	249.954
06S/22E-17B01S	006S022E26G001S	33.624750	-114.644680	260	79	77	183	79	181	7/1/1971	9	251.00	249.954
06S/22E-17B01S	006S022E26G002S	33.624750	-114.644680	260	21	19	241	21	239	3/28/1967	8.5	251.50	249.954
06S/22E-17B01S	006S022E26G002S	33.624750	-114.644680	260	21	19	241	21	239	7/1/1971	9	251.00	249.954
06S/22E-18A01S	006S022E12E001S	33.669170	-114.638110	410.54	230	160	250.54	220	190.54	10/19/1944	150	260.54	248.016
06S/22E-18A01S	006S022E12E001S	33.669170	-114.638110	410.54	230	160	250.54	220	190.54	8/19/1971	170.3	240.24	248.016
06S/22E-18A01S	006S022E29D001S	33.631410	-114.705520	394.2	193	173	221.2	193	201.2	7/1/1971	145	249.20	248.016
06S/22E-18A01S	006S022E29D001S	33.631410	-114.705520	394.2	193	173	221.2	193	201.2	7/15/1971	145.18	249.02	248.016
06S/22E-01H01S	005S022E26M001S	33.711130	-114.656630	460	790	745	-285	780	-320	9/1/1971	181	279.00	254.758
06S/22E-01H01S	005S022E35A001S	33.704190	-114.644400	439.3	450	200	239.3	450	-10.7	9/1/1971	191	248.30	254.758
06S/22E-01H01S	006S022E11N002S	33.660580	-114.658290	400	246.5	160	240	320	80	7/26/1979	149.27	250.73	254.758
06S/22E-01H01S	006S022E17L002S	33.653360	-114.702180	397	323	171	226	323	74	7/1/1971	156	241.00	254.758
06S/22E-02J01S	006S022E20A001S	33.646130	-114.693020	395.79	250	230	165.79	250	145.79	7/1/1971	148	247.79	253.149
06S/22E-02J01S	006S022E29G001S	33.626970	-114.698570	392.5	350	202	190.5	350	42.5	7/1/1971	142	250.50	253.149
06S/22E-02J01S	006S022E32F001S	33.613080	-114.704680	388.5	230	195	193.5	230	158.5	7/1/1971	139	249.50	253.149
06S/22E-02J01S	006S022E32F003S	33.612310	-114.705190	387.5	500	140	247.5	280	107.5	3/25/2002	147	240.50	253.149
06S/22E-02P01S	006S022E03R001S	33.675580	-114.659680	403	355	180	223	355	48	7/24/1980	157.8	245.20	245.800
06S/22E-02P01S	006S022E08L001S	33.668080	-114.668850	408	300	180	228	300	108	7/1/1971	160	248.00	245.800
06S/22E-02P01S	006S022E34L001S	33.608360	-114.667740	330	360	350	-20	360	-30	8/1/1972	93	237.00	245.800
06S/22E-02P01S	006S022E35M001S	33.609190	-114.653570	260	310	295	-35	310	-50	2/7/1962	7	253.00	245.800
07S/21E-14H01S	006S022E11R001S	33.660856	-114.641903	276	77	75	201	77	199	6/1/1967	16.63	259.37	253.334

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GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
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BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
07S/21E-14H01S	006S022E11R001S	33.660856	-114.641903	276	77	75	201	77	199	6/10/1968	17	259.00	253.334
07S/21E-14H01S	006S022E11R001S	33.660856	-114.641903	276	77	75	201	77	199	3/21/1967	18.26	257.74	253.334
07S/21E-14H01S	006S022E11R001S	33.660856	-114.641903	276	77	75	201	77	199	7/7/1971	18.94	257.06	253.334
07S/22E-03D01S	006S022E11R002S	33.660856	-114.641903	276	21	18	258	21	255	3/21/1967	16.4	259.60	256.359
07S/22E-03D01S	006S022E11R002S	33.660856	-114.641903	276	21	18	258	21	255	6/10/1968	16.75	259.25	256.359
07S/22E-03D01S	006S022E11R002S	33.660856	-114.641903	276	21	18	258	21	255	7/7/1971	18.76	257.24	256.359
07S/22E-03D01S	006S023E29R001S	33.619469	-114.588568	270	382	264	6	354	-84	2/7/1961	11.4	258.60	256.359
07S/22E-03H01S	006S023E29R001S	33.619469	-114.588568	270	382	264	6	354	-84	8/3/1971	37.85	232.15	251.039
07S/22E-03H01S	006S023E29R001S	33.619469	-114.588568	270	382	264	6	354	-84	11/17/1999	--	270.00	251.039
07S/22E-03H01S	006S023E31J001S	33.609108	-114.608235	266	390	350	-84	380	-114	2/6/1962	4.5	261.50	251.039
07S/22E-03H01S	006S023E31J001S	33.609108	-114.608235	266	390	--	--	--	--	7/20/1972	--	266.00	251.039
07S/22E-03H02S	006S023E32D001S	33.617246	-114.605235	268	316	122	146	168	100	7/30/1953	5	263.00	252.244
07S/22E-03H02S	006S023E32D001S	33.617246	-114.605235	268	316	122	146	168	100	2/7/1961	9	259.00	252.244
07S/22E-03H02S	006S023E32E001S	33.612802	-114.603290	267	660	421	-154	505	-238	2/1/1966	7	260.00	252.244
07S/22E-03H02S	006S023E32F001S	33.613080	-114.597735	268	188	128	140	168	100	1937	11	257.00	252.244
06S/22E-14L02S	006S023E32F001S	33.613080	-114.597735	268	188	128	140	168	100	12/13/1962	8	260.00	259.668
06S/22E-14L02S	006S023E32F001S	33.613080	-114.597735	268	188	128	140	168	100	11/8/1962	8.03	259.97	259.668
06S/22E-14L02S	006S023E32F001S	33.613080	-114.597735	268	188	128	140	168	100	10/10/1962	8.31	259.69	259.668
06S/22E-14L02S	006S023E32F001S	33.613080	-114.597735	268	188	128	140	168	100	6/20/1962	8.6	259.40	259.668
06S/22E-14L02S	006S023E32F001S	33.613080	-114.597735	268	188	128	140	168	100	5/24/1962	8.72	259.28	259.668
06S/22E-21B01S	006S023E32F001S	33.613080	-114.597735	268	188	128	140	168	100	7/20/1962	9.08	258.92	213.277
06S/22E-21B01S	006S023E32F001S	33.613080	-114.597735	268	188	128	140	168	100	8/16/1962	9.14	258.86	213.277
06S/22E-21B01S	006S023E32F001S	33.613080	-114.597735	268	188	128	140	168	100	9/20/1962		0.00	213.277
06S/22E-21K01S	006S023E32F001S	33.613080	-114.597735	268	188	128	140	168	100	1/10/1963	8.91	259.09	249.695
06S/22E-21K01S	006S023E32F001S	33.613080	-114.597735	268	188	128	140	168	100	8/3/1971	10.68	257.32	249.695
06S/22E-21K01S	006S023E32G001S	33.611969	-114.594401	270	190	112	158	144	126	12/15/1961	7.2	262.80	249.695
06S/22E-32K01S	006S023E32G001S	33.611969	-114.594401	270	190	112	158	144	126	10/1/1961	8	262.00	254.475
06S/22E-32K01S	006S023E32G002S	33.613302	-114.594929	270	590	544	-274	560	-290	12/21/1961	8	262.00	254.475
06S/22E-32K01S	006S023E32G002S	33.613302	-114.594929	270	590	544	-274	560	-290	12/15/1961	8.09	261.91	254.475
06S/22E-13Q01S	006S023E32J001S	33.608636	-114.590234	270	400	342	-72	366	-96	3/1/1958	11.5	258.50	207.648
06S/22E-13Q01S	006S023E32M001S	33.609747	-114.602179	267	300	310	-43	335	-68	2/7/1961	7.3	259.70	207.648

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
06S/22E-13Q01S	006S023E32M001S	33.609747	-114.602179	267	300	310	-43	335	-68	8/2/1971		0.00	207.648
06S/22E-13Q02S	006S023E32P001S	33.604219	-114.598846	265	430	245	20	290	-25	8/3/1971	20.75	244.25	255.546
06S/22E-13Q02S	006S023E32P001S	33.604219	-114.598846	265	430	245	20	290	-25	11/4/1999	11.1	253.90	255.546
06S/22E-13Q02S	006S023E33E001S	33.611136	-114.586345	270	368	290	-20	324	-54	8/2/1947	10.7	259.30	255.546
06S/22E-26E01S	006S023E33E001S	33.611136	-114.586345	270	368	290	-20	324	-54	8/3/1971	36.17	233.83	200.390
06S/22E-26E01S	006S023E33E001S	33.611136	-114.586345	270	368	290	-20	324	-54	1/24/2000		0.00	200.390
06S/22E-26E01S	006S023E33G001S	33.614249	-114.577290	270.2	600	500	-229.8	600	-329.8	4/30/1959	8.5	261.70	200.390
06S/22E-26E02S	006S023E33G001S	33.614249	-114.577290	270.2	600	500	-229.8	600	-329.8	2/7/1962	9	261.20	205.288
06S/22E-26E02S	006S023E33G001S	33.614249	-114.577290	270.2	600	500	-229.8	600	-329.8	7/20/1972		0.00	205.288
06S/22E-26E02S	006S023E33G001S	33.614249	-114.577290	270.2	600	500	-229.8	600	-329.8	11/19/1999	12.76	257.44	205.288
06S/22E-26G01S	006S023E33G001S	33.614249	-114.577290	270.2	600	500	-229.8	600	-329.8	4/18/2002	13.38	256.82	254.798
06S/22E-26G01S	006S023E33K001S	33.610080	-114.576678	267	426	351	-84	408	-141	6/22/1960	7	260.00	254.798
06S/22E-26G01S	006S023E33K001S	33.610080	-114.576678	267	426	351	-84	408	-141	7/20/1972	11.8	255.20	254.798
06S/22E-26G02S	006S023E33K001S	33.610080	-114.576678	267	426	351	-84	408	-141	11/19/1999	12.31	254.69	255.122
06S/22E-26G02S	006S023E33M001S	33.609830	-114.582567	270	306	70	200	306	-36	1/1/1949	8	262.00	255.122
06S/22E-26G02S	006S023E33M001S	33.609830	-114.582567	270	306	70	200	306	-36	11/19/1999	13.58	256.42	255.122
06S/22E-12E01S	006S023E33M001S	33.609830	-114.582567	270	306	70	200	306	-36	11/19/1999	13.64	256.36	249.955
06S/22E-12E01S	008S023E06P001S	33.507249	-114.614456	253	390	362	-109	370	-117	2/8/1962	10.32	242.68	249.955
06S/22E-29D01S	008S023E06P001S	33.507249	-114.614456	253	390	362	-109	370	-117	8/1/1972	11.8	241.20	184.855
06S/22E-29D01S	008S023E06P001S	33.507249	-114.614456	253	390	362	-109	370	-117	3/15/2001		0.00	184.855
05S/22E-26M01S	008S023E07B001S	33.505860	-114.611900	254	390	370	-116	382	-128	2/13/1962	15.00	239.00	239.000
05S/22E-35A01S													
06S/22E-11N02S	006S021E35B002S	33.617005	-114.750445	409.56						3/30/2006			
06S/22E-17L02S	006S021E35B002S	33.617005	-114.750445	409.56									
06S/22E-20A01S	006S022E33C002S	33.617019	-114.687823	335	600					5/28/2003			
06S/22E-29G01S	006S022E33C002S	33.617019	-114.687823	335	600								
06S/22E-32F01S	006S021E35B001S	33.617246	-114.749961	409						8/17/1971			
06S/22E-32F03S	006S021E35B001S	33.617246	-114.749961	409						9/21/1990			
06S/22E-03R01S	006S021E35B001S	33.617246	-114.749961	409						2/17/2000			
06S/22E-08L01S	006S022E28G001S	33.626944	-114.676611	362	535								
06S/22E-34L01S	006S022E28C001S	33.631111	-114.685650	392.2									

Table A-1
GROUNDWATER LEVEL DATA
FOR PALO VERDE VALLEY
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA[1]				WELL COMPLETION DATA						GROUNDWATER LEVELS			
STATE WELL NUMBER (DWR)	STATE WELL NUMBER (USGS)	LATITUDE	LONGTUDE	Ground Surface Elevation	Total Depth	Depth to Top of Sample Interval	Elevation of the Top of Sample Interval	Depth to Bottom of Sample Interval	Elevation of the Bottom of Sample Interval	Depth to Groundwater		Groundwater Surface Elevation	Average Water Level
		NAD83	NAD83	feet-msl	feet-bgs	feet-bgs	feet-msl	feet-bgs	feet-msl	Date	feet-bgs	feet-msl	feet-msl
06S/22E-35M01S	006S021E25A001S	33.631389	-114.728056	398	260								
06S/22E-11R01S	006S022E19N001S	33.633333	-114.726111	398									
06S/22E-11R01S	006S022E17L001S	33.653333	-114.704444	400	445								
06S/22E-11R01S	006S022E18J001S	33.653333	-114.712500	408	302								
06S/22E-11R01S	006S022E16D001S	33.660556	-114.691944	398	420								
06S/22E-11R02S	006S022E09Q001S	33.660833	-114.682778	403	302								
06S/22E-11R02S	006S022E09L001S	33.667778	-114.683889	402	332					3/30/2006	148.74		
06S/22E-11R02S	006S022E09L001S	33.667778	-114.683889	402	332								
06S/23E-29R01S	006S022E09M001S	33.667778	-114.688056	404	292								
06S/23E-29R01S	006S022E08J001S	33.667778	-114.692500	408	302								
06S/23E-29R01S	006S021E01R001S	33.675833	-114.675833	448									
06S/23E-31J01S	006S023E02G001S	33.683889	-114.691389	280									
06S/23E-31J01S	006S023E02F001S	33.684167	-114.695556	280									
06S/23E-32D01S	005S022E33J001S	33.696389	-114.677500	438	380								
06S/23E-32D01S	005S022E31D001S	33.701389	-114.727500	476									

APPENDIX B

WATER QUALITY DATABASE

Table B-1
WATER CHEMISTRY DATA
FOR PALO VERDE Valley
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA [1]						WATER CHEMISTRY																					
STATE WELL NUMBER (DWR)	STATE WELL NAME (USGS)	LATITUDE	LONGITUDE	Ground Surface Elevation	Well Depth	Sample Date Mo/Yr	Temperature, degrees Celsius	Specific conductance, microsiemens per cm at 25 degrees Celsius	pH, standard units	Bicarbonate, mg/L	Carbonate, mg/L	Nitrate plus nitrite as nitrogen mg/L	Hardness as calcium carbonate mg/L	Calcium, mg/L	Magnesium, mg/L	Sodium, mg/L	Potassium, mg/L	Chloride, mg/L	Sulfate, mg/L	Fluoride, mg/L	Silica as SiO2 mg/L	Arsenic, ug/L	Boron, ug/L	Iron, ug/L	Manganese, ug/L	Selenium, ug/L	Total Dissolved Solids (TDS) mg/L
333000114440701	008S021E12E001S	33.50002719	-114.7360705	241.44	15	25-Nov-80	20	1240	8	218	0	-	400	106	32.2	124	6.6	100	344	-	-	-	-	-	-	-	825
333000114440701	008S021E12E001S	33.50002719	-114.7360705	241.44	15	19-Dec-80	17.5	1080	8.3	188	0	-	350	88.8	31.7	117	5.9	94.1	303	-	-	-	-	-	-	-	736
333000114440701	008S021E12E001S	33.50002719	-114.7360705	241.44	15	12-Jan-81	17.9	1100	8.3	126	12	-	300	70.4	31.2	117	5.9	94.1	300	-	-	-	-	-	-	-	693
333000114440701	008S021E12E001S	33.50002719	-114.7360705	241.44	15	04-Feb-81	18.5	1200	8.3	157	0	-	310	71	31.7	130	7	102	305	-	-	-	-	-	-	-	730
333000114440701	008S021E12E001S	33.50002719	-114.7360705	241.44	15	25-Feb-81	18.5	1180	8.2	168	0	-	330	73.6	34.7	114	5.9	94.4	298	-	-	-	-	-	-	-	706
333000114440701	008S021E12E001S	33.50002719	-114.7360705	241.44	15	31-Mar-81	22.1	1240	8.1	184	0	-	360	88	32.9	116	5.5	96.2	314	-	-	-	-	-	-	-	745
333000114440701	008S021E12E001S	33.50002719	-114.7360705	241.44	15	21-May-81	21.1	1520	7.9	195	0	-	370	92	33.6	121	5.1	98	327	-	-	-	-	-	-	-	775
333000114440702	008S021E12E002S	33.50002719	-114.7360705	241.69	25	25-Nov-80	23.3	1090	8.5	160	0	-	330	86	28.3	112	8.2	90	309	-	-	-	-	-	-	-	714
333000114440702	008S021E12E002S	33.50002719	-114.7360705	241.69	25	19-Dec-80	21.8	1060	8.4	171	0	-	340	88.8	28.3	110	7.4	77.7	312	-	-	-	-	-	-	-	711
333000114440702	008S021E12E002S	33.50002719	-114.7360705	241.69	25	12-Jan-81	21.2	1120	8.3	171	0	-	330	82.4	29.3	110	6.7	92.7	292	-	-	-	-	-	-	-	698
333000114440702	008S021E12E002S	33.50002719	-114.7360705	241.69	25	04-Feb-81	22.2	1100	8.1	161	0	-	320	78	29.9	113	7	93	293	-	-	-	-	-	-	-	696
333000114440702	008S021E12E002S	33.50002719	-114.7360705	241.69	25	25-Feb-81	21.7	1150	8	183	0	-	360	92.8	30.3	98	6.7	95.5	294	-	-	-	-	-	-	-	711
333000114440702	008S021E12E002S	33.50002719	-114.7360705	241.69	25	31-Mar-81	22.2	1200	8	176	0	-	380	98	31.7	110	6.6	96.9	312	-	-	-	-	-	-	-	744
333000114440702	008S021E12E002S	33.50002719	-114.7360705	241.69	25	21-May-81	22.4	1600	7.8	187	0	-	400	104	33.6	113	6.2	100	347	-	-	-	-	-	-	-	799
333000114440703	008S021E12E003S	33.50002719	-114.7360705	241.92	40	25-Nov-80	22.7	1660	8	289	0	-	170	15.2	31.1	178	8.6	123	456	-	-	-	-	-	-	-	1090
333000114440703	008S021E12E003S	33.50002719	-114.7360705	241.92	40	19-Dec-80	21.1	1520	8.2	267	0	-	480	142	30.5	185	9	123	475	-	-	-	-	-	-	-	1100
333000114440703	008S021E12E003S	33.50002719	-114.7360705	241.92	40	12-Jan-81	21.8	1600	8.1	264	0	-	470	135	31.7	182	9.8	130	456	-	-	-	-	-	-	-	1080
333000114440703	008S021E12E003S	33.50002719	-114.7360705	241.92	40	04-Feb-81	22.6	1640	8	279	0	-	470	136	31.2	190	9.4	129	449	-	-	-	-	-	-	-	1080
333000114440703	008S021E12E003S	33.50002719	-114.7360705	241.92	40	25-Feb-81	20.5	1600	8	271	0	-	480	140	31.7	178	9	126	451	-	-	-	-	-	-	-	1070
333000114440703	008S021E12E003S	33.50002719	-114.7360705	241.92	40	31-Mar-81	22.5	1600	7.8	250	0	-	460	135	30.5	166	8.6	120	422	-	-	-	-	-	-	-	1010
333000114440703	008S021E12E003S	33.50002719	-114.7360705	241.92	40	21-May-81	22.3	2050	8.2	237	0	-	450	130	30.5	161	8.2	113	464	-	-	-	-	-	-	-	1030
333000114440704	008S021E12E004S	33.50002719	-114.7360705	241.41	100	25-Nov-80	22	1120	8.6	126	0	-	230	50	25.4	142	6.3	93	307	-	-	-	-	-	-	-	689
333000114440704	008S021E12E004S	33.50002719	-114.7360705	241.41	100	19-Dec-80	22.3	2000	8.1	281	0	-	470	133	34.2	311	8.6	228	541	-	-	-	-	-	-	-	1400
333000114440704	008S021E12E004S	33.50002719	-114.7360705	241.41	100	12-Jan-81	21.5	2220	8.1	274	0	-	470	136	31.2	304	8.2	233	549	-	-	-	-	-	-	-	1400
333000114440704	008S021E12E004S	33.50002719	-114.7360705	241.41	100	04-Feb-81	22.5	2250	8	253	0	-	420	118	30.5	513	9	246	538	-	-	-	-	-	-	-	1380
333000114440704	008S021E12E004S	33.50002719	-114.7360705	241.41	100	25-Feb-81	21	2300	8.1	248	0	-	400	112	29.3	334	9	256	562	-	-	-	-	-	-	-	1430
333000114440704	008S021E12E004S	33.50002719	-114.7360705	241.41	100	31-Mar-81	22.6	2280	8.2	214	0	-	310	80	26.4	364	9	263	530	-	-	-	-	-	-	-	1380
333000114440704	008S021E12E004S	33.50002719	-114.7360705	241.41	100	21-May-81	22.3	2400	8.2	235	0	-	290	76	24.4	359	9	238	564	-	-	-	-	-	-	-	1390
333057114360801	007S023E32M001S	33.5158602	-114.6030113	256	-	14-Feb-62	20	897	7.8	240	0	-	250	68	19	-	-	97	100	-	15	-	-	-	-	-	507
333124114392301	007S022E34H001S	33.52335998	-114.6571796	245	114	15-May-57	-	3700	7.9	400	0	-	1000	270	81	540	7	920	540	0.6	30	-	280	-	-	-	2590
333131114392401	007S022E34H002S	33.52530437	-114.6574574	245	101	24-Mar-51	21.1	1290	7.9	260	0	-	320	80	29	180	4.8	250	130	-	-	-	180	-	-	-	802
333131114392401	007S022E34H002S	33.52530437	-114.6574574	245	101	15-May-57	-	1680	8	300	0	-	380	97	33	200	5	260	180	0.5	30	-	160	-	-	-	953
333140114390401	007S022E35C001S	33.5278043	-114.6519017	247	648	18-Oct-84	24	-	-	-	-	-	460	108	48	173	7	162	499	-	-	-	-	-	-	-	1200
333140114390401	007S022E35C001S	33.5278043	-114.6519017	247	648	18-Oct-84	23.8	-	-	-	-	-	560	144	49	219	5	165	523	-	-	-	-	-	-	-	1390
333140114390401	007S022E35C001S	33.5278043	-114.6519017	247	648	15-May-85	26	-	7.7	303	-	-	650	170	55	316	7	448	516	-	-	-	-	-	-	-	1660
333140114390401	007S022E35C001S	33.5278043	-114.6519017	247	648	15-May-85	25	-	7.5	-	-	-	710	180	64	351	7	382	684	-	-	-	-	-	-	-	1820
333140114390401	007S022E35C001S	33.5278043	-114.6519017	247	648	16-May-85	25	-	7.6	-	-	-	650	172	54	225	5	406	317	-	-	-	-	-	-	-	1310
333140114390401	007S022E35C001S	33.5278043	-114.6519017	247	648	16-May-85	24	-	7.7	-	-	-	550	135	52	391	8	266	672	-	-	-	-	-	-	-	1700
333216114434901	007S021E25H001S	33.53780397	-114.7310708	255	472	18-Oct-84	35	-		-	-	-	340	120	9	972	13	1320	552	-	-	-	-	-	-	-	3270
333216114434901	007S021E25H001S	33.53780397	-114.7310708	255	472	14-May-85	37	-	8.1	71	-	-	450	155	15	1380	10	1840	804	-	-	-	-	-	-	-	4240
333216114434901	007S021E25H001S	33.53780397	-114.7310708	255	472	14-May-85	39	-	8	-	-	-	520	180	18	1620	12	2150	1100	-	-	-	-	-	-	-	5120
333216114434901	007S021E25H001S	33.53780397	-114.7310708	255	472	14-May-85	40	-	7.9	-	-	-	500	175	15	1480	12	2050	936	-	-	-	-	-	-	-	4710
333216114434901	007S021E25H001S	33.53780397	-114.7310708	255	472	14-May-85	36	-	7.8	90	-	-	520	175	21	1350	11	1740	792	-	-	-	-	-	-	-	4120
333307114341101	007S023E21H001S	33.5519704	-114.5705108	260	-	15-Feb-62	19.4	1020	8.1	240	0	-	120	36	9	-	-	110	140	-	11	-	-	-	-	-	604
333345114371901	007S022E13J001S	33.56252566	-114.6227346	260	128	15-May-57	-	1690	7.3	280	0	-	620	170	48	130	8.4	140	470	0.4	20	-	180	-	-	-	1130
333418114362401	007S023E18A001S	33.5715532	-114.6067065	255	486	14-Feb-62	25.6	1700	7.7	220	0	-	440	120	34	-	-	290	230	-	12	-	-	-	-	-	976
333418114362501	007S023E17D001S	33.57163655	-114.6044286	255	176	14-Feb-62	24.4	1880	7.7	300	0	-	470	130	36	-	-	250	380	-	17	-	-	-	-	-	1200
333428114385001	007S022E11Q001S	33.57446976	-114.6480133	256	-	14-Feb-62	18.9	1080	7.9	240	0	-	160	44	12	-	-	130	140	-	12	-	-	-	-	-	623
333518114344301	007S023E09C001S	33.58835837	-114.5794003	261	-	12-Dec-56	-	1820	7.7	170	0	-	500	130	42	210	3.7	160	550	0.5	-	-	320	-	-	-	1180
333522114410101	007S022E04P001S	33.5894693	-114.6844034	310	136	13-Aug-59	-	1750	7.9	180	0	-	160	41	14	280	5.1	270	230	1.5	25	-	-	300	0	-	860
333522114410101	007S022E04P001S	33.5894693	-114.6844034	310	136	29-Feb-60	-	1950	7.9	200	0	-	210	53	18	350	-	350	290	2.2	-	-	550	-	-	-	-
333522114410101	007S022E04P001S	33.5894693	-114.6844034	310	136	25-May-61	28.3	2950	7.4	180	0	-	390	110	29	500	-	520	520	-	30	-	650	-	-	-	1840
333522114410101	007S022E04P001S	33.5894693	-114.6844034	310	136	22-Oct-62	27.8	3790	7.3	170	-	-	510	120	46	-	-	600	700	-	25	-	-	-	-	-	2140
333542114360501	007S023E05E001S	33.59502484	-114.6021789	265	-	15-Feb-62	21.7	997	7.8	230	0	-	230	63	17	-	-	120	130	-	16	-	-	-	-	-	592
333544114483701	007S021E05F001S	33.59558004	-114.811074	-	-	27-Apr-79	-	-	-	-	-	-	160	54	5.7	2000	15	2400	1100	5.8	17	-	-	-	-	-	5640
333547114341501	007S023E04H001S	33.5964137	-114.5716224	262	115	12-Dec-56	-	1850	8	350	0	-	600	170	43	180	3.9	190	410	0.5	-	-	70	-	-	-	1170
333600114360401	007S023E05D001S	33.5999969	-114.6018178	265	200	07-Feb-62	-	1290	7.8	293	-	-	380	108	26	-	-	147	225	-	14	-	-	-	-	-	-
333600114360401	007S023E05D001S	33.5999969	-114.6018178	265	200	07-Feb-62	23.3	1290	7.8	290	0	-	380	110	26	-	-	150	220	-	14	-	-	-	-	-	806
333600114360401	007S023E05D001S	33.6000247	-114.6019011	265	190	07-Feb-62	-	1290	7.8	293	-	-	380	108	26	-	-	147	225	-	14	-	-	-	-	-	-
333600114360401	007S023E05D001S	33.6000247	-114.6019011	265	190	07-Feb-62	23.3	1290	7.8	290	0	-	380	110	26	-	-	150	220	-	14	-	-	-	-	-	806
333610114383701	006S022E35R002S	33.60280236	-114.6444024	256	328	23-Oct-62	26.1	1320	7.4	260	0	-	310	79	28	-	-	180	170	0.5	19	-	-	-	-	-	752
333612114434001	006S021E36R001S	33.6031772	-114.7288021	389.09	636	15-Jul-54	-	4700	7.6	100	0	-	-	150	-	930	-	840	1060	4	-	-	1540	-	-	-	-
333612114434001	006S021E36R001S	33.6031772	-114.7288021	389.09	636	13-Jun-61	33.3	2350	7.8	120	0	-	120	36	8.5	440	5.5	400	410	1.1	32	-	620	-	-	-	1390
333612114434001	006S021E36R001S	33.6031772	-114.7288021	389.09	636	14-May-64	-	2300	7.9	120	0	-	130	38	8.1	470	6.5	420	440	3	27	-	1070	-	-	-	1470
333615114355401	006S023E32P001S	33.60421905	-114.5988455	265	430	11-Mar-60	-	900	7.8	230	0	-	220	68	11	100	5	120	90	0.1	-	-	-	200	-	-	525
333615114355401	006S023E32P001S	33.60421905	-114.5988455	265	430	07-Feb-61	-	1150	7.6	250	0	-	320	91	22	120	3	150	150	0.4	21	-	-	10	-	-	690
333615114355401	006S023E32P001S	33.60421905	-114.5988455	265	430	23-Oct-62	25.6	1370	7.4	260	0	-	370	100	27	-	-	180	190	0.5	18	-	-	-	-	-	787
333615114413201	006S022E32R001S	33.60423559	-114.6929594	334.2	560	11-Jun-63	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
333615114413201	006S022E32R001S	33.60423559	-114.6929594	334.2	560	11-Jun-63	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
333615114413201	006S022E32R001S	33.60423559	-114.6929594	334.2	560	11-Jun-63	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
333617114321501	006S023E35R001S	33.60474689	-114.5382882	270		08-Mar-56	-	1720	7.5	340	0	-	610	160	52	140	5.5	120	480	0.6		-	220	-	-	-	1130
333621114315801	006S023E36N001S	33.60585798	-114.5335658	270	248	14-Feb-52	-		7.6	310	0	-	1000	260	90	810		1100	870	0.4	-	-	-	-	-	-	-
333621114315801	006S023E36N001S	33.60585798	-114.5335658	270	248	08-Mar-56	-	3510	7.6	320	0	-	810	220	63	440	8.6	660	540	0.1	-	-	630	-	-	-	2090
333621114315801	006S023E36N001S	33.60585798	-114.5335658	270	248	30-May-56	20	3380	7.6	320	0	-	790	-	-	420	-	660	-	-	25	-	-	-	-	-	-
333621114315801	006S023E36N001S	33.60585798	-114.5335658	270	248	15-May-61	21.7	1260	7.8	300	0	-	410	120	29	120	4	120	240	0.5	25	-	120	-	-	-	806

Table B-1
WATER CHEMISTRY DATA
FOR PALO VERDE Valley
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA [1]						WATER CHEMISTRY																					
STATE WELL NUMBER (DWR)	STATE WELL NAME (USGS)	LATITUDE	LONGITUDE	Ground Surface Elevation	Well Depth	Sample Date Mo/Yr	Temperature, degrees Celsius	Specific conductance, microsiemens per cm at 25 degrees Celsius	pH, standard units	Bicarbonate, mg/L	Carbonate, mg/L	Nitrate plus nitrite as nitrogen mg/L	Hardness as calcium carbonate mg/L	Calcium, mg/L	Magnesium, mg/L	Sodium, mg/L	Potassium, mg/L	Chloride, mg/L	Sulfate, mg/L	Fluoride, mg/L	Silica as SiO2 mg/L	Arsenic, ug/L	Boron, ug/L	Iron, ug/L	Manganese, ug/L	Selenium, ug/L	Total Dissolved Solids (TDS) mg/L
333621114315801	006S023E36N001S	33.60585798	-114.5335658	270	248	23-May-62	-	1320	7.9	310	0	-	420	110	34	120	3.2	140	240	0.02	19	-	180	-	-	-	819
333621114315801	006S023E36N001S	33.60585798	-114.5335658	270	248	22-May-63	-	1350	7.8	320	0	-	450	130	28	11	5.9	140	260	0.2	13	-	220	-	-	-	746
333621114315801	006S023E36N001S	33.60585798	-114.5335658	270	248	16-May-67	-	1610	7.7	330	0	-	540	140	42	140	4	210	280	0.6		-	200	-	-	-	979
333623114352101	006S023E32Q001S	33.60641345	-114.5899564	268	366	14-Sep-60	-	817	7.8	220	0	-	160	46	11	120	2	110	90	0.2		-	-	-	-	-	487
333623114361001	006S023E32N001S	33.6064134	-114.6035679	265	335	07-Feb-61	30.8	881	7.7	220	0	-	160	44	12	130	2.6	110	94	0.6	21	-	-	10	-	-	522
333627114420001	006S022E32K001S	33.60752438	-114.700793	362.8	464	12-Mar-54	-	1690	7.5	82	0	-	-	75	-	280	-	300	300	-	-	-	1080	-	-	-	-
333627114420001	006S022E32K001S	33.60752438	-114.700793	362.8	464	15-Jul-54	-	1670		100	M	-	-	70	-	280	-	300	-	-	-	-	1180	-	-	-	-
333627114420001	006S022E32K001S	33.60752438	-114.700793	362.8	464	13-Feb-59	-	2700	7.9	100	0	-	-	140	-	460	-	410	670	-	-	-	1970	-	-	-	-
333627114420001	006S022E32K001S	33.60752438	-114.700793	362.8	464	23-Sep-59	-	2480	8	100	0	-	-	120	-	420	-	380	580	-	-	-	1630	-	-	-	-
333627114420001	006S022E32K001S	33.60752438	-114.700793	362.8	464	23-May-61	-	1960	8.2	86	0	-	220	62	17	320	-	330	370	-	24	-	1200	-	-	-	1180
333627114420001	006S022E32K001S	33.60752438	-114.700793	362.8	464	04-Dec-61	-	2230		100	0	-	-	100	-	370	-	360	460	1.8	-	-	1410	-	-	-	-
333627114420001	006S022E32K001S	33.60752438	-114.700793	362.8	464	14-May-64	-	2000	8	96	0	-	280	86	16	340	5.5	370	400	2	22	-	1440	-	-	-	1290
333627114420001	006S022E32K001S	33.60752438	-114.700793	362.8	464	20-May-05	-	2220	7.9	100	0	-	290	84	18	360	5	380	440	2.3	-	-	1500	-	-	-	1340
333630114400101	006S022E34L001S	33.6083577	-114.6677365	330	360	25-May-61	-	2220	7.8	270	0	-	310	81	26	370	4.8	370	350	0.6	16	-	-	0	-	-	1350
333633114391001	006S022E35M001S	33.60919106	-114.6535694	260	310	07-Feb-62	20	1490	8	250	0	-	220	57	20	-	-	200	180	-	8	-	-	-	-	-	797
333636114345501	006S023E33M001S	33.60983003	-114.5825673	270	100	16-Jun-58	23.9	-	7.7	230	0	-	250	70	17	96	0	110	99	0.2	-	-	-	-	100	-	505
333636114345501	006S023E33M001S	33.60983003	-114.5825673	270	100	07-Feb-62	23.9	1010	7.7	250	0	-	270	78	19	-	-	120	160	-	11	-	-	-	-	-	634
333636114535601	006S020E33C001S	33.61002387	-114.899688	-	-	19-Apr-79	-	-	-	-	-	-	170	67	0.6	800	16	950	450	6.3	38	-	-	-	-	-	2350
333637114343401	006S023E33K001S	33.61030225	-114.5769005	267	408	07-Feb-62	23.9	874	8	230	0	-	230	63	17	-	-	93	92	-	11	-	-	-	-	-	478
333639114363901	006S023E31G002S	33.61085775	-114.6116238	265	135	13-Sep-51	-	2140	7.3	430	0	-	630	170	49	240	-	190	560	-	-	-	270	-	-	-	-
333647114421401	006S022E32F001S	33.61307978	-114.704682	388.5	230	24-Sep-59	-	1360	7.8	110	0	-	-	34	-	250	-	210	230	-	-	-	1280	-	-	-	-
333647114421401	006S022E32F001S	33.61307978	-114.704682	388.5	230	23-May-61	-	1340	8.1	120	0	-	100	24	11	240	3.8	210	220	2.5	32	-	-	240	-	-	813
333650114343501	006S023E33G001S	33.61424659	-114.5772339	270	600	07-Feb-62	24.4	997	7.7	250	0	-	270	80	17	-	-	120	160		12	-	-	-	-	-	621
333702114361601	006S023E32D001S	33.61724648	-114.6052348	268	316	23-Oct-62	24.4	1610	7.4	340	0	-	510	140	38	-	-	140	380	0.6	21	-	-	-	-	-	1050
333711114360601	006S023E29N002S	33.6197464	-114.6024569	270	25	23-Oct-56	-	2050	8	210	0	-	-	220	-	220	-	360	320	0.6	-	-	300	-	-	-	-
333716114355801	006S023E29N001S	33.62113527	-114.6002347	270	266	07-Feb-62	20	1480	7.7	290	0	-	500	140	34	-	-	110	450		14	-	-	-	-	-	1060
333729114383801	006S022E26G001S	33.6247462	-114.6446805	260	79	28-Mar-67	21.7	2080	7.7	330	0	-	640	160	60	-	-	190	500	0.8	20	-	-	-	-	-	1790
333729114383802	006S022E26G002S	33.6247462	-114.6446805	260	21	28-Mar-67	21.7	1930	7.5	250	0	-	670	150	74	-	-	180	500	1.3	22	-	-	-	-	-	1180
333736114392501	006S022E26E001S	33.6266906	-114.6577364	270	64	28-Mar-67	23.3	1740	7.8	240	0	-	580	140	59	-	-	210	350	0.8	16	-	-	-	-	-	1020
333736114392502	006S022E26E002S	33.6266906	-114.6577364	270	21	28-Mar-67	24.4	1420	7.4	280	0	-	470	120	41	-	-	110	310	0.7	16	-	-	-	-	-	857
333737114403401	006S022E28G001S	33.62696834	-114.6769037	362	535	09-Feb-66	30.6	1550	7.7	210	0	-	120	38	7.1	-	-	240	230	2	18	-	130	-	-	-	937
333737114415201	006S022E29G001S	33.6269683	-114.698571	392.5	350	08-Jan-47	-	1510	7.7	97	0	-	170	50	11	240	-	260	250	2.2	-	-	1160	-	-	-	-
333808114405701	006S022E21K001S	33.63552644	-114.6832262	375.3	323	-	-	1500	7.6	140	0	-	150	44	10	260	2	270	200	3.6	-	-	900	40	0	-	859
333836114405801	006S022E21B001S	33.64343179	-114.6837652	373.9	378	19-Sep-66	-	1450	7.8	180	0	-	150	50	7	240	6	230	210	2.7	-	-	1200	40	0	-	835
333845114394901	006S022E22B001S	33.64585675	-114.6644035	367	372	28-Apr-66	-	1300	8.3	200	0	-	62	18	4	290	5	200	200	0.2	-	-	-	40	0	-	816
333846114413201	006S022E20A001S	33.64613448	-114.6930155	395.79	250	15-Jun-67	31.1	1510	8	76	0	-	180	55	10	-	-	270	210	1.8	30	-	-	-	-	-	838
333847114375301	006S022E13Q001S	33.64641234	-114.6321804	268	116	23-Mar-67	22.2	1450	7.5	320	0	-	430	110	39	-	-	140	260	0.5	22	-	-	-	-	-	867
333847114375302	006S022E13Q002S	33.64641234	-114.6321804	268	22	24-Mar-67	21.1	2630	7.7	300	0	-	600	130	69	-	-	210	800	1.3	20	-	-	-	-	-	1730
333858114394901	006S022E15Q001S	33.64949555	-114.6645897	372.54	585	07-Sep-63	32.8	1390	8	200	0	-	66	22	27	-	-	210	180	3.2	14	-	-	-	-	-	796
333858114394901	006S022E15Q001S	33.64949555	-114.6645897	372.54	585	16-Sep-63	33.3	1320	7.9	240	0	-	58	23	0.1	260	-	180	150	2.3	17	-	-	-	-	-	752
333905114385801	006S022E14L001S	33.65141219	-114.6502365	395	94	31-Mar-67	24.4	2600	7.7	300	0	-	580	140	59	-	-	350	500	1	24	-	-	-	-	-	1540
333905114385802	006S022E14L002S	33.65141219	-114.6502365	295	34	31-Mar-67	23.9	2590	7.7	300	0	-	580	130	60	-	-	360	500	0.9	22	-	-	-	-	-	1540
333911114402701	006S022E15M001S	33.65327876	-114.675079	396.6	315	23-Nov-59	-	1370	8	200	0	-	120	32	9.8	240	-	210	190	3.2	-	-	570	-	-	-	-
333911114402701	006S022E15M001S	33.65327876	-114.675079	396.6	315	06-Feb-62	20	1440	8	200	0	-	120	35	8	-	-	220	220	-	10	-	-	-	-	-	863
333911114402701	006S022E15M001S	33.65327876	-114.675079	396.6	315	27-Mar-62	-	1380		200	0	-	120	34	8.8	250	-	220	190	3.5	-	-	560	-	-	-	-
333911114402701	006S022E15M001S	33.65327876	-114.675079	396.6	315	20-Jun-62	26.7	1400	7.4	190	0	-	120	33	10	-	-	220	190	3.8	20	-	-	-	-	-	820
333911114402701	006S022E15M001S	33.65327876	-114.675079	396.6	315	12-Jun-63	-	1400	8.1	200	0	-	120	35	8.9	-	-	220	190	-	19	-	450	-	-	-	-
333912114420501	006S022E17L002S	33.6533565	-114.7021825	397	323	09-Sep-66	-	2350	7.5	95	0	-	430	160	10	320	10	320	600	2	-	-	1500	40	0	-	1470
333912114421601	006S022E17L001S	33.65335649	-114.7052382	400	445	01-Apr-66	-	2060	7.7	67	0	-	350	120	10	300	8	380	400	-	-	-	1400	-	-	-	1250
333912114424501	006S022E18J001S	33.65335648	-114.713294	408	302	-	-	2950	7.6	67	0	-	720	260	14	360	12	480	720	1.8	-	-	2000	300	0	-	1880
333927114423501	006S022E18A001S	33.6574119	-114.7102356	406.88	298	-	-	2000	7.7	61	0	-	400	140	12	320	9	370	500	1.6	-	-	1200	40	0	-	1380
333939114382801	006S022E11R001S	33.6608564	-114.641903	276	77	27-Mar-67	24.4	2420	7.7	290	0	-	580	140	56	-	-	360	450	0.9	21	-	-	-	-	-	1470
333939114382802	006S022E11R002S	33.6608564	-114.641903	276	21	21-Mar-67	24.4	2400	7.5	440	0	-	660	120	84	-	-	200	580	0.9	39	-	-	-	-	-	1510
333939114405801	006S022E09Q001S	33.6608563	-114.683571	403	302	-	-	1700	7.4	82	0	-	270	84	14	260	6	390	220	3.4		-	1600	40	0	-	1020
333939114411501	006S022E09P001S	33.66108687	-114.6883017	399.64	252	13-Jun-67	32.2	2920	7.5	34	0	-	430	150	9.4	-	-	580	480	-	16	-	-	-	-	-	1670
333959114375901	006S022E12L002S	33.66673403	-114.633575	279.57	442	22-Jan-62	-	966	8.1	220	0	-	170	45	13	150	-	120	120	0.9	-	-	120	-	-	-	-
333959114375901	006S022E12L002S	33.66673403	-114.633575	279.57	442	22-May-64	-	980	8.1	230	0	-	170	50	11	140	-	120	110	0.8	-	-	80	-	-	-	-
334004114410201	006S022E09L001S	33.66780059	-114.6846822	402	332	-	-	1520	7.4	100	0	-	220	76	7	240	2	290	230	2.2	-	-	800	100	0	-	897
334004114411701	006S022E09M001S	33.66780058	-114.688849	404	292	-	-	1800	7.6	100	0	-	230	84	5	280	14	370	250	2.1	-	-	900	160	0	-	1060
334004114413301	006S022E08J001S	33.66780057	-114.6932936	408	302	-	-	1700	7.5	82	0	-	270	84	14	250	12	360	250	2	-	-	1100	60	0	-	1010
334005114382901	006S022E11H001S	33.6680062	-114.6421365	407.97	235	23-Oct-56	-	1600	7.8	330	0	-	-	220	-	140	-	120	430	-	-	-	160	-	-	-	-
334005114382901	006S022E11H001S	33.6680062	-114.6421365	407.97	235	26-Mar-63	-	1870		230	0	-	-	170	-	250	-	310	300	-	-	-	390	-	-	-	-
334005114382901	006S022E11H001S	33.6680062	-114.6421365	407.97	235	19-Jun-64	27.2	2060	7.2	220	0	-	430	110	39	-	-	330	310	1	22	-	200	-	-	-	1180
334005114400501	006S022E08L001S	33.66807838	-114.6688484	408	300	09-Sep-66	-	2600	7.6	85	0	-	640	210	29	310	12	440	600	2.1	-	-	2000	400	0	-	1650
334009114381401	006S022E12E001S	33.6691673	-114.6381058	410.54	230	16-Jun-58	-	1940	7.7	260	0	-	360	84	36	280	-	280	340	0.9	-	-	400	-	-	-	-
334009114381401	006S022E12E001S	33.6691673	-114.6381058	410.54	230	23-Sep-60	-	2060	8.2	240	0	-	390	94	37	300	-	310	380	0.9	-	-	480	-	-	-	-
334009114381401	006S022E12E001S	33.6691673	-114.6381058	410.54	230	22-Oct-60	-	2300	-	240	0	-	-	170	-	330	-	370	-	-	-	-	720	-	-	-	1370
334014114380301	006S022E12F001S	33.67055338	-114.6352502	409.64	252	29-Aug-52	-	2420	-	200	M	-	-	-	-	380	-	410	-	-	-	-	830	-	-	-	-
334014114380301	006S022E12F001S	33.67055338	-114.6352502	409.64	252	22-Oct-60	-	2300	-	240	0	-	-	170	-	330	-	370	-	-	-	-	720	-	-	-	-
334014114380301	006S022E12F001S	33.67055338	-114.6352502	409.64	252	05-Jan-61	-	-	8	260	0	-	400	100	35	310	4.8	320	400	0.8	-	-		-	0	-	1300
334016114394501	006S022E10H001S	33.67146164	-114.6631066	404.21	304	-	-	1400	7.7	210	0	-	150	32	17	240	8	220	160	5	-	-	700	140	-	-	786
334031114390301	006S022E02P001S	33.6753421	-114.6513757	400.85	250	14-May-64	-	1150	8.2	180	0	-	76	21	6	210	4	180	120	-	-	-	M	-	-	-	640
334031114390301	006S022E02P001S	33.6753421	-114.6513757	400.85	250	01-Jul-64	-	1190	8.3	200	0	-	-	-	29	230	-	170	150	-	-	-	220	-	-	-	-
334031114390301	006S022E02P001S	33.6753421	-114.6513757	400.85	250	10-Feb-66	-	1220	8.2	210	0	-	64	16	5.8	-	-	180	150	1.7	15	-	340	-	-	-	711
334034114382501	006S022E01N001S	33.67613378	-114.6410699	405	426	09-Feb-66	-	1210	7.7	240	0	-	86	20	8.8	-	-	160	150	1.2	16	-		-	-	-	-
334057114375901	006S022E01F001S	33.68260584	-114.6335253	406.54	350	10-Nov-66	-	1440	8	230	0	-	370	110	24	180	8	240	210	-	-	-	100	-	-	-	885
334120114400001	006S022E03B001S	33.68903339	-114.6676125	420	414	27-Oct-66	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1400	-	-	-	-
334128114333301	005S023E34Q001S	33.6911335	-114.5599565	280	266	15-Feb-63	-	1330	8	300	0	-	480	140	30	-	-	130	290	-	17	-	40	-	-	-	868
334147114403901	005S022E33J001S	33.69641096	-114.6782935	438	380	16-Mar-62	31.1	2090	7.2	58	0	-	330	130	2.1	-	-	400	380	2.2	29	-	-	-	-	-	-

Table B-1
WATER CHEMISTRY DATA
FOR PALO VERDE Valley
PALO VERDE SOLAR I, LLC
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

WELL DATA [1]						WATER CHEMISTRY																					
STATE WELL NUMBER (DWR)	**STATE WELL NAME (USGS)**	**LATITUDE**	**LONGITUDE**	**Ground Surface Elevation**	**Well Depth**	**Sample Date Mo/Yr**	**Temperature, degrees Celsius**	**Specific conductance, microsiemens per cm at 25 degrees Celsius**	**pH, standard units**	**Bicarbonate, mg/L**	**Carbonate, mg/L**	**Nitrate plus nitrite as nitrogen mg/L**	**Hardness as calcium carbonate mg/L**	**Calcium, mg/L**	**Magnesium, mg/L**	**Sodium, mg/L**	**Potassium, mg/L**	**Chloride, mg/L**	**Sulfate, mg/L**	**Fluoride, mg/L**	**Silica as SiO2 mg/L**	**Arsenic, ug/L**	**Boron, ug/L**	**Iron, ug/L**	**Manganese, ug/L**	**Selenium, ug/L**	**Total Dissolved Solids (TDS) mg/L**
334147114403901	005S022E33J001S	33.69641096	-114.6782935	438	380	16-Apr-62	-	2080	7.6	49	0	-	310	120	2.7	300	-	380	380	-	-	-	1280	-	-	-	-
334147114403901	005S022E33J001S	33.69641096	-114.6782935	438	380	26-Oct-62	-	2200	7.4	50	0	-	340	120	7.4	-	-	400	380	1.7	24	-	-	-	-	-	-
334148114392701	005S022E35M001S	33.69668876	-114.6582929	425	400	27-Jan-64	30.6	1940	7.6	82	0	-	220	84	2.1	-	-	340	340	1.9	19	-	1000	-	-	-	-
334148114392701	005S022E35M001S	33.69668876	-114.6582929	425	400	10-Feb-66	30.6	2160	7.1	64	0	-	260	98	4.7	-	-	410	400	1.6	20	-	-	-	-	-	-
334148114392701	005S022E35M001S	33.69668876	-114.6582929	425	400	21-Jun-66	-	2030		85	M	-	250	95	2.7	330	-	390	350	-	-	-	1060	-	-	-	-
334215114383701	005S022E35A001S	33.70418859	-114.6444037	439.3	450	05-Nov-64	-	2060	8	120	0	-	180	66	3.9	370	6.6	390	330	-	-	-	1060	-	-	-	1230
334215114383701	005S022E35A001S	33.70418859	-114.6444037	439.3	450	10-Feb-66	30.6	2160	7.4	120	0	-	190	63	7.5	-	-	900	350	1.6	18	-	-	-	-	-	-
334301114411301	005S022E28C001S	33.71696595	-114.6877385	485	601	27-Jun-60	-	2980	7.3	21	0	-	640	240	8.9	420	-	400	950	-	-	-	1570	-	-	-	-
334301114411301	005S022E28C001S	33.71696595	-114.6877385	485	601	17-Nov-60	-	3030		20	-	-	-	260	-	420	-	420	-	2.8	-	-	1570	-	-	-	-
334301114411301	005S022E28C001S	33.71696595	-114.6877385	485	601	08-Feb-62	32.2	3160	7.7	22	-	-	680	260	12	-	-	420	1000	-	11	-	-	-	-	-	2190
334301114411301	005S022E28C001S	33.71696595	-114.6877385	485	601	25-Oct-62	32.8	3090	7.7	38	0	-	700	270	8.9	-	-	440	970	-	16	-	-	-	-	-	2160
334302114302801	005S024E30B001S	33.71724406	-114.5085663	289	130	18-Jun-64	22.2	1740	7.7	350	0	-	560	150	42	-	-	130	420	0.5	19	-	-	-	-	-	1100
334302114411401	005S022E28C002S	33.7172437	-114.6880163	485	400	16-Mar-59	-	2940	7.8	21	0	-	710	270	8.1	410	-	390	1000	2.8	-	-	1530	-	-	-	-
334302114411401	005S022E28C002S	33.7172437	-114.6880163	485	400	27-Sep-63	-	3060	7.3	20	0	-	700	260	13	420	-	430	970	-	-	-	1600	-	-	-	-
335217114531301	003S020E33Z001S	33.8714065	-114.8877464	1360	17	03-Nov-17	-	-	-	260	0	-	640	160	56	-	-	380	260	-	47	-	-	300	-	-	-

Notes

mg/L	Milligram per Liter
ug/L	Microgram per Liter
Survey Datum	NAD 83
-	Data not provided
1	Data not provided in the USGS National Water Information System Database - http://:nwis/waterdata.usgs.gov/ and the Department of Water Resources Database - http://wdl.water.ca.gov/gw/ and DWR Bulletin 91-23 (October 1978).

APPENDIX C

COLORADO RIVER GAUGING DATA (USGS)

APPENDIX C
TABLE C-1
SUMMARY OF USGS STREAMSTATS DATABASE
PALO VERDE DAM to CIBOLA GAUGES
BLYTHE SOLAR POWER PROJECT
PALO VERDE I LLC
RIVERSIDE COUNTY, CALIFORNIA

YEAR	SUMMARY FLOW AND SPILL DATA (AF)			DIFFERENCE THROUGH PALO VERDE AND CIBOLA VALLEY (AF)[2]	
	PALO VERDE DAM (1969-1988)	SPILL[1]	COLORADO RIVER BELOW CIBOLA	MONTHLY POSITIVE - LOSING NEGATIVE - GAINING	ANNUAL POSITIVE - LOSING NEGATIVE - GAINING
	9429010		9429300		
1970-1980	467,520	40,008	523,452	-15,924	-159,099
1980-1987	942,451	40,027	997,725	-15,248	-151,148

Note:
1 - Spill recorded at gauging stations: 9429130, 9429155, 9429160, 9429170, 9429180, 9429190, 9429200, 9429210, 9429220, 9429225, 9429320
2 - Annual accounting includes diversion from the Arizona side and spill returns along the western part of the river.
AF - acre-feet

APPENDIX C
TABLE C-2
SUMMARY OF USGS STREAMSTATS DATA
1970-1980
PALO VERDE DAM TO CIBOLA GAUGE
BLYTHE SOLAR POWER PROJECT

YEAR	MONTH	DAY	MONTHLY MEAN VALUE (cfs)															SUMMARY FLOW AND SPILL DATA (AF)			DIFFERENCE THROUGH PALO VERDE VALLEY (AF)	
			DIVERSION PALO VERDE DAM	PALO VERDE DAM (1969-1988)	PALO VERDE DAM (1989-2009)	OLIVE LAKE DRAIN	F-CANAL SPILL	PVID D-10-11-2 SPILL	PVID D-10-11-5 SPILL	PVID D23 Spill Near Blythe, CA	P.V.I.D. D-23-1	PVID C Canal Spill NR Blythe, CA	P.V.I.D. C-28 UPPER SPILL	PALO VERDE OUTFALL DRAIN	PVID ANDERSON DRAIN	PVID C28 LOWER SPILL	COLORADO RIVER BELOW CIBOLA	PALO VERDE DAM (1969-1988)	SPILL	COLORADO RIVER BELOW CIBOLA	MONTHLY POSITIVE - LOSING NEGATIVE - GAINING	ANNUAL [1] POSITIVE - LOSING NEGATIVE - GAINING
		STATION	9429000	9429010	9429100	9429130	9429155	9429160	9429170	9429180	9429190	9429200	9429210	9429220	9429225	9429230	9429300	9429010		9429300		
1970	1	31	624.7	5184	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	6007	318,752	40,775	369,356	-9,829	
1970	2	28	1013	6220	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	6489	345,441	36,829	360,381	21,890	
1970	3	31	1006	8656	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	9482	532,236	40,775	583,025	-10,014	
1970	4	30	1563	10240	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	11370	609,322	39,460	676,562	-27,780	
1970	5	31	1500	8106	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	8958	498,418	40,775	550,806	-11,612	
1970	6	30	1550	8954	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	9703	532,800	39,460	577,368	-5,109	
1970	7	31	1749	9612	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	10370	591,018	40,775	637,626	-5,832	
1970	8	31	1420	7983	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	9369	490,855	40,775	576,077	-44,447	
1970	9	30	1321	6616	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	7566	393,679	39,460	450,208	-17,069	
1970	10	31	988.2	6057	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	7763	372,430	40,775	477,328	-64,123	
1970	11	30	930.5	3972	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	5594	236,350	39,460	332,866	-57,056	
1970	12	31	762.5	4340	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	5461	266,856	40,775	335,784	-28,152	-227,050
1971	1	31	632.8	4741	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	5485	291,513	40,775	337,259	-4,972	
1971	2	28	1109	6578	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	7231	365,323	36,829	401,589	563	
1971	3	31	1223	9605	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	10010	590,588	40,775	615,491	15,873	
1971	4	30	1506	9523	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	10440	566,658	39,460	621,223	-15,105	
1971	5	31	1524	7851	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	8739	482,739	40,775	537,340	-13,826	
1971	6	30	1522	9081	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	10130	540,357	39,460	602,776	-22,960	
1971	7	31	1884	10620	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	11500	652,998	40,775	707,107	-13,334	
1971	8	31	1399	8603	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	10110	528,978	40,775	621,639	-51,887	
1971	9	30	1381	7068	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	8160	420,575	39,460	485,553	-25,519	
1971	10	31	881.5	5113	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	6060	314,386	40,775	372,615	-17,454	
1971	11	30	919.7	4029	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	4942	239,742	39,460	294,069	-14,867	
1971	12	31	879.3	4473	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	5428	275,034	40,775	333,755	-17,945	-149,350
1972	1	31	632	4879	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	5528	299,998	40,775	339,903	870	
1972	2	28	1039	6279	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	6912	348,718	36,829	383,873	1,674	
1972	3	31	1300	9375	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	10020	576,446	40,775	616,105	1,116	
1972	4	30	1607	9964	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	10600	592,899	39,460	630,743	1,615	
1972	5	31	1570	8403	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	9137	516,680	40,775	561,812	-4,357	
1972	6	30	1537	8766	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	9320	521,613	39,460	554,578	6,495	
1972	7	31	1830	10250	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	10820	630,248	40,775	665,295	5,727	
1972	8	31	1530	9085	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	10030	558,615	40,775	616,720	-17,331	
1972	9	30	1310	7487	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	8258	445,507	39,460	491,385	-6,418	
1972	10	31	542.3	3295	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	4517	202,602	40,775	277,739	-34,363	
1972	11	30	849.5	3623	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	4691	215,583	39,460	279,134	-24,091	
1972	12	31	904.8	4802	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	5649	295,263	40,775	347,343	-11,305	-49,077
1973	1	31	607.6	5085	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	5739	312,664	40,775	352,877	562	
1973	2	28	716.9	4932	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	5690	273,909	36,829	316,006	-5,268	
1973	3	31	975.5	8385	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	8680	515,573	40,775	533,712	22,636	
1973	4	30	1713	10560	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	11080	628,363	39,460	659,305	8,518	
1973	5	31	1791	8414	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	9204	517,356	40,775	565,932	-7,800	
1973	6	30	1721	8111	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	8940	482,638	39,460	531,967	-9,869	
1973	7	31	1917	9917	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	10470	609,772	40,775	643,775	6,773	
1973	8	31	1702	8685	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	9596	534,020	40,775	590,035	-15,240	
1973	9	30	1555	7918	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	8944	471,153	39,460	532,205	-21,591	
1973	10	31	1002	6124	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	7445	376,550	40,775	457,775	-40,450	
1973	11	30	809	4136	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	5158	246,109	39,460	306,922	-21,353	
1973	12	31	712.9	4417	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	5085	271,591	40,775	312,664	-299	-60,481
1974	1	31	596	3408	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	4077	209,550	40,775	250,685	-360	
1974	2	28	1174	6683	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	7188	371,155	36,829	399,201	8,783	
1974	3	31	1287	8860	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	9535	544,780	40,775	586,284	-729	
1974	4	30	1644	11030	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	11870	656,330	39,460	706,314	-10,524	
1974	5	31	1636	8729	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	10030	536,725	40,775	616,720	-39,220	
1974	6	30	1726	10120	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	10950	602,181	39,460	651,570	-9,929	
1974	7	31	1771	11130	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	11950	684,357	40,775	734,776	-9,645	
1974	8	31	1636	10640	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	11530	654,228	40,775	708,952	-13,949	
1974	9	30	1550	8332	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	9297	495,788	39,460	553,210	-17,962	
1974	10	31	882	5405	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	6583	332,340	40,775	404,773	-31,657	
1974	11	30	841.5	3868	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	4660	230,162	39,460	277,289	-7,667	
1974	12	31	714.6	4106	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	4806	252,468	40,775	295,509	-2,266	-104,491
1975	1	31	875.3	5134	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	5770	315,677	40,775	354,783	1,669	
1975	2	28	1083	6306	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	6851	350,217	36,829	380,485	6,561	
1975	3	31	1276	8749	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	9299	537,955	40,775	571,773	6,957	
1975	4	30	1532	10200	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	11020	606,942	39,460	655,735	-9,333	
1975	5	31	1745	9367	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	10270	575,954	40,775	631,477	-14,748	
1975	6	30	1416	8767	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	9474	521,672	39,460	563,742	-2,610	
1975	7	31	1690	10090	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	10960	620,410	40,775	673,904	-12,719	
1975	8	31	1656	9833	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	10750	604,607	40,775	660,991	-15,609	
1975	9	30	1479	8592	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	9374	511,259	39,460	557,791	-7,072	
1975	10	31	1097	6208	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	7233	381,715	40,775	444,740	-22,250	
1975	11	30	876.2	4634	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	5600	275,742	39,460	333,223	-18,021	
1975	12	31	737.5	4806	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	5694	295,509	40,775	350,110	-13,826	-64,401

APPENDIX C
TABLE C-2
SUMMARY OF USGS STREAMSTATS DATA
1970-1980
PALO VERDE DAM TO CIBOLA GAUGE
BLYTHE SOLAR POWER PROJECT

YEAR	MONTH	DAY	MONTHLY MEAN VALUE (cfs)															SUMMARY FLOW AND SPILL DATA (AF)			DIFFERENCE THROUGH PALO VERDE VALLEY (AF)	
			DIVERSION PALO VERDE DAM	PALO VERDE DAM (1969-1988)	PALO VERDE DAM (1989-2009)	OLIVE LAKE DRAIN	F-CANAL SPILL	PVID D-10-11-2 SPILL	PVID D-10-11-5 SPILL	PVID D23 Spill Near Blythe, CA	P.V.I.D. D-23-1	PVID C Canal Spill NR Blythe, CA	P.V.I.D. C-28 UPPER SPILL	PALO VERDE OUTFALL DRAIN	PVID ANDERSON DRAIN	PVID C28 LOWER SPILL	COLORADO RIVER BELOW CIBOLA	PALO VERDE DAM (1969-1988)	SPILL	COLORADO RIVER BELOW CIBOLA	MONTHLY POSITIVE - LOSING NEGATIVE - GAINING	ANNUAL [1] POSITIVE - LOSING NEGATIVE - GAINING
		STATION	9429000	9429010	9429100	9429130	9429155	9429160	9429170	9429180	9429190	9429200	9429210	9429220	9429225	9429230	9429300	9429010		9429300		
1976	1	31	634.5	4960	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	5634	304,978	40,775	346,421	-667	
1976	2	28	724.7	5192	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	5678	288,349	36,829	315,340	9,838	
1976	3	31	1428	10560	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	10940	649,309	40,775	672,674	17,410	
1976	4	30	1533	10280	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	11570	611,702	39,460	688,462	-37,300	
1976	5	31	1670	8606	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	9728	529,162	40,775	598,151	-28,214	
1976	6	30	1697	8548	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	9703	508,641	39,460	577,368	-29,267	
1976	7	31	1850	9650	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	10550	593,355	40,775	648,694	-14,564	
1976	8	31	1778	10180	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	11160	625,943	40,775	686,201	-19,483	
1976	9	30	1084	5477	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	7215	325,904	39,460	429,322	-63,958	
1976	10	31	829.3	4699	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	5585	288,930	40,775	343,408	-13,703	
1976	11	30	857.3	3334	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	4129	198,387	39,460	245,692	-7,846	
1976	12	31	675.6	4916	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	5705	302,273	40,775	350,787	-7,738	-160,932
1977	1	31	656.6	3556	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	4307	218,650	40,775	264,827	-5,402	
1977	2	28	1070	6660	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	7340	369,877	36,829	407,643	-936	
1977	3	31	1257	8517	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	9438	523,690	40,775	580,320	-15,855	
1977	4	30	1614	10470	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	11400	623,008	39,460	678,347	-15,879	
1977	5	31	1563	7745	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	8786	476,221	40,775	540,230	-23,233	
1977	6	30	1863	9263	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	10190	551,186	39,460	606,347	-15,700	
1977	7	31	2068	11820	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	12450	726,783	40,775	765,520	2,038	
1977	8	31	1589	8532	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	9852	524,612	40,775	605,775	-40,388	
1977	9	30	1185	5865	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	7305	348,992	39,460	434,677	-46,226	
1977	10	31	831.4	4446	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	5283	273,374	40,775	324,839	-10,690	
1977	11	30	847.7	3765	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	4788	224,033	39,460	284,906	-21,413	
1977	12	31	736.2	4158	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	5187	255,665	40,775	318,936	-22,496	-175,209
1978	1	31	331.7	2011	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	2908	123,651	40,775	178,806	-14,379	
1978	2	28	909.4	5840	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	6201	324,337	36,829	344,386	16,780	
1978	3	31	1301	8592	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	9162	528,301	40,775	563,349	5,727	
1978	4	30	1830	10920	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	11790	649,785	39,460	701,553	-12,309	
1978	5	31	1563	8365	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	9273	514,343	40,775	570,174	-15,056	
1978	6	30	1793	9414	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	10230	560,172	39,460	608,727	-9,095	
1978	7	31	1987	10930	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	11920	672,059	40,775	732,932	-20,097	
1978	8	31	1572	9706	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	10870	596,798	40,775	668,370	-30,796	
1978	9	30	1213	7161	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	8400	426,109	39,460	499,834	-34,266	
1978	10	31	829.1	4719	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	6052	290,160	40,775	372,123	-41,188	
1978	11	30	791.1	3765	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	4758	224,033	39,460	283,120	-19,628	
1978	12	31	587.1	3631	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	4522	223,261	40,775	278,047	-14,010	-155,137
1979	1	31	489.5	2197	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	3001	135,088	40,775	184,524	-8,661	
1979	2	28	962.9	4456	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	4896	247,474	36,829	271,910	12,393	
1979	3	31	1327	6685	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	7615	411,044	40,775	468,228	-16,408	
1979	4	30	1779	9180	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	10600	546,248	39,460	630,743	-45,036	
1979	5	31	1743	9310	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	10520	572,449	40,775	646,849	-33,625	
1979	6	30	1812	10380	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	11450	617,653	39,460	681,322	-24,210	
1979	7	31	1851	11530	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	12830	708,952	40,775	788,885	-39,159	
1979	8	31	1626	10260	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	11620	630,862	40,775	714,486	-42,848	
1979	9	30	1593	9149	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	10340	544,403	39,460	615,272	-31,410	
1979	10	31	930.7	6924	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	8089	425,740	40,775	497,373	-30,858	
1979	11	30	843.6	5136	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	6129	305,613	39,460	364,701	-19,628	
1979	12	31	808.9	4507	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	5488	277,124	40,775	337,444	-19,544	-271,403
1980	1	31	516.5	4470	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	5276	274,849	40,775	324,408	-8,784	
1980	2	28	686.2	5401	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	5971	299,956	36,829	331,612	5,173	
1980	3	31	1351	13910	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	14490	855,292	40,775	890,955	5,112	
1980	4	30	1790	15230	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	16450	906,247	39,460	978,842	-33,135	
1980	5	31	1395	12510	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	13890	769,209	40,775	854,062	-44,078	
1980	6	30	1661	15150	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	16540	901,487	39,460	984,198	-43,251	
1980	7	31	1892	15820	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	17600	972,733	40,775	1,082,181	-68,673	
1980	8	31	1746	14850	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	16440	913,090	40,775	1,010,856	-56,990	
1980	9	30	1508	13420	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	14560	798,545	39,460	866,380	-28,375	
1980	10	31	948.7	12240	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	13370	752,608	40,775	822,089	-28,706	
1980	11	30	776.2	11380	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	12470	677,157	39,460	742,016	-25,400	
1980	12	31	699.2	10150	--	8.9	16.5	2.6	8.5	19.9	6.0	33.8	1.3	551	0.3	14.7	11390	624,099	40,775	700,343	-35,469	-332,560
AVERAGE			**1,254**	**7,739**	**--**	**8.9**	**16.5**	**2.6**	**8.5**	**19.9**	**6.0**	**33.8**	**1.3**	**551**	**0.34**	**14.7**	**8,664**	**467,520**	**40,008**	**523,452**	**-15,924**	**-159,099**

NOTES

1 **INCLUDES DIVERSIONS IN ARIZONA FROM ANNUAL INFORMAITON PROVIDED BY THE USBR IN THEIR ACCOUNTING AND COMPILATION OF RECORDS REPORTING (1972-1980). ANY YEARS BEYOND THIS PERIOD THE AVERAGE FOR 1972-1980 WAS APPLIED.**

APPENDIX C
TABLE C-3
SUMMARY OF USGS STREAMSTATS DATABASE
1980-1987
PALO VERDE DAM TO CIBOLA GAUGE
BLYTHE SOLAR POWER PROJECT

YEAR	MONTH	DAY	MONTHLY MEAN VALUE (cfs)															SUMMARY FLOW AND SPILL DATA (AF)			DIFFERENCE THROUGH PALO VERDE VALLEY (AF)	
			DIVERSION PALO VERDE DAM	PALO VERDE DAM (1969-1988)	PALO VERDE DAM (1989-2009)	OLIVE LAKE DRAIN	F-CANAL SPILL	PVID D-10-11-2 SPILL	PVID D-10-11-5 SPILL	PVID D23 Spill Near Blythe, CA	P.V.I.D. D-23-1	PVID C Canal Spill NR Blythe, CA	P.V.I.D. C-28 UPPER SPILL	PALO VERDE OUTFALL DRAIN	PVID ANDERSON DRAIN	PVID C28 LOWER SPILL	COLORADO RIVER BELOW CIBOLA	PALO VERDE DAM (1969-1988)	SPILL	COLORADO RIVER BELOW CIBOLA	MONTHLY POSITIVE - LOSING NEGATIVE - GAINING	ANNUAL POSITIVE - LOSING NEGATIVE - GAINING
		STATION	9429000	9429010	9429100	9429130	9429155	9429160	9429170	9429180	9429190	9429200	9429210	9429220	9429225	9429230	9429300	9429010		9429300		
1980	1	31	517	4,470	--	2.7	13.8	0.6	7.3	20.5	5.5	19.3	1.1	409	--	7.6	5,276	274,849	29,981	324,408	-19,578	
1980	2	28	686	5,401	--	3.2	22.0	1.9	10.8	27.9	5.8	51.6	2.2	432	--	18.0	5,971	299,956	31,936	331,612	280	
1980	3	31	1,351	13,910	--	2.3	7.8	1.4	6.4	26.4	2.9	34.6	7.4	463	--	12.6	14,490	855,292	34,734	890,955	-929	
1980	4	30	1,790	15,230	--	9.8	15.3	2.5	6.8	22.8	7.0	59.2	4.5	587	--	12.3	16,450	906,247	43,272	978,842	-29,323	
1980	5	31	1,395	12,510	--	12.4	12.0	2.6	8.9	22.2	6.6	49.6	2.3	629	--	14.0	13,890	769,209	46,731	854,062	-38,122	
1980	6	30	1,661	15,150	--	14.7	8.1	1.7	4.5	18.1	4.7	34.4	1.2	631	--	9.2	16,540	901,487	43,312	984,198	-39,399	
1980	7	31	1,892	15,820	--	12.6	20.4	3.1	6.1	8.8	2.5	24.0	1.6	652	--	12.8	17,600	972,733	45,753	1,082,181	-63,695	
1980	8	31	1,746	14,850	--	12.5	29.5	1.3	6.9	14.3	3.5	29.1	2.0	692	--	10.5	16,440	913,090	49,279	1,010,856	-48,486	
1980	9	30	1,508	13,420	--	11.4	15.5	0.2	8.3	10.5	2.4	48.4	1.9	693	--	11.1	14,560	798,545	47,752	866,380	-20,082	
1980	10	31	949	12,240	--	11.6	24.1	2.9	14.4	18.3	8.2	44.0	2.8	615	0.0	10.7	13,370	752,608	46,250	822,089	-23,231	
1980	11	30	776	11,380	--	5.3	14.8	4.3	12.5	19.1	9.7	51.8	1.5	539	0.0	15.5	12,470	677,157	40,087	742,016	-24,773	
1980	12	31	699	10,150	--	2.4	15.2	2.9	13.4	29.2	8.6	43.7	1.0	462	0.0	16.6	11,390	624,099	36,589	700,343	-39,656	-316,979
1981	1	31	673	6,936	--	2.3	11.5	0.3	6.5	19.9	5.1	30.0	1.6	437	0.0	11.3	8,064	426,478	32,296	495,836	-37,062	
1981	2	28	1,223	6,133	--	3.0	17.9	1.3	8.3	15.8	2.8	37.8	4.0	474	0.0	16.3	6,661	340,609	32,279	369,933	2,956	
1981	3	31	1,176	9,054	--	4.6	22.0	2.2	13.4	10.7	6.3	42.7	2.3	489	0.0	11.1	10,050	556,708	37,124	617,950	-24,117	
1981	4	30	1,747	11,330	--	11.2	9.4	1.0	6.0	10.3	6.4	34.0	4.1	580	0.0	10.9	12,260	674,181	40,080	729,520	-15,259	
1981	5	31	1,709	8,259	--	13.6	17.4	0.3	9.3	14.4	5.4	34.5	3.3	633	0.3	11.2	9,290	507,826	45,655	571,219	-17,738	
1981	6	30	2,031	10,230	--	12.4	15.0	0.2	8.0	17.7	1.8	24.4	1.3	648	0.5	7.0	11,170	608,727	43,806	664,661	-12,128	
1981	7	31	2,117	11,350	--	13.5	10.4	0.8	3.9	10.7	0.4	22.8	0.8	666	0.5	3.5	12,400	697,884	45,104	762,446	-19,458	
1981	8	31	2,057	10,790	--	13.6	9.2	0.6	4.3	5.6	1.1	36.3	2.2	667	0.0	4.2	11,800	663,451	45,719	725,553	-16,383	
1981	9	30	1,725	7,218	--	14.9	6.7	0.5	1.3	10.2	3.2	49.5	2.4	725	0.1	3.8	8,411	429,501	48,677	500,489	-22,312	
1981	10	31	875	4,327	--	10.3	11.4	1.3	11.0	8.7	7.9	41.0	2.0	635	0.2	14.0	5,403	266,057	45,679	332,217	-20,482	
1981	11	30	691	3,338	--	2.5	19.9	1.8	14.8	21.3	8.4	43.7	4.2	530	0.1	15.1	4,531	198,625	39,363	269,613	-31,625	
1981	12	31	653	3,914	--	3.4	13.3	5.5	14.6	21.1	5.5	33.2	3.5	462	0.2	16.0	4,524	240,662	35,574	278,170	-1,934	-183,460
1982	1	31	609	4,628	--	2.6	8.9	1.7	11.1	13.2	4.7	20.5	5.4	388	0.0	11.9	5,363	284,564	28,796	329,758	-16,397	
1982	2	28	1,115	6,989	--	7.1	12.8	1.7	14.1	11.8	3.9	27.6	1.2	431	0.2	17.8	6,819	388,149	29,408	378,708	38,849	
1982	3	31	1,250	8,665	--	10.2	16.0	2.3	11.1	18.5	4.9	37.7	2.1	495	0.1	13.4	8,659	532,790	37,604	532,421	37,973	
1982	4	30	1,820	11,320	--	13.0	17.6	1.0	8.1	9.2	4.1	40.9	2.0	605	0.4	11.3	11,430	673,586	42,402	680,132	35,856	
1982	5	31	1,629	8,076	--	13.9	12.5	0.4	7.8	11.9	5.2	40.9	2.7	632	0.5	16.6	8,579	496,574	45,735	527,502	14,806	
1982	6	30	1,796	7,770	--	13.3	11.6	0.4	11.6	13.9	1.8	31.4	3.8	622	0.5	14.2	8,289	462,347	43,119	493,229	12,236	
1982	7	31	1,985	9,330	--	12.3	8.0	0.1	6.9	10.8	1.0	21.4	1.6	654	0.5	8.5	9,711	573,679	44,573	597,106	21,146	
1982	8	31	1,741	8,165	--	15.2	14.5	0.3	13.1	10.7	1.2	28.1	1.6	723	0.3	13.7	8,966	502,046	50,530	551,298	1,279	
1982	9	30	1,618	6,010	--	18.4	17.5	1.1	8.4	13.1	3.4	25.7	1.6	680	0.5	11.5	6,607	357,620	46,477	393,144	10,954	
1982	10	31	917	4,911	--	16.3	12.5	2.0	7.8	12.1	4.8	39.0	6.2	594	0.5	12.0	6,131	301,965	43,457	376,980	-31,558	
1982	11	30	635	3,113	--	14.3	19.9	1.7	8.6	13.1	9.9	31.7	4.3	489	0.5	19.9	4,271	185,236	36,451	254,142	-32,455	
1982	12	31	503	3,313	--	9.3	29.7	1.1	8.2	35.7	2.2	52.9	0.3	439	0.5	14.4	4,060	203,708	36,502	249,640	-9,429	115,342
1983	1	31	553	14,770	--	3.7	14.6	0.7	6.5	17.1	3.4	31.7	0.9	399	0.5	11.4	14,750	908,171	30,086	906,942	31,315	
1983	2	28	816	6,029	--	7.6	20.5	3.1	8.5	22.5	7.8	23.4	1.3	396	0.5	13.5	8,014	334,834	28,030	445,075	-82,211	
1983	3	31	1,051	7,939	--	7.2	21.6	2.4	11.1	15.6	2.5	28.2	1.5	451	0.5	12.6	8,335	488,150	34,095	512,499	9,746	
1983	4	30	1,427	14,210	--	8.9	12.1	0.7	9.2	14.6	3.8	40.3	1.1	534	0.5	12.7	14,600	845,553	37,926	868,760	14,719	
1983	5	31	1,388	14,940	--	13.9	12.0	0.1	7.3	11.6	7.2	35.3	0.8	545	0.5	17.8	16,390	918,624	40,056	1,007,781	-49,101	
1983	6	30	1,553	22,930	--	13.8	11.4	0.2	10.7	15.4	5.0	34.7	2.0	576	0.5	13.7	23,100	1,364,429	40,679	1,374,545	30,563	
1983	7	31	1,543	35,730	--	14.5	16.5	0.6	7.3	13.2	2.8	35.8	0.2	573	0.5	15.2	35,970	2,196,951	41,773	2,211,708	27,016	
1983	8	31	1,171	37,120	--	14.4	21.2	1.1	7.1	26.4	2.4	38.9	0.8	635	0.5	12.8	36,850	2,282,418	46,743	2,265,817	63,345	
1983	9	30	1,355	34,490	--	13.1	38.4	4.8	9.1	29.1	6.8	32.3	0.1	639	0.5	15.9	34,830	2,052,296	46,967	2,072,528	26,735	
1983	10	31	771	34,240	--	13.4	18.6	8.0	10.0	28.8	3.6	37.5	0.4	570	0.5	14.6	34,290	2,105,334	43,382	2,108,409	40,307	
1983	11	30	740	25,830	--	9.1	14.9	2.4	6.8	18.0	4.0	31.0	0.0	521	0.5	14.6	26,780	1,536,991	37,018	1,593,520	-19,511	
1983	12	31	670	23,060	--	4.9	19.5	6.5	13.9	28.6	6.5	32.2	0.0	478	0.5	13.6	24,230	1,417,903	37,116	1,489,844	-34,824	90,182

APPENDIX C
TABLE C-3
SUMMARY OF USGS STREAMSTATS DATABASE
1980-1987
PALO VERDE DAM TO CIBOLA GAUGE
BLYTHE SOLAR POWER PROJECT

YEAR	MONTH	DAY	MONTHLY MEAN VALUE (cfs)															SUMMARY FLOW AND SPILL DATA (AF)			DIFFERENCE THROUGH PALO VERDE VALLEY (AF)	
			DIVERSION PALO VERDE DAM	PALO VERDE DAM (1969-1988)	PALO VERDE DAM (1989-2009)	OLIVE LAKE DRAIN	F-CANAL SPILL	PVID D-10-11-2 SPILL	PVID D-10-11-5 SPILL	PVID D23 Spill Near Blythe, CA	P.V.I.D. D-23-1	PVID C Canal Spill NR Blythe, CA	P.V.I.D. C-28 UPPER SPILL	PALO VERDE OUTFALL DRAIN	PVID ANDERSON DRAIN	PVID C28 LOWER SPILL	COLORADO RIVER BELOW CIBOLA	PALO VERDE DAM (1969-1988)	SPILL	COLORADO RIVER BELOW CIBOLA	MONTHLY POSITIVE - LOSING NEGATIVE - GAINING	ANNUAL POSITIVE - LOSING NEGATIVE - GAINING
		STATION	9429000	9429010	9429100	9429130	9429155	9429160	9429170	9429180	9429190	9429200	9429210	9429220	9429225	9429230	9429300	9429010		9429300		
1984	1	31	551	25,940	--	4.3	9.5	0.7	7.5	7.4	2.6	21.9	0.0	443	0.5	6.3	27,540	1,594,987	30,946	1,693,368	-67,434	
1984	2	28	1,162	25,510	--	9.1	15.2	1.8	10.8	10.9	9.5	31.5	0.0	533	0.5	9.7	27,830	1,416,753	35,104	1,545,599	-93,742	
1984	3	31	1,317	24,880	--	11.2	9.9	0.8	9.0	16.9	7.1	25.1	0.0	577	0.5	7.3	26,260	1,529,811	40,857	1,614,663	-43,995	
1984	4	30	1,567	24,510	--	11.5	14.8	0.1	7.5	17.5	5.9	26.7	0.0	582	0.5	11.0	24,800	1,458,445	40,289	1,475,702	23,033	
1984	5	31	1,543	23,800	--	13.0	18.2	0.1	5.5	11.8	5.1	30.3	0.0	627	0.5	7.4	24,580	1,463,404	44,179	1,511,364	-3,782	
1984	6	30	1,570	28,130	--	15.5	13.3	0.1	6.2	18.0	7.8	23.9	2.7	680	--	10.9	28,280	1,673,850	46,331	1,682,776	37,405	
1984	7	31	1,426	28,600	--	10.5	9.6	1.1	8.1	21.5	10.0	31.5	0.0	764	--	15.5	29,500	1,758,544	53,593	1,813,883	-1,746	
1984	8	31	1,434	26,290	--	16.0	17.4	0.3	7.0	9.6	7.9	26.8	0.4	644	--	12.0	27,520	1,616,508	45,580	1,692,138	-30,050	
1984	9	30	1,449	24,700	--	16.3	25.4	1.0	8.1	12.6	5.7	25.0	0.0	642	--	15.9	25,810	1,469,751	44,757	1,535,801	-21,293	
1984	10	31	811	23,630	--	10.6	21.9	0.0	5.3	26.8	7.6	18.4	0.0	580	--	19.8	24,440	1,452,951	42,421	1,502,756	-7,384	
1984	11	30	664	23,120	--	6.5	20.3	0.0	8.5	37.4	17.1	18.8	0.0	524	--	20.8	23,770	1,375,735	38,867	1,414,412	190	
1984	12	31	328	23,890	--	3.1	26.8	16.5	7.7	50.6	14.5	35.3	0.0	451	--	26.9	24,790	1,468,938	38,860	1,524,277	-16,479	-193,194
1985	1	31	432	23,560	--	1.3	20.2	7.5	10.4	24.4	8.4	24.4	0.0	380	--	19.0	24,140	1,448,647	30,463	1,484,310	-5,199	
1985	2	28	988	23,910	--	5.9	18.0	4.6	15.2	16.4	19.1	26.4	0.0	411	--	24.5	24,680	1,327,893	30,026	1,370,657	-12,737	
1985	3	31	1,332	19,420	--	11.6	23.2	2.9	11.7	28.5	7.5	29.2	0.0	521	--	19.4	21,080	1,194,089	40,276	1,296,158	-61,793	
1985	4	30	1,661	16,950	--	10.2	18.8	2.8	5.6	36.5	5.4	28.2	0.0	561	--	16.4	18,380	1,008,594	40,754	1,093,685	-44,337	
1985	5	31	1,578	18,610	--	11.7	11.1	1.4	9.8	32.0	7.1	39.4	0.0	584	--	17.4	19,580	1,144,284	43,905	1,203,927	-15,738	
1985	6	30	1,763	22,500	--	15.0	13.4	0.5	7.2	20.1	6.9	35.8	0.0	602	--	17.8	23,100	1,338,842	42,750	1,374,545	7,047	
1985	7	31	1,777	22,670	--	13.9	26.2	0.6	7.3	18.8	9.6	34.7	0.0	627	--	17.2	23,560	1,393,923	46,405	1,448,647	-8,319	
1985	8	31	1,759	22,440	--	14.3	27.8	1.4	5.0	14.4	5.6	46.9	1.2	645	--	14.6	23,200	1,379,781	47,737	1,426,512	1,007	
1985	9	30	1,188	20,380	--	12.0	34.3	8.7	13.1	24.5	6.9	52.1	0.0	634	--	21.6	22,040	1,212,693	48,026	1,311,470	-50,751	
1985	10	31	748	15,560	--	4.8	32.5	5.9	11.0	48.8	16.2	37.6	0.0	564	--	23.8	17,380	956,747	45,753	1,068,654	-66,154	
1985	11	30	761	14,660	--	8.3	23.7	6.3	14.0	47.9	9.1	35.7	0.0	483	--	22.0	16,030	872,330	38,703	953,851	-42,817	
1985	12	31	592	16,850	--	3.1	11.7	6.3	14.6	59.5	18.0	39.0	0.0	452	--	16.8	18,310	1,036,065	38,168	1,125,837	-51,604	-319,315
1986	1	31	601	20,620	--	2.7	16.4	5.3	7.6	33.1	9.2	18.4	0.0	428	--	7.8	20,840	1,267,874	32,475	1,281,401	18,948	
1986	2	28	953	16,380	--	3.7	18.7	3.8	16.2	20.3	11.7	27.8	0.0	440	--	17.5	17,630	909,699	31,065	979,120	-38,357	
1986	3	31	1,324	20,160	--	5.0	10.7	1.8	9.1	23.8	9.5	30.3	0.4	510	--	18.8	21,210	1,239,589	38,078	1,304,151	-26,484	
1986	4	30	1,589	19,150	--	8.5	17.2	0.7	8.5	17.4	6.6	32.2	0.0	544	--	23.3	20,360	1,139,503	39,180	1,211,503	-32,820	
1986	5	31	1,475	25,900	--	11.4	19.4	4.5	6.6	20.2	4.4	29.7	0.5	580	--	14.7	25,520	1,592,528	42,515	1,569,163	65,880	
1986	6	30	1,626	24,240	--	13.0	18.2	4.5	8.5	22.8	6.8	34.5	0.0	576	--	14.2	25,280	1,442,379	41,567	1,504,264	-20,318	
1986	7	31	1,672	21,200	--	10.2	16.5	4.6	6.4	14.7	4.4	30.6	0.0	612	--	11.9	22,720	1,303,536	43,698	1,396,997	-49,763	
1986	8	31	1,745	20,180	--	7.6	8.0	2.5	3.8	14.9	3.6	32.8	0.3	643	--	14.3	20,950	1,240,819	44,917	1,288,164	-2,428	
1986	9	30	1,369	18,850	--	5.3	20.2	3.7	7.5	24.8	3.0	47.8	0.2	619	--	21.1	20,280	1,121,652	44,767	1,206,743	-40,324	
1986	10	31	770	15,580	--	2.4	19.4	3.5	10.8	23.1	5.1	36.1	0.0	541	--	19.4	16,790	957,976	40,601	1,032,376	-33,799	
1986	11	30	718	15,130	--	1.5	22.6	5.5	7.6	27.3	8.7	30.2	0.0	472	--	18.7	15,960	900,297	35,344	949,685	-14,045	
1986	12	31	602	17,950	--	0.4	22.3	10.5	6.5	20.5	5.0	23.4	0.0	434	--	18.1	17,940	1,103,702	33,233	1,103,087	33,848	-107,579
1987	1	31	550	19,820	--	0.7	10.8	5.7	2.0	25.9	6.6	23.8	0.0	414	--	14.7	20,580	1,218,684	30,980	1,265,414	-15,750	
1987	2	28	1,082	16,450	--	2.6	8.1	2.9	5.6	13.4	3.6	36.1	0.0	435	--	18.3	17,950	913,586	29,180	996,892	-54,125	
1987	3	31	1,176	13,150	--	4.3	8.1	1.0	5.3	23.0	9.7	59.3	0.1	494	--	17.8	14,380	808,561	38,301	884,191	-37,329	
1987	4	30	1,508	10,830	--	6.0	15.7	0.2	4.0	14.5	3.9	56.5	0.0	496	--	21.8	12,350	644,429	36,800	734,876	-53,647	
1987	5	31	1,477	10,060	--	8.3	15.2	4.3	8.4	14.7	5.8	33.3	1.1	525	--	18.9	10,420	618,565	39,024	640,700	16,889	
1987	6	30	1,719	10,640	--	11.9	10.9	1.4	6.1	23.9	1.0	28.5	2.0	565	--	20.7	10,910	633,124	39,928	649,190	23,862	
1987	7	31	1,743	10,630	--	12.7	14.9	2.0	5.8	15.0	4.7	24.4	2.6	586	--	9.8	11,410	653,613	41,689	701,573	-6,271	
1987	8	31	1,700	11,020	--	7.4	14.8	2.5	3.7	9.5	2.2	27.2	0.6	604	--	16.2	11,850	677,593	42,333	728,628	-8,702	
1987	9	30	1,286	11,090	--	6.2	9.7	0.8	1.7	12.5	1.9	32.0	0.6	586	--	12.1	10,640	600,396	39,499	633,124	6,772	
1987	10	31	873	7,875	--	4.0	12.3	4.3	7.8	15.3	5.7	33.8	0.9	531	--	15.7	9,011	484,215	38,776	554,064	-31,074	
1987	11	30	598	4,411	--	1.3	13.2	10.5	12.9	22.2	2.5	19.4	0.0	484	--	16.6	6,044	262,473	34,682	359,643	-62,488	
1987	12	31	619	6,132	--	0.0	14.9	4.8	8.9	23.2	3.6	28.9	3.7	431	--	21.5	8,370	377,042	33,211	514,651	-104,398	-294,179
AVERAGE			**1,224**	**15,604**	**--**	**8.9**	**16.5**	**2.6**	**8.5**	**19.9**	**6.0**	**33.8**	**1.3**	**551**	**0.34**	**14.7**	**16,521**	**942,451**	**40,027**	**997,725**	**-15,248**	**-151,148**

NOTES
1 INCLUDES DIVERSIONS IN ARIZONA FROM ANNUAL INFORMAITON PROVIDED BY THE USBR IN THEIR ACCOUNTING AND COMPILATION OF RECORDS REPORTING. THE AVERAGE FOR 1972-1980 WAS APPLIED FOR YEARS BEYOND 198

APPENDIX D

SUMMARY OF PALO VERDE IRRIGATION DISTRICT WATER LEVEL DATA

1982	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation	1983	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation
3	8N-7E	1	289.11	286.9	13.30416667	273.5958333	3	8N-7E	1	289.11	286.9	9.4475	277.4525
1	7.5N-5.62E	2	285.26	283.47	3.326666667	280.1433333	1	7.5N-5.62E	2	285.26	283.47	3.943333333	279.5266667
1	7.41N-5.41E	3	284.49	284.1	3.858333333	280.2416667	1	7.41N-5.41E	3	284.49	284.1	4.404166667	279.6958333
	7.37N-5.12E	4	284.37	283	3.2825	279.7175		7.37N-5.12E	4	284.37	283	3.9	279.1
1	7.37N-4.87E	5	284.65	283.1	3.6225	279.4775	1	7.37N-4.87E	5	284.65	283.1	4.5325	278.5675
1	7.37N-4.75E	6	288.65	285.43	4.138333333	281.2916667	1	7.37N-4.75E	6	288.65	285.43	5.296666667	280.1333333
1	7.37N-4.25E	7	284.76	283	2.429166667	280.5708333	1	7.37N-4.25E	7	284.76	283	3.731666667	279.2683333
1	7.25N-4.31E	8	284.04	282.02	2.794545455	279.2254545	1	7.25N-4.31E	8	284.04	282.02	6.007272727	276.0127273
1	7.18N-4.06E	9	284.93	281	1.8125	279.1875	1	7.18N-4.06E	9	284.93	281	5.699	275.301
1	7.12N-4E	10	283.39	280.09	3.875833333	276.2141667	1	7.12N-4E	10	283.39	280.09	5.574	274.516
1	7N-7E	11	285.48	283.26	8.5575	274.7025	1	7N-7E	11	285.48	283.26	7.305833333	275.9541667
2	7N-6.25E	12	286.06	283.51	6.445	277.065	1	7N-6.25E	12	286.06	283.51	7.756666667	275.7533333
1	7N-4.62E	13	285.1	282.5	4.06	278.44	2	7N-4.62E	13	285.1	282.5	5.553333333	276.9466667
1	6.87N-3.93E	14	281.8	280.21	3.91	276.3	1	6.87N-3.93E	14	281.8	280.21	6.090833333	274.1191667
1	6.87N-3.81E	15	280.88	279.01	2.3875	276.6225	1	6.87N-3.81E	15	280.88	279.01	5.686	273.324
1	6.75N-3.43E	16	282.35	280.36	7.895	272.465	1	6.75N-3.43E	16	282.35	280.36	9.933333333	270.4266667
2	6.56N-3E	17	279.72	278.64	5.626666667	273.0133333	1	6.56N-3E	17	279.72	278.64	7.438333333	271.2016667
1	6.62N-3.75E	18	279.73	279.26	4.251666667	275.0083333	2	6.62N-3.75E	18	279.73	279.26	6.586666667	272.6733333
1	6.62N-3E	19	278.02	277.4	5.439166667	271.9608333	1	6.62N-3E	19	278.02	277.4	7.105	270.295
1	6.5N-3.68E	21	282.44	277.68	6.668333333	271.0116667	1	6.5N-3.68E	21	282.44	279.57	8.3625	271.2075
1	6.68N-3E	22	279.41	279.57	5.5975	273.9725		6.68N-3E	20	278.86	277.68	8.145833333	269.5341667
	6.5N-3E	23	279.34	277.32	3.655833333	273.6641667	1	6.5N-3E	22	279.41	277.32	6.080909091	271.2390909
1	6.5N-2.81E			275.74	4.688333333	271.0516667	1	6.5N-2.81E	23	279.34	275.74	6.284166667	269.4558333
1	6.37N-3E	24	279.41	277.45	5.468333333	271.9816667	1	6.37N-3E	24	279.41	277.45	7.603636364	269.8463636
	6.25N-6E	25	285.89	283.47	10.25083333	273.2191667	1	6.25N-6E	25	285.89	283.47	9.270833333	274.1991667
1	6.25N-4E	26	283.8	280.6	6.135833333	274.4641667	1	6.25N-4E	26	283.8	280.6	8.258333333	272.3416667
2	6.25N-3.68E	27	281.44	278.37		273.0125	1	6.25N-3.68E	27	281.44	278.37	7.990833333	270.3791667
1	6.25N-3E	29	279	276.43	6.205555556	270.2244444		6.25N-3E	28	280.23	277.58	8.005833333	269.5741667
	6.25N-2.81E	30	283.01	281.07	5.973333333	275.0966667	1	6.25N-2.81E	29	279	276.43	7.452727273	268.9772727
1	6N-4.75E	31	281.23	279.95	5.41	274.54	1	6N-4.75E	30	283.01	281.07	6.8975	274.1725
1	6N-4E	32	278.7	276.85	4.581666667	272.2683333	1	6N-4E	31	281.23	279.95	7.910833333	272.0391667
1	6N-3E	33	278.53	275.59	7.559166667	268.0308333	1	6N-3E	32	278.7	276.85	5.560833333	271.2891667
2	6N-2E	34	277.72	273.44	5.056	268.384	2	6N-2E	33	278.53	275.59	9.064166667	266.5258333
1	5.93N-2E	35	277.52	273.24	5.212727273	268.0272727	1	5.93N-2E	34	277.72	273.44	6.221666667	267.2183333
2	5.87N-2E	36	276.73	273.71	5.61	268.1	2	5.87N-2E	35	277.52	273.24	6.580833333	266.6591667
1	5.75N-2E	37	275.74	273.16	7.994	265.166	1	5.75N-2E	36	276.73	273.71	6.833333333	266.8766667
1	5.75N-1.75E	38	273.84	272.48	7.434166667	265.0458333	1	5.75N-1.75E	37	275.74	273.16	8.7125	264.4475
1	5.75N-1.5E	39	281.09	278.82	16.31363636	262.5063636	1	5.75N-1.5E	38	273.84	272.48	9.312222222	263.1677778
2	5.75N-1E	40	275.29	273.25	7.795	265.455	2	5.75N-1E	39	281.09	278.82	16.71916667	262.1008333
2	5.5N-1.75E	41	272.47	271.58	8.964166667	262.6158333	2	5.5N-1.75E	40	275.29	273.25	8.481666667	264.7683333
3	5.5N-1.25E	42	269.25	267.2	9.493333333	257.7066667	3	5.5N-1.25E	41	272.47	271.58	9.7175	261.8625
2	5.37N-0	43	279.89	278.25	11.475	266.775	2	5.37N-0	42	269.25	267.2	10.13	257.07
2	5N-4.87E	44	274.73	274.33	9.495833333	264.8341667	2	5N-4.87E	43	279.89	278.25	10.89166667	267.3583333
2	5N-4E	45	274.96	274.96	9.7775	265.1825	2	5N-4E	44	274.73	274.33	11.17	263.16
2	5N-3E	46	276.6	271.19	3.89	267.3	2	5N-3E	45	274.96	274.96	11.45	263.51
2	5N-2E	47	274.64	272.8	8.4275	264.3725	2	5N-2E	46	276.6	271.19	5.2825	265.9075
2	5N-1.75E	48	272.45	270.25	7.88	262.37	2	5N-1.75E	47	274.64	272.8	9.355	263.445
1	5N-1.25E	49	270.79	268.88	7.208333333	261.6716667	1	5N-1.25E	48	272.45	270.25	8.660833333	261.5891667
2	5N-1E	50	268.53	267.38	9.925454545	257.4545455	2	5N-1E	49	270.79	268.88	7.988333333	260.8916667
2	5N-0	51	268.73	267.01	10.93666667	256.0733333	2	5N-0	50	268.53	267.38	10.548	256.832
1	5N-.18W	52	275.05	272.66	8.838181818	263.8218182	1	5N-.18W	51	268.73	267.01	11.20333333	255.8066667
2	4.5N-1.75E	53	270.97	265.72	3.867272727	261.8527273	2	4.5N-1.75E	52	275.05	272.66	9.885	262.775
2	4.5N-1.25E	54	266.99	267.29	15.09333333	252.1966667	2	4.5N-1.25E	53	270.97	265.72	4.784166667	260.9358333
2	4.37N-.5W	55	272.11	267.99	14.3725	253.6175	2	4.37N-.5W	54	266.99	267.29	15.59166667	251.6983333

1982	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation	1983	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation
1	4.37N-.87W	56	275.43	274.2	9.3575	264.8425	1	4.37N-.87W	55	272.11	267.99	14.64333333	253.3466667
3	4N-4.87E	57	278.71	276.19	11.0975	265.0925	3	4N-4.87E	56	275.43	274.2	8.740833333	265.4591667
3	4N-4E	58	276.66	274.76	9.773333333	264.9866667	3	4N-4E	57	278.71	276.19	12.2325	263.9575
2	4N-3E	59	273.97	272.17	7.9125	264.2575	2	4N-3E	58	276.66	274.76	12.5325	262.2275
3	4N-2E	60	272.16	270.91	8.944166667	261.9658333	3	4N-2E	59	273.97	272.17	9.333333333	262.8366667
2	4N-1.75E	61	270.54	269.73	8.896666667	260.8333333	2	4N-1.75E	60	272.16	270.91	10.1075	260.8025
2	4N-1.25E	62	271.19	268.04	7.585833333	260.4541667	2	4N-1.25E	61	270.54	269.73	9.799166667	259.9308333
2	4N-1E	63	274.94	273.86	19.305	254.555	2	4N-1E	62	271.19	268.04	8.510833333	259.5291667
2	4N-1W	64	267.21	266.76	9.145	257.615	2	4N-1W	63	274.94	273.86	19.85909091	254.0009091
1	4N-0	65	272.59	271.02	7.9475	263.0725	1	4N-0	64	267.21	266.76	10.07916667	256.6808333
3	3.62N-2E	66	273.11	269.32	4.401666667	264.9183333	3	3.62N-2E	65	272.59	271.02	9.5625	261.4575
2	3.5N-1.75E	67	273.21	271.27	8.048333333	263.2216667	2	3.5N-1.75E	66	273.11	269.32	6.181	263.139
2	3N-5E	68	269.84	268.38	7.528333333	260.8516667	2	3N-5E	67	273.21	271.27	6.810833333	264.4591667
1	3N-4E	69	275.12	272.06	9.478333333	262.5816667	1	3N-4E	68	269.84	268.38	7.641666667	260.7383333
2	3N-3E	70	273.31	271.28	7.624166667	263.6558333	2	3N-3E	69	275.12	272.06	11.26545455	260.7945455
1	3N-2E	71	270.9	270.29	7.805	262.485	1	3N-2E	70	273.31	271.28	9.224166667	262.0558333
2	3N-1.75E	72	265.42	264.39	8.8025	255.5875	2	3N-1.75E	71	270.9	270.29	9.158333333	261.1316667
2	3N-.25W	73	276.84	276.15	22.31166667	253.8383333	2	3N-.25W	72	265.42	264.39	9.075	255.315
2	3N-1W	74	272.86	271.44	6.515	264.925	2	3N-1W	73	276.84	276.15	22.38	253.77
2	2.75N-2.25E	75	268.35	267.35	7.7425	259.6075	2	2.75N-2.25E	74	272.86	271.44	9.185	262.255
3	2.75N-1E	76	272.63	270.57	6.465	264.105	3	2.75N-1E	75	268.35	267.35	8.355833333	258.9941667
2	2.5N-2.5E	77	270.66	269.83	5.081666667	264.7483333	2	2.5N-2.5E	76	272.63	270.57	7.6575	262.9125
1	2.5N-2.62E	78	273.36	271.98	6.476666667	265.5033333	1	2.5N-2.62E	77	270.66	269.83	6.215	263.615
1	2.5N-2E	79	271.88	271.1	5.661666667	265.4383333	1	2.5N-2E	78	273.36	271.98	7.799166667	264.1808333
1	2.5N-1.87E	80	269.69	269.43	4.735833333	264.6941667	1	2.5N-1.87E	79	271.88	271.1	6.974166667	264.1258333
1	2.5N-1.75E	81	270.91	262.69	9.290833333	253.3991667	1	2.5N-1.75E	80	269.69	269.43	6.044166667	263.3858333
1	2.18N-1.5W	82	272.91	270.39	7.838333333	262.5516667	1	2.18N-1.5W	81	270.91	262.69	10.5	252.19
1	2.25N-2.37E	83	273.99	270.92	5.301666667	265.6183333	1	2.25N-2.37E	82	272.91	270.39	9.114166667	261.2758333
2	2.25N-2E	84	274.41	272.2	6.47	265.73	2	2.25N-2E	83	273.99	270.92	6.5875	264.3325
2	2.25N-1.75E	85	272.67	269.05	8.673333333	260.3766667	2	2.25N-1.75E	84	274.41	272.2	8.159090909	264.0409091
1	2N-5E	86	270.92	270.8	5.5325	265.2675	1	2N-5E	85	272.67	269.05	7.795	261.255
1	2N-2E	87	272.09	268.81	6.327272727	262.4827273	1	2N-2E	86	270.92	270.8	6.368333333	264.4316667
2	2N-1E	88	267.59	265.5	7.905	257.595	2	2N-1E	87	272.09	268.81	6.945833333	261.8641667
1	2N-.25E	89	263.31	260.77	8.521666667	252.2483333	1	2N-.25E	88	267.59	265.5	8.100833333	257.3991667
1	2N-1.25W	90	264.28	261.73	9.389090909	252.3409091	1	2N-1.25W	89	263.31	260.77	9.133333333	251.6366667
2	1.75N-1.25W	91	264.11	261.43	11.62583333	249.8041667	2	1.75N-1.25W	90	264.28	261.73	10.11416667	251.6158333
2	1.75N-1.75W	92	264.18	261.32	10.03	251.29	2	1.75N-1.75W	91	264.11	261.43	12.38083333	249.0491667
2	1.5N-1.25W	93	261.32	260.83	10.63083333	250.1991667	2	1.5N-1.25W	92	264.18	261.32	10.5025	250.8175
2	1.5N-2W	94	264.6	261.91	13.5775	248.3325	2	1.5N-2W	93	261.32	260.83	11.49416667	249.3358333
2	1.5N-2.25W	95	262.06	260.49	7.893636364	252.5963636	2	1.5N-2.25W	94	264.6	261.91	13.9125	247.9975
2	1.25N-1.5W	96	271.74	268.72	11.78	256.94	2	1.25N-1.5W	95	262.06	260.49	9.318181818	251.1718182
3	1N-5E	97	266.29	266.02	9.405	256.615	3	1N-5E	96	271.74	268.72	9.674166667	259.0458333
2	1N-4E	98	267.49	266.62	8.4175	258.2025	2	1N-4E	97	266.29	266.02	9.500833333	256.5191667
2	1N-3E	99	270.74	270.7	11.99916667	258.7008333	2	1N-3E	98	267.49	266.62	8.966666667	257.6533333
2	1N-2.12E	100	266.52	266.74	8.365	258.375	2	1N-2.12E	99	270.74	270.7	12.95083333	257.7491667
2	1N-1E	101	264.79	264.5	8.426666667	256.0733333	2	1N-1E	100	266.52	266.74	8.9075	257.8325
3	1N-0	102	261.87	261.01	8.870833333	252.1391667	3	1N-0	101	264.79	264.5	8.524166667	255.9758333
2	1N-.75W	103	259.68	258.34	9.7075	248.6325	2	1N-.75W	102	261.87	261.01	8.79	252.22
2	1N-2W	104	257.8	257.52	9.565833333	247.9541667	2	1N-2W	103	259.68	258.34	10.15636364	248.1836364
2	1N-2.25W	105	258.52	256.72	10.42	246.3	2	1N-2.25W	104	257.8	257.52	10.07454545	247.4454545
2	0.5N-2.37W	106	269.45	267.07	11.13	255.94	2	0.5N-2.37W	105	258.52	256.72	10.69083333	246.0291667
2	0.12N-5E	107	266.9	266.3	12.16181818	254.1381818	2	0.12N-5E	106	269.45	267.07	9.176666667	257.8933333
2	0-4.12E	108	263.76	262.77	8.351666667	254.4183333	2	0-4.12E	107	266.9	266.3	12.27909091	254.0209091
2	0-3E	109	267.84	265.18	8.481666667	256.6983333	2	0-3E	108	263.76	262.77	8.9875	253.7825
2	0-2E	110	261.7	261.42	6.86	254.56	2	0-2E	109	267.84	265.18	9.575833333	255.6041667

1982	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation	1983	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation
2	0-1E	111	262.37	261.83	7.978333333	253.8516667	2	0-1E	110	261.7	261.42	8.126363636	253.2936364
2	0-0	112	260.19	259.7	11.29583333	248.4041667	2	0-0	111	262.37	261.83	8.209166667	253.6208333
1	0-1W	113	258.18	256.12	10.59166667	245.5283333	1	0-1W	112	260.19	259.7	11.00727273	248.6927273
2	0-2W	114	256.48	255.13	11.21	243.92	2	0-2W	113	258.18	256.12	10.58166667	245.5383333
2	0-2.75W	115	257.77	255.36	10.24833333	245.1116667	2	0-2.75W	114	256.48	255.13	11.31416667	243.8158333
2	0.5S-2.75W	116	257.35	255.03	12.76416667	242.2658333	2	0.5S-2.75W	115	257.77	255.36	10.44833333	244.9116667
2	0.5S-3W	117	257.79	254.4	11.86583333	242.5341667	2	0.5S-3W	116	257.35	255.03	12.86583333	242.1641667
2	0.5S-3.18W	118	268.56	266.74	12.3775	254.3625	2	0.5S-3.18W	117	257.79	254.4	12.17	242.23
3	1S-4E	119	263.55	260.73	11.09	249.64	3	1S-4E	118	268.56	266.74	11.09666667	255.6433333
2	1S-3E	120	260.54	259.92	11.63363636	248.2863636	2	1S-3E	119	263.55	260.73	11.15083333	249.5791667
3	1S-2E	121	261.85	258.57	5.81	252.76	3	1S-2E	120	260.54	259.92	12.23833333	247.6816667
2	1S-1E	122	258.55	258.53	8.715833333	249.8141667	2	1S-1E	121	261.85	258.57	6.84	251.73
2	1S-.25W	123	259.49	258.92	10.04666667	248.8733333	2	1S-.25W	122	258.55	258.53	8.794166667	249.7358333
1	1S-1W	124	255.99	254.74	11.18083333	243.5591667	1	1S-1W	123	259.49	258.92	9.9025	249.0175
2	1S-2W	125	255.47	253.89	11.61	242.28	2	1S-2W	124	255.99	254.74	10.84833333	243.8916667
2	1S-3W	126	253.86	252.6	11.575	241.025	2	1S-3W	125	255.47	253.89	11.67083333	242.2191667
2	1S-3.37W	127	255.89	252.21	11.74166667	240.4683333	2	1S-3.37W	126	253.86	252.6	11.6225	240.9775
2	1.25S-4W	128	254.24	250.98	11.67666667	239.3033333	2	1.25S-4W	127	255.89	252.21	12.08583333	240.1241667
2	1.5S-4.5W	129	252.55	250.98	11.18083333	239.7991667	2	1.5S-4.5W	128	254.24	250.98	11.87666667	239.1033333
2	1.5S-4.75W	130	261.59	257.83	10.46916667	247.3608333	2	1.5S-4.75W	129	252.55	250.98	11.51166667	239.4683333
2	2S-2.75E	131	265.35	262.89	11.9325	250.9575	2	2S-2.75E	130	261.59	257.83	11.05166667	246.7783333
2	2S-3.75E	132	258.15	257.56	9.811666667	247.7483333	2	2S-3.75E	131	265.35	262.89	10.87083333	252.0191667
2	2S-2E	133	258.01	255.81	7.3525	248.4575	2	2S-2E	132	258.15	257.56	10.6925	246.8675
3	2S-1E	134	256.3	255.56	7.089166667	248.4708333	3	2S-1E	133	258.01	255.81	7.8825	247.9275
2	2S-0	135	256.21	254.2	7.49	246.71	2	2S-0	134	256.3	255.56	7.553333333	248.0066667
2	2S-1W	136	254.96	253.48	9.166666667	244.3133333	2	2S-1W	135	256.21	254.2	7.785	246.415
1	2S-2W	137	252.16	252.1	10.16333333	241.9366667	1	2S-2W	136	254.96	253.48	9.870833333	243.6091667
2	2S-3W	138	252.33	251.88	11.00333333	240.8766667	2	2S-3W	137	252.16	252.1	10.54666667	241.5533333
2	2S-4W	139	254.87	252.25	12.44	239.81	2	2S-4W	138	252.33	251.88	12.0975	239.7825
2	2S-4.5W	140	250.86	249.04	12.25	236.79	2	2S-4.5W	139	254.87	252.25	12.84833333	239.4016667
2	2S-5.12W	141	252.87	249.19	10.47583333	238.7141667	2	2S-5.12W	140	250.86	249.04	12.46727273	236.5727273
3	2.5S-5.25W	142	260.23	258.41	10.47583333	247.9341667	3	2.5S-5.25W	141	252.87	249.19	11.1375	238.0525
3	2.75S-3.5E	143	251.32	249.21	12.3675	236.8425	3	2.75S-3.5E	142	260.23	258.41	9.846666667	248.5633333
2	2.75S-5.25W	144	263.96	262.35	6.028181818	256.3218182	2	2.75S-5.25W	143	251.32	249.21	13.2825	235.9275
1	3S-4.37E	145	258.93	257.22	10.925	246.295	1	3S-4.37E	144	263.96	262.35	6.384166667	255.9658333
3	3S-3E	146	257.91	255.88	10.29333333	245.5866667	3	3S-3E	145	258.93	257.22	10.68583333	246.5341667
1	3S-2E	147	256.81	254.64	8.315833333	246.3241667	1	3S-2E	146	257.91	255.88	10.6575	245.2225
2	3S-1E	148	253.44	252.09	7.0275	245.0625	2	3S-1E	147	256.81	254.64	8.7775	245.8625
2	3S-0	149	254.56	252.57	8.36	244.21	2	3S-0	148	253.44	252.09	7.410833333	244.6791667
2	3S-1W	150	253.78	250.84	9.596666667	241.2433333	2	3S-1W	149	254.56	252.57	8.7325	243.8375
2	3S-2W	151	247.32	248.8	8.644166667	240.1558333	2	3S-2W	150	253.78	250.84	11.2475	239.5925
2	3S-3W	152	252.11	249.83	10.3075	239.5225	2	3S-3W	151	247.32	248.8	9.474166667	239.3258333
2	3S-4W	153	251.33	248.77	11.71416667	237.0558333	2	3S-4W	152	252.11	249.83	11.57083333	238.2591667
2	3S-5.25W	154	249.57	246.8	8.49	238.31	2	3S-5.25W	153	251.33	248.77	12.87416667	235.8958333
2	3S-5.5W	155	251.39	247.97	11.06363636	236.9063636	2	3S-5.5W	154	249.57	246.8	9.67	237.13
3	3.12S-4.5W	156	248.74	247.84	10.23833333	237.6016667	3	3.12S-4.5W	155	251.39	247.97	12	235.97
2	3.37S-4.5W	157	249.04	247.15	9.765	237.385	2	3.37S-4.5W	156	248.74	247.84	11.06416667	236.7758333
2	3.5S-5.25W	158	248.33	246.1	8.473333333	237.6266667	2	3.5S-5.25W	157	249.04	247.15	11.00666667	236.1433333
2	3.5S-5.5W	159	252.31	248.59	9.1525	239.4375	2	3.5S-5.5W	158	248.33	246.1	9.611666667	236.4883333
2	3.62S-4.75W	160	247.38	246.61	9.258333333	237.3516667	2	3.62S-4.75W	159	252.31	248.59	10.11583333	238.4741667
2	3.75S-5.5W	161	248.14	247.62	9.6675	237.9525	2	3.75S-5.5W	160	247.38	246.61	10.17454545	236.4354545
2	3.87S-4.25W	162	265.61	261.39	10.85833333	250.5316667	2	3.87S-4.25W	161	248.14	247.62	10.9375	236.6825
2	4S-4E	163	260.08	258.94	9.270833333	249.6691667	2	4S-4E	162	265.61	261.39	9.205	252.185
2	4S-3E	164	259.63	257.4	13.98833333	243.4116667	2	4S-3E	163	260.08	258.94	9.2125	249.7275

1982	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation	1983	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation
2	4S-2E	165	259.23	254.05	9.446666667	244.6033333	2	4S-2E	164	259.63	257.4	13.98583333	243.4141667
2	4S-1E	166	252.02	251.67	10.46166667	241.2083333	2	4S-1E	165	259.23	254.05	12.706	241.344
3	4S-0	167	253.41	251.47	9.703333333	241.7666667	3	4S-0	166	252.02	251.67	10.94333333	240.7266667
3	4S-.5W	168	253.23	251.32	9.245833333	242.0741667	3	4S-.5W	167	253.41	251.47	10.28083333	241.1891667
2	4S-.75W	169	250.85	249.2	13.42583333	235.7741667	2	4S-.75W	168	253.23	251.32	9.480833333	241.8391667
2	4S-2W	170	250.85	249.68	12.38181818	237.2981818	2	4S-2W	169	250.85	249.2	13.82916667	235.3708333
2	4S-3W	171	246.83	246.34	6.9525	239.3875	2	4S-3W	170	250.85	249.68	12.96916667	236.7108333
3	4S-4W	172	248.53	248.16	11.585	236.575	3	4S-4W	171	246.83	246.34	7.31	239.03
3	4S-4.5W	173	249.14	245.96	8.7575	237.2025	3	4S-4.5W	172	248.53	248.16	12.49916667	235.6608333
1	4S-5.25W	174	249.08	246.39	9.506666667	236.8833333	1	4S-5.25W	173	249.14	245.96	9.280833333	236.6791667
3	4S-5.5W	175	252.9	246.47	9.06	237.41	3	4S-5.5W	174	249.08	246.39	10.36916667	236.0208333
2	4S-5.87W	176	250.26	247.26	9.763333333	237.4966667	2	4S-5.87W	175	252.9	246.47	9.744166667	236.7258333
2	4.25S-4.12W	177	250.4	246.8	10.83833333	235.9616667	2	4.25S-4.12W	176	250.26	247.26	10.56333333	236.6966667
2	4.25S-4.5W	178	249.4	246.25	8.413333333	237.8366667	2	4.25S-4.5W	177	250.4	246.8	11.94083333	234.8591667
2	4.25S-5.5W	179	247.36	245.52	9.826666667	235.6933333	2	4.25S-5.5W	178	249.4	246.25	8.870833333	237.3791667
2	4.5S-4.75W	180	249.47	246.08	8.5775	237.5025	2	4.5S-4.75W	179	247.36	245.52	10.94	234.58
2	4.5S-5.5W	181	248.63	246.47	11.01333333	235.4566667	2	4.5S-5.5W	180	249.47	246.08	8.929166667	237.1508333
2	4.5S-6.25W	182	249.14	246.78	9.5125	237.2675	2	4.5S-6.25W	181	248.63	246.47	11.13	235.34
2	4.75S-4.25W	183	246.3	244.5	9.9625	234.5375	2	4.75S-4.25W	182	249.14	246.78	10.17416667	236.6058333
2	4.75S-4.75W	184	257.68	256.65	9.544166667	247.1058333	2	4.75S-4.75W	183	246.3	244.5	10.10333333	234.3966667
2	5S-3E	185	259.3	257.61	11.09166667	246.5183333	2	5S-3E	184	257.68	256.65	8.32	248.33
2	5S-2.25E	186	255.81	253.72	13.76916667	239.9508333	2	5S-2.25E	185	259.3	257.61	10.65	246.96
2	5S-1E	187	254.3	251.38	14.44	236.94	2	5S-1E	186	255.81	253.72	13.97916667	239.7408333
3	5S-0	188	249.17	248.95	11.765	237.185	3	5S-0	187	254.3	251.38	14.64666667	236.7333333
3	5S-.75W	189	245.35	245.3	12.07583333	233.2241667	3	5S-.75W	188	249.17	248.95	12.325	236.625
3	5S-2W	190	244.17	242.59	11.2175	231.3725	3	5S-2W	189	245.35	245.3	12.3325	232.9675
3	5S-2.75W	191	249.28	247.77	9.728571429	238.0414286	3	5S-2.75W	190	244.17	242.59	11.89545455	230.6945455
3	5S-3.75W	192	248.93	246.83	10.1475	236.6825	3	5S-3.75W	191	249.28	247.77	10.21666667	237.5533333
2	5S-4.12W	193	247.04	244.83	10.71083333	234.1191667	2	5S-4.12W	192	248.93	246.83	11.3975	235.4325
2	5S-4.5W	194	246.64	244.38	9.920833333	234.4591667	2	5S-4.5W	193	247.04	244.83	11.23333333	233.5966667
2	5S-4.75W	195	245.46	243.81	8.644166667	235.1658333	2	5S-4.75W	194	246.64	244.38	10.85	233.53
2	5S-5.5W	196	246.48	244.45	10.38083333	234.0691667	2	5S-5.5W	195	245.46	243.81	9.5175	234.2925
2	5S-6.18W	197	247.78	247.18	11.13666667	236.0433333	2	5S-6.18W	196	246.48	244.45	10.10666667	234.3433333
2	5.5S-.5W	198	247.32	245.49	11.80416667	233.6858333	2	5.5S-.5W	197	247.78	247.18	11.37	235.81
2	5.5S-1.25W	199	248.3	246.29	9.904166667	236.3858333	2	5.5S-1.25W	198	247.32	245.49	12.2525	233.2375
2	5.5S-4.25W	200	245.9	244.75	12.17833333	232.5716667	2	5.5S-4.25W	199	248.3	246.29	11.84083333	234.4491667
3	5.5S-4.5W	201	246.28	244.05	12.585	231.465	3	5.5S-4.5W	200	245.9	244.75	13.0725	231.6775
2	5.5S-4.75W	202	246.66	242.63	9.315833333	233.3141667	2	5.5S-4.75W	201	246.28	244.05	12.63916667	231.4108333
3	5.5S-6.37W	203	243.63	242.33	9.834166667	232.4958333	3	5.5S-6.37W	202	246.66	242.63	9.051666667	233.5783333
3	5.75S-2W	204	258.01	256.13	13.78666667	242.3433333	3	5.75S-2W	203	243.63	242.33	10.0025	232.3275
2	6S-3E	205	255.23	254.45	10.13416667	244.3158333	2	6S-3E	204	258.01	256.13	10.63083333	245.4991667
2	6S-2E	206	256.31	253.73	11.81583333	241.9141667	2	6S-2E	205	255.23	254.45	8.545	245.905
3	6S-1.12E	207	243.98	241.97	12.58583333	229.3841667	3	6S-1.12E	206	256.31	253.73	11.38666667	242.3433333
2	6S-2.75W	208	245.48	243.84	10.80416667	233.0358333	2	6S-2.75W	207	243.98	241.97	12.43727273	229.5327273
3	6S-4W	209	246.86	243.84	12.03166667	231.8083333	3	6S-4W	208	245.48	243.84	11.66083333	232.1791667
3	6S-4.5W	210	244.17	242.61	9.7625	232.8475	3	6S-4.5W	209	246.86	243.84	12.43083333	231.4091667
2	6S-5.5W	211	242.64	240.09	7.535	232.555	2	6S-5.5W	210	244.17	242.61	10.32833333	232.2816667
2	6S-6.25W	212	253.73	249.73	11.05166667	238.6783333	2	6S-6.25W	211	242.64	240.09	7.586666667	232.5033333
2	6.75S-0	213	252.93	252.8	11.63181818	241.1681818	2	6.75S-0	212	253.73	249.73	11.67333333	238.0566667
1	6.87S-1.87E	214	256.75	252.93	10.69833333	242.2316667	1	6.87S-1.87E	213	252.93	252.8	9.138333333	243.6616667
3	7S-1E	215	251.43	250.34	11.07333333	239.2666667	3	7S-1E	214	256.75	252.93	9.7975	243.1325
2	7S-0	216	247.64	245.6	10.99363636	234.6063636	2	7S-0	215	251.43	250.34	11.3	239.04
2	7S-1W	217	241.33	240.97	10.99166667	229.9783333	2	7S-1W	216	247.64	245.6	12.17583333	233.4241667

1982	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation	1983	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation
2	7S-2W	218	241.62	240.88	12.33833333	228.5416667	2	7S-2W	217	241.33	240.97	11.21666667	229.7533333
2	7S-3W	219	242.52	241.91	11.44083333	230.4691667	2	7S-3W	218	241.62	240.88	12.64416667	228.2358333
2	7S-4W	220	243.43	241.59	10.09916667	231.4908333	2	7S-4W	219	242.52	241.91	11.62833333	230.2816667
3	7S-5W	221	244.57	241.86	9.6825	232.1775	3	7S-5W	220	243.43	241.59	9.989166667	231.6008333
2	7S-5.75W	222	244.09	241.02	9.825	231.195	2	7S-5.75W	221	244.57	241.86	9.855833333	232.0041667
2	7S-6.5W	223	253.45	251.73	10.92583333	240.8041667	2	7S-6.5W	222	244.09	241.02	10.23916667	230.7808333
2	7.25S-.5E	224	253.46	249.77	9.180909091	240.5890909	2	7.25S-.5E	223	253.45	251.73	10.4925	241.2375
2	7.25S-.25E	225	248.92	246.58	8.9825	237.5975	2	7.25S-.25E	224	253.46	249.77	10.22416667	239.5458333
2	7.25S-.5W	226	250.44	247.1	9.206666667	237.8933333	2	7.25S-.5W	225	248.92	246.58	9.8	236.78
2	7.25S-.25W	227	252.5	248.19	9.6675	238.5225	2	7.25S-.25W	226	250.44	247.1	9.66	237.44
2	7.75S-0	228	253.51	250.64	11.425	239.215	2	7.75S-0	227	252.5	248.19	9.6875	238.5025
2	8S-1E	229	253.44	250.07	10.715	239.355	2	8S-1E	228	253.51	250.64	9.617777778	241.0222222
2	8S-.5E	230	246.82	245.02	6.974545455	238.0454545	2	8S-.5E	229	253.44	250.07	9.584166667	240.4858333
2	8S-.25W	231	245.28	243.91	5.699166667	238.2108333	2	8S-.25W	230	246.82	245.02	7.520833333	237.4991667
2	8S-.5W	232	246.82	242.57	6.196666667	236.3733333	2	8S-.5W	231	245.28	243.91	5.463333333	238.4466667
2	8S-1W	233	244.92	242.5	9.205833333	233.2941667	2	8S-1W	232	246.82	242.57	7.545	235.025
1	8S-2W	234	239.43	238.57	10.66166667	227.9083333	1	8S-2W	233	244.92	242.5	10.2725	232.2275
1	8S-3W	235	241.01	239.2	10.985	228.215	1	8S-3W	234	239.43	238.57	11.125	227.445
2	8S-5W	236	239.2	238.37	8.223333333	230.1466667	2	8S-5W	235	241.01	239.2	10.86416667	228.3358333
2	8S-5.5W	237	242.17	238.59	6.306666667	232.2833333	2	8S-5.5W	236	239.2	238.37	7.903333333	230.4666667
2	8S-6.5W	238	240.34	237.41	10.86083333	226.5491667	2	8S-6.5W	237	242.17	238.59	7.373333333	231.2166667
1	8.25S-4.25W	239	250.45	249.42	13.7975	235.6225	1	8.25S-4.25W	238	240.34	237.41	11.23416667	226.1758333
1	9S-0	240	243.23	241.76	7.635	234.125	1	9S-0	239	250.45	249.42	13.04333333	236.3766667
2	9S-1.25W	241	244.64	241.7	9.385833333	232.3141667	2	9S-1.25W	240	243.23	241.76	9.124166667	232.6358333
3	9S-2W	242	239.98	237.81	8.613333333	229.1966667	3	9S-2W	241	244.64	241.7	10.12583333	231.5741667
2	9S-3W	243	236.84	235.23	10.09166667	225.1383333	2	9S-3W	242	239.98	237.81	9.248333333	228.5616667
2	9S-4W	244	236.62	235.18	9.0975	226.0825	2	9S-4W	243	236.84	235.23	10.4875	224.7425
2	9S-5W	245	235.74	236.1	11.21333333	224.8866667	2	9S-5W	244	236.62	235.18	8.695	226.485
2	9S-5.75W	246	237.54	235.17	7.273333333	227.8966667	2	9S-5.75W	245	235.74	236.1	11.18363636	224.9163636
2	9S-6.5W	247	251.76	249.13	15.45333333	233.6766667	2	9S-6.5W	246	237.54	235.17	7.645	227.525
2	10S-0	248	249.69	248.18	15.71916667	232.4608333	2	10S-0	247	251.76	249.13	12.33833333	236.7916667
1	10S-1W	249	242	239.93	8.984166667	230.9458333	1	10S-1W	248	249.69	248.18	15.70833333	232.4716667
3	10S-2W	250	240.34	237.37	8.521666667	228.8483333	3	10S-2W	249	242	239.93	9.4525	230.4775
3	10S-3W	251	237.45	235.16	7.010833333	228.1491667	3	10S-3W	250	240.34	237.37	8.650833333	228.7191667
2	10S-3.87W	252	236.47	233.49	9.711666667	223.7783333	2	10S-3.87W	251	237.45	235.16	7.67	227.49
2	10S-5W	253	236.85	234.71	8.7925	225.9175	2	10S-5W	252	236.47	233.49	9.7475	223.7425
1	10S-6.75W	254	235.76	233.22	8.285833333	224.9341667	1	10S-6.75W	253	236.85	234.71	8.5925	226.1175
2	10S-5.75W	255	236.58	233.4	8.84	224.56	2	10S-5.75W	254	235.76	233.22	8.696666667	224.5233333
2	10.75S-4W	256	244.62	243.3	12.67583333	230.6241667	2	10.75S-4W	255	236.58	233.4	9.425833333	223.9741667
2	11S-1W	257	238.8	237.75	8.933	228.817	2	11S-1W	256	244.62	243.3	12.285	231.015
2	11S-2W	258	237.96	236.02	9.495833333	226.5241667	2	11S-2W	257	238.8	237.75	8.516363636	229.2336364
3	11S-3W	259	235.02	231.19	8.168333333	223.0216667	3	11S-3W	258	237.96	236.02	9.350833333	226.6691667
2	11S-5W	260	234.78	232.35	8.490833333	223.8591667	2	11S-5W	259	235.02	231.19	8.685833333	222.5041667
2	11S-5.75W	261	233.32	231.42	9.655	221.765	2	11S-5.75W	260	234.78	232.35	8.849166667	223.5008333
2	11S-6.87W	262	231.3	231	8.1975	222.8025	2	11S-6.87W	261	233.32	231.42	9.805833333	221.6141667
2	11.75S-6.75W	263	238.84	238.29	9.885833333	228.4041667	2	11.75S-6.75W	262	231.3	231	8.618333333	222.3816667
2	12S-1W	264	237.63	237.11	9.9325	227.1775	2	12S-1W	263	238.84	238.29	9.460909091	228.8290909
2	12S-2W	265	242.36	240.04	13.63583333	226.4041667	2	12S-2W	264	237.63	237.11	9.6025	227.5075
2	12S-3W	266	237.71	234.84	11.66	223.18	2	12S-3W	265	242.36	240.04	12.6825	227.3575
2	12S-4W	267	236.8	233.16	10.38111111	222.7788889	2	12S-4W	266	237.71	234.84	10.79833333	224.0416667
3	12S-5W	268	233.06	231.72	10.33	221.39	3	12S-5W	267	236.8	233.16	10.43416667	222.7258333
2	12S-6W	269	242.29	240.58	10.545	230.035	2	12S-6W	268	233.06	231.72	10.77916667	220.9408333
2	13S-2W	270	243.53	240.58	13.61083333	226.9691667	2	13S-2W	269	242.29	240.58	8.7875	231.7925

1982	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation	1983	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation
2	13.12S-2.87W	271	234.53	234.31	7.683636364	226.6263636	2	13.12S-2.87W	270	243.53	240.58	10.46083333	230.1191667
2	13S-4.25W	272	235.57	233.88	9.433333333	224.4466667	2	13S-4.25W	271	234.53	234.31	5.774166667	228.5358333
2	13S-5W	273	232.62	231.6	9.0025	222.5975	2	13S-5W	272	235.57	233.88	8.0775	225.8025
1	13S-6W	274	230.69	228.55	6.993636364	221.5563636	1	13S-6W	273	232.62	231.6	8.653333333	222.9466667
2	13S-6.5W	275	233.57	232.23	11.90166667	220.3283333	2	13S-6.5W	274	230.69	228.55	7.240833333	221.3091667
2	13S-7.12W	276	231.67	228.46	5.263333333	223.1966667	2	13S-7.12W	275	233.57	232.23	11.43636364	220.7936364
1	14.25S-6.5W	277	234.11	228.1	9.215	218.885	1	14.25S-6.5W	276	231.67	228.46	3.503333333	224.9566667
2	14.25S-7.18W	278	229.73	228.93	5.34	223.59	2	14.25S-7.18W	277	234.11	228.1	8.976666667	219.1233333
1	15S-6W	279	228.81	226.48	3.639090909	222.8409091	1	15S-6W	278	229.73	228.93	3.760833333	225.1691667
2	15S-6.75W	280	227.88	226.33	4.057272727	222.2727273	2	15S-6.75W	279	228.81	226.48	3.1775	223.3025
1	16S-6W	281	230.06	228.14	5.1775	222.9625	1	16S-6W	280	227.88	226.33	4.09	222.24
1	17S-5W	282	227.63	226.14	8.164166667	217.9758333	1	17S-5W	281	230.06	228.14	4.745714286	223.3942857
1	17S-5.75W	283	227.16	224.12	2.63	221.49	1	17S-5.75W	282	227.63	226.14	7.793333333	218.3466667
1	18S-5W							18S-5W	283	227.16	224.12	2.53	221.59
	6.5N-3.56E						7.44N-5.44E	OL	286.89	283.47	279.9109091	4.189090909	
	7.44N-5.44E	OL	286.89	283.47	279.0016667	4.734166667							
			281.79	279.51	270.935	10.365	6.25N-3.56E						
	6.25N-3.56E								281.9	279.51	269.6408333	9.869166667	

1984	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation	1985	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation
3	8N-7E	1	289.11	286.9	8.901666667	277.9983333	3	8N-7E	1	289.11	286.9	11.37454545	275.5254545
1	7.5N-5.62E	2	285.26	283.47	3.394	280.076	1	7.5N-5.62E	2	285.26	283.47	3.094545455	280.3754545
1	7.41N-5.41E	3	284.49	284.1	4.032	280.068	1	7.41N-5.41E	3	284.49	284.1	3.748181818	280.3518182
1	7.37N-5.12E	4	284.37	283	3.355	279.645	1	7.37N-5.12E	4	284.37	283	2.907272727	280.0927273
1	7.37N-4.87E	5	284.65	283.1	4.184	278.916	1	7.37N-4.87E	5	284.65	283.1	3.392727273	279.7072727
1	7.37N-4.75E	6	288.65	285.43	6.071	279.359	1	7.37N-4.75E	6	288.65	285.43	5.04	280.39
1	7.37N-4.25E	7	284.76	283	3.512	279.488	1	7.37N-4.25E	7	284.76	283	3.319090909	279.6809091
1	7.25N-4.31E	8	284.04	282.02	6.238	275.782	1	7.25N-4.31E	8	284.04	282.02	6.308181818	275.7118182
1	7.18N-4.06E	9	284.93	281	6.191	274.809	1	7.18N-4.06E	9	284.93	281	6.337272727	274.6627273
1	7.12N-4E	10	283.39	280.09	5.423	274.667	1	7.12N-4E	10	283.39	280.09	5.341818182	274.7481818
2	7N-7E	11	285.48	283.26	5.954166667	277.3058333	2	7N-7E	11	285.48	283.26	7.163636364	276.0963636
1	7N-6.25E	12	286.06	283.51	6.188333333	277.3216667	1	7N-6.25E	12	286.06	283.51	6.091818182	277.4181818
1	7N-4.62E	13	285.1	282.5	5.009	277.491	1	7N-4.62E	13	285.1	282.5	4.799090909	277.7009091
1	6.87N-3.93E	14	281.8	280.21	5.737	274.473	1	6.87N-3.93E	14	281.8	280.21	5.671818182	274.5381818
1	6.87N-3.81E	15	280.88	279.01	5.035	273.975	1	6.87N-3.81E	15	280.88	279.01	4.356363636	274.6536364
2	6.75N-3.43E	16	282.35	280.36	9.02	271.34	2	6.75N-3.43E	16	282.35	280.36	8.609090909	271.7509091
1	6.56N-3E	17	279.72	278.64	7.581	271.059	1	6.56N-3E	17	279.72	278.64	8.406363636	270.2336364
1	6.62N-3.75E	18	279.73	279.26	5.693	273.567	1	6.62N-3.75E	18	279.73	279.26	5.694545455	273.5654545
1	6.62N-3E	19	278.02	277.4	7.17	270.23	1	6.62N-3E	19	278.02	277.4	7.042727273	270.3572727
1	6.5N-3.68E	21	282.44	279.57	6.976	272.594	1	6.5N-3.68E	21	282.44	279.57	7.28	272.29
1	6.68N-3E	20	278.86	277.68	8.3	269.38	1	6.68N-3E	20	278.86	277.68	7.159090909	270.5209091
1	6.5N-3E	22	279.41	277.32	7.407	269.913	1	6.5N-3E	22	279.41	277.32	7.363636364	269.9563636
1	6.5N-2.81E	23	279.34	275.74	6.656666667	269.0833333	1	6.5N-2.81E	23	279.34	275.74	6.450909091	269.2890909
1	6.37N-3E	24	279.41	277.45	7.298	270.152	1	6.37N-3E	24	279.41	277.45	7.187	270.263
2	6.25N-6E	25	285.89	283.47	8.976666667	274.4933333	2	6.25N-6E	25	285.89	283.47	9.768181818	273.7018182
1	6.25N-4E	26	283.8	280.6	7.554	273.046	1	6.25N-4E	26	283.8	280.6	7.294545455	273.3054545
1	6.25N-3.68E	27	281.44	278.37	7.217	271.153	1	6.25N-3.68E	27	281.44	278.37	6.891818182	271.4781818
1	6.25N-3E	28	280.23	277.58	7.853	269.727	1	6.25N-3E	28	280.23	277.58	6.395454545	271.1845455
1	6.25N-2.81E	29	279	276.43	7.414444444	269.0155556	1	6.25N-2.81E	29	279	276.43	7.554545455	268.8754545
1	6N-4.75E	30	283.01	281.07	5.980833333	275.0891667	1	6N-4.75E	30	283.01	281.07	5.766363636	275.3036364
2	6N-4E	31	281.23	279.95	7.6675	272.2825	2	6N-4E	31	281.23	279.95	7.651818182	272.2981818
1	6N-3E	32	278.7	276.85	4.721818182	272.1281818	1	6N-3E	32	278.7	276.85	5.79	271.06
2	6N-2E	33	278.53	275.59	9.216363636	266.3736364	2	6N-2E	33	278.53	275.59	8.722727273	266.8672727
1	5.93N-2E	34	277.72	273.44	6.706363636	266.7336364	1	5.93N-2E	34	277.72	273.44	6.480909091	266.9590909
1	5.87N-2E	35	277.52	273.24	7.057272727	266.1827273	1	5.87N-2E	35	277.52	273.24	6.494545455	266.7454545
1	5.75N-2E	36	276.73	273.71	7.63	266.08	1	5.75N-2E	36	276.73	273.71	6.736363636	266.9736364
2	5.75N-1.75E	37	275.74	273.16	8.933636364	264.2263636	2	5.75N-1.75E	37	275.74	273.16	8.506363636	264.6536364
2	5.75N-1.5E	38	273.84	272.48	9.737272727	262.7427273	2	5.75N-1.5E	38	273.84	272.48	9.247272727	263.2327273
3	5.75N-1E	39	281.09	278.82	16.98	261.84	3	5.75N-1E	39	281.09	278.82	16.82272727	261.9972727
2	5.5N-1.75E	40	275.29	273.25	9.029090909	264.2209091	2	5.5N-1.75E	40	275.29	273.25	8.549090909	264.7009091
2	5.5N-1.25E	41	272.47	271.58	10.11545455	261.4645455	2	5.5N-1.25E	41	272.47	271.58	9.518181818	262.0618182
2	5.37N-0	42	269.25	267.2	10.35545455	256.8445455	2	5.37N-0	42	269.25	267.2	9.805454545	257.3945455
2	5N-4.87E	43	279.89	278.25	9.5525	268.6975	2	5N-4.87E	43	279.89	278.25	10.65454545	267.5954545
2	5N-4E	44	274.73	274.33	10.971	263.359	2	5N-4E	44	274.73	274.33	10.41272727	263.9172727
2	5N-3E	45	274.96	274.96	11.30181818	263.6581818	2	5N-3E	45	274.96	274.96	10.97090909	263.9890909
1	5N-2E	46	276.6	271.19	5.685454545	265.5045455	1	5N-2E	46	276.6	271.19	5.226363636	265.9636364
2	5N-1.75E	47	274.64	272.8	9.842727273	262.9572727	2	5N-1.75E	47	274.64	272.8	9.117272727	263.6827273
2	5N-1.25E	48	272.45	270.25	9.153636364	261.0963636	2	5N-1.25E	48	272.45	270.25	8.771818182	261.4781818
1	5N-1E	49	270.79	268.88	8.237272727	260.6427273	1	5N-1E	49	270.79	268.88	8.046363636	260.8336364
2	5N-0	50	268.53	267.38	10.79909091	256.5809091	2	5N-0	50	268.53	267.38	10.15818182	257.2218182
2	5N-.18W	51	268.73	267.01	9.635714286	257.3742857	2	5N-.18W	51	268.73	267.01	10.739	256.271
2	4.5N-1.75E	52	275.05	272.66	9.916	262.744	2	4.5N-1.75E	52	275.05	272.66	9.834545455	262.8254545
1	4.5N-1.25E	53	270.97	265.72	4.893	260.827	1	4.5N-1.25E	53	270.97	265.72	4.655	261.065
3	4.37N-.5W	54	266.99	267.29	15.75363636	251.5363636	3	4.37N-.5W	54	266.99	267.29	15.16454545	252.1254545

1984	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation	1985	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation
3	4.37N-.87W	55	272.11	267.99	14.87272727	253.1172727	3	4.37N-.87W	55	272.11	267.99	14.41454545	253.5754545
2	4N-4.87E	56	275.43	274.2	7.456666667	266.7433333	2	4N-4.87E	56	275.43	274.2	8.774545455	265.4254545
3	4N-4E	57	278.71	276.19	11.589	264.601	3	4N-4E	57	278.71	276.19	11.46181818	264.7281818
2	4N-3E	58	276.66	274.76	11.52272727	263.2372727	2	4N-3E	58	276.66	274.76	11.10727273	263.6527273
2	4N-2E	59	273.97	272.17	9.34	262.83	2	4N-2E	59	273.97	272.17	8.891818182	263.2781818
2	4N-1.75E	60	272.16	270.91	10.12545455	260.7845455	2	4N-1.75E	60	272.16	270.91	9.380909091	261.5290909
2	4N-1.25E	61	270.54	269.73	9.852727273	259.8772727	2	4N-1.25E	61	270.54	269.73	9.517272727	260.2127273
1	4N-1E	62	271.19	268.04	8.565454545	259.4745455	1	4N-1E	62	271.19	268.04	7.993636364	260.0463636
3	4N-1W	63	274.94	273.86	20.05818182	253.8018182	3	4N-1W	63	274.94	273.86	19.21454545	254.6454545
2	4N-0	64	267.21	266.76	9.347272727	257.4127273	2	4N-0	64	267.21	266.76	9.543636364	257.2163636
2	3.62N-2E	65	272.59	271.02	9.072727273	261.9472727	2	3.62N-2E	65	272.59	271.02	8.912	262.108
1	3.5N-1.75E	66	273.11	269.32	7.685454545	261.6345455	1	3.5N-1.75E	66	273.11	269.32	6.771818182	262.5481818
2	3N-5E	67	273.21	271.27	6.198333333	265.0716667	2	3N-5E	67	273.21	271.27	6.892727273	264.3772727
1	3N-4E	68	269.84	268.38	6.155	262.225	1	3N-4E	68	269.84	268.38	6.821818182	261.5581818
2	3N-3E	69	275.12	272.06	10.78454545	261.2754545	2	3N-3E	69	275.12	272.06	10.90727273	261.1527273
2	3N-2E	70	273.31	271.28	9.005454545	262.2745455	2	3N-2E	70	273.31	271.28	8.622727273	262.6572727
2	3N-1.75E	71	270.9	270.29	9.048181818	261.2418182	2	3N-1.75E	71	270.9	270.29	8.854545455	261.4354545
2	3N-.25W	72	265.42	264.39	9.220909091	255.1690909	2	3N-.25W	72	265.42	264.39	8.967272727	255.4227273
3	3N-1W	73	276.84	276.15	22.54363636	253.6063636	3	3N-1W	73	276.84	276.15	22.11363636	254.0363636
2	2.75N-2.25E	74	272.86	271.44	9.41	262.03	2	2.75N-2.25E	74	272.86	271.44	9.076363636	262.3636364
1	2.75N-1E	75	268.35	267.35	8.47	258.88	1	2.75N-1E	75	268.35	267.35	8.103636364	259.2463636
1	2.5N-2.5E	76	272.63	270.57	6.98	263.59	1	2.5N-2.5E	76	272.63	270.57	7.213636364	263.3563636
1	2.5N-2.62E	77	270.66	269.83	6.224545455	263.6054545	1	2.5N-2.62E	77	270.66	269.83	6.015454545	263.8145455
1	2.5N-2E	78	273.36	271.98	7.530909091	264.4490909	1	2.5N-2E	78	273.36	271.98	7.473636364	264.5063636
1	2.5N-1.87E	79	271.88	271.1	6.510909091	264.5890909	1	2.5N-1.87E	79	271.88	271.1	6.289090909	264.8109091
1	2.5N-1.75E	80	269.69	269.43	5.894545455	263.5354545	1	2.5N-1.75E	80	269.69	269.43	5.925454545	263.5045455
2	2.18N-1.5W	81	270.91	262.69	11.23888889	251.4511111	2	2.18N-1.5W	81	270.91	262.69	9.422	253.268
2	2.25N-2.37E	82	272.91	270.39	8.993636364	261.3963636	2	2.25N-2.37E	82	272.91	270.39	8.696363636	261.6936364
1	2.25N-2E	83	273.99	270.92	6.368181818	264.5518182	1	2.25N-2E	83	273.99	270.92	5.953636364	264.9663636
1	2.25N-1.75E	84	274.41	272.2	8.281818182	263.9181818	1	2.25N-1.75E	84	274.41	272.2	7.584545455	264.6154545
2	2N-5E	85	272.67	269.05	7.645833333	261.4041667	2	2N-5E	85	272.67	269.05	8.477272727	260.5727273
1	2N-2E	86	270.92	270.8	5.869090909	264.9309091	1	2N-2E	86	270.92	270.8	5.65	265.15
1	2N-1E	87	272.09	268.81	7.48	261.33	1	2N-1E	87	272.09	268.81	6.914545455	261.8954545
2	2N-.25E	88	267.59	265.5	8.411818182	257.0881818	2	2N-.25E	88	267.59	265.5	8.49	257.01
2	2N-1.25W	89	263.31	260.77	8.723636364	252.0463636	2	2N-1.25W	89	263.31	260.77	8.859090909	251.9109091
2	1.75N-1.25W	90	264.28	261.73	9.453636364	252.2763636	2	1.75N-1.25W	90	264.28	261.73	9.777272727	251.9527273
2	1.75N-1.75W	91	264.11	261.43	12.00909091	249.4209091	2	1.75N-1.75W	91	264.11	261.43	12.38111111	249.0488889
2	1.5N-1.25W	92	264.18	261.32	10.08181818	251.2381818	2	1.5N-1.25W	92	264.18	261.32	10.27181818	251.0481818
2	1.5N-2W	93	261.32	260.83	11.49090909	249.3390909	2	1.5N-2W	93	261.32	260.83	11.47636364	249.3536364
3	1.5N-2.25W	94	264.6	261.91	14.06454545	247.8454545	3	1.5N-2.25W	94	264.6	261.91	13.65	248.26
2	1.25N-1.5W	95	262.06	260.49	9.097272727	251.3927273	2	1.25N-1.5W	95	262.06	260.49	9.661818182	250.8281818
2	1N-5E	96	271.74	268.72	9.2725	259.4475	2	1N-5E	96	271.74	268.72	10.52	258.2
2	1N-4E	97	266.29	266.02	8.684545455	257.3354545	2	1N-4E	97	266.29	266.02	9.433636364	256.5863636
2	1N-3E	98	267.49	266.62	8.221818182	258.3981818	2	1N-3E	98	267.49	266.62	8.61	258.01
3	1N-2.12E	99	270.74	270.7	12.55909091	258.1409091	3	1N-2.12E	99	270.74	270.7	12.61	258.09
2	1N-1E	100	266.52	266.74	9.46	257.28	2	1N-1E	100	266.52	266.74	9.079090909	257.6609091
2	1N-0	101	264.79	264.5	8.902727273	255.5972727	2	1N-0	101	264.79	264.5	8.896363636	255.6036364
2	1N-.75W	102	261.87	261.01	8.797272727	252.2127273	2	1N-.75W	102	261.87	261.01	9.001818182	252.0081818
2	1N-2W	103	259.68	258.34	9.906363636	248.4336364	2	1N-2W	103	259.68	258.34	10.35727273	247.9827273
2	1N-2.25W	104	257.8	257.52	10.14545455	247.3745455	2	1N-2.25W	104	257.8	257.52	10.62545455	246.8945455
2	0.5N-2.37W	105	258.52	256.72	10.59272727	246.1272727	2	0.5N-2.37W	105	258.52	256.72	10.98636364	245.7336364
2	0.12N-5E	106	269.45	267.07	8.580833333	258.4891667	2	0.12N-5E	106	269.45	267.07	9.77	257.3
2	0-4.12E	107	266.9	266.3	10.99090909	255.3090909	2	0-4.12E	107	266.9	266.3	10.75090909	255.5490909
2	0-3E	108	263.76	262.77	8.558181818	254.2118182	2	0-3E	108	263.76	262.77	8.340909091	254.4290909
2	0-2E	109	267.84	265.18	9.577272727	255.6027273	2	0-2E	109	267.84	265.18	8.888181818	256.2918182

1984	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation	1985	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation
1	0-1E	110	261.7	261.42	7.849090909	253.5709091	1	0-1E	110	261.7	261.42	7.465454545	253.9545455
2	0-0	111	262.37	261.83	8.53	253.3	2	0-0	111	262.37	261.83	8.457272727	253.3727273
2	0-1W	112	260.19	259.7	10.96090909	248.7390909	2	0-1W	112	260.19	259.7	10.75727273	248.9427273
2	0-2W	113	258.18	256.12	10.62181818	245.4981818	2	0-2W	113	258.18	256.12	10.82090909	245.2990909
2	0-2.75W	114	256.48	255.13	11.47454545	243.6554545	2	0-2.75W	114	256.48	255.13	11.72	243.41
2	0.5S-2.75W	115	257.77	255.36	10.27727273	245.0827273	2	0.5S-2.75W	115	257.77	255.36	11.13363636	244.2263636
3	0.5S-3W	116	257.35	255.03	12.87727273	242.1527273	3	0.5S-3W	116	257.35	255.03	13.22636364	241.8036364
2	0.5S-3.18W	117	257.79	254.4	12.20454545	242.1954545	2	0.5S-3.18W	117	257.79	254.4	12.50909091	241.8909091
3	1S-4E	118	268.56	266.74	9.839166667	256.9008333	3	1S-4E	118	268.56	266.74	10.76818182	255.9718182
2	1S-3E	119	263.55	260.73	10.727	250.003	2	1S-3E	119	263.55	260.73	11.145	249.585
2	1S-2E	120	260.54	259.92	11.05363636	248.8663636	2	1S-2E	120	260.54	259.92	11.509	248.411
1	1S-1E	121	261.85	258.57	6.621818182	251.9481818	1	1S-1E	121	261.85	258.57	6.58	251.99
2	1S-.25W	122	258.55	258.53	9.203636364	249.3263636	2	1S-.25W	122	258.55	258.53	9.411818182	249.1181818
2	1S-1W	123	259.49	258.92	10.01636364	248.9036364	2	1S-1W	123	259.49	258.92	10.49727273	248.4227273
2	1S-2W	124	255.99	254.74	10.77454545	243.9654545	2	1S-2W	124	255.99	254.74	11.13727273	243.6027273
2	1S-3W	125	255.47	253.89	11.29	242.6	2	1S-3W	125	255.47	253.89	12.24	241.65
2	1S-3.37W	126	253.86	252.6	11.41545455	241.1845455	2	1S-3.37W	126	253.86	252.6	11.82272727	240.7772727
2	1.25S-4W	127	255.89	252.21	12.07090909	240.1390909	2	1.25S-4W	127	255.89	252.21	12.38545455	239.8245455
2	1.5S-4.5W	128	254.24	250.98	11.997	238.983	2	1.5S-4.5W	128	254.24	250.98	12.34363636	238.6363636
2	1.5S-4.75W	129	252.55	250.98	11.54363636	239.4363636	2	1.5S-4.75W	129	252.55	250.98	12.01636364	238.9636364
2	2S-2.75E	130	261.59	257.83	9.983333333	247.8466667	2	2S-2.75E	130	261.59	257.83	10.32363636	247.5063636
3	2S-3.75E	131	265.35	262.89	10.23083333	252.6591667	3	2S-3.75E	131	265.35	262.89	11.29	251.6
2	2S-2E	132	258.15	257.56	9.771666667	247.7883333	2	2S-2E	132	258.15	257.56	9.981818182	247.5781818
2	2S-1E	133	258.01	255.81	7.83	247.98	2	2S-1E	133	258.01	255.81	7.627	248.183
1	2S-0	134	256.3	255.56	7.880833333	247.6791667	1	2S-0	134	256.3	255.56	8.388181818	247.1718182
2	2S-1W	135	256.21	254.2	7.886666667	246.3133333	2	2S-1W	135	256.21	254.2	8.55	245.65
2	2S-2W	136	254.96	253.48	9.6025	243.8775	2	2S-2W	136	254.96	253.48	9.283636364	244.1963636
2	2S-3W	137	252.16	252.1	11.26416667	240.8358333	2	2S-3W	137	252.16	252.1	11.42454545	240.6754545
2	2S-4W	138	252.33	251.88	12.02	239.86	2	2S-4W	138	252.33	251.88	12.01909091	239.8609091
3	2S-4.5W	139	254.87	252.25	12.99272727	239.2572727	3	2S-4.5W	139	254.87	252.25	13.257	238.993
3	2S-5.12W	140	250.86	249.04	12.42090909	236.6190909	3	2S-5.12W	140	250.86	249.04	12.87	236.17
2	2.5S-5.25W	141	252.87	249.19	11.18666667	238.0033333	2	2.5S-5.25W	141	252.87	249.19	11.84545455	237.3445455
1	2.75S-3.5E	142	260.23	258.41	9.433333333	248.9766667	1	2.75S-3.5E	142	260.23	258.41	10.31444444	248.0955556
3	2.75S-5.25W	143	251.32	249.21	13.24083333	235.9691667	3	2.75S-5.25W	143	251.32	249.21	13.30545455	235.9045455
1	3S-4.37E	144	263.96	262.35	6.2475	256.1025	1	3S-4.37E	144	263.96	262.35	7.016363636	255.3336364
2	3S-3E	145	258.93	257.22	10.21333333	247.0066667	2	3S-3E	145	258.93	257.22	10.79	246.43
2	3S-2E	146	257.91	255.88	10.28333333	245.5966667	2	3S-2E	146	257.91	255.88	10.10909091	245.7709091
2	3S-1E	147	256.81	254.64	9.403333333	245.2366667	2	3S-1E	147	256.81	254.64	9.029090909	245.6109091
2	3S-0	148	253.44	252.09	8.005833333	244.0841667	2	3S-0	148	253.44	252.09	8.381818182	243.7081818
2	3S-1W	149	254.56	252.57	8.5375	244.0325	2	3S-1W	149	254.56	252.57	9.474545455	243.0954545
2	3S-2W	150	253.78	250.84	10.3075	240.5325	2	3S-2W	150	253.78	250.84	9.778181818	241.0618182
2	3S-3W	151	247.32	248.8	9.613333333	239.1866667	2	3S-3W	151	247.32	248.8	9.312727273	239.4872727
2	3S-4W	152	252.11	249.83	11.38166667	238.4483333	2	3S-4W	152	252.11	249.83	11.76454545	238.0654545
3	3S-5.25W	153	251.33	248.77	12.72333333	236.0466667	3	3S-5.25W	153	251.33	248.77	12.77454545	235.9954545
2	3S-5.5W	154	249.57	246.8	9.57	237.23	2	3S-5.5W	154	249.57	246.8	9.757272727	237.0427273
2	3.12S-4.5W	155	251.39	247.97	12.04833333	235.9216667	2	3.12S-4.5W	155	251.39	247.97	11.67727273	236.2927273
2	3.37S-4.5W	156	248.74	247.84	11.31916667	236.5208333	2	3.37S-4.5W	156	248.74	247.84	11.39272727	236.4472727
2	3.5S-5.25W	157	249.04	247.15	10.88666667	236.2633333	2	3.5S-5.25W	157	249.04	247.15	11.08727273	236.0627273
2	3.5S-5.5W	158	248.33	246.1	9.400833333	236.6991667	2	3.5S-5.5W	158	248.33	246.1	9.519090909	236.5809091
2	3.62S-4.75W	159	252.31	248.59	9.883333333	238.7066667	2	3.62S-4.75W	159	252.31	248.59	9.763	238.827
2	3.75S-5.5W	160	247.38	246.61	10.0875	236.5225	2	3.75S-5.5W	160	247.38	246.61	10.19363636	236.4163636
2	3.87S-4.25W	161	248.14	247.62	11.37416667	236.2458333	2	3.87S-4.25W	161	248.14	247.62	11.45272727	236.1672727
2	4S-4E	162	265.61	261.39	8.455454545	252.9345455	2	4S-4E	162	265.61	261.39	10.764	250.626
2	4S-3E	163	260.08	258.94	8.7925	250.1475	2	4S-3E	163	260.08	258.94	9.924545455	249.0154545

1984	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation	1985	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation
3	4S-2E	164	259.63	257.4	13.83583333	243.5641667	3	4S-2E	164	259.63	257.4	14.10090909	243.2990909
3	4S-1E	165	259.23	254.05	13.24083333	240.8091667	3	4S-1E	165	259.23	254.05	13.37454545	240.6754545
2	4S-0	166	252.02	251.67	11.3925	240.2775	2	4S-0	166	252.02	251.67	11.40090909	240.2690909
2	4S-.5W	167	253.41	251.47	11.44333333	240.0266667	2	4S-.5W	167	253.41	251.47	11.14090909	240.3290909
2	4S-.75W	168	253.23	251.32	11.07583333	240.2441667	2	4S-.75W	168	253.23	251.32	11.17272727	240.1472727
3	4S-2W	169	250.85	249.2	14.1125	235.0875	3	4S-2W	169	250.85	249.2	13.78454545	235.4154545
3	4S-3W	170	250.85	249.68	12.74333333	236.9366667	3	4S-3W	170	250.85	249.68	13.04181818	236.6381818
1	4S-4W	171	246.83	246.34	8.188333333	238.1516667	1	4S-4W	171	246.83	246.34	8.176363636	238.1636364
3	4S-4.5W	172	248.53	248.16	12.40416667	235.7558333	3	4S-4.5W	172	248.53	248.16	12.52	235.64
2	4S-5.25W	173	249.14	245.96	9.666666667	236.2933333	2	4S-5.25W	173	249.14	245.96	9.761818182	236.1981818
2	4S-5.5W	174	249.08	246.39	10.10666667	236.2833333	2	4S-5.5W	174	249.08	246.39	10.17636364	236.2136364
2	4S-5.87W	175	252.9	246.47	9.455	237.015	2	4S-5.87W	175	252.9	246.47	9.453636364	237.0163636
2	4.25S-4.12W	176	250.26	247.26	10.65666667	236.6033333	2	4.25S-4.12W	176	250.26	247.26	10.77818182	236.4818182
2	4.25S-4.5W	177	250.4	246.8	11.805	234.995	2	4.25S-4.5W	177	250.4	246.8	12.06090909	234.7390909
2	4.25S-5.5W	178	249.4	246.25	8.415	237.835	2	4.25S-5.5W	178	249.4	246.25	8.881818182	237.3681818
2	4.5S-4.75W	179	247.36	245.52	10.87833333	234.6416667	2	4.5S-4.75W	179	247.36	245.52	10.4	235.12
2	4.5S-5.5W	180	249.47	246.08	8.181666667	237.8983333	2	4.5S-5.5W	180	249.47	246.08	8.43	237.65
2	4.5S-6.25W	181	248.63	246.47	10.42833333	236.0416667	2	4.5S-6.25W	181	248.63	246.47	10.28636364	236.1836364
2	4.75S-4.25W	182	249.14	246.78	10.48916667	236.2908333	2	4.75S-4.25W	182	249.14	246.78	10.77363636	236.0063636
2	4.75S-4.75W	183	246.3	244.5	10.10916667	234.3908333	2	4.75S-4.75W	183	246.3	244.5	10.20272727	234.2972727
2	5S-3E	184	257.68	256.65	7.485	249.165	2	5S-3E	184	257.68	256.65	8.473636364	248.1763636
3	5S-2.25E	185	259.3	257.61	10.08166667	247.5283333	3	5S-2.25E	185	259.3	257.61	11.07222222	246.5377778
3	5S-1E	186	255.81	253.72	13.71181818	240.0081818	3	5S-1E	186	255.81	253.72	14.094	239.626
3	5S-0	187	254.3	251.38	15.04333333	236.3366667	3	5S-0	187	254.3	251.38	14.88818182	236.4918182
3	5S-.75W	188	249.17	248.95	13.8175	235.1325	3	5S-.75W	188	249.17	248.95	13.45818182	235.4918182
3	5S-2W	189	245.35	245.3	12.40833333	232.8916667	3	5S-2W	189	245.35	245.3	12.45909091	232.8409091
2	5S-2.75W	190	244.17	242.59	11.49333333	231.0966667	2	5S-2.75W	190	244.17	242.59	11.32909091	231.2609091
2	5S-3.75W	191	249.28	247.77	9.760833333	238.0091667	2	5S-3.75W	191	249.28	247.77	11.65	236.12
2	5S-4.12W	192	248.93	246.83	10.58916667	236.2408333	2	5S-4.12W	192	248.93	246.83	12.29363636	234.5363636
2	5S-4.5W	193	247.04	244.83	10.88333333	233.9466667	2	5S-4.5W	193	247.04	244.83	10.70363636	234.1263636
2	5S-4.75W	194	246.64	244.38	10.375	234.005	2	5S-4.75W	194	246.64	244.38	9.945454545	234.4345455
2	5S-5.5W	195	245.46	243.81	8.720833333	235.0891667	2	5S-5.5W	195	245.46	243.81	8.153636364	235.6563636
2	5S-6.18W	196	246.48	244.45	9.345833333	235.1041667	2	5S-6.18W	196	246.48	244.45	9.180909091	235.2690909
2	5.5S-.5W	197	247.78	247.18	12.01166667	235.1683333	2	5.5S-.5W	197	247.78	247.18	11.74727273	235.4327273
3	5.5S-1.25W	198	247.32	245.49	12.73833333	232.7516667	3	5.5S-1.25W	198	247.32	245.49	12.73727273	232.7527273
2	5.5S-4.25W	199	248.3	246.29	10.94416667	235.3458333	2	5.5S-4.25W	199	248.3	246.29	12.24454545	234.0454545
3	5.5S-4.5W	200	245.9	244.75	12.42833333	232.3216667	3	5.5S-4.5W	200	245.9	244.75	12.934	231.816
3	5.5S-4.75W	201	246.28	244.05	12.3725	231.6775	3	5.5S-4.75W	201	246.28	244.05	12.80545455	231.2445455
2	5.5S-6.37W	202	246.66	242.63	8.246666667	234.3833333	2	5.5S-6.37W	202	246.66	242.63	8.079090909	234.5509091
2	5.75S-2W	203	243.63	242.33	11.04454545	231.2854545	2	5.75S-2W	203	243.63	242.33	12.12272727	230.2072727
3	6S-3E	204	258.01	256.13	9.83	246.3	3	6S-3E	204	258.01	256.13	11.13727273	244.9927273
2	6S-2E	205	255.23	254.45	7.561666667	246.8883333	2	6S-2E	205	255.23	254.45	8.669090909	245.7809091
3	6S-1.12E	206	256.31	253.73	9.826666667	243.9033333	3	6S-1.12E	206	256.31	253.73	10.97818182	242.7518182
3	6S-2.75W	207	243.98	241.97	11.97083333	229.9991667	3	6S-2.75W	207	243.98	241.97	12.65090909	229.3190909
2	6S-4W	208	245.48	243.84	10.82	233.02	2	6S-4W	208	245.48	243.84	12.00636364	231.8336364
2	6S-4.5W	209	246.86	243.84	11.90916667	231.9308333	2	6S-4.5W	209	246.86	243.84	13.30909091	230.5309091
2	6S-5.5W	210	244.17	242.61	9.294166667	233.3158333	2	6S-5.5W	210	244.17	242.61	8.86	233.75
1	6S-6.25W	211	242.64	240.09	6.140833333	233.9491667	1	6S-6.25W	211	242.64	240.09	6.691818182	233.3981818
3	6.75S-0	212	253.73	249.73	12.04333333	237.6866667	3	6.75S-0	212	253.73	249.73	12.49818182	237.2318182
2	6.87S-1.87E	213	252.93	252.8	7.739	245.061	2	6.87S-1.87E	213	252.93	252.8	9.245454545	243.5545455
2	7S-1E	214	256.75	252.93	8.389166667	244.5408333	2	7S-1E	214	256.75	252.93	9.912727273	243.0172727
2	7S-0	215	251.43	250.34	10.635	239.705	2	7S-0	215	251.43	250.34	11.13090909	239.2090909
2	7S-1W	216	247.64	245.6	11.54333333	234.0566667	2	7S-1W	216	247.64	245.6	11.39545455	234.2045455

1984	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation	1985	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation
2	7S-2W	217	241.33	240.97	10.76	230.21	2	7S-2W	217	241.33	240.97	10.81454545	230.1554545
3	7S-3W	218	241.62	240.88	11.8925	228.9875	3	7S-3W	218	241.62	240.88	12.30363636	228.5763636
2	7S-4W	219	242.52	241.91	11.22083333	230.6891667	2	7S-4W	219	242.52	241.91	11.37090909	230.5390909
2	7S-5W	220	243.43	241.59	9.130833333	232.4591667	2	7S-5W	220	243.43	241.59	9.318181818	232.2718182
2	7S-5.75W	221	244.57	241.86	8.805833333	233.0541667	2	7S-5.75W	221	244.57	241.86	8.666363636	233.1936364
2	7S-6.5W	222	244.09	241.02	9.083333333	231.9366667	2	7S-6.5W	222	244.09	241.02	9.241818182	231.7781818
2	7.25S-.5E	223	253.45	251.73	9.47	242.26	2	7.25S-.5E	223	253.45	251.73	10.66	241.07
2	7.25S-.25E	224	253.46	249.77	9.2	240.57	2	7.25S-.25E	224	253.46	249.77	10.00181818	239.7681818
2	7.25S-.5W	225	248.92	246.58	9.344166667	237.2358333	2	7.25S-.5W	225	248.92	246.58	9.550909091	237.0290909
2	7.25S-.25W	226	250.44	247.1	9.001666667	238.0983333	2	7.25S-.25W	226	250.44	247.1	9.397272727	237.7027273
2	7.75S-0	227	252.5	248.19	8.561666667	239.6283333	2	7.75S-0	227	252.5	248.19	9.706	238.484
2	8S-1E	228	253.51	250.64	8.2025	242.4375	2	8S-1E	228	253.51	250.64	9.309090909	241.3309091
2	8S-.5E	229	253.44	250.07	8.8125	241.2575	2	8S-.5E	229	253.44	250.07	9.469090909	240.6009091
2	8S-.25W	230	246.82	245.02	7.194545455	237.8254545	2	8S-.25W	230	246.82	245.02	8.030909091	236.9890909
1	8S-.5W	231	245.28	243.91	5.807	238.103	1	8S-.5W	231	245.28	243.91	7.18	236.73
1	8S-1W	232	246.82	242.57	6.916666667	235.6533333	1	8S-1W	232	246.82	242.57	6.550909091	236.0190909
2	8S-2W	233	244.92	242.5	9.839166667	232.6608333	2	8S-2W	233	244.92	242.5	8.922727273	233.5772727
2	8S-3W	234	239.43	238.57	10.8775	227.6925	2	8S-3W	234	239.43	238.57	10.18727273	228.3827273
2	8S-5W	235	241.01	239.2	9.965	229.235	2	8S-5W	235	241.01	239.2	10.07272727	229.1272727
1	8S-5.5W	236	239.2	238.37	6.968333333	231.4016667	1	8S-5.5W	236	239.2	238.37	6.943636364	231.4263636
1	8S-6.5W	237	242.17	238.59	7.067272727	231.5227273	1	8S-6.5W	237	242.17	238.59	8.637272727	229.9527273
2	8.25S-4.25W	238	240.34	237.41	10.385	227.025	2	8.25S-4.25W	238	240.34	237.41	10.71727273	226.6927273
3	9S-0	239	250.45	249.42	12.01	237.41	3	9S-0	239	250.45	249.42	12.20545455	237.2145455
2	9S-1.25W	240	243.23	241.76	7.930833333	233.8291667	2	9S-1.25W	240	243.23	241.76	7.651818182	234.1081818
2	9S-2W	241	244.64	241.7	9.639166667	232.0608333	2	9S-2W	241	244.64	241.7	9.191818182	232.5081818
2	9S-3W	242	239.98	237.81	8.894166667	228.9158333	2	9S-3W	242	239.98	237.81	8.88	228.93
2	9S-4W	243	236.84	235.23	10.15727273	225.0727273	2	9S-4W	243	236.84	235.23	10.98	224.25
2	9S-5W	244	236.62	235.18	7.791666667	227.3883333	2	9S-5W	244	236.62	235.18	8.315454545	226.8645455
2	9S-5.75W	245	235.74	236.1	10.01333333	226.0866667	2	9S-5.75W	245	235.74	236.1	10.258	225.842
1	9S-6.5W	246	237.54	235.17	7.445	227.725	1	9S-6.5W	246	237.54	235.17	7.58	227.59
3	10S-0	247	251.76	249.13	11.10833333	238.0216667	3	10S-0	247	251.76	249.13	11.99777778	237.1322222
3	10S-1W	248	249.69	248.18	14.72583333	233.4541667	3	10S-1W	248	249.69	248.18	14.64181818	233.5381818
2	10S-2W	249	242	239.93	9.028333333	230.9016667	2	10S-2W	249	242	239.93	8.526363636	231.4036364
2	10S-3W	250	240.34	237.37	8.3825	228.9875	2	10S-3W	250	240.34	237.37	8.606363636	228.7636364
1	10S-3.87W	251	237.45	235.16	7.689166667	227.4708333	1	10S-3.87W	251	237.45	235.16	7.813636364	227.3463636
2	10S-5W	252	236.47	233.49	9.136666667	224.3533333	2	10S-5W	252	236.47	233.49	8.562222222	224.9277778
2	10S-6.75W	253	236.85	234.71	8.879166667	225.8308333	2	10S-6.75W	253	236.85	234.71	8.650909091	226.0590909
2	10S-5.75W	254	235.76	233.22	7.6625	225.5575	2	10S-5.75W	254	235.76	233.22	7.895454545	225.3245455
2	10.75S-4W	255	236.58	233.4	8.286666667	225.1133333	2	10.75S-4W	255	236.58	233.4	8.682727273	224.7172727
3	11S-1W	256	244.62	243.3	10.69583333	232.6041667	3	11S-1W	256	244.62	243.3	10.90090909	232.3990909
2	11S-2W	257	238.8	237.75	8.173333333	229.5766667	2	11S-2W	257	238.8	237.75	7.434545455	230.3154545
2	11S-3W	258	237.96	236.02	8.035	227.985	2	11S-3W	258	237.96	236.02	8.269090909	227.7509091
2	11S-5W	259	235.02	231.19	8.128181818	223.0618182	2	11S-5W	259	235.02	231.19	8.355454545	222.8345455
2	11S-5.75W	260	234.78	232.35	8.289166667	224.0608333	2	11S-5.75W	260	234.78	232.35	7.798181818	224.5518182
2	11S-6.87W	261	233.32	231.42	9.760833333	221.6591667	2	11S-6.87W	261	233.32	231.42	9.534545455	221.8854545
2	11.75S-6.75W	262	231.3	231	8.28	222.72	2	11.75S-6.75W	262	231.3	231	8.262727273	222.7372727
2	12S-1W	263	238.84	238.29	8.124166667	230.1658333	2	12S-1W	263	238.84	238.29	8.344545455	229.9454545
2	12S-2W	264	237.63	237.11	8.650833333	228.4591667	2	12S-2W	264	237.63	237.11	8.398181818	228.7118182
3	12S-3W	265	242.36	240.04	11.19083333	228.8491667	3	12S-3W	265	242.36	240.04	11.42727273	228.6127273
2	12S-4W	266	237.71	234.84	10.06083333	224.7791667	2	12S-4W	266	237.71	234.84	10.32636364	224.5136364
2	12S-5W	267	236.8	233.16	9.835833333	223.3241667	2	12S-5W	267	236.8	233.16	9.551818182	223.6081818
2	12S-6W	268	233.06	231.72	10.30083333	221.4191667	2	12S-6W	268	233.06	231.72	10.59909091	221.1209091
2	13S-2W	269	242.29	240.58	7.651666667	232.9283333	2	13S-2W	269	242.29	240.58	8.28	232.3

1984	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation	1985	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation
2	13.12S-2.87W	270	243.53	240.58	8.125833333	232.4541667	2	13.12S-2.87W	270	243.53	240.58	9	231.58
1	13S-4.25W	271	234.53	234.31	4.504166667	229.8058333	1	13S-4.25W	271	234.53	234.31	4.684545455	229.6254545
2	13S-5W	272	235.57	233.88	6.741666667	227.1383333	2	13S-5W	272	235.57	233.88	6.594545455	227.2854545
2	13S-6W	273	232.62	231.6	7.705	223.895	2	13S-6W	273	232.62	231.6	8.12	223.48
1	13S-6.5W	274	230.69	228.55	6.778333333	221.7716667	1	13S-6.5W	274	230.69	228.55	7.240909091	221.3090909
2	13S-7.12W	275	233.57	232.23	10.895	221.335	2	13S-7.12W	275	233.57	232.23	11.22181818	221.0081818
1	14.25S-6.5W	276	231.67	228.46	3.801111111	224.6588889	1	14.25S-6.5W	276	231.67	228.46	4.834545455	223.6254545
2	14.25S-7.18W	277	234.11	228.1	8.850833333	219.2491667	2	14.25S-7.18W	277	234.11	228.1	9.376363636	218.7236364
1	15S-6W	278	229.73	228.93	3.7525	225.1775	1	15S-6W	278	229.73	228.93	3.925454545	225.0045455
1	15S-6.75W	279	228.81	226.48	4.319	222.161	1	15S-6.75W	279	228.81	226.48	5.42	221.06
1	16S-6W	280	227.88	226.33	4.16	222.17	1	16S-6W	280	227.88	226.33	3.888181818	222.4418182
1	17S-5W	281	230.06	228.14	3.703636364	224.4363636	1	17S-5W	281	230.06	228.14	3.414545455	224.7254545
1	17S-5.75W	282	227.63	226.14	7.207777778	218.9322222	1	17S-5.75W	282	227.63	226.14	5.281818182	220.8581818
1	18S-5W	283	227.16	224.12			1	18S-5W	283	227.16	224.12		
7.44N-5.44E	OL	286.89	284.1	279.0727273	5.027272727			284.49	284.1	279.5222222	4.577777778	#REF!	
6.25N-3.56E		281.9	279.51	269.3645455	10.14545455			281.44	278.37	268.634	9.736		

1986	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation	1987	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation
3	8N-7E	1	289.11	286.9	12.48416667	274.4158333	3	8N-7E	1	289.11	286.9	14.025	272.875
1	7.5N-5.62E	2	285.26	283.47	3.5425	279.9275	1	7.5N-5.62E	2	285.26	283.47	3.675555556	279.7944444
1	7.41N-5.41E	3	284.49	284.1	4.048333333	280.0516667	1	7.41N-5.41E	3	284.49	284.1	4.164545455	279.9354545
1	7.37N-5.12E	4	284.37	283	3.373333333	279.6266667	1	7.37N-5.12E	4	284.37	283	3.470909091	279.5290909
1	7.37N-4.87E	5	284.65	283.1	4.626666667	278.4733333	1	7.37N-4.87E	5	284.65	283.1	3.893	279.207
1	7.37N-4.75E	6	288.65	285.43	4.58	280.85	1	7.37N-4.75E	6	288.65	285.43	3.849	281.581
1	7.37N-4.25E	7	284.76	283	4.036363636	278.9636364	1	7.37N-4.25E	7	284.76	283	3.783636364	279.2163636
1	7.25N-4.31E	8	284.04	282.02	6.145833333	275.8741667	1	7.25N-4.31E	8	284.04	282.02	5.872	276.148
1	7.18N-4.06E	9	284.93	281	5.7575	275.2425	1	7.18N-4.06E	9	284.93	281	5.968	275.032
1	7.12N-4E	10	283.39	280.09	5.489166667	274.6008333	1	7.12N-4E	10	283.39	280.09	5.587777778	274.5022222
2	7N-7E	11	285.48	283.26	8.432	274.828	2	7N-7E	11	285.48	283.26	10.56454545	272.6954545
1	7N-6.25E	12	286.06	283.51	5.62	277.89	1	7N-6.25E	12	286.06	283.51	#DIV/0!	
1	7N-4.62E	13	285.1	282.5	5.124166667	277.3758333	1	7N-4.62E	13	285.1	282.5	4.527	277.973
1	6.87N-3.93E	14	281.8	280.21	6.016666667	274.1933333	1	6.87N-3.93E	14	281.8	280.21	6.181818182	274.0281818
1	6.87N-3.81E	15	280.88	279.01	4.7625	274.2475	1	6.87N-3.81E	15	280.88	279.01	4.299090909	274.7109091
2	6.75N-3.43E	16	282.35	280.36	9.099166667	271.2608333	2	6.75N-3.43E	16	282.35	280.36	9.726	270.634
1	6.56N-3E	17	279.72	278.64	8.716666667	269.9233333	1	6.56N-3E	17	279.72	278.64	8.990909091	269.6490909
1	6.62N-3.75E	18	279.73	279.26	5.6725	273.5875	1	6.62N-3.75E	18	279.73	279.26	6.729090909	272.5309091
1	6.62N-3E	19	278.02	277.4	7.423333333	269.9766667	1	6.62N-3E	19	278.02	277.4	7.700909091	269.6990909
1	6.5N-3.68E	21	282.44	279.57	8.636666667	270.9333333	1	6.5N-3.68E	21	282.44	279.57	9.068	270.502
1	6.68N-3E	20	278.86	277.68	7.340833333	270.3391667	1	6.68N-3E	20	278.86	277.68	7.757272727	269.9227273
1	6.5N-3E	22	279.41	277.32	7.851666667	269.4683333	1	6.5N-3E	22	279.41	277.32	8.152	269.168
1	6.5N-2.81E	23	279.34	275.74	6.640833333	269.0991667	1	6.5N-2.81E	23	279.34	275.74	7.009090909	268.7309091
1	6.37N-3E	24	279.41	277.45	7.474166667	269.9758333	1	6.37N-3E	24	279.41	277.45	7.931	269.519
2	6.25N-6E	25	285.89	283.47	9.434166667	274.0358333	2	6.25N-6E	25	285.89	283.47	11.05	272.42
1	6.25N-4E	26	283.8	280.6	8.055833333	272.5441667	1	6.25N-4E	26	283.8	280.6	8.146363636	272.4536364
1	6.25N-3.68E	27	281.44	278.37	8.809166667	269.5608333	1	6.25N-3.68E	27	281.44	278.37	9.128181818	269.2418182
1	6.25N-3E	28	280.23	277.58	7.2375	270.3425	1	6.25N-3E	28	280.23	277.58	8.211818182	269.3681818
1	6.25N-2.81E	29	279	276.43	7.6225	268.8075	1	6.25N-2.81E	29	279	276.43	7.746	268.684
1	6N-4.75E	30	283.01	281.07	6.583333333	274.4866667	1	6N-4.75E	30	283.01	281.07	7.095	273.975
2	6N-4E	31	281.23	279.95	8.19	271.76	2	6N-4E	31	281.23	279.95	8.885	271.065
1	6N-3E	32	278.7	276.85	6.945	269.905	1	6N-3E	32	278.7	276.85	6.862	269.988
2	6N-2E	33	278.53	275.59	9.383333333	266.2066667	2	6N-2E	33	278.53	275.59	9.05	266.54
1	5.93N-2E	34	277.72	273.44	6.491666667	266.9483333	1	5.93N-2E	34	277.72	273.44	6.678181818	266.7618182
1	5.87N-2E	35	277.52	273.24	6.83	266.41	1	5.87N-2E	35	277.52	273.24	6.638	266.602
1	5.75N-2E	36	276.73	273.71	7.078333333	266.6316667	1	5.75N-2E	36	276.73	273.71	6.849090909	266.8609091
2	5.75N-1.75E	37	275.74	273.16	8.87	264.29	2	5.75N-1.75E	37	275.74	273.16	8.963636364	264.1963636
2	5.75N-1.5E	38	273.84	272.48	9.583333333	262.8966667	2	5.75N-1.5E	38	273.84	272.48	9.731818182	262.7481818
3	5.75N-1E	39	281.09	278.82	17.33166667	261.4883333	3	5.75N-1E	39	281.09	278.82	17.362	261.458
2	5.5N-1.75E	40	275.29	273.25	9.016666667	264.2333333	2	5.5N-1.75E	40	275.29	273.25	8.947272727	264.3027273
2	5.5N-1.25E	41	272.47	271.58	9.725833333	261.8541667	2	5.5N-1.25E	41	272.47	271.58	10.02272727	261.5572727
2	5.37N-0	42	269.25	267.2	10.19333333	257.0066667	2	5.37N-0	42	269.25	267.2	9.882727273	257.3172727
2	5N-4.87E	43	279.89	278.25	10.40666667	267.8433333	2	5N-4.87E	43	279.89	278.25	12.139	266.111
2	5N-4E	44	274.73	274.33	11.16777778	263.1622222	2	5N-4E	44	274.73	274.33	9.616666667	264.7133333
2	5N-3E	45	274.96	274.96	11.95583333	263.0041667	2	5N-3E	45	274.96	274.96	11.899	263.061
1	5N-2E	46	276.6	271.19	5.188333333	266.0016667	1	5N-2E	46	276.6	271.19	5.149	266.041
2	5N-1.75E	47	274.64	272.8	9.309166667	263.4908333	2	5N-1.75E	47	274.64	272.8	9.461818182	263.3381818
2	5N-1.25E	48	272.45	270.25	8.889166667	261.3608333	2	5N-1.25E	48	272.45	270.25	9.041818182	261.2081818
1	5N-1E	49	270.79	268.88	8.1025	260.7775	1	5N-1E	49	270.79	268.88	8.05	260.83
2	5N-0	50	268.53	267.38	10.34916667	257.0308333	2	5N-0	50	268.53	267.38	10.24545455	257.1345455
2	5N-.18W	51	268.73	267.01	10.64333333	256.3666667	2	5N-.18W	51	268.73	267.01	10.37545455	256.6345455
2	4.5N-1.75E	52	275.05	272.66	9.590909091	263.0690909	2	4.5N-1.75E	52	275.05	272.66	9.95625	262.70375
1	4.5N-1.25E	53	270.97	265.72	4.7825	260.9375	1	4.5N-1.25E	53	270.97	265.72	4.921818182	260.7981818
3	4.37N-.5W	54	266.99	267.29	15.4975	251.7925	3	4.37N-.5W	54	266.99	267.29	15.31909091	251.9709091

1986	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation	1987	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation
3	4.37N-.87W	55	272.11	267.99	14.62416667	253.3658333	3	4.37N-.87W	55	272.11	267.99	14.40818182	253.5818182
2	4N-4.87E	56	275.43	274.2	8.886666667	265.3133333	2	4N-4.87E	56	275.43	274.2	10.255	263.945
3	4N-4E	57	278.71	276.19	12.05166667	264.1383333	3	4N-4E	57	278.71	276.19	12	264.19
2	4N-3E	58	276.66	274.76	12.29166667	262.4683333	2	4N-3E	58	276.66	274.76	12.495	262.265
2	4N-2E	59	273.97	272.17	9.0875	263.0825	2	4N-2E	59	273.97	272.17	9.086666667	263.0833333
2	4N-1.75E	60	272.16	270.91	9.595833333	261.3141667	2	4N-1.75E	60	272.16	270.91	8.564	262.346
2	4N-1.25E	61	270.54	269.73	9.449090909	260.2809091	2	4N-1.25E	61	270.54	269.73	9.283636364	260.4463636
1	4N-1E	62	271.19	268.04	7.795833333	260.2441667	1	4N-1E	62	271.19	268.04	7.952	260.088
3	4N-1W	63	274.94	273.86	20.02416667	253.8358333	3	4N-1W	63	274.94	273.86	19.84090909	254.0190909
2	4N-0	64	267.21	266.76	9.731666667	257.0283333	2	4N-0	64	267.21	266.76	#DIV/0!	
2	3.62N-2E	65	272.59	271.02	9.004166667	262.0158333	2	3.62N-2E	65	272.59	271.02	9.089090909	261.9309091
1	3.5N-1.75E	66	273.11	269.32	7.4075	261.9125	1	3.5N-1.75E	66	273.11	269.32	7.238181818	262.0818182
2	3N-5E	67	273.21	271.27	7.8175	263.4525	2	3N-5E	67	273.21	271.27	9.405454545	261.8645455
1	3N-4E	68	269.84	268.38	7.141666667	261.2383333	1	3N-4E	68	269.84	268.38	7.273636364	261.1063636
2	3N-3E	69	275.12	272.06	11.32333333	260.7366667	2	3N-3E	69	275.12	272.06	11.19181818	260.8681818
2	3N-2E	70	273.31	271.28	8.715	262.565	2	3N-2E	70	273.31	271.28	8.57	262.71
2	3N-1.75E	71	270.9	270.29	8.721666667	261.5683333	2	3N-1.75E	71	270.9	270.29	8.453636364	261.8363636
2	3N-.25W	72	265.42	264.39	9.090833333	255.2991667	2	3N-.25W	72	265.42	264.39	9.095454545	255.2945455
3	3N-1W	73	276.84	276.15	22.66	253.49	3	3N-1W	73	276.84	276.15	22.38181818	253.7681818
2	2.75N-2.25E	74	272.86	271.44	9.113333333	262.3266667	2	2.75N-2.25E	74	272.86	271.44	8.76	262.68
1	2.75N-1E	75	268.35	267.35	7.559166667	259.7908333	1	2.75N-1E	75	268.35	267.35	7.141	260.209
1	2.5N-2.5E	76	272.63	270.57	6.895	263.675	1	2.5N-2.5E	76	272.63	270.57	7.132	263.438
1	2.5N-2.62E	77	270.66	269.83	5.776666667	264.0533333	1	2.5N-2.62E	77	270.66	269.83	5.799	264.031
1	2.5N-2E	78	273.36	271.98	7.015833333	264.9641667	1	2.5N-2E	78	273.36	271.98	6.91	265.07
1	2.5N-1.87E	79	271.88	271.1	5.941666667	265.1583333	1	2.5N-1.87E	79	271.88	271.1	5.693	265.407
1	2.5N-1.75E	80	269.69	269.43	5.36	264.07	1	2.5N-1.75E	80	269.69	269.43	5.159090909	264.2709091
2	2.18N-1.5W	81	270.91	262.69	11.54272727	251.1472727	2	2.18N-1.5W	81	270.91	262.69	11.21818182	251.4718182
2	2.25N-2.37E	82	272.91	270.39	8.162	262.228	2	2.25N-2.37E	82	272.91	270.39	7.899	262.491
1	2.25N-2E	83	273.99	270.92	5.240833333	265.6791667	1	2.25N-2E	83	273.99	270.92	5.215555556	265.7044444
1	2.25N-1.75E	84	274.41	272.2	7.025833333	265.1741667	1	2.25N-1.75E	84	274.41	272.2	7.314	264.886
2	2N-5E	85	272.67	269.05	8.565	260.485	2	2N-5E	85	272.67	269.05	9.374545455	259.6754545
1	2N-2E	86	270.92	270.8	4.578333333	266.2216667	1	2N-2E	86	270.92	270.8	5.143	265.657
1	2N-1E	87	272.09	268.81	6.879166667	261.9308333	1	2N-1E	87	272.09	268.81	7.442	261.368
2	2N-.25E	88	267.59	265.5	8.15	257.35	2	2N-.25E	88	267.59	265.5	8.193	257.307
2	2N-1.25W	89	263.31	260.77	8.865833333	251.9041667	2	2N-1.25W	89	263.31	260.77	8.785454545	251.9845455
2	1.75N-1.25W	90	264.28	261.73	9.839166667	251.8908333	2	1.75N-1.25W	90	264.28	261.73	9.803	251.927
2	1.75N-1.75W	91	264.11	261.43	12.40583333	249.0241667	2	1.75N-1.75W	91	264.11	261.43	12.01818182	249.4118182
2	1.5N-1.25W	92	264.18	261.32	10.64833333	250.6716667	2	1.5N-1.25W	92	264.18	261.32	10.615	250.705
2	1.5N-2W	93	261.32	260.83	11.13666667	249.6933333	2	1.5N-2W	93	261.32	260.83	11.23545455	249.5945455
3	1.5N-2.25W	94	264.6	261.91	13.64583333	248.2641667	3	1.5N-2.25W	94	264.6	261.91	13.819	248.091
2	1.25N-1.5W	95	262.06	260.49	9.995833333	250.4941667	2	1.25N-1.5W	95	262.06	260.49	9.436	251.054
2	1N-5E	96	271.74	268.72	10.96833333	257.7516667	2	1N-5E	96	271.74	268.72	12.38909091	256.3309091
2	1N-4E	97	266.29	266.02	9.800833333	256.2191667	2	1N-4E	97	266.29	266.02	10.11454545	255.9054545
2	1N-3E	98	267.49	266.62	8.469166667	258.1508333	2	1N-3E	98	267.49	266.62	9.546363636	257.0736364
3	1N-2.12E	99	270.74	270.7	12.17916667	258.5208333	3	1N-2.12E	99	270.74	270.7	12.58363636	258.1163636
2	1N-1E	100	266.52	266.74	8.895	257.845	2	1N-1E	100	266.52	266.74	8.941818182	257.7981818
2	1N-0	101	264.79	264.5	8.705	255.795	2	1N-0	101	264.79	264.5	8.447272727	256.0527273
2	1N-.75W	102	261.87	261.01	8.781666667	252.2283333	2	1N-.75W	102	261.87	261.01	8.56	252.45
2	1N-2W	103	259.68	258.34	10.60333333	247.7366667	2	1N-2W	103	259.68	258.34	10.3	248.04
2	1N-2.25W	104	257.8	257.52	10.85	246.67	2	1N-2.25W	104	257.8	257.52	10.50636364	247.0136364
2	0.5N-2.37W	105	258.52	256.72	11.41416667	245.3058333	2	0.5N-2.37W	105	258.52	256.72	11.19545455	245.5245455
2	0.12N-5E	106	269.45	267.07	10.4075	256.6625	2	0.12N-5E	106	269.45	267.07	11.80636364	255.2636364
2	0-4.12E	107	266.9	266.3	10.92375	255.37625	2	0-4.12E	107	266.9	266.3	10.99363636	255.3063636
2	0-3E	108	263.76	262.77	8.728333333	254.0416667	2	0-3E	108	263.76	262.77	8.709090909	254.0609091
2	0-2E	109	267.84	265.18	8.808333333	256.3716667	2	0-2E	109	267.84	265.18	9.079090909	256.1009091

1986	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation	1987	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation
1	0-1E	110	261.7	261.42	7.3125	254.1075	1	0-1E	110	261.7	261.42	7.367272727	254.0527273
2	0-0	111	262.37	261.83	8.37	253.46	2	0-0	111	262.37	261.83	7.704545455	254.1254545
2	0-1W	112	260.19	259.7	10.84916667	248.8508333	2	0-1W	112	260.19	259.7	10.64181818	249.0581818
2	0-2W	113	258.18	256.12	11.17833333	244.9416667	2	0-2W	113	258.18	256.12	11.18636364	244.9336364
2	0-2.75W	114	256.48	255.13	11.835	243.295	2	0-2.75W	114	256.48	255.13	11.59727273	243.5327273
2	0.5S-2.75W	115	257.77	255.36	11.07	244.29	2	0.5S-2.75W	115	257.77	255.36	10.69454545	244.6654545
3	0.5S-3W	116	257.35	255.03	13.1275	241.9025	3	0.5S-3W	116	257.35	255.03	12.897	242.133
2	0.5S-3.18W	117	257.79	254.4	12.725	241.675	2	0.5S-3.18W	117	257.79	254.4	12.21272727	242.1872727
3	1S-4E	118	268.56	266.74	11.95416667	254.7858333	3	1S-4E	118	268.56	266.74	13.092	253.648
2	1S-3E	119	263.55	260.73	9.723	251.007	2	1S-3E	119	263.55	260.73	11.02818182	249.7018182
2	1S-2E	120	260.54	259.92	10.37333333	249.5466667	2	1S-2E	120	260.54	259.92	10.28090909	249.6390909
1	1S-1E	121	261.85	258.57	6.509166667	252.0608333	1	1S-1E	121	261.85	258.57	6.677	251.893
2	1S-.25W	122	258.55	258.53	8.471666667	250.0583333	2	1S-.25W	122	258.55	258.53	8.251818182	250.2781818
2	1S-1W	123	259.49	258.92	10.69166667	248.2283333	2	1S-1W	123	259.49	258.92	10.686	248.234
2	1S-2W	124	255.99	254.74	11.51833333	243.2216667	2	1S-2W	124	255.99	254.74	11.92727273	242.8127273
2	1S-3W	125	255.47	253.89	12.23333333	241.6566667	2	1S-3W	125	255.47	253.89	11.92909091	241.9609091
2	1S-3.37W	126	253.86	252.6	11.89166667	240.7083333	2	1S-3.37W	126	253.86	252.6	11.49272727	241.1072727
2	1.25S-4W	127	255.89	252.21	12.33333333	239.8766667	2	1.25S-4W	127	255.89	252.21	12.36454545	239.8454545
2	1.5S-4.5W	128	254.24	250.98	12.17545455	238.8045455	2	1.5S-4.5W	128	254.24	250.98	11.92818182	239.0518182
2	1.5S-4.75W	129	252.55	250.98	11.8325	239.1475	2	1.5S-4.75W	129	252.55	250.98	11.62636364	239.3536364
2	2S-2.75E	130	261.59	257.83	10.59416667	247.2358333	2	2S-2.75E	130	261.59	257.83	10.90727273	246.9227273
3	2S-3.75E	131	265.35	262.89	11.66166667	251.2283333	3	2S-3.75E	131	265.35	262.89	12.57222222	250.3177778
2	2S-2E	132	258.15	257.56	10.09916667	247.4608333	2	2S-2E	132	258.15	257.56	10.74818182	246.8118182
2	2S-1E	133	258.01	255.81	7.108333333	248.7016667	2	2S-1E	133	258.01	255.81	8.156363636	247.6536364
1	2S-0	134	256.3	255.56	8.425454545	247.1345455	1	2S-0	134	256.3	255.56	9	246.56
2	2S-1W	135	256.21	254.2	9.175	245.025	2	2S-1W	135	256.21	254.2	9.68	244.52
2	2S-2W	136	254.96	253.48	9.225	244.255	2	2S-2W	136	254.96	253.48	10.508	242.972
2	2S-3W	137	252.16	252.1	9.7925	242.3075	2	2S-3W	137	252.16	252.1	10.46727273	241.6327273
2	2S-4W	138	252.33	251.88	11.41636364	240.4636364	2	2S-4W	138	252.33	251.88	11.59909091	240.2809091
3	2S-4.5W	139	254.87	252.25	13.10916667	239.1408333	3	2S-4.5W	139	254.87	252.25	12.70727273	239.5427273
3	2S-5.12W	140	250.86	249.04	12.72166667	236.3183333	3	2S-5.12W	140	250.86	249.04	12.19181818	236.8481818
2	2.5S-5.25W	141	252.87	249.19	12.11916667	237.0708333	2	2.5S-5.25W	141	252.87	249.19	11.89454545	237.2954545
1	2.75S-3.5E	142	260.23	258.41	11.37666667	247.0333333	1	2.75S-3.5E	142	260.23	258.41	12.20818182	246.2018182
3	2.75S-5.25W	143	251.32	249.21	13.0475	236.1625	3	2.75S-5.25W	143	251.32	249.21	12.85545455	236.3545455
1	3S-4.37E	144	263.96	262.35	7.370833333	254.9791667	1	3S-4.37E	144	263.96	262.35	7.896666667	254.4533333
2	3S-3E	145	258.93	257.22	11.38583333	245.8341667	2	3S-3E	145	258.93	257.22	11.46272727	245.7572727
2	3S-2E	146	257.91	255.88	10.75666667	245.1233333	2	3S-2E	146	257.91	255.88	11.55181818	244.3281818
2	3S-1E	147	256.81	254.64	9.1675	245.4725	2	3S-1E	147	256.81	254.64	10.404	244.236
2	3S-0	148	253.44	252.09	9.253333333	242.8366667	2	3S-0	148	253.44	252.09	9.459090909	242.6309091
2	3S-1W	149	254.56	252.57	10.05	242.52	2	3S-1W	149	254.56	252.57	10.78363636	241.7863636
2	3S-2W	150	253.78	250.84	10.63083333	240.2091667	2	3S-2W	150	253.78	250.84	10.98545455	239.8545455
2	3S-3W	151	247.32	248.8	10.14333333	238.6566667	2	3S-3W	151	247.32	248.8	10.072	238.728
2	3S-4W	152	252.11	249.83	11.56083333	238.2691667	2	3S-4W	152	252.11	249.83	11.55181818	238.2781818
3	3S-5.25W	153	251.33	248.77	12.22666667	236.5433333	3	3S-5.25W	153	251.33	248.77	11.949	236.821
2	3S-5.5W	154	249.57	246.8	9.3075	237.4925	2	3S-5.5W	154	249.57	246.8	9.299090909	237.5009091
2	3.12S-4.5W	155	251.39	247.97	11.7125	236.2575	2	3.12S-4.5W	155	251.39	247.97	11.63090909	236.3390909
2	3.37S-4.5W	156	248.74	247.84	11.635	236.205	2	3.37S-4.5W	156	248.74	247.84	11.54545455	236.2945455
2	3.5S-5.25W	157	249.04	247.15	10.83583333	236.3141667	2	3.5S-5.25W	157	249.04	247.15	10.49272727	236.6572727
2	3.5S-5.5W	158	248.33	246.1	9.865	236.235	2	3.5S-5.5W	158	248.33	246.1	9.66	236.44
2	3.62S-4.75W	159	252.31	248.59	9.949166667	238.6408333	2	3.62S-4.75W	159	252.31	248.59	9.77	238.82
2	3.75S-5.5W	160	247.38	246.61	10.13333333	236.4766667	2	3.75S-5.5W	160	247.38	246.61	9.802	236.808
2	3.87S-4.25W	161	248.14	247.62	11.43666667	236.1833333	2	3.87S-4.25W	161	248.14	247.62	11.27090909	236.3490909
2	4S-4E	162	265.61	261.39	11.195	250.195	2	4S-4E	162	265.61	261.39	12.59272727	248.7972727
2	4S-3E	163	260.08	258.94	11.07416667	247.8658333	2	4S-3E	163	260.08	258.94	12.19	246.75

1986	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation	1987	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation
3	4S-2E	164	259.63	257.4	15.00083333	242.3991667	3	4S-2E	164	259.63	257.4	15.30363636	242.0963636
3	4S-1E	165	259.23	254.05	13.8625	240.1875	3	4S-1E	165	259.23	254.05	14.14545455	239.9045455
2	4S-0	166	252.02	251.67	12.05416667	239.6158333	2	4S-0	166	252.02	251.67	12.171	239.499
2	4S-.5W	167	253.41	251.47	11.99833333	239.4716667	2	4S-.5W	167	253.41	251.47	11.95	239.52
2	4S-.75W	168	253.23	251.32	11.825	239.495	2	4S-.75W	168	253.23	251.32	11.64	239.68
3	4S-2W	169	250.85	249.2	13.9975	235.2025	3	4S-2W	169	250.85	249.2	14.34181818	234.8581818
3	4S-3W	170	250.85	249.68	13.37272727	236.3072727	3	4S-3W	170	250.85	249.68	13.099	236.581
1	4S-4W	171	246.83	246.34	8.295	238.045	1	4S-4W	171	246.83	246.34	8.222	238.118
3	4S-4.5W	172	248.53	248.16	12.36916667	235.7908333	3	4S-4.5W	172	248.53	248.16	#DIV/0!	
2	4S-5.25W	173	249.14	245.96	9.359166667	236.6008333	2	4S-5.25W	173	249.14	245.96	9.04	236.92
2	4S-5.5W	174	249.08	246.39	10.24083333	236.1491667	2	4S-5.5W	174	249.08	246.39	10.01454545	236.3754545
2	4S-5.87W	175	252.9	246.47	9.355	237.115	2	4S-5.87W	175	252.9	246.47	9.355454545	237.1145455
2	4.25S-4.12W	176	250.26	247.26	10.58333333	236.6766667	2	4.25S-4.12W	176	250.26	247.26	10.45	236.81
2	4.25S-4.5W	177	250.4	246.8	11.75916667	235.0408333	2	4.25S-4.5W	177	250.4	246.8	11.856	234.944
2	4.25S-5.5W	178	249.4	246.25	9.126666667	237.1233333	2	4.25S-5.5W	178	249.4	246.25	8.993	237.257
2	4.5S-4.75W	179	247.36	245.52	10.805	234.715	2	4.5S-4.75W	179	247.36	245.52	10.84818182	234.6718182
2	4.5S-5.5W	180	249.47	246.08	9.133333333	236.9466667	2	4.5S-5.5W	180	249.47	246.08	8.711	237.369
2	4.5S-6.25W	181	248.63	246.47	10.72583333	235.7441667	2	4.5S-6.25W	181	248.63	246.47	10.61272727	235.8572727
2	4.75S-4.25W	182	249.14	246.78	10.8525	235.9275	2	4.75S-4.25W	182	249.14	246.78	10.362	236.418
2	4.75S-4.75W	183	246.3	244.5	10.47083333	234.0291667	2	4.75S-4.75W	183	246.3	244.5	10.27545455	234.2245455
2	5S-3E	184	257.68	256.65	9.471818182	247.1781818	2	5S-3E	184	257.68	256.65	11.40727273	245.2427273
3	5S-2.25E	185	259.3	257.61	11.89833333	245.7116667	3	5S-2.25E	185	259.3	257.61	13.31727273	244.2927273
3	5S-1E	186	255.81	253.72	14.64833333	239.0716667	3	5S-1E	186	255.81	253.72	15.046	238.674
3	5S-0	187	254.3	251.38	14.7525	236.6275	3	5S-0	187	254.3	251.38	14.82909091	236.5509091
3	5S-.75W	188	249.17	248.95	13.51416667	235.4358333	3	5S-.75W	188	249.17	248.95	13.43636364	235.5136364
3	5S-2W	189	245.35	245.3	12.26583333	233.0341667	3	5S-2W	189	245.35	245.3	12.438	232.862
2	5S-2.75W	190	244.17	242.59	11.62454545	230.9654545	2	5S-2.75W	190	244.17	242.59	11.74777778	230.8422222
2	5S-3.75W	191	249.28	247.77	11.7125	236.0575	2	5S-3.75W	191	249.28	247.77	11.548	236.222
2	5S-4.12W	192	248.93	246.83	10.76416667	236.0658333	2	5S-4.12W	192	248.93	246.83	10.99	235.84
2	5S-4.5W	193	247.04	244.83	11.04916667	233.7808333	2	5S-4.5W	193	247.04	244.83	10.957	233.873
2	5S-4.75W	194	246.64	244.38	10.0225	234.3575	2	5S-4.75W	194	246.64	244.38	10.334	234.046
2	5S-5.5W	195	245.46	243.81	8.895833333	234.9141667	2	5S-5.5W	195	245.46	243.81	8.968181818	234.8418182
2	5S-6.18W	196	246.48	244.45	9.893333333	234.5566667	2	5S-6.18W	196	246.48	244.45	9.869090909	234.5809091
2	5.5S-.5W	197	247.78	247.18	11.89	235.29	2	5.5S-.5W	197	247.78	247.18	12.059	235.121
3	5.5S-1.25W	198	247.32	245.49	12.66	232.83	3	5.5S-1.25W	198	247.32	245.49	12.81818182	232.6718182
2	5.5S-4.25W	199	248.3	246.29	10.65583333	235.6341667	2	5.5S-4.25W	199	248.3	246.29	10.471	235.819
3	5.5S-4.5W	200	245.9	244.75	12.26333333	232.4866667	3	5.5S-4.5W	200	245.9	244.75	12.231	232.519
3	5.5S-4.75W	201	246.28	244.05	12.775	231.275	3	5.5S-4.75W	201	246.28	244.05	13.39	230.66
2	5.5S-6.37W	202	246.66	242.63	8.9675	233.6625	2	5.5S-6.37W	202	246.66	242.63	8.97	233.66
2	5.75S-2W	203	243.63	242.33	12.34416667	229.9858333	2	5.75S-2W	203	243.63	242.33	11.87363636	230.4563636
3	6S-3E	204	258.01	256.13	12.271	243.859	3	6S-3E	204	258.01	256.13	13.68727273	242.4427273
2	6S-2E	205	255.23	254.45	9.16	245.29	2	6S-2E	205	255.23	254.45	11.40636364	243.0436364
3	6S-1.12E	206	256.31	253.73	10.89083333	242.8391667	3	6S-1.12E	206	256.31	253.73	12.02181818	241.7081818
3	6S-2.75W	207	243.98	241.97	13.25166667	228.7183333	3	6S-2.75W	207	243.98	241.97	11.90181818	230.0681818
2	6S-4W	208	245.48	243.84	10.9375	232.9025	2	6S-4W	208	245.48	243.84	11.513	232.327
2	6S-4.5W	209	246.86	243.84	12.46333333	231.3766667	2	6S-4.5W	209	246.86	243.84	12.38272727	231.4572727
2	6S-5.5W	210	244.17	242.61	9.564166667	233.0458333	2	6S-5.5W	210	244.17	242.61	9.553636364	233.0563636
1	6S-6.25W	211	242.64	240.09	7.395833333	232.6941667	1	6S-6.25W	211	242.64	240.09	7.203	232.887
3	6.75S-0	212	253.73	249.73	12.39363636	237.3363636	3	6.75S-0	212	253.73	249.73	13.097	236.633
2	6.87S-1.87E	213	252.93	252.8	9.345	243.455	2	6.87S-1.87E	213	252.93	252.8	11.5	241.3
2	7S-1E	214	256.75	252.93	9.37	243.56	2	7S-1E	214	256.75	252.93	11.309	241.621
2	7S-0	215	251.43	250.34	10.89	239.45	2	7S-0	215	251.43	250.34	11.26363636	239.0763636
2	7S-1W	216	247.64	245.6	11.74090909	233.8590909	2	7S-1W	216	247.64	245.6	11.84818182	233.7518182

1986	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation	1987	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation
2	7S-2W	217	241.33	240.97	10.9175	230.0525	2	7S-2W	217	241.33	240.97	10.82818182	230.1418182
3	7S-3W	218	241.62	240.88	12.36166667	228.5183333	3	7S-3W	218	241.62	240.88	12.203	228.677
2	7S-4W	219	242.52	241.91	11.5	230.41	2	7S-4W	219	242.52	241.91	11.726	230.184
2	7S-5W	220	243.43	241.59	9.145833333	232.4441667	2	7S-5W	220	243.43	241.59	9.099	232.491
2	7S-5.75W	221	244.57	241.86	9.359166667	232.5008333	2	7S-5.75W	221	244.57	241.86	9.388181818	232.4718182
2	7S-6.5W	222	244.09	241.02	9.981666667	231.0383333	2	7S-6.5W	222	244.09	241.02	9.489090909	231.5309091
2	7.25S-.5E	223	253.45	251.73	10.394	241.336	2	7.25S-.5E	223	253.45	251.73	11.81272727	239.9172727
2	7.25S-.25E	224	253.46	249.77	9.802727273	239.9672727	2	7.25S-.25E	224	253.46	249.77	10.90545455	238.8645455
2	7.25S-.5W	225	248.92	246.58	9.726666667	236.8533333	2	7.25S-.5W	225	248.92	246.58	10.17363636	236.4063636
2	7.25S-.25W	226	250.44	247.1	9.43	237.67	2	7.25S-.25W	226	250.44	247.1	10.10727273	236.9927273
2	7.75S-0	227	252.5	248.19	9.443333333	238.7466667	2	7.75S-0	227	252.5	248.19	10.39818182	237.7918182
2	8S-1E	228	253.51	250.64	9.4325	241.2075	2	8S-1E	228	253.51	250.64	11.57363636	239.0663636
2	8S-.5E	229	253.44	250.07	9.206666667	240.8633333	2	8S-.5E	229	253.44	250.07	10.937	239.133
2	8S-.25W	230	246.82	245.02	8.4275	236.5925	2	8S-.25W	230	246.82	245.02	8.426363636	236.5936364
1	8S-.5W	231	245.28	243.91	7.464166667	236.4458333	1	8S-.5W	231	245.28	243.91	7.945454545	235.9645455
1	8S-1W	232	246.82	242.57	6.434166667	236.1358333	1	8S-1W	232	246.82	242.57	7.079	235.491
2	8S-2W	233	244.92	242.5	9.245833333	233.2541667	2	8S-2W	233	244.92	242.5	9.535	232.965
2	8S-3W	234	239.43	238.57	10.35166667	228.2183333	2	8S-3W	234	239.43	238.57	10.459	228.111
2	8S-5W	235	241.01	239.2	11.13	228.07	2	8S-5W	235	241.01	239.2	10.812	228.388
1	8S-5.5W	236	239.2	238.37	7.543333333	230.8266667	1	8S-5.5W	236	239.2	238.37	7.582727273	230.7872727
1	8S-6.5W	237	242.17	238.59	8.331666667	230.2583333	1	8S-6.5W	237	242.17	238.59	8.444	230.146
2	8.25S-4.25W	238	240.34	237.41	10.8925	226.5175	2	8.25S-4.25W	238	240.34	237.41	11.243	226.167
3	9S-0	239	250.45	249.42	12.56666667	236.8533333	3	9S-0	239	250.45	249.42	13.97545455	235.4445455
2	9S-1.25W	240	243.23	241.76	8.04	233.72	2	9S-1.25W	240	243.23	241.76	8.225454545	233.5345455
2	9S-2W	241	244.64	241.7	9.495	232.205	2	9S-2W	241	244.64	241.7	9.812	231.888
2	9S-3W	242	239.98	237.81	8.753333333	229.0566667	2	9S-3W	242	239.98	237.81	9.249	228.561
2	9S-4W	243	236.84	235.23	11.33	223.9	2	9S-4W	243	236.84	235.23	11.27545455	223.9545455
2	9S-5W	244	236.62	235.18	9.440833333	225.7391667	2	9S-5W	244	236.62	235.18	9.453	225.727
2	9S-5.75W	245	235.74	236.1	10.54333333	225.5566667	2	9S-5.75W	245	235.74	236.1	10.71818182	225.3818182
1	9S-6.5W	246	237.54	235.17	7.8675	227.3025	1	9S-6.5W	246	237.54	235.17	7.836	227.334
3	10S-0	247	251.76	249.13	12.6925	236.4375	3	10S-0	247	251.76	249.13	15.011	234.119
3	10S-1W	248	249.69	248.18	15.4025	232.7775	3	10S-1W	248	249.69	248.18	16.07	232.11
2	10S-2W	249	242	239.93	8.874166667	231.0558333	2	10S-2W	249	242	239.93	9.319090909	230.6109091
2	10S-3W	250	240.34	237.37	8.651666667	228.7183333	2	10S-3W	250	240.34	237.37	#DIV/0!	#DIV/0!
1	10S-3.87W	251	237.45	235.16	6.5375	228.6225	1	10S-3.87W	251	237.45	235.16	7.074	228.086
2	10S-5W	252	236.47	233.49	10.1375	223.3525	2	10S-5W	252	236.47	233.49	10.22454545	223.2654545
2	10S-6.75W	253	236.85	234.71	8.590833333	226.1191667	2	10S-6.75W	253	236.85	234.71	8.93	225.78
2	10S-5.75W	254	235.76	233.22	8.323333333	224.8966667	2	10S-5.75W	254	235.76	233.22	8.463333333	224.7566667
2	10.75S-4W	255	236.58	233.4	9.096363636	224.3036364	2	10.75S-4W	255	236.58	233.4	8.677272727	224.7227273
3	11S-1W	256	244.62	243.3	11.76363636	231.5363636	3	11S-1W	256	244.62	243.3	12.55909091	230.7409091
2	11S-2W	257	238.8	237.75	8.715	229.035	2	11S-2W	257	238.8	237.75	8.947272727	228.8027273
2	11S-3W	258	237.96	236.02	8.295833333	227.7241667	2	11S-3W	258	237.96	236.02	9.196666667	226.8233333
2	11S-5W	259	235.02	231.19	9.0825	222.1075	2	11S-5W	259	235.02	231.19	8.748181818	222.4418182
2	11S-5.75W	260	234.78	232.35	8.785833333	223.5641667	2	11S-5.75W	260	234.78	232.35	8.63	223.72
2	11S-6.87W	261	233.32	231.42	9.231818182	222.1881818	2	11S-6.87W	261	233.32	231.42	8.476666667	222.9433333
2	11.75S-6.75W	262	231.3	231	7.900833333	223.0991667	2	11.75S-6.75W	262	231.3	231	8.200909091	222.7990909
2	12S-1W	263	238.84	238.29	8.5	229.79	2	12S-1W	263	238.84	238.29	9.206363636	229.0836364
2	12S-2W	264	237.63	237.11	9.258333333	227.8516667	2	12S-2W	264	237.63	237.11	9.478181818	227.6318182
3	12S-3W	265	242.36	240.04	12.16	227.88	3	12S-3W	265	242.36	240.04	13.21909091	226.8209091
2	12S-4W	266	237.71	234.84	11.2075	223.6325	2	12S-4W	266	237.71	234.84	10.806	224.034
2	12S-5W	267	236.8	233.16	10.1125	223.0475	2	12S-5W	267	236.8	233.16	9.720909091	223.4390909
2	12S-6W	268	233.06	231.72	10.81583333	220.9041667	2	12S-6W	268	233.06	231.72	10.79454545	220.9254545
2	13S-2W	269	242.29	240.58	8.300833333	232.2791667	2	13S-2W	269	242.29	240.58	10.388	230.192

1986	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation	1987	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation
2	13.12S-2.87W	270	243.53	240.58	9.498333333	231.0816667	2	13.12S-2.87W	270	243.53	240.58	11.75636364	228.8236364
1	13S-4.25W	271	234.53	234.31	5.530833333	228.7791667	1	13S-4.25W	271	234.53	234.31	6.48	227.83
2	13S-5W	272	235.57	233.88	7.053333333	226.8266667	2	13S-5W	272	235.57	233.88	7.954545455	225.9254545
2	13S-6W	273	232.62	231.6	8.143333333	223.4566667	2	13S-6W	273	232.62	231.6	8.589090909	223.0109091
1	13S-6.5W	274	230.69	228.55	7.571666667	220.9783333	1	13S-6.5W	274	230.69	228.55	7.147272727	221.4027273
2	13S-7.12W	275	233.57	232.23	11.25333333	220.9766667	2	13S-7.12W	275	233.57	232.23	11.59727273	220.6327273
1	14.25S-6.5W	276	231.67	228.46	4.365	224.095	1	14.25S-6.5W	276	231.67	228.46	5.241	223.219
2	14.25S-7.18W	277	234.11	228.1	9.471666667	218.6283333	2	14.25S-7.18W	277	234.11	228.1	9.499090909	218.6009091
1	15S-6W	278	229.73	228.93	3.885	225.045	1	15S-6W	278	229.73	228.93	5.642727273	223.2872727
1	15S-6.75W	279	228.81	226.48	5.453333333	221.0266667	1	15S-6.75W	279	228.81	226.48	5.746363636	220.7336364
1	16S-6W	280	227.88	226.33	4.004166667	222.3258333	1	16S-6W	280	227.88	226.33	4.528181818	221.8018182
1	17S-5W	281	230.06	228.14	4.0075	224.1325	1	17S-5W	281	230.06	228.14	5.264	222.876
1	17S-5.75W	282	227.63	226.14	5.301666667	220.8383333	1	17S-5.75W	282	227.63	226.14	5.3	220.84
1	18S-5W	283	227.16	224.12			1	18S-5W	283	227.16	224.12	2.98	221.14

1988	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation	1989	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation
3	8N-7E	1	289.11	286.9	15.8975	271.0025	3	8N-7E	1	289.11	286.9	16.603	270.297
1	7.5N-5.62E	2	285.26	283.47	3.29	280.18	1	7.5N-5.62E	2	285.26	283.47	3.863	279.607
1	7.41N-5.41E	3	284.49	284.1	3.846666667	280.2533333	1	7.41N-5.41E	3	284.49	284.1	4.265	279.835
1	7.37N-5.12E	4	284.37	283	3.225454545	279.7745455	1	7.37N-5.12E	4	284.37	283	3.812	279.188
1	7.37N-4.87E	5	284.65	283.1	3.696666667	279.4033333	1	7.37N-4.87E	5	284.65	283.1	4.273	278.827
1	7.37N-4.75E	6	288.65	285.43	3.4025	282.0275	1	7.37N-4.75E	6	288.65	285.43	3.287	282.143
1	7.37N-4.25E	7	284.76	283	3.273333333	279.7266667	1	7.37N-4.25E	7	284.76	283	3.366	279.634
1	7.25N-4.31E	8	284.04	282.02	5.53	276.49	1	7.25N-4.31E	8	284.04	282.02	5.772	276.248
1	7.18N-4.06E	9	284.93	281	4.743333333	276.2566667	1	7.18N-4.06E	9	284.93	281	4.746	276.254
1	7.12N-4E	10	283.39	280.09	3.963333333	276.1266667	1	7.12N-4E	10	283.39	280.09	4.172	275.918
2	7N-7E	11	285.48	283.26	11.57833333	271.6816667	2	7N-7E	11	285.48	283.26	12.336	270.924
1	7N-6.25E	12	286.06	283.51	6.211428571	277.2985714	1	7N-6.25E	12	286.06	283.51	7.764	275.746
1	7N-4.62E	13	285.1	282.5	4.739166667	277.7608333	1	7N-4.62E	13	285.1	282.5	5.297	277.203
1	6.87N-3.93E	14	281.8	280.21	5.620833333	274.5891667	1	6.87N-3.93E	14	281.8	280.21	5.394	274.816
1	6.87N-3.81E	15	280.88	279.01	4.716363636	274.2936364	1	6.87N-3.81E	15	280.88	279.01	5.101	273.909
2	6.75N-3.43E	16	282.35	280.36	8.6025	271.7575	2	6.75N-3.43E	16	282.35	280.36	8.36	272
1	6.56N-3E	17	279.72	278.64	7.8125	270.8275	1	6.56N-3E	17	279.72	278.64	7.739	270.901
1	6.62N-3.75E	18	279.73	279.26	6.135833333	273.1241667	1	6.62N-3.75E	18	279.73	279.26	5.734	273.526
1	6.62N-3E	19	278.02	277.4	6.265833333	271.1341667	1	6.62N-3E	19	278.02	277.4	6.249	271.151
1	6.5N-3.68E	21	282.44	279.57	7.623333333	271.9466667	1	6.5N-3.68E	21	282.44	279.57	7.562	272.008
1	6.68N-3E	20	278.86	277.68	6.378333333	271.3016667	1	6.68N-3E	20	278.86	277.68	6.406	271.274
1	6.5N-3E	22	279.41	277.32	6.81	270.51	1	6.5N-3E	22	279.41	277.32	6.77	270.55
1	6.5N-2.81E	23	279.34	275.74	5.5375	270.2025	1	6.5N-2.81E	23	279.34	275.74	5.557	270.183
1	6.37N-3E	24	279.41	277.45	7.326666667	270.1233333	1	6.37N-3E	24	279.41	277.45	7.179	270.271
2	6.25N-6E	25	285.89	283.47	11.35833333	272.1116667	2	6.25N-6E	25	285.89	283.47	12.084	271.386
1	6.25N-4E	26	283.8	280.6	7.988333333	272.6116667	1	6.25N-4E	26	283.8	280.6	7.858	272.742
1	6.25N-3.68E	27	281.44	278.37	7.6575	270.7125	1	6.25N-3.68E	27	281.44	278.37	7.621	270.749
1	6.25N-3E	28	280.23	277.58	8.068333333	269.5116667	1	6.25N-3E	28	280.23	277.58	7.792	269.788
1	6.25N-2.81E	29	279	276.43	7.084166667	269.3458333	1	6.25N-2.81E	29	279	276.43	6.937	269.493
1	6N-4.75E	30	283.01	281.07	7.765	273.305	1	6N-4.75E	30	283.01	281.07	7.846	273.224
2	6N-4E	31	281.23	279.95	8.848333333	271.1016667	2	6N-4E	31	281.23	279.95	8.526	271.424
1	6N-3E	32	278.7	276.85	6.273333333	270.5766667	1	6N-3E	32	278.7	276.85	6.14	270.71
2	6N-2E	33	278.53	275.59	8.5675	267.0225	2	6N-2E	33	278.53	275.59	7.958	267.632
1	5.93N-2E	34	277.72	273.44	5.6675	267.7725	1	5.93N-2E	34	277.72	273.44	5.491	267.949
1	5.87N-2E	35	277.52	273.24	5.904166667	267.3358333	1	5.87N-2E	35	277.52	273.24	5.179	268.061
1	5.75N-2E	36	276.73	273.71	5.9125	267.7975	1	5.75N-2E	36	276.73	273.71	5.384	268.326
2	5.75N-1.75E	37	275.74	273.16	8.186666667	264.9733333	2	5.75N-1.75E	37	275.74	273.16	7.602	265.558
2	5.75N-1.5E	38	273.84	272.48	8.986666667	263.4933333	2	5.75N-1.5E	38	273.84	272.48	8.435	264.045
3	5.75N-1E	39	281.09	278.82	16.6575	262.1625	3	5.75N-1E	39	281.09	278.82	15.11	263.71
2	5.5N-1.75E	40	275.29	273.25	8.185833333	265.0641667	2	5.5N-1.75E	40	275.29	273.25	7.724	265.526
2	5.5N-1.25E	41	272.47	271.58	9.334545455	262.2454545	2	5.5N-1.25E	41	272.47	271.58	8.548	263.032
2	5.37N-0	42	269.25	267.2	9.705	257.495	2	5.37N-0	42	269.25	267.2	9.528	257.672
2	5N-4.87E	43	279.89	278.25	11.86416667	266.3858333	2	5N-4.87E	43	279.89	278.25	12.347	265.903
2	5N-4E	44	274.73	274.33	9.884166667	264.4458333	2	5N-4E	44	274.73	274.33	9.377	264.953
2	5N-3E	45	274.96	274.96	11.47583333	263.4841667	2	5N-3E	45	274.96	274.96	11.206	263.754
1	5N-2E	46	276.6	271.19	4.103333333	267.0866667	1	5N-2E	46	276.6	271.19	3.697	267.493
2	5N-1.75E	47	274.64	272.8	8.836666667	263.9633333	2	5N-1.75E	47	274.64	272.8	8.425	264.375
2	5N-1.25E	48	272.45	270.25	8.575	261.675	2	5N-1.25E	48	272.45	270.25	7.924	262.326
1	5N-1E	49	270.79	268.88	7.758333333	261.1216667	1	5N-1E	49	270.79	268.88	7.077	261.803
2	5N-0	50	268.53	267.38	10.0375	257.3425	2	5N-0	50	268.53	267.38	9.711	257.669
2	5N-.18W	51	268.73	267.01	10.23	256.78	2	5N-.18W	51	268.73	267.01	9.965	257.045
2	4.5N-1.75E	52	275.05	272.66	9.6275	263.0325	2	4.5N-1.75E	52	275.05	272.66	9.21	263.45
1	4.5N-1.25E	53	270.97	265.72	4.483333333	261.2366667	1	4.5N-1.25E	53	270.97	265.72	3.75	261.97
3	4.37N-.5W	54	266.99	267.29	15.09666667	252.1933333	3	4.37N-.5W	54	266.99	267.29	14.81	252.48

1988	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation	1989	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation
3	4.37N-.87W	55	272.11	267.99	14.05916667	253.9308333	3	4.37N-.87W	55	272.11	267.99	13.59	254.4
2	4N-4.87E	56	275.43	274.2	10.67333333	263.5266667	2	4N-4.87E	56	275.43	274.2	10.683	263.517
3	4N-4E	57	278.71	276.19	12.595	263.595	3	4N-4E	57	278.71	276.19	12.293	263.897
2	4N-3E	58	276.66	274.76	11.3625	263.3975	2	4N-3E	58	276.66	274.76	11.028	263.732
2	4N-2E	59	273.97	272.17	8.766363636	263.4036364	2	4N-2E	59	273.97	272.17	8.351	263.819
2	4N-1.75E	60	272.16	270.91	8.250833333	262.6591667	2	4N-1.75E	60	272.16	270.91	7.906	263.004
2	4N-1.25E	61	270.54	269.73	8.950833333	260.7791667	2	4N-1.25E	61	270.54	269.73	8.447	261.283
1	4N-1E	62	271.19	268.04	7.531666667	260.5083333	1	4N-1E	62	271.19	268.04	7.176	260.864
3	4N-1W	63	274.94	273.86	19.57666667	254.2833333	3	4N-1W	63	274.94	273.86	18.92	254.94
2	4N-0	64	267.21	266.76	#DIV/0!		2	4N-0	64	267.21	266.76	#DIV/0!	
2	3.62N-2E	65	272.59	271.02	8.6025	262.4175	2	3.62N-2E	65	272.59	271.02	8.245	262.775
1	3.5N-1.75E	66	273.11	269.32	6.913333333	262.4066667	1	3.5N-1.75E	66	273.11	269.32	6.406	262.914
2	3N-5E	67	273.21	271.27	9.63	261.64	2	3N-5E	67	273.21	271.27	9.898	261.372
1	3N-4E	68	269.84	268.38	7.619166667	260.7608333	1	3N-4E	68	269.84	268.38	7.047777778	261.3322222
2	3N-3E	69	275.12	272.06	10.785	261.275	2	3N-3E	69	275.12	272.06	10.195	261.865
2	3N-2E	70	273.31	271.28	8.075	263.205	2	3N-2E	70	273.31	271.28	7.604	263.676
2	3N-1.75E	71	270.9	270.29	8.130833333	262.1591667	2	3N-1.75E	71	270.9	270.29	7.76	262.53
2	3N-.25W	72	265.42	264.39	8.8275	255.5625	2	3N-.25W	72	265.42	264.39	8.457	255.933
3	3N-1W	73	276.84	276.15	21.93	254.22	3	3N-1W	73	276.84	276.15	21.348	254.802
2	2.75N-2.25E	74	272.86	271.44	8.5575	262.8825	2	2.75N-2.25E	74	272.86	271.44	8.039	263.401
1	2.75N-1E	75	268.35	267.35	7.487272727	259.8627273	1	2.75N-1E	75	268.35	267.35	7.347	260.003
1	2.5N-2.5E	76	272.63	270.57	7.175	263.395	1	2.5N-2.5E	76	272.63	270.57	6.872	263.698
1	2.5N-2.62E	77	270.66	269.83	5.085833333	264.7441667	1	2.5N-2.62E	77	270.66	269.83	4.891	264.939
1	2.5N-2E	78	273.36	271.98	6.52	265.46	1	2.5N-2E	78	273.36	271.98	6.083	265.897
1	2.5N-1.87E	79	271.88	271.1	5.234166667	265.8658333	1	2.5N-1.87E	79	271.88	271.1	4.885	266.215
1	2.5N-1.75E	80	269.69	269.43	4.435	264.995	1	2.5N-1.75E	80	269.69	269.43	4.115	265.315
2	2.18N-1.5W	81	270.91	262.69	11.025	251.665	2	2.18N-1.5W	81	270.91	262.69	8.653	254.037
2	2.25N-2.37E	82	272.91	270.39	7.449166667	262.9408333	2	2.25N-2.37E	82	272.91	270.39	7.423	262.967
1	2.25N-2E	83	273.99	270.92	5.125	265.795	1	2.25N-2E	83	273.99	270.92	4.734	266.186
1	2.25N-1.75E	84	274.41	272.2	7.0475	265.1525	1	2.25N-1.75E	84	274.41	272.2	6.644	265.556
2	2N-5E	85	272.67	269.05	10.15916667	258.8908333	2	2N-5E	85	272.67	269.05	10.205	258.845
1	2N-2E	86	270.92	270.8	4.658333333	266.1416667	1	2N-2E	86	270.92	270.8	4.709	266.091
1	2N-1E	87	272.09	268.81	6.3425	262.4675	1	2N-1E	87	272.09	268.81	6.689	262.121
2	2N- 25E	88	267.59	265.5	7.824166667	257.6758333	2	2N-.25E	88	267.59	265.5	7.377	258.123
2	2N-1.25W	89	263.31	260.77	8.871818182	251.8981818	2	2N-1.25W	89	263.31	260.77	8.799	251.971
2	1.75N-1.25W	90	264.28	261.73	8.963333333	252.7666667	2	1.75N-1.25W	90	264.28	261.73	8.732	252.998
2	1.75N-1.75W	91	264.11	261.43	11.31333333	250.1166667	2	1.75N-1.75W	91	264.11	261.43	10.682	250.748
2	1.5N-1.25W	92	264.18	261.32	9.966666667	251.3533333	2	1.5N-1.25W	92	264.18	261.32	9.743	251.577
2	1.5N-2W	93	261.32	260.83	11.2225	249.6075	2	1.5N-2W	93	261.32	260.83	10.57	250.26
3	1.5N-2.25W	94	264.6	261.91	13.02666667	248.8833333	3	1.5N-2.25W	94	264.6	261.91	12.251	249.659
2	1.25N-1.5W	95	262.06	260.49	9.264166667	251.2258333	2	1.25N-1.5W	95	262.06	260.49	8.158	252.332
2	1N-5E	96	271.74	268.72	12.7025	256.0175	2	1N-5E	96	271.74	268.72	12.463	256.257
2	1N-4E	97	266.29	266.02	10.2	255.82	2	1N-4E	97	266.29	266.02	9.645	256.375
2	1N-3E	98	267.49	266.62	9.2175	257.4025	2	1N-3E	98	267.49	266.62	8.778	257.842
3	1N-2.12E	99	270.74	270.7	12.60916667	258.0908333	3	1N-2.12E	99	270.74	270.7	12.766	257.934
2	1N-1E	100	266.52	266.74	8.643333333	258.0966667	2	1N-1E	100	266.52	266.74	8.623	258.117
2	1N-0	101	264.79	264.5	8.413333333	256.0866667	2	1N-0	101	264.79	264.5	8.282	256.218
2	1N-.75W	102	261.87	261.01	8.424166667	252.5858333	2	1N-.75W	102	261.87	261.01	8.345	252.665
2	1N-2W	103	259.68	258.34	9.5675	248.7725	2	1N-2W	103	259.68	258.34	8.679	249.661
2	1N-2.25W	104	257.8	257.52	9.668333333	247.8516667	2	1N-2.25W	104	257.8	257.52	9.011	248.509
2	0.5N-2.37W	105	258.52	256.72	10.24818182	246.4718182	2	0.5N-2.37W	105	258.52	256.72	9.814	246.906
2	0.12N-5E	106	269.45	267.07	13.34333333	253.7266667	2	0.12N-5E	106	269.45	267.07	13.275	253.795
2	0-4.12E	107	266.9	266.3	12.32083333	253.9791667	2	0-4.12E	107	266.9	266.3	11.968	254.332
2	0-3E	108	263.76	262.77	8.940833333	253.8291667	2	0-3E	108	263.76	262.77	8.821	253.949
2	0-2E	109	267.84	265.18	8.953636364	256.2263636	2	0-2E	109	267.84	265.18	9.051	256.129

1988	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation	1989	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation
1	0-1E	110	261.7	261.42	7.126666667	254.2933333	1	0-1E	110	261.7	261.42	6.974	254.446
2	0-0	111	262.37	261.83	7.795833333	254.0341667	2	0-0	111	262.37	261.83	7.736	254.094
2	0-1W	112	260.19	259.7	10.0725	249.6275	2	0-1W	112	260.19	259.7	10.12	249.58
2	0-2W	113	258.18	256.12	10.16833333	245.9516667	2	0-2W	113	258.18	256.12	9.937	246.183
2	0-2.75W	114	256.48	255.13	10.59916667	244.5308333	2	0-2.75W	114	256.48	255.13	10.326	244.804
2	0.5S-2.75W	115	257.77	255.36	9.410909091	245.9490909	2	0.5S-2.75W	115	257.77	255.36	9.624	245.736
3	0.5S-3W	116	257.35	255.03	11.92333333	243.1066667	3	0.5S-3W	116	257.35	255.03	11.791	243.239
2	0.5S-3.18W	117	257.79	254.4	11.39583333	243.0041667	2	0.5S-3.18W	117	257.79	254.4	11.154	243.246
3	1S-4E	118	268.56	266.74	13.85	252.89	3	1S-4E	118	268.56	266.74	13.856	252.884
2	1S-3E	119	263.55	260.73	11.09666667	249.6333333	2	1S-3E	119	263.55	260.73	10.827	249.903
2	1S-2E	120	260.54	259.92	10.03583333	249.8841667	2	1S-2E	120	260.54	259.92	10.05	249.87
1	1S-1E	121	261.85	258.57	8.269166667	250.3008333	1	1S-1E	121	261.85	258.57	8.225	250.345
2	1S-.25W	122	258.55	258.53	9.399166667	249.1308333	2	1S-.25W	122	258.55	258.53	8.804	249.726
2	1S-1W	123	259.49	258.92	10.41	248.51	2	1S-1W	123	259.49	258.92	10.277	248.643
2	1S-2W	124	255.99	254.74	10.88916667	243.8508333	2	1S-2W	124	255.99	254.74	10.464	244.276
2	1S-3W	125	255.47	253.89	10.80416667	243.0858333	2	1S-3W	125	255.47	253.89	10.616	243.274
2	1S-3.37W	126	253.86	252.6	10.57916667	242.0208333	2	1S-3.37W	126	253.86	252.6	10.459	242.141
2	1.25S-4W	127	255.89	252.21	11.21166667	240.9983333	2	1.25S-4W	127	255.89	252.21	11.022	241.188
2	1.5S-4.5W	128	254.24	250.98	11.02	239.96	2	1.5S-4.5W	128	254.24	250.98	11.052	239.928
2	1.5S-4.75W	129	252.55	250.98	11.2275	239.7525	2	1.5S-4.75W	129	252.55	250.98	11.626	239.354
2	2S-2.75E	130	261.59	257.83	10.69416667	247.1358333	2	2S-2.75E	130	261.59	257.83	11.104	246.726
3	2S-3.75E	131	265.35	262.89	14.21333333	248.6766667	3	2S-3.75E	131	265.35	262.89	13.951	248.939
2	2S-2E	132	258.15	257.56	10.43083333	247.1291667	2	2S-2E	132	258.15	257.56	10.40222222	247.1577778
2	2S-1E	133	258.01	255.81	9.135	246.675	2	2S-1E	133	258.01	255.81	9.653	246.157
1	2S-0	134	256.3	255.56	8.481666667	247.0783333	1	2S-0	134	256.3	255.56	7.638	247.922
2	2S-1W	135	256.21	254.2	8.9025	245.2975	2	2S-1W	135	256.21	254.2	8.323	245.877
2	2S-2W	136	254.96	253.48	9.435	244.045	2	2S-2W	136	254.96	253.48	8.676	244.804
2	2S-3W	137	252.16	252.1	8.824166667	243.2758333	2	2S-3W	137	252.16	252.1	9.204	242.896
2	2S-4W	138	252.33	251.88	10.52	241.36	2	2S-4W	138	252.33	251.88	11.002	240.878
3	2S-4.5W	139	254.87	252.25	11.85833333	240.3916667	3	2S-4.5W	139	254.87	252.25	11.94	240.31
3	2S-5.12W	140	250.86	249.04	11.44916667	237.5908333	3	2S-5.12W	140	250.86	249.04	11.426	237.614
2	2.5S-5.25W	141	252.87	249.19	11.23583333	237.9541667	2	2.5S-5.25W	141	252.87	249.19	10.802	238.388
1	2.75S-3.5E	142	260.23	258.41	12.11916667	246.2908333	1	2.75S-3.5E	142	260.23	258.41	11.712	246.698
3	2.75S-5.25W	143	251.32	249.21	12.04	237.17	3	2.75S-5.25W	143	251.32	249.21	11.739	237.471
1	3S-4.37E	144	263.96	262.35	8.076666667	254.2733333	1	3S-4.37E	144	263.96	262.35	5.45	256.9
2	3S-3E	145	258.93	257.22	12.17333333	245.0466667	2	3S-3E	145	258.93	257.22	11.764	245.456
2	3S-2E	146	257.91	255.88	11.4475	244.4325	2	3S-2E	146	257.91	255.88	11.151	244.729
2	3S-1E	147	256.81	254.64	11.435	243.205	2	3S-1E	147	256.81	254.64	11.157	243.483
2	3S-0	148	253.44	252.09	8.846666667	243.2433333	2	3S-0	148	253.44	252.09	8.228	243.862
2	3S-1W	149	254.56	252.57	9.8375	242.7325	2	3S-1W	149	254.56	252.57	9.092	243.478
2	3S-2W	150	253.78	250.84	10.08166667	240.7583333	2	3S-2W	150	253.78	250.84	9.233	241.607
2	3S-3W	151	247.32	248.8	8.443333333	240.3566667	2	3S-3W	151	247.32	248.8	8.384	240.416
2	3S-4W	152	252.11	249.83	10.32083333	239.5091667	2	3S-4W	152	252.11	249.83	10.393	239.437
3	3S-5.25W	153	251.33	248.77	11.36272727	237.4072727	3	3S-5.25W	153	251.33	248.77	11.182	237.588
2	3S-5.5W	154	249.57	246.8	8.858333333	237.9416667	2	3S-5.5W	154	249.57	246.8	8.294	238.506
2	3.12S-4.5W	155	251.39	247.97	11.10333333	236.8666667	2	3.12S-4.5W	155	251.39	247.97	10.48	237.49
2	3.37S-4.5W	156	248.74	247.84	10.17666667	237.6633333	2	3.37S-4.5W	156	248.74	247.84	10.051	237.789
2	3.5S-5.25W	157	249.04	247.15	9.92	237.23	2	3.5S-5.25W	157	249.04	247.15	9.709	237.441
2	3.5S-5.5W	158	248.33	246.1	8.587272727	237.5127273	2	3.5S-5.5W	158	248.33	246.1	8.225	237.875
2	3.62S-4.75W	159	252.31	248.59	8.882727273	239.7072727	2	3.62S-4.75W	159	252.31	248.59	10.949	237.641
2	3.75S-5.5W	160	247.38	246.61	9.378333333	237.2316667	2	3.75S-5.5W	160	247.38	246.61	8.904	237.706
2	3.87S-4.25W	161	248.14	247.62	9.711666667	237.9083333	2	3.87S-4.25W	161	248.14	247.62	9.918	237.702
2	4S-4E	162	265.61	261.39	12.72	248.67	2	4S-4E	162	265.61	261.39	12.557	248.833
2	4S-3E	163	260.08	258.94	11.29166667	247.6483333	2	4S-3E	163	260.08	258.94	10.338	248.602

1988	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation	1989	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation
3	4S-2E	164	259.63	257.4	14.96083333	242.4391667	3	4S-2E	164	259.63	257.4	14.119	243.281
3	4S-1E	165	259.23	254.05	13.87166667	240.1783333	3	4S-1E	165	259.23	254.05	13.387	240.663
2	4S-0	166	252.02	251.67	11.665	240.005	2	4S-0	166	252.02	251.67	11.373	240.297
2	4S-.5W	167	253.41	251.47	10.95416667	240.5158333	2	4S-.5W	167	253.41	251.47	10.491	240.979
2	4S-.75W	168	253.23	251.32	11.21583333	240.1041667	2	4S-.75W	168	253.23	251.32	11.01	240.31
3	4S-2W	169	250.85	249.2	13.3675	235.8325	3	4S-2W	169	250.85	249.2	13.134	236.066
3	4S-3W	170	250.85	249.68	10.923	238.757	3	4S-3W	170	250.85	249.68	12.454	237.226
1	4S-4W	171	246.83	246.34	7.1525	239.1875	1	4S-4W	171	246.83	246.34	7.798	238.542
3	4S-4.5W	172	248.53	248.16	#DIV/0!		3	4S-4.5W	172	248.53	248.16	#DIV/0!	
2	4S-5.25W	173	249.14	245.96	8.966666667	236.9933333	2	4S-5.25W	173	249.14	245.96	8.865	237.095
2	4S-5.5W	174	249.08	246.39	9.501666667	236.8883333	2	4S-5.5W	174	249.08	246.39	9.004	237.386
2	4S-5.87W	175	252.9	246.47	8.915833333	237.5541667	2	4S-5.87W	175	252.9	246.47	8.469	238.001
2	4.25S-4.12W	176	250.26	247.26	9.245833333	238.0141667	2	4.25S-4.12W	176	250.26	247.26	9.509	237.751
2	4.25S-4.5W	177	250.4	246.8	10.39583333	236.4041667	2	4.25S-4.5W	177	250.4	246.8	10.34555556	236.4544444
2	4.25S-5.5W	178	249.4	246.25	8.4425	237.8075	2	4.25S-5.5W	178	249.4	246.25	7.891	238.359
2	4.5S-4.75W	179	247.36	245.52	9.991666667	235.5283333	2	4.5S-4.75W	179	247.36	245.52	10.105	235.415
2	4.5S-5.5W	180	249.47	246.08	8.589166667	237.4908333	2	4.5S-5.5W	180	249.47	246.08	7.631	238.449
2	4.5S-6.25W	181	248.63	246.47	9.899166667	236.5708333	2	4.5S-6.25W	181	248.63	246.47	9.452	237.018
2	4.75S-4.25W	182	249.14	246.78	9.52	237.26	2	4.75S-4.25W	182	249.14	246.78	9.943	236.837
2	4.75S-4.75W	183	246.3	244.5	10.46416667	234.0358333	2	4.75S-4.75W	183	246.3	244.5	10.18	234.32
2	5S-3E	184	257.68	256.65	10.85416667	245.7958333	2	5S-3E	184	257.68	256.65	10.25	246.4
3	5S-2.25E	185	259.3	257.61	13.275	244.335	3	5S-2.25E	185	259.3	257.61	12.452	245.158
3	5S-1E	186	255.81	253.72	15.58363636	238.1363636	3	5S-1E	186	255.81	253.72	15.497	238.223
3	5S-0	187	254.3	251.38	15.21416667	236.1658333	3	5S-0	187	254.3	251.38	15.211	236.169
3	5S-.75W	188	249.17	248.95	13.1575	235.7925	3	5S-.75W	188	249.17	248.95	12.972	235.978
3	5S-2W	189	245.35	245.3	11.8975	233.4025	3	5S-2W	189	245.35	245.3	11.756	233.544
2	5S-2.75W	190	244.17	242.59	11.13	231.46	2	5S-2.75W	190	244.17	242.59	10.751	231.839
2	5S-3.75W	191	249.28	247.77	10.75416667	237.0158333	2	5S-3.75W	191	249.28	247.77	10.543	237.227
2	5S-4.12W	192	248.93	246.83	10.205	236.625	2	5S-4.12W	192	248.93	246.83	9.811	237.019
2	5S-4.5W	193	247.04	244.83	10.76727273	234.0627273	2	5S-4.5W	193	247.04	244.83	10.713	234.117
2	5S-4.75W	194	246.64	244.38	10.76416667	233.6158333	2	5S-4.75W	194	246.64	244.38	9.947	234.433
2	5S-5.5W	195	245.46	243.81	8.465833333	235.3441667	2	5S-5.5W	195	245.46	243.81	8.347	235.463
2	5S-6.18W	196	246.48	244.45	9.3175	235.1325	2	5S-6.18W	196	246.48	244.45	8.965	235.485
2	5.5S-.5W	197	247.78	247.18	12.04	235.14	2	5.5S-.5W	197	247.78	247.18	11.399	235.781
3	5.5S-1.25W	198	247.32	245.49	12.64583333	232.8441667	3	5.5S-1.25W	198	247.32	245.49	12.324	233.166
2	5.5S-4.25W	199	248.3	246.29	10.34416667	235.9458333	2	5.5S-4.25W	199	248.3	246.29	9.543	236.747
3	5.5S-4.5W	200	245.9	244.75	11.16333333	233.5866667	3	5.5S-4.5W	200	245.9	244.75	10.857	233.893
3	5.5S-4.75W	201	246.28	244.05	12.31333333	231.7366667	3	5.5S-4.75W	201	246.28	244.05	12.282	231.768
2	5.5S-6.37W	202	246.66	242.63	8.478333333	234.1516667	2	5.5S-6.37W	202	246.66	242.63	8.08	234.55
2	5.75S-2W	203	243.63	242.33	12.10333333	230.2266667	2	5.75S-2W	203	243.63	242.33	11.648	230.682
3	6S-3E	204	258.01	256.13	15.83333333	240.2966667	3	6S-3E	204	258.01	256.13	15.726	240.404
2	6S-2E	205	255.23	254.45	13.00083333	241.4491667	2	6S-2E	205	255.23	254.45	12.957	241.493
3	6S-1.12E	206	256.31	253.73	13.40333333	240.3266667	3	6S-1.12E	206	256.31	253.73	13.613	240.117
3	6S-2.75W	207	243.98	241.97	10.58666667	231.3833333	3	6S-2.75W	207	243.98	241.97	13.645	228.325
2	6S-4W	208	245.48	243.84	10.4775	233.3625	2	6S-4W	208	245.48	243.84	9.875	233.965
2	6S-4.5W	209	246.86	243.84	11.3525	232.4875	2	6S-4.5W	209	246.86	243.84	10.676	233.164
2	6S-5.5W	210	244.17	242.61	9.438333333	233.1716667	2	6S-5.5W	210	244.17	242.61	9.118888889	233.4911111
1	6S-6.25W	211	242.64	240.09	6.916666667	233.1733333	1	6S-6.25W	211	242.64	240.09	6.728	233.362
3	6.75S-0	212	253.73	249.73	13.33833333	236.3916667	3	6.75S-0	212	253.73	249.73	13.332	236.398
2	6.87S-1.87E	213	252.93	252.8	13.365	239.435	2	6.87S-1.87E	213	252.93	252.8	13.52	239.28
2	7S-1E	214	256.75	252.93	12.54833333	240.3816667	2	7S-1E	214	256.75	252.93	12.893	240.037
2	7S-0	215	251.43	250.34	12.52166667	237.8183333	2	7S-0	215	251.43	250.34	12.36	237.98
2	7S-1W	216	247.64	245.6	11.50916667	234.0908333	2	7S-1W	216	247.64	245.6	11.253	234.347

1988	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation	1989	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation
2	7S-2W	217	241.33	240.97	10.69	230.28	2	7S-2W	217	241.33	240.97	10.364	230.606
3	7S-3W	218	241.62	240.88	11.92833333	228.9516667	3	7S-3W	218	241.62	240.88	11.511	229.369
2	7S-4W	219	242.52	241.91	10.54666667	231.3633333	2	7S-4W	219	242.52	241.91	10.398	231.512
2	7S-5W	220	243.43	241.59	8.945	232.645	2	7S-5W	220	243.43	241.59	8.932	232.658
2	7S-5.75W	221	244.57	241.86	9.225833333	232.6341667	2	7S-5.75W	221	244.57	241.86	8.985	232.875
2	7S-6.5W	222	244.09	241.02	9.94	231.08	2	7S-6.5W	222	244.09	241.02	9.525	231.495
2	7.25S-.5E	223	253.45	251.73	12.58333333	239.1466667	2	7.25S-.5E	223	253.45	251.73	13.012	238.718
2	7.25S-.25E	224	253.46	249.77	11.4125	238.3575	2	7.25S-.25E	224	253.46	249.77	11.686	238.084
2	7.25S-.5W	225	248.92	246.58	10.48416667	236.0958333	2	7.25S-.5W	225	248.92	246.58	10.006	236.574
2	7.25S-.25W	226	250.44	247.1	10.36583333	236.7341667	2	7.25S-.25W	226	250.44	247.1	10.083	237.017
2	7.75S-0	227	252.5	248.19	10.77166667	237.4183333	2	7.75S-0	227	252.5	248.19	10.515	237.675
2	8S-1E	228	253.51	250.64	11.81818182	238.8218182	2	8S-1E	228	253.51	250.64	12.651	237.989
2	8S-.5E	229	253.44	250.07	11.18166667	238.8883333	2	8S-.5E	229	253.44	250.07	11.894	238.176
2	8S-.25W	230	246.82	245.02	8.751666667	236.2683333	2	8S-.25W	230	246.82	245.02	8.306	236.714
1	8S-.5W	231	245.28	243.91	7.724166667	236.1858333	1	8S-.5W	231	245.28	243.91	7.323	236.587
1	8S-1W	232	246.82	242.57	6.345833333	236.2241667	1	8S-1W	232	246.82	242.57	6.982	235.588
2	8S-2W	233	244.92	242.5	8.801666667	233.6983333	2	8S-2W	233	244.92	242.5	8.903	233.597
2	8S-3W	234	239.43	238.57	9.97	228.6	2	8S-3W	234	239.43	238.57	9.75	228.82
2	8S-5W	235	241.01	239.2	10.43916667	228.7608333	2	8S-5W	235	241.01	239.2	10.105	229.095
1	8S-5.5W	236	239.2	238.37	7.233333333	231.1366667	1	8S-5.5W	236	239.2	238.37	7.182	231.188
1	8S-6.5W	237	242.17	238.59	8.4025	230.1875	1	8S-6.5W	237	242.17	238.59	7.459	231.131
2	8.25S-4.25W	238	240.34	237.41	10.99166667	226.4183333	2	8.25S-4.25W	238	240.34	237.41	10.936	226.474
3	9S-0	239	250.45	249.42	14.245	235.175	3	9S-0	239	250.45	249.42	13.817	235.603
2	9S-1.25W	240	243.23	241.76	8.014166667	233.7458333	2	9S-1.25W	240	243.23	241.76	7.738	234.022
2	9S-2W	241	244.64	241.7	9.106666667	232.5933333	2	9S-2W	241	244.64	241.7	8.321	233.379
2	9S-3W	242	239.98	237.81	8.39	229.42	2	9S-3W	242	239.98	237.81	7.725	230.085
2	9S-4W	243	236.84	235.23	10.95916667	224.2708333	2	9S-4W	243	236.84	235.23	10.61	224.62
2	9S-5W	244	236.62	235.18	9.106666667	226.0733333	2	9S-5W	244	236.62	235.18	8.716	226.464
2	9S-5.75W	245	235.74	236.1	10.56666667	225.5333333	2	9S-5.75W	245	235.74	236.1	9.861111111	226.2388889
1	9S-6.5W	246	237.54	235.17	7.405	227.765	1	9S-6.5W	246	237.54	235.17	7.076	228.094
3	10S-0	247	251.76	249.13	16.50666667	232.6233333	3	10S-0	247	251.76	249.13	16.711	232.419
3	10S-1W	248	249.69	248.18	16.175	232.005	3	10S-1W	248	249.69	248.18	15.762	232.418
2	10S-2W	249	242	239.93	8.963333333	230.9666667	2	10S-2W	249	242	239.93	7.544	232.386
2	10S-3W	250	240.34	237.37	7.454285714	229.9157143	2	10S-3W	250	240.34	237.37	7.311111111	230.0588889
1	10S-3.87W	251	237.45	235.16	8.2275	226.9325	1	10S-3.87W	251	237.45	235.16	7.59	227.57
2	10S-5W	252	236.47	233.49	9.963333333	223.5266667	2	10S-5W	252	236.47	233.49	9.696	223.794
2	10S-6.75W	253	236.85	234.71	8.2775	226.4325	2	10S-6.75W	253	236.85	234.71	7.96	226.75
2	10S-5.75W	254	235.76	233.22	8.1625	225.0575	2	10S-5.75W	254	235.76	233.22	7.71	225.51
2	10.75S-4W	255	236.58	233.4	8.5425	224.8575	2	10.75S-4W	255	236.58	233.4	8.308	225.092
3	11S-1W	256	244.62	243.3	12.83666667	230.4633333	3	11S-1W	256	244.62	243.3	12.893	230.407
2	11S-2W	257	238.8	237.75	8.5	229.25	2	11S-2W	257	238.8	237.75	8.034444444	229.7155556
2	11S-3W	258	237.96	236.02	8.017272727	228.0027273	2	11S-3W	258	237.96	236.02	7.997777778	228.0222222
2	11S-5W	259	235.02	231.19	8.758181818	222.4318182	2	11S-5W	259	235.02	231.19	8.848	222.342
2	11S-5.75W	260	234.78	232.35	7.9125	224.4375	2	11S-5.75W	260	234.78	232.35	7.291	225.059
2	11S-6.87W	261	233.32	231.42	7.654166667	223.7658333	2	11S-6.87W	261	233.32	231.42	8.054	223.366
2	11.75S-6.75W	262	231.3	231	7.505	223.495	2	11.75S-6.75W	262	231.3	231	8.057	222.943
2	12S-1W	263	238.84	238.29	8.819090909	229.4709091	2	12S-1W	263	238.84	238.29	9.191	229.099
2	12S-2W	264	237.63	237.11	9.754166667	227.3558333	2	12S-2W	264	237.63	237.11	9.755	227.355
3	12S-3W	265	242.36	240.04	13.64166667	226.3983333	3	12S-3W	265	242.36	240.04	13.344	226.696
2	12S-4W	266	237.71	234.84	10.7	224.14	2	12S-4W	266	237.71	234.84	10.442	224.398
2	12S-5W	267	236.8	233.16	9.64	223.52	2	12S-5W	267	236.8	233.16	9.171	223.989
2	12S-6W	268	233.06	231.72	10.31333333	221.4066667	2	12S-6W	268	233.06	231.72	10.116	221.604
2	13S-2W	269	242.29	240.58	11.53916667	229.0408333	2	13S-2W	269	242.29	240.58	10.448	230.132

1988	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation	1989	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation
2	13.12S-2.87W	270	243.53	240.58	13.7525	226.8275	2	13.12S-2.87W	270	243.53	240.58	14.35	226.23
1	13S-4.25W	271	234.53	234.31	7.163333333	227.1466667	1	13S-4.25W	271	234.53	234.31	7.004	227.306
2	13S-5W	272	235.57	233.88	8.818333333	225.0616667	2	13S-5W	272	235.57	233.88	8.927	224.953
2	13S-6W	273	232.62	231.6	8.921666667	222.6783333	2	13S-6W	273	232.62	231.6	8.939	222.661
1	13S-6.5W	274	230.69	228.55	7.354166667	221.1958333	1	13S-6.5W	274	230.69	228.55	7.052	221.498
2	13S-7.12W	275	233.57	232.23	11.13666667	221.0933333	2	13S-7.12W	275	233.57	232.23	10.883	221.347
1	14.25S-6.5W	276	231.67	228.46	6.3825	222.0775	1	14.25S-6.5W	276	231.67	228.46	6.645	221.815
2	14.25S-7.18W	277	234.11	228.1	9.02	219.08	2	14.25S-7.18W	277	234.11	228.1	8.877	219.223
1	15S-6W	278	229.73	228.93	6.12	222.81	1	15S-6W	278	229.73	228.93	6.597	222.333
1	15S-6.75W	279	228.81	226.48	6.004166667	220.4758333	1	15S-6.75W	279	228.81	226.48	5.759	220.721
1	16S-6W	280	227.88	226.33	5.064166667	221.2658333	1	16S-6W	280	227.88	226.33	4.972	221.358
1	17S-5W	281	230.06	228.14	6.615	221.525	1	17S-5W	281	230.06	228.14	7.283	220.857
1	17S-5.75W	282	227.63	226.14	6.990833333	219.1491667	1	17S-5.75W	282	227.63	226.14	6.475	219.665
1	18S-5W	283	227.16	224.12	4.920909091	219.1990909	1	18S-5W	283	227.16	224.12	6.317	217.803

1991	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation	1992	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation
3	8N-7E	1	289.11	286.9	16.67	270.23	3	8N-7E	1	289.11	286.9	17.32727273	269.5727273
1	7.5N-5.62E	2	285.26	283.47	3.538888889	279.9311111	1	7.5N-5.62E	2	285.26	283.47	4.097272727	279.3727273
1	7.41N-5.41E	3	284.49	284.1	3.992222222	280.1077778	1	7.41N-5.41E	3	284.49	284.1	4.877272727	279.2227273
1	7.37N-5.12E	4	284.37	283	3.728888889	279.2711111	1	7.37N-5.12E	4	284.37	283	4.456363636	278.5436364
1	7.37N-4.87E	5	284.65	283.1	4.1	279	1	7.37N-4.87E	5	284.65	283.1	4.823	278.277
1	7.37N-4.75E	6	288.65	285.43	5.705	279.725	1	7.37N-4.75E	6	288.65	285.43	6.017272727	279.4127273
1	7.37N-4.25E	7	284.76	283	5.424444444	277.5755556	1	7.37N-4.25E	7	284.76	283	5.665454545	277.3345455
1	7.25N-4.31E	8	284.04	282.02	6.111111111	275.9088889	1	7.25N-4.31E	8	284.04	282.02	6.335454545	275.6845455
1	7.18N-4.06E	9	284.93	281	4.714444444	276.2855556	1	7.18N-4.06E	9	284.93	281	5.09	275.91
1	7.12N-4E	10	283.39	280.09	4.841111111	275.2488889	1	7.12N-4E	10	283.39	280.09	4.63	275.46
2	7N-7E	11	285.48	283.26	12.06222222	271.1977778	2	7N-7E	11	285.48	283.26	14.31090909	268.9490909
1	7N-6.25E	12	286.06	283.51	7.544444444	275.9655556	1	7N-6.25E	12	286.06	283.51	9.619090909	273.8909091
1	7N-4.62E	13	285.1	282.5	5.302222222	277.1977778	1	7N-4.62E	13	285.1	282.5	5.599090909	276.9009091
1	6.87N-3.93E	14	281.8	280.21	6.047777778	274.1622222	1	6.87N-3.93E	14	281.8	280.21	6.429090909	273.7809091
1	6.87N-3.81E	15	280.88	279.01	4.924444444	274.0855556	1	6.87N-3.81E	15	280.88	279.01	5.692727273	273.3172727
2	6.75N-3.43E	16	282.35	280.36	8.962222222	271.3977778	2	6.75N-3.43E	16	282.35	280.36	8.608181818	271.7518182
1	6.56N-3E	17	279.72	278.64	8.137777778	270.5022222	1	6.56N-3E	17	279.72	278.64	8.44	270.2
1	6.62N-3.75E	18	279.73	279.26	5.911111111	273.3488889	1	6.62N-3.75E	18	279.73	279.26	6.207	273.053
1	6.62N-3E	19	278.02	277.4	6.734444444	270.6655556	1	6.62N-3E	19	278.02	277.4	6.920909091	270.4790909
1	6.5N-3.68E	21	282.44	279.57	7.813333333	271.7566667	1	6.5N-3.68E	21	282.44	279.57	8.303636364	271.2663636
1	6.68N-3E	20	278.86	277.68	6.96	270.72	1	6.68N-3E	20	278.86	277.68	7.330909091	270.3490909
1	6.5N-3E	22	279.41	277.32	7.103333333	270.2166667	1	6.5N-3E	22	279.41	277.32	7.478181818	269.8418182
1	6.5N-2.81E	23	279.34	275.74	5.878888889	269.8611111	1	6.5N-2.81E	23	279.34	275.74	6.436363636	269.3036364
1	6.37N-3E	24	279.41	277.45	7.758888889	269.6911111	1	6.37N-3E	24	279.41	277.45	8.487272727	268.9627273
2	6.25N-6E	25	285.89	283.47	11.73777778	271.7322222	2	6.25N-6E	25	285.89	283.47	13.72272727	269.7472727
1	6.25N-4E	26	283.8	280.6	8.395555556	272.2044444	1	6.25N-4E	26	283.8	280.6	9.075454545	271.5245455
1	6.25N-3.68E	27	281.44	278.37	8.42625	269.94375	1	6.25N-3.68E	27	281.44	278.37	9.01	269.36
1	6.25N-3E	28	280.23	277.58	8.441111111	269.1388889	1	6.25N-3E	28	280.23	277.58	9.23	268.35
1	6.25N-2.81E	29	279	276.43	7.264444444	269.1655556	1	6.25N-2.81E	29	279	276.43	8.107272727	268.3227273
1	6N-4.75E	30	283.01	281.07	7.985555556	273.0844444	1	6N-4.75E	30	283.01	281.07	9.287272727	271.7827273
2	6N-4E	31	281.23	279.95	8.714444444	271.2355556	2	6N-4E	31	281.23	279.95	9.567272727	270.3827273
1	6N-3E	32	278.7	276.85	5.997777778	270.8522222	1	6N-3E	32	278.7	276.85	6.874545455	269.9754545
2	6N-2E	33	278.53	275.59	8.473333333	267.1166667	2	6N-2E	33	278.53	275.59	9.250909091	266.3390909
1	5.93N-2E	34	277.72	273.44	6.433333333	267.0066667	1	5.93N-2E	34	277.72	273.44	7.360909091	266.0790909
1	5.87N-2E	35	277.52	273.24	5.722222222	267.5177778	1	5.87N-2E	35	277.52	273.24	6.643636364	266.5963636
1	5.75N-2E	36	276.73	273.71	5.942222222	267.7677778	1	5.75N-2E	36	276.73	273.71	6.816363636	266.8936364
2	5.75N-1.75E	37	275.74	273.16	7.924444444	265.2355556	2	5.75N-1.75E	37	275.74	273.16	8.666363636	264.4936364
2	5.75N-1.5E	38	273.84	272.48	8.937777778	263.5422222	2	5.75N-1.5E	38	273.84	272.48	9.587272727	262.8927273
3	5.75N-1E	39	281.09	278.82	15.52875	263.29125	3	5.75N-1E	39	281.09	278.82	16.39285714	262.4271429
2	5.5N-1.75E	40	275.29	273.25	8.192222222	265.0577778	2	5.5N-1.75E	40	275.29	273.25	8.895454545	264.3545455
2	5.5N-1.25E	41	272.47	271.58	8.967777778	262.6122222	2	5.5N-1.25E	41	272.47	271.58	9.361818182	262.2181818
2	5.37N-0	42	269.25	267.2	9.772222222	257.4277778	2	5.37N-0	42	269.25	267.2	10.05545455	257.1445455
2	5N-4.87E	43	279.89	278.25	12.85666667	265.3933333	2	5N-4.87E	43	279.89	278.25	13.78181818	264.4681818
2	5N-4E	44	274.73	274.33	9.014444444	265.3155556	2	5N-4E	44	274.73	274.33	9.820909091	264.5090909
2	5N-3E	45	274.96	274.96	12.17555556	262.7844444	2	5N-3E	45	274.96	274.96	13.11909091	261.8409091
1	5N-2E	46	276.6	274.19	4.754444444	269.4355556	1	5N-2E	46	276.6	274.19	5.405454545	268.7845455
2	5N-1.75E	47	274.64	272.8	9.256666667	263.5433333	2	5N-1.75E	47	274.64	272.8	9.597272727	263.2027273
2	5N-1.25E	48	272.45	270.25	8.592222222	261.6577778	2	5N-1.25E	48	272.45	270.25	8.980909091	261.2690909
1	5N-1E	49	270.79	268.88	7.788888889	261.0911111	1	5N-1E	49	270.79	268.88	8.287272727	260.5927273
2	5N-0	50	268.53	267.38	9.95	257.43	2	5N-0	50	268.53	267.38	9.982	257.398
2	5N-.18W	51	268.73	267.01	10.09555556	256.9144444	2	5N-.18W	51	268.73	267.01	10.45909091	256.5509091
2	4.5N-1.75E	52	275.05	272.66	9.954444444	262.7055556	2	4.5N-1.75E	52	275.05	272.66	10.32272727	262.3372727
1	4.5N-1.25E	53	270.97	265.72	4.5325	261.1875	1	4.5N-1.25E	53	270.97	265.72	4.880909091	260.8390909
3	4.37N-.5W	54	266.99	267.29	14.70222222	252.5877778	3	4.37N-.5W	54	266.99	267.29	15.00909091	252.2809091

1991	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation	1992	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation
3	4.37N-.87W	55	272.11	267.99	13.66444444	254.3255556	3	4.37N-.87W	55	272.11	267.99	13.91636364	254.0736364
2	4N-4.87E	56	275.43	274.2	11.38222222	262.8177778	2	4N-4.87E	56	275.43	274.2	12.61090909	261.5890909
3	4N-4E	57	278.71	276.19	13.58444444	262.6055556	3	4N-4E	57	278.71	276.19	14.22090909	261.9690909
2	4N-3E	58	276.66	274.76	12.14888889	262.6111111	2	4N-3E	58	276.66	274.76	12.74909091	262.0109091
2	4N-2E	59	273.97	272.17	9.338888889	262.8311111	2	4N-2E	59	273.97	272.17	9.880909091	262.2890909
2	4N-1.75E	60	272.16	270.91	8.571111111	262.3388889	2	4N-1.75E	60	272.16	270.91	9.1	261.81
2	4N-1.25E	61	270.54	269.73	9.226666667	260.5033333	2	4N-1.25E	61	270.54	269.73	9.621818182	260.1081818
1	4N-1E	62	271.19	268.04	7.414444444	260.6255556	1	4N-1E	62	271.19	268.04	8.314545455	259.7254545
3	4N-1W	63	274.94	273.86	18.75444444	255.1055556	3	4N-1W	63	274.94	273.86	19.446	254.414
2	4N-0	64	267.21	266.76	9.34	257.42	2	4N-0	64	267.21	266.76	9.225454545	257.5345455
2	3.62N-2E	65	272.59	271.02	8.938888889	262.0811111	2	3.62N-2E	65	272.59	271.02	9.206363636	261.8136364
1	3.5N-1.75E	66	273.11	269.32	6.738888889	262.5811111	1	3.5N-1.75E	66	273.11	269.32	7.537272727	261.7827273
2	3N-5E	67	273.21	271.27	9.374444444	261.8955556	2	3N-5E	67	273.21	271.27	11.19545455	260.0745455
1	3N-4E	68	269.84	268.38	7.424444444	260.9555556	1	3N-4E	68	269.84	268.38	7.442727273	260.9372727
2	3N-3E	69	275.12	272.06	11.07222222	260.9877778	2	3N-3E	69	275.12	272.06	11.44636364	260.6136364
2	3N-2E	70	273.31	271.28	8.073333333	263.2066667	2	3N-2E	70	273.31	271.28	7.967272727	263.3127273
2	3N-1.75E	71	270.9	270.29	8.342222222	261.9477778	2	3N-1.75E	71	270.9	270.29	8.675454545	261.6145455
2	3N-.25W	72	265.42	264.39	8.633333333	255.7566667	2	3N-.25W	72	265.42	264.39	9.466363636	254.9236364
3	3N-1W	73	276.84	276.15	21.37	254.78	3	3N-1W	73	276.84	276.15	22.06636364	254.0836364
2	2.75N-2.25E	74	272.86	271.44	8.955555556	262.4844444	2	2.75N-2.25E	74	272.86	271.44	9.447272727	261.9927273
1	2.75N-1E	75	268.35	267.35	8.016666667	259.3333333	1	2.75N-1E	75	268.35	267.35	8.311	259.039
1	2.5N-2.5E	76	272.63	270.57	7.783333333	262.7866667	1	2.5N-2.5E	76	272.63	270.57	8.196363636	262.3736364
1	2.5N-2.62E	77	270.66	269.83	5.386666667	264.4433333	1	2.5N-2.62E	77	270.66	269.83	5.985454545	263.8445455
1	2.5N-2E	78	273.36	271.98	6.614444444	265.3655556	1	2.5N-2E	78	273.36	271.98	7.25	264.73
1	2.5N-1.87E	79	271.88	271.1	5.155555556	265.9444444	1	2.5N-1.87E	79	271.88	271.1	5.471	265.629
1	2.5N-1.75E	80	269.69	269.43	4.616666667	264.8133333	1	2.5N-1.75E	80	269.69	269.43	4.787272727	264.6427273
2	2.18N-1.5W	81	270.91	262.69	8.552222222	254.1377778	2	2.18N-1.5W	81	270.91	262.69	9.817272727	252.8727273
2	2.25N-2.37E	82	272.91	270.39	8.47	261.92	2	2.25N-2.37E	82	272.91	270.39	8.766	261.624
1	2.25N-2E	83	273.99	270.92	5.208888889	265.7111111	1	2.25N-2E	83	273.99	270.92	5.907272727	265.0127273
1	2.25N-1.75E	84	274.41	272.2	6.997777778	265.2022222	1	2.25N-1.75E	84	274.41	272.2	7.179090909	265.0209091
2	2N-5E	85	272.67	269.05	10.05222222	258.9977778	2	2N-5E	85	272.67	269.05	11.16454545	257.8854545
1	2N-2E	86	270.92	270.8	5.818888889	264.9811111	1	2N-2E	86	270.92	270.8	7.345	263.455
1	2N-1E	87	272.09	268.81	9.028888889	259.7811111	1	2N-1E	87	272.09	268.81	9.000909091	259.8090909
2	2N-.25E	88	267.59	265.5	8.053333333	257.4466667	2	2N-.25E	88	267.59	265.5	8.576363636	256.9236364
2	2N-1.25W	89	263.31	260.77	9.91	250.86	2	2N-1.25W	89	263.31	260.77	10.11454545	250.6554545
2	1.75N-1.25W	90	264.28	261.73	9.441111111	252.2888889	2	1.75N-1.25W	90	264.28	261.73	10.18909091	251.5409091
2	1.75N-1.75W	91	264.11	261.43	10.36888889	251.0611111	2	1.75N-1.75W	91	264.11	261.43	10.57454545	250.8554545
2	1.5N-1.25W	92	264.18	261.32	10.19222222	251.1277778	2	1.5N-1.25W	92	264.18	261.32	10.38090909	250.9390909
2	1.5N-2W	93	261.32	260.83	10.12222222	250.7077778	2	1.5N-2W	93	261.32	260.83	10.32090909	250.5090909
3	1.5N-2.25W	94	264.6	261.91	11.58	250.33	3	1.5N-2.25W	94	264.6	261.91	11.74636364	250.1636364
2	1.25N-1.5W	95	262.06	260.49	9.021111111	251.4688889	2	1.25N-1.5W	95	262.06	260.49	9.241818182	251.2481818
2	1N-5E	96	271.74	268.72	12.98777778	255.7322222	2	1N-5E	96	271.74	268.72	13.77272727	254.9472727
2	1N-4E	97	266.29	266.02	9.73	256.29	2	1N-4E	97	266.29	266.02	10.195	255.825
2	1N-3E	98	267.49	266.62	9.271111111	257.3488889	2	1N-3E	98	267.49	266.62	9.621818182	256.9981818
3	1N-2.12E	99	270.74	270.7	13.28	257.42	3	1N-2.12E	99	270.74	270.7	13.59818182	257.1018182
2	1N-1E	100	266.52	266.74	8.99	257.75	2	1N-1E	100	266.52	266.74	7.66125	259.07875
2	1N-0	101	264.79	264.5	9.058888889	255.4411111	2	1N-0	101	264.79	264.5	9.535454545	254.9645455
2	1N-.75W	102	261.87	261.01	8.742222222	252.2677778	2	1N-.75W	102	261.87	261.01	9.340909091	251.6690909
2	1N-2W	103	259.68	258.34	8.65	249.69	2	1N-2W	103	259.68	258.34	8.604	249.736
2	1N-2.25W	104	257.8	257.52	8.643333333	248.8766667	2	1N-2.25W	104	257.8	257.52	8.699090909	248.8209091
2	0.5N-2.37W	105	258.52	256.72	9.597777778	247.1222222	2	0.5N-2.37W	105	258.52	256.72	9.810909091	246.9090909
2	0.12N-5E	106	269.45	267.07	13.69555556	253.3744444	2	0.12N-5E	106	269.45	267.07	14.55181818	252.5181818
2	0-4.12E	107	266.9	266.3	12.10888889	254.1911111	2	0-4.12E	107	266.9	266.3	12.93818182	253.3618182
2	0-3E	108	263.76	262.77	8.413333333	254.3566667	2	0-3E	108	263.76	262.77	8.730909091	254.0390909
2	0-2E	109	267.84	265.18	11.15375	254.02625	2	0-2E	109	267.84	265.18	11.56181818	253.6181818

1991	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation	1992	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation
1	0-1E	110	261.7	261.42	7.728888889	253.6911111	1	0-1E	110	261.7	261.42	7.840909091	253.5790909
2	0-0	111	262.37	261.83	8.206666667	253.6233333	2	0-0	111	262.37	261.83	8.48	253.35
2	0-1W	112	260.19	259.7	10.30125	249.39875	2	0-1W	112	260.19	259.7	10.57181818	249.1281818
2	0-2W	113	258.18	256.12	10.03777778	246.0822222	2	0-2W	113	258.18	256.12	10.06727273	246.0527273
2	0-2.75W	114	256.48	255.13	10.33555556	244.7944444	2	0-2.75W	114	256.48	255.13	10.48636364	244.6436364
2	0.5S-2.75W	115	257.77	255.36	11.33777778	244.0222222	2	0.5S-2.75W	115	257.77	255.36	11.53636364	243.8236364
3	0.5S-3W	116	257.35	255.03	12.02666667	243.0033333	3	0.5S-3W	116	257.35	255.03	12.25	242.78
2	0.5S-3.18W	117	257.79	254.4	11.25222222	243.1477778	2	0.5S-3.18W	117	257.79	254.4	11.43727273	242.9627273
3	1S-4E	118	268.56	266.74	14.06666667	252.6733333	3	1S-4E	118	268.56	266.74	15.27636364	251.4636364
2	1S-3E	119	263.55	260.73	10.96888889	249.7611111	2	1S-3E	119	263.55	260.73	11.17363636	249.5563636
2	1S-2E	120	260.54	259.92	10.09444444	249.8255556	2	1S-2E	120	260.54	259.92	9.914545455	250.0054545
1	1S-1E	121	261.85	258.57	8.531111111	250.0388889	1	1S-1E	121	261.85	258.57	8.378181818	250.1918182
2	1S-.25W	122	258.55	258.53	8.763333333	249.7666667	2	1S-.25W	122	258.55	258.53	9.316363636	249.2136364
2	1S-1W	123	259.49	258.92	10.36222222	248.5577778	2	1S-1W	123	259.49	258.92	10.76272727	248.1572727
2	1S-2W	124	255.99	254.74	10.55777778	244.1822222	2	1S-2W	124	255.99	254.74	10.99	243.75
2	1S-3W	125	255.47	253.89	11.00666667	242.8833333	2	1S-3W	125	255.47	253.89	11.25818182	242.6318182
2	1S-3.37W	126	253.86	252.6	10.49888889	242.1011111	2	1S-3.37W	126	253.86	252.6	10.59454545	242.0054545
2	1.25S-4W	127	255.89	252.21	10.71555556	241.4944444	2	1.25S-4W	127	255.89	252.21	11.42272727	240.7872727
2	1.5S-4.5W	128	254.24	250.98	10.76777778	240.2122222	2	1.5S-4.5W	128	254.24	250.98	11.08272727	239.8972727
2	1.5S-4.75W	129	252.55	250.98	11.27666667	239.7033333	2	1.5S-4.75W	129	252.55	250.98	11.75727273	239.2227273
2	2S-2.75E	130	261.59	257.83	10.54333333	247.2866667	2	2S-2.75E	130	261.59	257.83	10.55	247.28
3	2S-3.75E	131	265.35	262.89	14.13	248.76	3	2S-3.75E	131	265.35	262.89	14.56636364	248.3236364
2	2S-2E	132	258.15	257.56	10.59222222	246.9677778	2	2S-2E	132	258.15	257.56	10.49909091	247.0609091
2	2S-1E	133	258.01	255.81	9.875555556	245.9344444	2	2S-1E	133	258.01	255.81	10.28545455	245.5245455
1	2S-0	134	256.3	255.56	7.623333333	247.9366667	1	2S-0	134	256.3	255.56	8.681111111	246.8788889
2	2S-1W	135	256.21	254.2	8.415555556	245.7844444	2	2S-1W	135	256.21	254.2	9.153636364	245.0463636
2	2S-2W	136	254.96	253.48	9.053333333	244.4266667	2	2S-2W	136	254.96	253.48	9.642727273	243.8372727
2	2S-3W	137	252.16	252.1	9.068888889	243.0311111	2	2S-3W	137	252.16	252.1	9.402	242.698
2	2S-4W	138	252.33	251.88	10.20777778	241.6722222	2	2S-4W	138	252.33	251.88	11.47454545	240.4054545
3	2S-4.5W	139	254.87	252.25	11.97555556	240.2744444	3	2S-4.5W	139	254.87	252.25	12.53454545	239.7154545
3	2S-5.12W	140	250.86	249.04	11.85	237.19	3	2S-5.12W	140	250.86	249.04	11.93545455	237.1045455
2	2.5S-5.25W	141	252.87	249.19	11.26888889	237.9211111	2	2.5S-5.25W	141	252.87	249.19	11.54909091	237.6409091
1	2.75S-3.5E	142	260.23	258.41	11.95333333	246.4566667	1	2.75S-3.5E	142	260.23	258.41	12.47454545	245.9354545
3	2.75S-5.25W	143	251.32	249.21	12.1875	237.0225	3	2.75S-5.25W	143	251.32	249.21	12.19909091	237.0109091
1	3S-4.37E	144	263.96	262.35	9.032222222	253.3177778	1	3S-4.37E	144	263.96	262.35	7.810909091	254.5390909
2	3S-3E	145	258.93	257.22	11.78333333	245.4366667	2	3S-3E	145	258.93	257.22	12.29090909	244.9290909
2	3S-2E	146	257.91	255.88	11.41888889	244.4611111	2	3S-2E	146	257.91	255.88	11.40545455	244.4745455
2	3S-1E	147	256.81	254.64	11.80222222	242.8377778	2	3S-1E	147	256.81	254.64	12.19090909	242.4490909
2	3S-0	148	253.44	252.09	8.691111111	243.3988889	2	3S-0	148	253.44	252.09	9.395454545	242.6945455
2	3S-1W	149	254.56	252.57	9.243333333	243.3266667	2	3S-1W	149	254.56	252.57	9.887	242.683
2	3S-2W	150	253.78	250.84	9.953333333	240.8866667	2	3S-2W	150	253.78	250.84	10.88090909	239.9590909
2	3S-3W	151	247.32	248.8	8.232222222	240.5677778	2	3S-3W	151	247.32	248.8	8.610909091	240.1890909
2	3S-4W	152	252.11	249.83	10.29222222	239.5377778	2	3S-4W	152	252.11	249.83	10.71272727	239.1172727
3	3S-5.25W	153	251.33	248.77	11.59555556	237.1744444	3	3S-5.25W	153	251.33	248.77	12.00818182	236.7618182
2	3S-5.5W	154	249.57	246.8	8.871111111	237.9288889	2	3S-5.5W	154	249.57	246.8	9.098181818	237.7018182
2	3.12S-4.5W	155	251.39	247.97	10.95666667	237.0133333	2	3.12S-4.5W	155	251.39	247.97	10.68363636	237.2863636
2	3.37S-4.5W	156	248.74	247.84	10.56555556	237.2744444	2	3.37S-4.5W	156	248.74	247.84	10.94	236.9
2	3.5S-5.25W	157	249.04	247.15	10.07111111	237.0788889	2	3.5S-5.25W	157	249.04	247.15	10.55545455	236.5945455
2	3.5S-5.5W	158	248.33	246.1	8.612222222	237.4877778	2	3.5S-5.5W	158	248.33	246.1	9.058181818	237.0418182
2	3.62S-4.75W	159	252.31	248.59	11.50666667	237.0833333	2	3.62S-4.75W	159	252.31	248.59	11.85727273	236.7327273
2	3.75S-5.5W	160	247.38	246.61	9.295555556	237.3144444	2	3.75S-5.5W	160	247.38	246.61	9.852727273	236.7572727
2	3.87S-4.25W	161	248.14	247.62	10.64111111	236.9788889	2	3.87S-4.25W	161	248.14	247.62	11.02909091	236.5909091
2	4S-4E	162	265.61	261.39	13.72666667	247.6633333	2	4S-4E	162	265.61	261.39	15.19090909	246.1990909
2	4S-3E	163	260.08	258.94	11.11666667	247.8233333	2	4S-3E	163	260.08	258.94	12.293	246.647

1991	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation	1992	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation
3	4S-2E	164	259.63	257.4	14.45555556	242.9444444	3	4S-2E	164	259.63	257.4	13.152	244.248
3	4S-1E	165	259.23	254.05	13.95444444	240.0955556	3	4S-1E	165	259.23	254.05	14.38181818	239.6681818
2	4S-0	166	252.02	251.67	11.75444444	239.9155556	2	4S-0	166	252.02	251.67	12.48454545	239.1854545
2	4S-.5W	167	253.41	251.47	10.72666667	240.7433333	2	4S-.5W	167	253.41	251.47	11.97454545	239.4954545
2	4S-.75W	168	253.23	251.32	11.26333333	240.0566667	2	4S-.75W	168	253.23	251.32	12.62454545	238.6954545
3	4S-2W	169	250.85	249.2	13.62111111	235.5788889	3	4S-2W	169	250.85	249.2	14.16545455	235.0345455
3	4S-3W	170	250.85	249.68	12.65444444	237.0255556	3	4S-3W	170	250.85	249.68	12.69363636	236.9863636
1	4S-4W	171	246.83	246.34	8.432222222	237.9077778	1	4S-4W	171	246.83	246.34	8.928181818	237.4118182
3	4S-4.5W	172	248.53	248.16	11.81333333	236.3466667	3	4S-4.5W	172	248.53	248.16	12.47181818	235.6881818
2	4S-5.25W	173	249.14	245.96	8.995555556	236.9644444	2	4S-5.25W	173	249.14	245.96	9.943636364	236.0163636
2	4S-5.5W	174	249.08	246.39	9.324444444	237.0655556	2	4S-5.5W	174	249.08	246.39	10.11363636	236.2763636
2	4S-5.87W	175	252.49	246.47	9.21	237.26	2	4S-5.87W	175	252.49	246.47	9.534545455	236.9354545
2	4.25S-4.12W	176	250.26	247.26	10.18	237.08	2	4.25S-4.12W	176	250.26	247.26	10.885	236.375
2	4.25S-4.5W	177	250.4	246.8	10.7	236.1	2	4.25S-4.5W	177	250.4	246.8	10.686	236.114
2	4.25S-5.5W	178	249.4	246.25	8.016666667	238.2333333	2	4.25S-5.5W	178	249.4	246.25	9.357272727	236.8927273
2	4.5S-4.75W	179	247.36	245.52	10.09888889	235.4211111	2	4.5S-4.75W	179	247.36	245.52	11.03363636	234.4863636
2	4.5S-5.5W	180	249.47	246.08	8.343333333	237.7366667	2	4.5S-5.5W	180	249.47	246.08	9.430909091	236.6490909
2	4.5S-6.25W	181	248.63	246.47	9.951111111	236.5188889	2	4.5S-6.25W	181	248.63	246.47	10.35363636	236.1163636
2	4.75S-4.25W	182	249.14	246.78	10.51666667	236.2633333	2	4.75S-4.25W	182	249.14	246.78	11.45818182	235.3218182
2	4.75S-4.75W	183	246.3	244.5	10.39777778	234.1022222	2	4.75S-4.75W	183	246.3	244.5	11.18545455	233.3145455
2	5S-3E	184	257.68	256.65	11.29222222	245.3577778	2	5S-3E	184	257.68	256.65	12.61454545	244.0354545
3	5S-2.25E	185	259.3	257.61	13.68666667	243.9233333	3	5S-2.25E	185	259.3	257.61	14.78545455	242.8245455
3	5S-1E	186	255.81	253.72	15.50111111	238.2188889	3	5S-1E	186	255.81	253.72	15.96	237.76
3	5S-0	187	254.3	251.38	15.34	236.04	3	5S-0	187	254.3	251.38	15.66636364	235.7136364
3	5S-.75W	188	249.17	248.95	13.40222222	235.5477778	3	5S-.75W	188	249.17	248.95	14.31272727	234.6372727
3	5S-2W	189	245.35	245.3	11.53444444	233.7655556	3	5S-2W	189	245.35	245.3	12.751	232.549
2	5S-2.75W	190	244.17	242.59	11.28111111	231.3088889	2	5S-2.75W	190	244.17	242.59	11.81545455	230.7745455
2	5S-3.75W	191	249.28	247.77	11.5	236.27	2	5S-3.75W	191	249.28	247.77	11.81454545	235.9554545
2	5S-4.12W	192	248.93	246.83	10.19666667	236.6333333	2	5S-4.12W	192	248.93	246.83	10.69727273	236.1327273
2	5S-4.5W	193	247.04	244.83	10.59555556	234.2344444	2	5S-4.5W	193	247.04	244.83	11.017	233.813
2	5S-4.75W	194	246.64	244.38	10.26555556	234.1144444	2	5S-4.75W	194	246.64	244.38	11.18363636	233.1963636
2	5S-5.5W	195	245.46	243.81	8.866666667	234.9433333	2	5S-5.5W	195	245.46	243.81	9.349090909	234.4609091
2	5S-6.18W	196	246.48	244.45	9.285555556	235.1644444	2	5S-6.18W	196	246.48	244.45	9.58	234.87
2	5.5S-.5W	197	247.78	247.18	11.99777778	235.1822222	2	5.5S-.5W	197	247.78	247.18	12.168	235.012
3	5.5S-1.25W	198	247.32	245.49	12.42777778	233.0622222	3	5.5S-1.25W	198	247.32	245.49	13.44545455	232.0445455
2	5.5S-4.25W	199	248.3	246.29	10.56555556	235.7244444	2	5.5S-4.25W	199	248.3	246.29	10.62090909	235.6690909
3	5.5S-4.5W	200	245.9	244.75	11.49333333	233.2566667	3	5.5S-4.5W	200	245.9	244.75	11.84090909	232.9090909
3	5.5S-4.75W	201	246.28	244.05	12.67666667	231.3733333	3	5.5S-4.75W	201	246.28	244.05	13.19545455	230.8545455
2	5.5S-6.37W	202	246.66	242.63	8.546666667	234.0833333	2	5.5S-6.37W	202	246.66	242.63	8.784545455	233.8454545
2	5.75S-2W	203	243.63	242.33	11.82111111	230.5088889	2	5.75S-2W	203	243.63	242.33	12.41636364	229.9136364
3	6S-3E	204	258.01	256.13	15.92555556	240.2044444	3	6S-3E	204	258.01	256.13	16.63727273	239.4927273
2	6S-2E	205	255.23	254.45	13.45666667	240.9933333	2	6S-2E	205	255.23	254.45	14.45	240
3	6S-1.12E	206	256.31	253.73	13.81333333	239.9166667	3	6S-1.12E	206	256.31	253.73	14.30090909	239.4290909
3	6S-2.75W	207	243.98	241.97	13.76444444	228.2055556	3	6S-2.75W	207	243.98	241.97	14.12727273	227.8427273
2	6S-4W	208	245.48	243.84	10.61111111	233.2288889	2	6S-4W	208	245.48	243.84	10.69545455	233.1445455
2	6S-4.5W	209	246.86	243.84	11.38222222	232.4577778	2	6S-4.5W	209	246.86	243.84	11.63818182	232.2018182
2	6S-5.5W	210	244.17	242.61	9.901111111	232.7088889	2	6S-5.5W	210	244.17	242.61	10.101	232.509
1	6S-6.25W	211	242.64	240.09	7.224444444	232.8655556	1	6S-6.25W	211	242.64	240.09	7.389090909	232.7009091
3	6.75S-0	212	253.73	249.73	13.01111111	236.7188889	3	6.75S-0	212	253.73	249.73	13.84636364	235.8836364
2	6.87S-1.87E	213	252.93	252.8	13.62111111	239.1788889	2	6.87S-1.87E	213	252.93	252.8	13.843	238.957
2	7S-1E	214	256.75	252.93	12.98	239.95	2	7S-1E	214	256.75	252.93	13.15818182	239.7718182
2	7S-0	215	251.43	250.34	12.47666667	237.8633333	2	7S-0	215	251.43	250.34	13.42545455	236.9145455
2	7S-1W	216	247.64	245.6	11.33888889	234.2611111	2	7S-1W	216	247.64	245.6	12.14090909	233.4590909

1991	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation	1992	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation
2	7S-2W	217	241.33	240.97	10.70666667	230.2633333	2	7S-2W	217	241.33	240.97	11.36545455	229.6045455
3	7S-3W	218	241.62	240.88	11.99555556	228.8844444	3	7S-3W	218	241.62	240.88	12.27090909	228.6090909
2	7S-4W	219	242.52	241.91	10.87888889	231.0311111	2	7S-4W	219	242.52	241.91	11.00636364	230.9036364
2	7S-5W	220	243.43	241.59	10.08222222	231.5077778	2	7S-5W	220	243.43	241.59	9.475454545	232.1145455
2	7S-5.75W	221	244.57	241.86	9.701111111	232.1588889	2	7S-5.75W	221	244.57	241.86	9.727272727	232.1327273
2	7S-6.5W	222	244.09	241.02	9.833333333	231.1866667	2	7S-6.5W	222	244.09	241.02	9.813636364	231.2063636
2	7.25S-.5E	223	253.45	251.73	12.81222222	238.9177778	2	7.25S-.5E	223	253.45	251.73	13.37909091	238.3509091
2	7.25S-.25E	224	253.46	249.77	11.24888889	238.5211111	2	7.25S-.25E	224	253.46	249.77	12.22272727	237.5472727
2	7.25S-.5W	225	248.92	246.58	10.21555556	236.3644444	2	7.25S-.5W	225	248.92	246.58	10.95181818	235.6281818
2	7.25S-.25W	226	250.44	247.1	10.14444444	236.9555556	2	7.25S-.25W	226	250.44	247.1	10.89181818	236.2081818
2	7.75S-0	227	252.5	248.19	10.89444444	237.2955556	2	7.75S-0	227	252.5	248.19	11.63818182	236.5518182
2	8S-1E	228	253.51	250.64	12.58444444	238.0555556	2	8S-1E	228	253.51	250.64	12.97454545	237.6654545
2	8S-.5E	229	253.44	250.07	12.16	237.91	2	8S-.5E	229	253.44	250.07	12.54636364	237.5236364
2	8S-.25W	230	246.82	245.02	8.933333333	236.0866667	2	8S-.25W	230	246.82	245.02	9.89	235.13
1	8S-.5W	231	245.28	243.91	8.133333333	235.7766667	1	8S-.5W	231	245.28	243.91	9.193	234.717
1	8S-1W	232	246.82	242.57	7.226666667	235.3433333	1	8S-1W	232	246.82	242.57	7.831818182	234.7381818
2	8S-2W	233	244.92	242.5	9.3575	233.1425	2	8S-2W	233	244.92	242.5	9.900909091	232.5990909
2	8S-3W	234	239.43	238.57	9.971111111	228.5988889	2	8S-3W	234	239.43	238.57	10.32090909	228.2490909
2	8S-5W	235	241.01	239.2	10.31222222	228.8877778	2	8S-5W	235	241.01	239.2	9.018181818	230.1818182
1	8S-5.5W	236	239.2	238.37	7.436666667	230.9333333	1	8S-5.5W	236	239.2	238.37	6.414545455	231.9554545
1	8S-6.5W	237	242.17	238.59	7.932222222	230.6577778	1	8S-6.5W	237	242.17	238.59	8.835454545	229.7545455
2	8.25S-4.25W	238	240.34	237.41	10.49222222	226.9177778	2	8.25S-4.25W	238	240.34	237.41	10.53909091	226.8709091
3	9S-0	239	250.45	249.42	14.86222222	234.5577778	3	9S-0	239	250.45	249.42	15.93272727	233.4872727
2	9S-1.25W	240	243.23	241.76	9.226666667	232.5333333	2	9S-1.25W	240	243.23	241.76	10.38	231.38
2	9S-2W	241	244.64	241.7	8.823333333	232.8766667	2	9S-2W	241	244.64	241.7	9.896363636	231.8036364
2	9S-3W	242	239.98	237.81	7.697777778	230.1122222	2	9S-3W	242	239.98	237.81	8.491818182	229.3181818
2	9S-4W	243	236.84	235.23	10.4	224.83	2	9S-4W	243	236.84	235.23	10.67545455	224.5545455
2	9S-5W	244	236.62	235.18	8.216666667	226.9633333	2	9S-5W	244	236.62	235.18	7.9	227.28
2	9S-5.75W	245	235.74	236.1	9.423333333	226.6766667	2	9S-5.75W	245	235.74	236.1	9.268181818	226.8318182
1	9S-6.5W	246	237.54	235.17	6.848888889	228.3211111	1	9S-6.5W	246	237.54	235.17	6.720909091	228.4490909
3	10S-0	247	251.76	249.13	16.87111111	232.2588889	3	10S-0	247	251.76	249.13	17.38909091	231.7409091
3	10S-1W	248	249.69	248.18	16.80222222	231.3777778	3	10S-1W	248	249.69	248.18	17.48727273	230.6927273
2	10S-2W	249	242	239.93	8.75	231.18	2	10S-2W	249	242	239.93	9.930909091	229.9990909
2	10S-3W	250	240.34	237.37	7.132222222	230.2377778	2	10S-3W	250	240.34	237.37	8.118181818	229.2518182
1	10S-3.87W	251	237.45	235.16	7.241111111	227.9188889	1	10S-3.87W	251	237.45	235.16	7.906363636	227.2536364
2	10S-5W	252	236.47	233.49	9.461111111	224.0288889	2	10S-5W	252	236.47	233.49	9.071818182	224.4181818
2	10S-6.75W	253	236.85	234.71	7.916666667	226.7933333	2	10S-6.75W	253	236.85	234.71	7.477272727	227.2327273
2	10S-5.75W	254	235.76	233.22	7.418888889	225.8011111	2	10S-5.75W	254	235.76	233.22	7.238181818	225.9818182
2	10.75S-4W	255	236.58	233.4	7.541111111	225.8588889	2	10.75S-4W	255	236.58	233.4	8.263636364	225.1363636
3	11S-1W	256	244.62	243.3	13.38555556	229.9144444	3	11S-1W	256	244.62	243.3	14.06909091	229.2309091
2	11S-2W	257	238.8	237.75	8.36125	229.38875	2	11S-2W	257	238.8	237.75	8.956666667	228.7933333
2	11S-3W	258	237.96	236.02	7.926666667	228.0933333	2	11S-3W	258	237.96	236.02	7.407272727	228.6127273
2	11S-5W	259	235.02	231.19	8.333333333	222.8566667	2	11S-5W	259	235.02	231.19	8.72	222.47
2	11S-5.75W	260	234.78	232.35	7.678571429	224.6714286	2	11S-5.75W	260	234.78	232.35	6.253	226.097
2	11S-6.87W	261	233.32	231.42	7.926666667	223.4933333	2	11S-6.87W	261	233.32	231.42	7.891818182	223.5281818
2	11.75S-6.75W	262	231.3	231	7.734444444	223.2655556	2	11.75S-6.75W	262	231.3	231	7.787272727	223.2127273
2	12S-1W	263	238.84	238.29	9.62	228.67	2	12S-1W	263	238.84	238.29	10.085	228.205
2	12S-2W	264	237.63	237.11	9.485555556	227.6244444	2	12S-2W	264	237.63	237.11	9.960909091	227.1490909
3	12S-3W	265	242.36	240.04	13.27444444	226.7655556	3	12S-3W	265	242.36	240.04	14.05727273	225.9827273
2	12S-4W	266	237.71	234.84	10.47555556	224.3644444	2	12S-4W	266	237.71	234.84	11.25090909	223.5890909
2	12S-5W	267	236.8	233.16	9.04	224.12	2	12S-5W	267	236.8	233.16	10.51090909	222.6490909
2	12S-6W	268	233.06	231.72	9.455555556	222.2644444	2	12S-6W	268	233.06	231.72	10.72363636	220.9963636
2	13S-2W	269	242.29	240.58	10.85555556	229.7244444	2	13S-2W	269	242.29	240.58	11.977	228.603

1991	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation	1992	Well Location	Number	Pipe Elevation	Ground Elevation	Average Depth to Water Table	Water Elevation
2	13.12S-2.87W	270	243.53	240.58	14.06222222	226.5177778	2	13.12S-2.87W	270	243.53	240.58	15.13818182	225.4418182
1	13S-4.25W	271	234.53	234.31	7.558888889	226.7511111	1	13S-4.25W	271	234.53	234.31	7.790909091	226.5190909
2	13S-5W	272	235.57	233.88	9.127777778	224.7522222	2	13S-5W	272	235.57	233.88	10.01727273	223.8627273
2	13S-6W	273	232.62	231.6	8.995555556	222.6044444	2	13S-6W	273	232.62	231.6	9.714545455	221.8854545
1	13S-6.5W	274	230.69	228.55	6.974444444	221.5755556	1	13S-6.5W	274	230.69	228.55	7.605454545	220.9445455
2	13S-7.12W	275	233.57	232.23	10.74555556	221.4844444	2	13S-7.12W	275	233.57	232.23	11.06818182	221.1618182
1	14.25S-6.5W	276	231.67	228.46	6.694444444	221.7655556	1	14.25S-6.5W	276	231.67	228.46	7.684545455	220.7754545
2	14.25S-7.18W	277	234.11	228.1	8.764444444	219.3355556	2	14.25S-7.18W	277	234.11	228.1	9.64	218.46
1	15S-6W	278	229.73	228.93	6.218888889	222.7111111	1	15S-6W	278	229.73	228.93	7.129	221.801
1	15S-6.75W	279	228.81	226.48	5.566666667	220.9133333	1	15S-6.75W	279	228.81	226.48	6.894444444	219.5855556
1	16S-6W	280	227.88	226.33	5.006666667	221.3233333	1	16S-6W	280	227.88	226.33	5.494545455	220.8354545
1	17S-5W	281	230.06	228.14	6.858888889	221.2811111	1	17S-5W	281	230.06	228.14	7.917272727	220.2227273
1	17S-5.75W	282	227.63	226.14	6.793333333	219.3466667	1	17S-5.75W	282	227.63	226.14	5.989090909	220.1509091
1	18S-5W	283	227.16	224.12	6.136666667	217.9833333	1	18S-5W	283	227.16	224.12	6.692727273	217.4272727

2000	Pipe Elevation	Ground Elevation	Average Water Elevation	Average Depth to Water Table	2007	Well Location	Drainage Area	Pipe Elevation	Average Ground Elevation	Water Elevation	Average Depth to Water Table
	288.79	287.03	269.3555556	17.67444444		8N-7E	R	289.08	287.01	267.9018182	19.10818182
	285.26	283.47	279.2411111	4.228888889		7.5N-5.62E		285.26	287.01	267.9018182	4.468333333
	284.37	283	278.645	4.355		7.37N-5.12E		285.42	284.1	279.3658333	4.899
	284.65	283.09	278.1766667	4.913333333		7.37N-4.87E	J PMP	284.67	283.11	278.211	5.454
	288.65	282.31	278.59375	3.71625		7.37N-4.75E	J PMP	288.65	283.13	277.676	3.17
	284.76	281.9	276.505	5.395		7.37N-4.25E	J PMP	284.76	282.31	279.14	5.365
	284.04	282.02	274.9433333	7.076666667		7.25N-4.31E	J PMP	284.73	281.9	276.535	6.388333333
	284.93	281	275.3622222	5.637777778		7.18N-4.06E	J PMP	284.07	282.02	275.6316667	6.185454545
	282.67	280.02	274.3511111	5.668888889		7.12N-4E	J PMP	282.69	280.87	274.6845455	6.06125
	285.5	283.29	269.4966667	13.79333333		7N-7E	R	285.5	280.2	274.13875	15.535
	286.2	283.5	274.2025	9.2975		7N-6.25E	R	286.2	283.29	267.755	9.794166667
	285.1	282.5	275.4522222	7.047777778		7N-4.62E	J PMP	285.1	283.5	273.7058333	7.085
	281.8	280.21	272.7722222	7.437777778		6.87N-3.93E	J PMP	281.8	282.5	275.415	7.334
	280.9	279.15	273.685	5.465		6.87N-3.81E	J PMP	280.9	280.21	272.876	5.014166667
	281.87	281.18	269.6088889	11.57111111		6.75N-3.43E		281.87	279.15	274.1358333	#VALUE!
	278.86	277.68	269.49625	8.18375		6.56N-3E	Outfall	278.86	277.51	270.909	#VALUE!
	279.73	279.26	271.4833333	7.776666667		6.62N-3.75E	OL	279.73	278.69	271.0458333	7.415
	278.02	277.4	269.58	7.82		6.62N-3E		280.46	279.26	271.845	6.601
	279.9	278.64	269.4725	9.1675		6.68N-3E		280.08	281.18	273.535833	7.644166667
	279.34	277.2	269.15	8.05		6.5N-3E		279.06	277.16	269.9308333	6.715454545
	279.34	275.74	268.6255556	7.114444444		6.5N-2.81E		279.34	275.74	270.4445455	5.495
	279.22	277.4	268.3485714	9.051428571		6.37N-3E		279	277.38	270.245	7.7575
	286.57	283.81	270.6175	13.1925		6.25N-6E	R	286.56	283.79	269.6225	15.21083333
	283.81	280.89	270.50375	10.38625		6.25N-4E	OL	283.81		268.5791667	9.685
									280.62		
						6.25N-3E		280.07	277.68	269.145	8.467272727
	280.23	277.58	267.8925	9.6875		6.25N-2.81E		279	276.43	269.2127273	7.371666667
	279	276.43	267.4188889	9.011111111		6N-4.75E	OL	282.51	281.77	269.0583333	11.85727273
	282.8	281.07	269.56375	11.50625		6N-4E	OL	281.23	279.95	269.9127273	10.29916667
	281.23	279.95	269.2933333	10.65666667		6N-3E	OUTFL	278.7	276.85	269.6508333	7.2125
	278.7	276.85	269.4777778	7.372222222		6N-2E	OUTFL	283.16	275.38	269.6375	8.471666667
	278.53	275.59	265.76375	9.82625		5.93N-2E		276.22	275.69	266.9083333	8.843333333
	276.53	275.17	265.96	9.21		5.87N-2E		276.26	275.29	266.8466667	#VALUE!
	276.47	273.24	266.3228571	6.917142857		5.75N-2E		276.42	274.06	268.84833	6.741666667
	276.47	273.71	266.5425	7.1675		5.75N-1.75E	OUTFL	275.74	273.16	267.3183333	8.2925
	275.74	273.16	264.1775	8.9825		5.75N-1.5E		273.72	272.57	264.8675	9.2675
	273.84	272.48	262.8922222	9.587777778		5.75N-1E	MESA	281.22	278.8	263.3025	16.94636364
	281.22	278.8	261.4733333	17.32666667		5.5N-1.75E		275.29	272.5	261.8536364	#VALUE!
	275.29	272.25	264.0722222	8.177777778		5.5N-1.25E	OUTFL	272.61	271.52	263.46083	9.039166667
	272.77	271.52	262.0855556	9.434444444		5.37N-0	MESA	269.25	267.2	262.4808333	9.096363636
	269.25	267.2	258.0355556	9.164444444		5N-4.87E	OL	279.73	278.13	258.1036364	14.9225
	279.73	278.13	263.8488889	14.28111111		5N-4E	OUTFL	274.98	274.54	263.2075	10.149
	274.42	274.42	263.9657143	10.45428571		5N-3E	OUTFL	277.79	275.09	264.391	8.912727273
	277.97	275.17	265.63	9.54		5N-2E		276.6	274.19	266.1772727	7.805
	276.6	274.19	265.4633333	8.726666667		5N-1.75E	OUTFL	274.64	272.8	266.385	9.681818182
	274.64	272.8	262.8033333	9.996666667		5N-1.25E	OUTFL	272.78	270.25	263.1181818	#VALUE!
	272.78	270.25	261.1966667	9.053333333		5N-1E		270.79	268.88	262.319	7.931
	270.79	268.88	260.70625	8.17375		5N-0		268.51	267.49	260.949	9.659
	268.53	267.38	257.8825	9.4975		5N-18W	MESA	268.73	267.01	257.831	9.621
	268.73	267.01	257.4155556	9.594444444		4.5N-1.75E		275.07	272.71	257.389	10.16363636
	275.07	272.71	262.0344444	10.67555556		4.5N-1.25E		270.97	269.52	262.5463636	8.969
	270.97	269.52	260.6344444	8.885555556		4.37N-.5W	MESA	270.14	267.6	260.551	11.37

2000	Pipe Elevation	Ground Elevation	Average Water Elevation	Average Depth to Water Table	2007	Well Location	Drainage Area	Pipe Elevation	Average Ground Elevation	Water Elevation	Average Depth to Water Table
	266.99	267.37	252.6755556	14.69444444		4.37N-.87W	MESA	272.11	267.99	256.23	12.458
	272.11	267.99	255.2433333	12.74666667		4N-4.87E	R	275.41	274.23	255.532	13.62916667
	275.41	274.23	262.6111111	11.61888889		4N-4E	OUTFL	279.28	276.15	260.6008333	14.6425
	279	276.29	262.68	13.61		4N-3E	OUTFL	276.76	274.55	261.5075	#VALUE!
	276.76	274.55	263.5266667	11.02333333		4N-2E	OUTFL	273.97	272.17	262.1825	9.9875
	273.97	272.17	262.2466667	9.923333333		4N-1.75E	I 1	272.16	270.91	261.5241667	9.385833333
	272.16	270.91	261.58	9.33		4N-1.25E		270.54	269.73	259.8108333	9.919166667
	270.54	269.73	259.7333333	9.996666667		4N-1E	OUTFL	271.19	266.44	256.6681818	8.393333333
	271.19	268.04	259.35	8.69		4N-1W	MESA	275.58	268.04	259.6466667	18.19727273
	275.58	273.88	255.43	18.45		4N-0	OUTFL	268.54	273.88	255.6827273	9.771818182
	268.06	266.86	256.35875	10.50125		3.62N-2E	Outfall	272.59	271.02	261.5716667	9.448333333
	272.59	271.02	261.57125	9.44875		3.5N-1.75E	I 1	273.11	269.32	261.1481818	8.171818182
	273.11	269.32	261.3371429	7.982857143		3N-5E	R	273.85	271.44	259.0890909	12.35090909
	273.85	271.44	260.6657143	10.77428571		3N-4E	R	271.44	268.38	259.9733333	8.406666667
	271.44	268.38	261.6988889	6.681111111		3N-3E	OUTFL	275.02	272.03	260.6527273	11.37727273
	275.02	272.03	261.70375	10.32625		3N-2E	I 1	273.94	271.36		
	273.31	271.28	262.6622222	8.617777778		3N-1.75E	OUTFL	270.9	270.29	261.2981818	8.991818182
	270.9	270.29	261.1622222	9.127777778		3N-.25W	OUTFL	265.42	264.39	254.3072727	10.08272727
	265.42	264.39	254.2222222	10.16777778		3N-1W	MESA	276.84	271.14	259.8063636	21.9375
	276.84	276.15	254.50375	21.64625		2.75N-2.25E	D PMP	272.62	271.52	262.2436364	9.276363636
	272.86	271.44	262.37	9.07		2.75N-1E	OUTFL	269.11	269.57		8.920833333
	269.11	267.17	258.0833333	9.086666667		2.5N-2.5E	D PMP	272.59		259.9825	8.6725
	272.59	270.63	262.58	8.05							
						2.5N-2E					
									271.5		
						2.5N-1.75E	A PMP	269.36	269.43	265.5736364	5.669166667
	269.35	269.43	264.13	5.3		2.18N-1.5W	MESA	270.91	262.99	263.7608333	9.188333333
	270.91	262.69	255.5355556	7.154444444		2.25N-2.37E	D PMP	272.91	270.39	253.8016667	9.227272727
	272.91	270.39	262.0075	8.3825		2.25N-2E	A PMP	273.99	270.92	261.1627273	4.763
	273.99	270.92	266.59	4.33		2.25N-1.75E	A PMP	274.02	272.16	266.157	7.071818182
	274.02	272.16	265.6577778	6.502222222		2N-5E	R	272.67	267.94	265.0881818	11.676
	272.67	269.05	258.94	10.11		2N-2E	A PMP	271.07	270.21	260.2081818	4.877272727
	271.18	270.41	265.2325	5.1775		2N-1E	BLY	272.17	269.76	265.3327273	10.66909091
	272.09	268.81	259.2028571	9.607142857		2N- 25E	OUTFL	267.59	265.5	259.0909091	9.2925
	267.59	265.5	256.13	9.37		2N-1.25W		263.3	260.63	256.2075	9.685454545
	263.22	260.75	251.84125	8.90875		1.75N-1.25W	OUTFL	263.44	261.7	250.9445455	10.365
	263.65	261.74	253.135	8.605		1.75N-1.75W		264.11	270.22	251.335	10.34818182
	264.11	261.43	252.2033333	9.226666667		1.5N-1.25W		264.01	261.41	258.84	10.53416667
	264.01	261.41	251.8266667	9.583333333		1.5N-2W		261.32	260.68	250.8758333	10.00727273
	261.32	260.68	251.74	8.94		1.5N-2.25W	OUTFL	264.6	261.95	250.6727273	11.68545455
	264.6	261.95	251.455	10.495		1.25N-1.5W	OUTFL	262	260.45	250.2645455	9.276363636
	261.82	260.73	252.82875	7.90125		1N-5E	OUTFL	271.53	268.73	251.1736364	13.98166667
	271.53	268.73	255.58375	13.14625		1N-4E	OUTFL	266.52	266.1	254.7483333	11.235
	266.12	265.9	255.8233333	10.07666667		1N-3E	BLY	267.49	266.62	254.865	11.05583333
	267.49	266.62	257.63	8.99		1N-2.12E	BLY	270.74	270.7	255.5641667	14.01666667
	270.74	270.7	257.2014286	13.49857143		1N-1E	BLY	266.65	266.81	256.6833333	9.8325
	266.56	266.82	258.8233333	7.996666667		1N-0	OUTFL	264.19	264.48	256.9775	9.662727273
	264.79	264.48	256.00375	8.47625		1N-.75W	OUTFL	261.87	261.01	254.8172727	8.93
	261.87	261.01	252.56	8.45		1N-2W		259.68	258.34	252.08	8.84
	259.68	258.34	250.6577778	7.682222222		1N-2.25W	OUTFL	257.8	257.52	249.5	8.772727273
	257.8	257.52	249.9185714	7.601428571		0.5N-2.37W	OUTFL	258.52	256.72	248.7472727	9.434
	258.52	256.72	248.395	8.325		0.12N-5E	OUTFL	269.45	267.07	247.286	14.48
	269.45	267.07	253.42	13.65		0-4.12E	OUTFL	267.92	266.31	252.59	14.17181818
	268	266.55	253.3155556	13.23444444		0-3E	OUTFL	263.76	262.77	252.1381818	9.315
	263.76	262.77	254.1566667	8.613333333		0-2E	BLY	267.84	265.18	253.455	11.60818182

2000	Pipe Elevation	Ground Elevation	Average Water Elevation	Average Depth to Water Table	2007	Well Location	Drainage Area	Pipe Elevation	Average Ground Elevation	Water Elevation	Average Depth to Water Table
	267.84	265.18	253.4288889	11.75111111		0-1E	BLY	261.58	261.56	253.5718182	7.4675
	261.7	261.42	253.33375	8.08625		0-0	OUTFL	262.58	261.95	254.0925	7.96
	262.37	261.83	254.4385714	7.391428571		0-1W	OUTFL	261.33	259.66	253.99	9.200833333
	261.33	259.66	251.09	8.57		0-2W	OUTFL	258.18	256.12	250.4591667	8.12
	258.18	256.12	247.86875	8.25125			OUTFL	256.48		248	10.35583333
	256.48	255.13	245.8644444	9.265555556					255.13	244.7741667	
						0.5S-3W	OUTF	257.49	255	243.087	11.913
	257.35	255.03	243.8625	11.1675		0.5S-3.18W	MESA 2	255.65	254.34	243.98	10.36
	255.8	254.45	244.315	10.135		1S-4E	OUTFL	268.94	266.98	250.29	16.69
	268.94	266.98	251.8855556	15.09444444		1S-3E	OUTFL	263.55	260.73	249.5841667	11.14583333
	263.55	260.73	249.9155556	10.81444444		1S-2E	OUTFL	261.57	260.54	249.4058333	11.13416667
	260.44	259.85	249.3685714	10.48142857		1S-1E	OUTFL	261.42	259.24		#VALUE!
	261.85	258.57	250.0614286	8.508571429		1S-.25W	OUTFL	258.55	258.53		#VALUE!
	258.55	258.53	251.565	6.965		1S-1W	OUTFL	259.49	258.92	250.3791667	8.540833333
	259.49	258.92	250.9285714	7.991428571		1S-2W	OUTFL	257.47	254.38	245.74	8.64
	257.19	254.38	246.28875	8.09125		1S-3W	OUTFL	255.47	253.89	243.09	10.8
	255.47	253.89	243.97	9.92		1S-3.37W	MESA 2	253.86	252.6	241.8925	10.7075
	253.86	252.6	242.76	9.84		1.25S-4W	MESA 2	253.05	252.01	241.1408333	10.86916667
	253.05	252.01	241.9675	10.0425		1.5S-4.5W		254.26	251.06	239.2633333	11.79666667
	254.26	251.06	240.47625	10.58375		1.5S-4.75W	OUTFL	252.64	251.04	239.4009091	11.63909091
	252.64	251.04	240.1688889	10.87111111		2S-2.75E	OUTFL	261.18	257.83	247.5916667	10.23833333
	261.59	257.83	247.52625	10.30375		2S-3.75E	OUTFL	265.57	262.95	248.1808333	14.76916667
	265.35	262.89	248.28	14.61		2S-2E	OUTFL	258.15	257.56	247.215	10.345
	258.15	257.56	247.2822222	10.27777778		2S-1E	OUTFL	258.04	255.78	245.8916667	9.888333333
	258.04	255.78	246.5633333	9.216666667		2S-0	OUTFL	256.57	255.36	248.5136364	6.846363636
	256.3	255.56	249.4471429	6.112857143		2S-1W	OUTFL	256.26	254.48		
	256.21	254.3	247.68625	6.61375		2S-2W	OUTFL	254.78	253.47	245.4236364	8.046363636
	255.03	253.74	246.9777778	6.762222222		2S-3W	OUTFL	252.16	252.1	243.38	8.72
	252.16	252.1	243.33375	8.76625		2S-4W	OUTFL	245.73	251.94		#VALUE!
	252.33	251.88	242.0455556	9.834444444		2S-4.5W	OUTFL	253.87	251.25	238.7366667	12.51333333
	253.87	251.25	239.40875	11.84125		2S-5.12W	OUTFL	250.86	249.04	237.039	12.001
	250.86	249.04	237.2188889	11.82111111		2.5S-5.25W	MESA 3	252.67	248.68		#VALUE!
	252.67	248.68	237.5722222	11.10777778		2.75S-3.5E	OUTFL	260.32	261.84	249.9941667	11.84583333
	260.32	258.18	246.7077778	11.47222222							
						3S-3E	OUTFL	259.14	257.14	258.347	11.62545455
	259.33	257.28	246.0611111	11.21888889		3S-2E	OUTFL	258.07	255.6	245.5145455	10.82
	257.98	255.59	245.00375	10.58625		3S-1E	OUTFL	256.81	254.64	244.78	12.0275
	256.81	254.64	243.6325	11.0075		3S-0	OUTFL	253.43	252.04	242.6125	7.379090909
	253.63	252.19	245.0344444	7.155555556		3S-1W	OUTFL	254.56	252.57	244.6609091	8.27
	254.56	252.57	245.1971429	7.372857143		3S-2W	OUTFL	253.78	250.84	244.3	8.683636364
	253.78	250.84	242.215	8.625		3S-3W	OUTFL	252.36	249.54	242.1563636	8.717272727
	252.36	249.54	240.76625	8.77375		3S-4W	OUTFL	252.11	249.83	240.8227273	9.65
	252.11	249.83	240.4111111	9.418888889		3S-5.25W	OUTFL	251.53	248	240.18	10.21166667
	251.53	248	237.48625	10.51375		3S-5.5W	MESA 3	251.64		237.7883333	8.847272727
	249.57	246.8	238.7255556	8.074444444							
									247.89	239.0427273	
						3.5S-5.25W		248.88	247.14	238.1627273	8.977272727
	249.04	247.15	238.19625	8.95375		3.5S-5.5W		246.91	246.56	238.3216667	8.238333333
	246.91	246.56	238.4666667	8.093333333		3.62S-4.75W	OUTFL	251.28	247.82	237.0925	10.7275
	251.28	247.82	236.67375	11.14625		3.75S-5.5W	MESA 3	247.38	246.61	238.2675	8.3425
	247.38	246.61	238.34625	8.26375					261.14	246.1041667	15.03583333
						4S-4E	R	265.79	259.04	245.5016667	13.53833333
	265.79	261.14	248.7766667	12.36333333		4S-3E	OUTFL	260.52	258.44	241.9291667	16.51083333

2000	Pipe Elevation	Ground Elevation	Average Water Elevation	Average Depth to Water Table	2007	Well Location	Drainage Area	Pipe Elevation	Average Ground Elevation	Water Elevation	Average Depth to Water Table
	260.52	259.04	247.5144444	11.52555556		4S-2E	OUTFL	260.45	254.05	239.7666667	14.28333333
	259.93	257.26	242.44125	14.81875		4S-1E	OUTFL	259.23	251.92	240.0025	11.9175
	259.23	254.05	240.2355556	13.81444444		4S-0	OUTFL	253.08	251.47	240.354	11.116
	252.95	251.92	240.7344444	11.18555556		4S-.5W	OUTFL	253.41	251.33		#VALUE!
	253.41	251.47	240.9455556	10.52444444		4S-.75W		253.53	249.2	236.1454545	13.05454545
	253.12	251.33	240.15625	11.17375		4S-2W	OUTFL	250.85	249.68	237.8491667	11.83083333
	250.85	249.2	236.3144444	12.88555556		4S-3W	OUTFL	250.85	247.84	238.706	9.134
	250.85	249.68	238.1477778	11.53222222		4S-4W		247.76	248.16	237.3081818	10.85181818
	247.9	247.6	238.4188889	9.181111111		4S-4.5W	OUTFL	248.53	246.02	237.7258333	8.294166667
	248.53	248.16	237.14125	11.01875		4S-5.25W		249.29	246.31	237.9758333	8.334166667
	249.29	246.02	237.1122222	8.907777778		4S-5.5W	OUTFL	248.86			#VALUE!
	248.86	246.31	237.8814286	8.428571429		4S-5.87W	OUTFL	253.03			
	253.06	246.43	238.38	8.05							
						4.5S-5.5W		249.47	245.81	239.3291667	7.526363636
	249.47	246.08	237.9688889	8.111111111							
						4.75S-4.25W		249.14	246.08	238.5536364	10.33333333
	249.14	246.78	236.1488889	10.63111111							
						5S-3E	R	258.38	246.78	236.4466667	14.81454545
	257.68	256.65	244.35125	12.29875		5S-2.25E	i 2	259.59	256.75	241.9354545	15.227
	259.59	257.68	243.60125	14.07875		5S-1E	OUTFL	255.81	257.68	242.453	15.81181818
	255.81	253.72	238.25	15.47		5S-0	OUTFL	253.72	253.72	237.9081818	15.14636364
	254.11	251.27	236.4066667	14.86333333		5S-.75W	OUTFL	248.95	251.27	236.1236364	12.92416667
	248.95	248.5	235.625	12.875		5S-2W	OUTFL	245.35	248.5	235.5758333	#VALUE!
	245.35	245.45	233.5544444	11.89555556		5S-2.75W	OUTFL	243.86	245.45		11.07727273
	243.86	242.52	231.55	10.97		5S-3.75W	OUTFL	249.43	242.52	231.4427273	10.4575
	249.69	247.67	236.9966667	10.67333333							
						5S-4.75W	OUTFL	246.64	247.55	237.0925	9.605
	246.64	244.38	234.71	9.67		5S-5.5W	OUTFL	245.46	244.38	234.775	7.453
	245.46	243.81	235.9111111	7.898888889		5S-6.18W	OUTFL	246.41	243.81	236.357	7.846363636
	246.48	244.45	236.34375	8.10625		5.5S-.5W		248.06	243.91	236.0636364	12.23090909
	248.06	247.27	235.8477778	11.42222222		5.5S-1.25W	OUTFL	247.32	247.27	235.0390909	12.46545455
	247.32	245.4	233.49625	11.90375		5.5S-4.25W		249.02	245.4	232.9345455	#VALUE!
	248.73	246.38	238.0733333	8.306666667							
						5.5S-6.37W		246.66	246.17	235.0390909	7.590909091
	246.66	242.63	235.3711111	7.258888889		5.75S-2W		243.63	242.63	230.5991667	11.73083333
	243.63	242.33	230.7166667	11.61333333		6S-3E	R	257.88	242.33	239.2836364	16.68636364
	258.09	256.03	240.15375	15.87625		6S-2E	R	256.02	255.97	240.135	14.285
	256.02	254.42	240.9288889	13.49111111		6S-1.12E	i 2	256.31	254.42	240.0475	13.6825
	256.31	253.73	240.4388889	13.29111111		6S-2.75W	OUTFL	243.98	253.73	228.3963636	13.57363636
	243.98	241.97	228.38	13.59		6S-4W	OUTFL	244.95	241.97	234.1791667	10.16083333
	244.86	244.37	233.5125	10.8575		6S-4.5W	OUTFL	246.86	244.34	235.392	#VALUE!
	246.86	243.84	233.14	10.7		6S-5.5W	OUTFL	246.07	243.84	234.0718182	8.448181818
	246.07	242.52	233.3677778	9.152222222		6S-6.25W	OUTFL	242.64	242.52		6.405
	242.64	240.09	234.1766667	5.913333333						233.685	
						6.87S-1.87E	R	253.25	240.09	239.0918182	13.99818182
	253.67	253.18	241.23875	11.94125		7S-1E	R	254.68	253.09	239.9583333	12.66166667
	254.58	252.64	241.28	11.36		7S-0	OUTFL	251.69	252.62	237.1966667	12.48333333
	250.69	250.29	238.59375	11.69625		7S-1W	OUTFL	247.1	249.68	233.9591667	11.60083333

2000	Pipe Elevation	Ground Elevation	Average Water Elevation	Average Depth to Water Table	2007	Well Location	Drainage Area	Pipe Elevation	Average Ground Elevation	Water Elevation	Average Depth to Water Table
	247.1	245.56	234.6522222	10.90777778		7S-2W	OUTFL	241.33	245.56	#VALUE!	#VALUE!
	241.33	241.77	231.1288889	10.64111111		7S-3W	OUTFL	241.62	241.77	228.9308333	11.94916667
	241.62	240.88	229.4588889	11.42111111		7S-4W	OUTFL	242.84	240.88	#VALUE!	#VALUE!
	242.84	241.82	231.2266667	10.59333333		7S-5W		243.43	241.82	233.5166667	8.073333333
	243.43	241.59	233.1042857	8.485714286		7S-5.75W	OUTFL	244.57	241.59	233.3933333	8.466666667
	244.57	241.86	233.17	8.69		7S-6.5W	OUTFL	244.09	241.86	231.675	9.345
	244.09	241.02	231.0725	9.9475							
						7.75S-0	OUTFL	252.5	241.02	237.67375	10.51625
	252.5	248.19	239.0211111	9.168888889		8S-1E	R	253.78	248.19	#VALUE!	#VALUE!
	253.31	250.4	238.6425	11.7575							
						8S-.25W		247.38	250.43	236.6227273	8.237272727
	246.52	244.82	238.13	6.69		8S-.5W		245.92	244.86	236.0863636	7.483636364
	245.28	243.91	237.3057143	6.604285714		8S-1W	OUTFL	246.95	243.57	#VALUE!	#VALUE!
	246.95	243.3	236.4244444	6.875555556		8S-2W	OUTFL	244.99	243.3	232.853	9.407
	245.19	242.32	233.80125	8.51875		8S-3W	OUTFL	239.43	242.26	228.165	10.355
	239.43	238.52	228.8233333	9.696666667		8S-5W	OUTFL	241.38	238.52	227.2716667	12.11833333
	241.01	239.2	228.2733333	10.92666667		8S-5.5W	OUTFL	239.17	239.39	231.1811111	7.168888889
	239.17	238.35	231.56375	6.78625		8S-6.5W	OUTFL	242.39	238.35	228.7425	9.9275
	242.17	238.59	228.8675	9.7225		8.25S-4.25W		240.43	238.67	226.6288889	10.71111111
	240.43	237.41	226.405	11.005		9S-0	OUTFL	250.44	237.34	235.8741667	13.63583333
	250.44	249.15	236.5766667	12.57333333		9S-1.25W	OUTFL	243.23	249.51	232.7708333	8.989166667
	243.23	241.76	233.5122222	8.247777778		9S-2W	OUTFL	244.99	241.76	232.6366667	8.683333333
	244.77	241.47	232.83875	8.63125		9S-3W	OUTFL	239.98	241.32	228.9258333	8.884166667
	239.98	237.81	229.37875	8.43125		9S-4W	OUTFL	236.84	237.81	224.93125	10.30875
	236.84	235.24	224.6025	10.6375		9S-5W	OUTFL	236.66	235.24	226.1109091	9.079090909
	236.66	235.19	226.90625	8.28375		9S-5.75W	OUTFL	237.68	235.19	227.58	7.92
	237.68	235.5	227.7075	7.7925		9S-6.5W	OUTFL	238.18	235.5	227.2208333	7.789166667
	238.18	235.01	228.1444444	6.865555556		10S-0	R	251.37	235.01	233.0654545	16.08454545
	251.37	249.15	233.35625	15.79375		10S-1W	OUTFL	249.71	249.15	#VALUE!	#VALUE!
	249.71	248.09	232.16	15.93		10S-2W	OUTFL	242.5	248.09	230.4745455	9.645454545
	242.5	240.12	230.98625	9.13375		10S-3W	OUTFL	240.33	240.12	228.6733333	8.586666667
	240.33	237.26	229.1788889	8.081111111		10S-3.87W	OUTFL	238.57	237.26	228.20375	6.95625
	237.45	235.16	228.35875	6.80125		10S-5W	OUTFL	236.42	235.16	#VALUE!	#VALUE!
	236.42	233.54	224.3622222	9.177777778		10S-6.75W	OUTFL	235.76	233.54	#VALUE!	#VALUE!
	236.85	234.71	226.2466667	8.463333333		10S-5.75W	OUTFL	235.76	233.54	#VALUE!	#VALUE!
	235.76	233.22	225.6355556	7.584444444		10.75S-4W	OUTFL	236.85	233.22	226.0854545	8.624545455
	236.58	233.4	226.8177778	6.582222222		11S-1W	OUTFL	236.58	234.71	226.6072727	6.792727273
	244.48	243.37	229.5355556	13.83444444		11S-2W	OUTFL	244.82	233.4	#VALUE!	#VALUE!
	238.8	237.75	229.5471429	8.202857143		11S-3W	OUTFL	238.8	243.45	228.46	9.29
	237.96	236.02	229.3955556	6.624444444		11S-5W	OUTFL	237.96	237.75	229.5227273	6.497272727
	235.02	231.19	224.1877778	7.002222222		11S-5.75W	OUTFL	234.89	236.02	#VALUE!	#VALUE!
	234.78	232.62	225.465	7.155		11S-6.87W	OUTFL	234.78	232.59	225.894	6.726
	233.32	231.48	224.6622222	6.817777778		11.75S-6.75W	E PMP	233.32	232.62	223.5736364	7.906363636
	231.3	231	223.1233333	7.876666667		12S-1W	E PMP	231.3	231.48	223.3663636	7.633636364
	238.42	237.96	228.5177778	9.442222222		12S-2W	OUTFL	239.28	231	228.159	10.351
	237.63	237.11	227.665	9.445		12S-3W	OUTFL	237.63	238.51	227.3491667	9.760833333
	242.36	240.04	227.3033333	12.73666667		12S-4W	OUTFL	242.36	237.11	226.951	13.089
	237.71	234.84	225.295	9.545		12S-5W	OUTFL	237.71	240.04	224.2745455	10.56545455
	236.8	233.16	224.21	8.95		12S-6W	OUTFL	236.8	234.84	222.42	10.74
	233.05	232.55	221.55	11		13S-2W	OUTFL	233.04	233.16	220.7541667	11.61583333

2000	Pipe Elevation	Ground Elevation	Average Water Elevation	Average Depth to Water Table	2007	Well Location	Drainage Area	Pipe Elevation	Average Ground Elevation	Water Elevation	Average Depth to Water Table
	241.48	240.61	230.4022222	10.20777778		13.12S-2.87W	OUTFL	241.14	232.37	#VALUE!	#VALUE!
	243.53	240.58	227.4666667	13.11333333		13S-4.25W	R 2	243.53	240.42	226.8416667	13.73833333
	234.63	236.28	227.33625	8.94375		13S-5W	R 2	234.38	240.58	227.2633333	7.176666667
	235.57	231.38	225.1266667	6.253333333		13S-6W	OUTFL	235.57	234.44	#VALUE!	#VALUE!
	232.7	231.6	222.2666667	9.333333333		13S-6.5W	OUTFL	232.7	231.38	222.283	9.317
	230.69	228.55	220.59125	7.95875		13S-7.12W	OUTFL	230.69	231.6	#VALUE!	#VALUE!
	233.57	232.23	220.2233333	12.00666667		14.25S-6.5W	OUTFL	233.57	228.55	220.8525	11.3775
	231.67	228.46	221.2711111	7.188888889		14.25S-7.18W	OUTFL-2	231.67	232.23	218.9622222	7.188333333
	227.81	226.45	220.2455556	6.204444444		15S-6W	OUTFL	227.12	228.1		
	229.73	228.93	222.5811111	6.348888889						#VALUE!	#VALUE!
						16S-6W	R 3	229.73	226.56	221.5608333	6.949090909
	228.1	226.26	221.82625	4.43375		17S-5W	OUTFL 2	227.1	226.26	221.9809091	#VALUE!
						17S-5.75W	OUTFL-2	228.1	228.93	221.5608333	4.699166667
	227.53	226.11	220.2922222	5.817777778		18S-5W	OUTFL 2	227.1	226.26		#VALUE!
						6.5N-3.56E	OUTFL	282.44	279.57	268.040833	9.639166667
	282.44	279.57	269.54	10.03							

2008	Well Location	Drainage Area	Pipe Elevation	Average Ground Elevation	Water Elevation	Average Depth to Water Table	2009	Well Location	Drainage Area	Pipe Elevation	Average Ground Elevation	Water Elevation	Average Depth to Water Table
	8N-7E	R	289.08	287.01	267.54	19.47		8N-7E	R	289.08	287.01	268.2166667	18.79333333
	7.5N-5.62E		285.26	287.01	279.2145455	4.255454545		7.5N-5.62E		285.26	283.47	279.4566667	4.013333333
	7.37N-5.12E		285.42	284.1	278.6218182	4.488181818		7.37N-5.12E		285.42	283.11	278.1841667	4.925833333
	7.37N-4.87E	J PMP	284.67	283.11	277.4041667	5.725833333		7.37N-4.87E	J PMP	284.67	283.13	277.285	5.845
	7.37N-4.75E	J PMP	288.65	283.13	279.1436364	3.166363636		7.37N-4.75E	J PMP	288.65	282.31	279.7163636	2.593636364
	7.37N-4.25E	J PMP	284.76	282.31	276.9575	4.9425		7.37N-4.25E	J PMP	284.76	281.9	276.5654545	5.334545455
	7.25N-4.31E	J PMP	284.73	281.9	276.0525	5.9675		7.25N-4.31E	J PMP	284.73	282.02	275.9754545	6.044545455
	7.18N-4.06E	J PMP	284.07	282.02	275.1754545	5.694545455		7.18N-4.06E	J PMP	284.07	280.87	274.9025	5.9675
	7.12N-4E	J PMP	282.69	280.87	274.5572727	5.642727273		7.12N-4E	J PMP	282.69	280.2	273.7458333	6.454166667
	7N-7E	R	285.5	280.2	267.2041667	16.08583333		7N-7E	R	285.5	283.29	267.5627273	15.72727273
	7N-6.25E	R	286.2	283.29	273.0808333	10.41916667		7N-6.25E	R	286.2	283.5	273.3427273	10.15727273
	7N-4.62E	J PMP	285.1	283.5	275.5375	6.9625		7N-4.62E	J PMP	285.1	282.5	275.1536364	7.346363636
	6.87N-3.93E	J PMP	281.8	282.5	273.6391667	6.570833333		6.87N-3.93E	J PMP	281.8	280.21	273.6272727	6.582727273
	6.87N-3.81E	J PMP	280.9	280.21	274.5036364	4.646363636		6.87N-3.81E	J PMP	280.9	279.15	274.765	4.385
	6.75N-3.43E		281.87	279.15	270.0775	11.1025		6.75N-3.43E		281.87	281.18	269.9525	11.2275
	6.56N-3E	Outfall	278.86	277.51	270.5772727	7.102727273		6.56N-3E	Outfall	278.86	277.68	269.262	8.418
	6.62N-3.75E	OL	279.73	277.33	272.0483333	7.211666667		6.62N-3.75E	OL	279.73	279.26	271.9275	7.3325
	6.62N-3E		280.46	279.26	270.8627273	6.647272727		6.62N-3E		280.4	277.51	268.7018182	8.808181818
	6.68N-3E		279.64	281.18	270.3655556	6.964444444		6.68N-3E		279.03	277.33	268.6583333	8.671666667
	6.5N-3E		279.06	277.16	270.2563636	6.903636364		6.5N-3E		279.06	277.16	269.94	7.22
	6.5N-2.81E		279.34	275.74	269.9527273	5.787272727		6.5N-2.81E		279.34	275.74	269.5472727	6.192727273
	6.37N-3E		279	277.38	269.76	7.62		6.37N-3E		279	277.38	269.2090909	8.170909091
	6.25N-6E	R	286.56	283.79	268.8708333	14.91916667		6.25N-6E	R	286.56	283.79	269.2645455	14.52545455
	6.25N-4E	OL	284.52		271.4790909	9.140909091		6.25N-4E	OL	285.02	280.62	271.8266667	8.793333333
				280.62									
	6.25N-3E		280.07	277.68	269.2041667	8.475833333		6.25N-3E		280.07	277.68	268.89	8.79
	6.25N-2.81E		279	276.43	268.895	7.535		6.25N-2.81E		279	276.43	268.7154545	7.714545455
	6N-4.75E	OL	282.51	281.77	270.493	11.277		6N-4.75E	OL	282.51	281.77	270.0172727	11.75272727
	6N-4E	OL	281.23	279.95	269.559	10.391		6N-4E	OL	281.23	279.95	269.5458333	10.40416667
	6N-3E	OUTFL	278.7	276.85	269.4358333	7.414166667		6N-3E	OUTFL	278.7	276.85	269.368	7.482
	6N-2E	OUTFL	283.16	275.38	266.778	8.602		6N-2E	OUTFL	283.16	275.38	266.1418182	9.238181818
	5.93N-2E		276.22	275.69	266.7854545	8.904545455		5.93N-2E		276.22	275.69	265.9954545	9.694545455
	5.87N-2E		276.26	275.29	267.285	8.005		5.87N-2E		276.26	275.29	266.0427273	9.247272727
	5.75N-2E		276.42	274.06	267.1983333	6.861666667		5.75N-2E		276.42	274.06	266.1718182	7.888181818
	5.75N-1.75E	OUTFL	275.74	273.16	264.7800909	8.379909091		5.75N-1.75E	OUTFL	275.74	273.16	264.4558333	8.704166667
	5.75N-1.5E		273.72	272.57	263.3725	9.1975		5.75N-1.5E		273.72	272.57	262.7827273	9.787272727
	5.75N-1E	MESA	281.22	278.8	262.1018182	16.69818182		5.75N-1E	MESA	281.22	278.8	261.4183333	17.38166667
	5.5N-1.75E		275.29	272.5	264.807	7.693		5.5N-1.75E		275.29	272.5	264.3418182	8.158181818
	5.5N-1.25E	OUTFL	272.61	271.52	262.5872727	8.932727273		5.5N-1.25E	OUTFL	272.61	271.52	261.8191667	9.700833333
	5.37N-0	MESA	269.25	267.2	258.2158333	8.984166667		5.37N-0	MESA	269.25	267.2	257.7066667	9.493333333
	5N-4.87E	OL	279.73	278.13	263.5816667	14.54833333		5N-4.87E	OL	279.73	278.13	263.2108333	14.91916667
	5N-4E	OUTFL	275.13	274.54	264.538	10.002		5N-4E	OUTFL	276.73	274.54	265.5366667	9.003333333
	5N-3E	OUTFL	277.79	275.09	266.1025	8.9875		5N-3E	OUTFL	277.79	275.09	265.491	9.599
	5N-2E		276.6	274.19	265.7266667	8.463333333		5N-2E		276.6	274.19	265.5990909	8.590909091
	5N-1.75E	OUTFL	274.64	272.8	263.3181818	9.481818182		5N-1.75E	OUTFL	274.64	272.8	262.7433333	10.05666667
	5N-1.25E	OUTFL	272.78	270.25	261.7083333	8.541666667		5N-1.25E	OUTFL	272.78	270.25	260.9854545	9.264545455
	5N-1E		270.79	268.88	260.8772727	8.002727273		5N-1E		270.79	268.88	260.2463636	8.633636364
	5N-0		268.37	267.49	258.0427273	9.447272727		5N-0		268.57	267.49	257.9154545	9.574545455
	5N-.18W	MESA	268.73	267.01	257.4841667	9.525833333		5N-.18W	MESA	268.73	267.01	257.503	9.507
	4.5N-1.75E		275.07	272.71		#VALUE!		4.5N-1.75E		275.07	272.71	262.5754545	10.13454545
	4.5N-1.25E		270.97	269.52	260.5958333	8.924166667		4.5N-1.25E		270.97	269.52	260.1766667	9.343333333
	4.37N-.5W	MESA	270.15	267.6	256.9436364	10.65636364		4.37N-.5W	MESA	270.15	267.6	256.7358333	10.86416667

2008	Well Location	Drainage Area	Pipe Elevation	Average Ground Elevation	Water Elevation	Average Depth to Water Table	2009	Well Location	Drainage Area	Pipe Elevation	Average Ground Elevation	Water Elevation	Average Depth to Water Table
	4.37N-.87W	MESA	272.11	267.99	255.7045455	12.28545455		4.37N-.87W	MESA	272.11	267.99	255.8590909	12.13090909
	4N-4.87E	R	275.41	274.23	260.82	13.41		4N-4.87E	R	275.41	274.23	260.2291667	14.00083333
	4N-4E	OUTFL	279.28	276.15	261.4390909	14.71090909		4N-4E	OUTFL	279.28	276.15	261.065	15.085
	4N-3E	OUTFL	276.76	274.55	262.9608333	11.58916667		4N-3E	OUTFL	276.76	274.55	262.2825	12.2675
	4N-2E	OUTFL	273.97	272.17	262.3045455	9.865454545		4N-2E	OUTFL	273.97	272.17	261.81	10.36
	4N-1.75E	i 1	272.16	270.91	261.6966667	9.213333333		4N-1.75E	i 1	272.16	270.91	260.7675	10.1425
	4N-1.25E		270.54	269.73	259.7836364	9.946363636		4N-1.25E		270.54	269.73	259.4590909	10.27090909
	4N-1E	OUTFL	271.19	266.44	259.7791667	8.260833333		4N-1E	OUTFL	271.19	268.04	259.1336364	8.906363636
	4N-1W	MESA	275.58	268.04	255.7590909	18.12090909		4N-1W	MESA	275.58	273.88	255.6183333	18.26166667
	4N-0	OUTFL	268.7	273.88	257.295	9.145		4N-0	OUTFL	268.7	266.44	256.6754545	9.764545455
	3.62N-2E	Outfall	272.59	271.02	261.8166667	9.203333333		3.62N-2E	Outfall	272.59	271.02	261.4363636	9.583636364
	3.5N-1.75E	i 1	273.11	269.32	261.346	7.974		3.5N-1.75E	i 1	273.11	269.32	260.6627273	8.657272727
	3N-5E	R	273.85	271.44	259.0733333	12.36666667		3N-5E	R	273.85	271.44	258.79	12.65
	3N-4E	R	271.44	268.38	259.7918182	8.588181818		3N-4E	R	271.44	268.38	259.6388889	8.741111111
	3N-3E	OUTFL	275.02	272.03	260.8133333	11.21666667		3N-3E	OUTFL	275.02	272.03	260.1309091	11.89909091
	3N-2E	i 1	273.94	271.36	262.8045455	8.555454545		3N-2E	i 1	273.94	271.36	261.915	9.445
	3N-1.75E	OUTFL	270.9	270.29	261.365	8.925		3N-1.75E	OUTFL	270.9	270.29	260.613	9.677
	3N-.25W	OUTFL	265.42	264.39	254.362	10.028		3N-.25W	OUTFL	265.42	264.39	253.8963636	10.49363636
	3N-1W	MESA	276.84	271.14	254.8127273	21.33727273		3N-1W	MESA	276.84	276.15	254.495	21.655
	2.75N-2.25E	D PMP	272.62	271.52	262.1375	9.3825		2.75N-2.25E	D PMP	272.62	271.52	261.5672727	9.952727273
	2.75N-1E	OUTFL	269.31	269.57	258.367	8.673		2.75N-1E	OUTFL	269.37	267.04	257.5972727	9.442727273
	2.5N-2.5E	D PMP	272.59		262.2408333	8.449166667		2.5N-2.5E	D PMP	272.59	270.69	261.4991667	9.190833333
				271.5									
	2.5N-1.75E	A PMP	269.36	269.43	263.7316667	5.698333333		2.5N-1.75E	A PMP	269.36	269.43	263.5308333	5.899166667
	2.18N-1.5W	MESA	270.91	262.99	253.7508333	9.239166667		2.18N-1.5W	MESA	270.91	262.99	253.51	9.48
	2.25N-2.37E	D PMP	272.91	270.39	260.885	9.505		2.25N-2.37E	D PMP	272.91	270.39	260.4108333	9.979166667
	2.25N-2E	A PMP	273.99	270.92	265.78	5.14		2.25N-2E	A PMP	273.99	270.92	265.653	5.267
	2.25N-1.75E	A PMP	274.02	272.16	264.5958333	7.564166667		2.25N-1.75E	A PMP	274.02	272.16	264.06	8.1
	2N-5E	R	272.67	267.94	258.3418182	10.70818182		2N-5E	R	272.67	269.05	256.2772727	12.77272727
	2N-2E	A PMP	271.07	270.21	265.228	4.982		2N-2E	A PMP	271.07	270.21	264.09	6.12
	2N-1E	BLY	272.19	269.76	259.0272727	10.73272727		2N-1E	BLY	272.19	269.76	258.54	11.22
	2N-.25E	OUTFL	267.59	265.5	256.31	9.19		2N-.25E	OUTFL	267.59	265.5	255.1736364	10.32636364
	2N-1.25W		263.64	261.71	250.9936364	10.71636364		2N-1.25W		264.64	261.71	251.2258333	10.48416667
	1.75N-1.25W	OUTFL	263.44	261.7	251.4563636	10.24363636		1.75N-1.25W	OUTFL	263.44	261.7	250.8827273	10.81727273
	1.75N-1.75W		264.11	270.22	251.0658333	10.36416667		1.75N-1.75W		264.11	261.43	250.2936364	11.13636364
	1.5N-1.25W		264.01	261.41	250.9527273	10.45727273		1.5N-1.25W		264.01	261.41	250.9583333	10.45166667
	1.5N-2W		261.32	260.68	250.6618182	10.01818182		1.5N-2W		261.32	260.68	250.6090909	10.07090909
	1.5N-2.25W	OUTFL	264.6	261.95	250.1190909	11.83090909		1.5N-2.25W	OUTFL	264.6	261.95	250.0227273	11.92727273
	1.25N-1.5W	OUTFL	262.07	260.45	251.453	8.997		1.25N-1.5W	OUTFL	262.08	260.45	250.9825	9.4675
	1N-5E	OUTFL	271.53	268.73	254.785	13.945		1N-5E	OUTFL	271.53	268.73	254.3063636	14.42363636
	1N-4E	OUTFL	266.52	266.1		#VALUE!		1N-4E	OUTFL	266.52	266.1	254.1966667	11.90333333
	1N-3E	BLY	267.49	266.62	255.8091667	10.81083333		1N-3E	BLY	267.49	266.62	255.3909091	11.22909091
	1N-2.12E	BLY	270.74	270.7	256.455	14.245		1N-2.12E	BLY	270.74	270.7	256.185	14.515
	1N-1E	BLY	266.65	266.81		#VALUE!		1N-1E	BLY	266.65	266.81	256.5127273	10.29727273
	1N-0	OUTFL	264.19	264.48	255.0175	9.4625		1N-0	OUTFL	264.19	264.48	254.1954545	10.28454545
	1N-.75W	OUTFL	261.87	261.01	252.0783333	8.931666667		1N-.75W	OUTFL	261.87	261.01	251.5954545	9.414545455
	1N-2W		259.68	258.34	249.7861818	8.553818182		1N-2W		259.68	258.34	249.2545455	9.085454545
	1N-2.25W	OUTFL	257.8	257.52	248.6227273	8.897272727		1N-2.25W	OUTFL	257.8	257.52	248.6591667	8.860833333
	0.5N-2.37W	OUTFL	258.52	256.72	247.5918182	9.128181818		0.5N-2.37W	OUTFL	258.52	256.72	246.5566667	10.16333333
	0.12N-5E	OUTFL	269.42	267.19	252.5081818	14.68181818		0.12N-5E	OUTFL	269.41	267.19	252.1358333	15.05416667
	0-4.12E	OUTFL	267.92	266.31	252.241	14.069		0-4.12E	OUTFL	267.92	266.31	252.0241667	14.28583333
	0-3E	OUTFL	263.76	262.77	253.3458333	9.424166667		0-3E	OUTFL	263.76	262.77	253.3191667	9.450833333
	0-2E	BLY	267.84	265.18	253.5172727	11.66272727		0-2E	BLY	267.84	265.18	253.1372727	12.04272727

2008	Well Location	Drainage Area	Pipe Elevation	Average Ground Elevation	Water Elevation	Average Depth to Water Table	2009	Well Location	Drainage Area	Pipe Elevation	Average Ground Elevation	Water Elevation	Average Depth to Water Table
	0-1E	BLY	261.58	261.56	254.0283333	7.531666667		0-1E	BLY	261.54	261.56	253.3133333	8.246666667
	0-0	OUTFL	262.66	261.95	253.9118182	8.038181818		0-0	OUTFL	262.8	261.95	252.83	9.12
	0-1W	OUTFL	261.33	259.66	250.3841667	9.275833333		0-1W	OUTFL	261.33	259.66	250.224	9.436
	0-2W	OUTFL	258.18	256.12	247.2225	8.8975		0-2W	OUTFL	258.18	256.12	247.0009091	9.119090909
	0-2.75W	OUTFL	256.48		245.17	9.96		0-2.75W	OUTFL	256.48	255.13	245.3745455	9.755454545
				255.13									
	0.5S-3W	OUTF	257.54	255	244.8481818	10.15181818		0.5S-3W	OUTF	257.54	255	244.0891667	10.91083333
	0.5S-3.18W	MESA 2	255.65	254.34	244.6658333	9.674166667		0.5S-3.18W	MESA 2	255.65	254.34	243.7072727	10.63272727
	1S-4E	OUTFL	268.94	266.98	250.5616667	16.41833333		1S-4E	OUTFL	268.94	266.98	250.748	16.232
	1S-3E	OUTFL	263.55	260.73	249.2883333	11.44166667		1S-3E	OUTFL	263.55	260.73	249.3741667	11.35583333
	1S-2E	OUTFL	261.57	260.54	249.3427273	11.19727273		1S-2E	OUTFL	261.57	260.54	248.5733333	11.96666667
	1S-1E	OUTFL	261.42	259.24	249.6116667	9.628333333		1S-1E	OUTFL	261.42	259.24	249.2183333	10.02166667
	1S-.25W	OUTFL	258.55	258.53	250.6933333	7.836666667		1S-.25W	OUTFL	258.55	258.53	250.467	8.063
	1S-1W	OUTFL	259.49	258.92	250.301	8.619		1S-1W	OUTFL	259.49	258.92	250.242	8.678
	1S-2W	OUTFL	257.47	254.38	245.75	8.63		1S-2W	OUTFL	257.47	254.38	245.0258333	9.354166667
	1S-3W	OUTFL	255.47	253.89	244.153	9.737		1S-3W	OUTFL	255.47	253.89	243.8136364	10.07636364
	1S-3.37W	MESA 2	253.86	252.6	245.0125	7.5875		1S-3.37W	MESA 2	253.86	252.6	247.6555556	4.944444444
	1.25S-4W	MESA 2	255.5	252	242.152	9.848		1.25S-4W	MESA 2	256.73	252	242.246	9.754
	1.5S-4.5W		254.26	251.06	240.497	10.563		1.5S-4.5W		254.26	251.06	240.555	10.505
	1.5S-4.75W	OUTFL	252.64	251.04	239.89	11.15		1.5S-4.75W	OUTFL	252.64	251.04	239.7366667	11.30333333
	2S-2.75E	OUTFL	261.18	257.83	247.3925	10.4375		2S-2.75E	OUTFL	261.18	257.83	246.7058333	11.12416667
	2S-3.75E	OUTFL	265.57	262.95	248.1581818	14.79181818		2S-3.75E	OUTFL	265.57	262.95	248.1433333	14.80666667
	2S-2E	OUTFL	258.15	257.56	247.1118182	10.44818182		2S-2E	OUTFL	258.15	257.56	246.4863636	11.07363636
	2S-1E	OUTFL	258.04	255.78	245.7818182	9.998181818		2S-1E	OUTFL	258.04	255.78	244.7725	11.0075
	2S-0	OUTFL	256.57	255.36	248.4790909	6.880909091		2S-0	OUTFL	256.57	255.36	247.5566667	7.803333333
	2S-1W	OUTFL	256.26	254.48	247.1527273	7.327272727		2S-1W	OUTFL	256.26	254.48	247.1672727	7.312727273
	2S-2W	OUTFL	254.78	253.47	245.2690909	8.200909091		2S-2W	OUTFL	254.78	253.47	244.3775	9.0925
	2S-3W	OUTFL	252.16	252.1	242.61	9.49		2S-3W	OUTFL	252.16	252.1	241.4509091	10.64909091
	2S-4W	OUTFL	244.91	251.94	231.51	20.43		2S-4W	OUTFL	244.91	251.94	230.9958333	20.94416667
	2S-4.5W	OUTFL	253.87	251.25	239.388	11.862		2S-4.5W	OUTFL	253.87	251.25	239.1658333	12.08416667
	2S-5.12W	OUTFL	250.86	249.04	237.1291667	11.91083333		2S-5.12W	OUTFL	250.86	249.04	236.6866667	12.35333333
	2.5S-5.25W	MESA 3	252.67	248.68	238.051	10.629		2.5S-5.25W	MESA 3	252.67	248.68	237.6227273	11.05727273
	2.75S-3.5E	OUTFL	260.32		246.0763636	12.10363636		2.75S-3.5E	OUTFL	260.32	258.18	245.5436364	12.63636364
				261.68									
	3S-3E	OUTFL	259.14	257.14	244.9625	12.1775		3S-3E	OUTFL	259.14	257.14	244.7763636	12.36363636
	3S-2E	OUTFL	258.07	255.6	244.7363636	10.86363636		3S-2E	OUTFL	258.07	255.6	244.5554545	11.04454545
	3S-1E	OUTFL	256.81	254.64	242.665	11.975		3S-1E	OUTFL	256.81	254.64	242.5036364	12.13636364
	3S-0	OUTFL	253.43	252.04	244.4490909	7.590909091		3S-0	OUTFL	253.43	252.04	243.71	8.33
	3S-1W	OUTFL	254.56	252.57	243.8636364	8.706363636		3S-1W	OUTFL	254.56	252.57	243.86	8.71
	3S-2W	OUTFL	253.78	250.84	242.2391667	8.600833333		3S-2W	OUTFL	253.78	250.84	240.75	10.09
	3S-3W	OUTFL	252.36	249.54	241.1866667	8.353333333		3S-3W	OUTFL	252.36	249.54	240.659	8.881
	3S-4W	OUTFL	252.11	249.83	239.8091667	10.02083333		3S-4W	OUTFL	252.11	249.83	239.331	10.499
	3S-5.25W	OUTFL	251.53	248	237.7833333	10.21666667		3S-5.25W	OUTFL	251.53	248	237.4875	10.5125
	3S-5.5W	MESA 3	251.64		239.0825	8.8075		3S-5.5W	MESA 3	251.64	247.89	238.286	9.604
				247.89									
	3.5S-5.25W		249.12	248.07	237.9108333	10.15916667		3.5S-5.25W		249.23	248.07	236.8631818	11.20681818
	3.5S-5.5W		246.91	246.56	238.1827273	8.377272727		3.5S-5.5W		248.12	246.56	234.8855455	11.67445455
	3.62S-4.75W	OUTFL	251.28	247.82	236.5	11.32		3.62S-4.75W	OUTFL	251.28	247.82	235.967	11.853
	3.75S-5.5W	MESA 3	247.38		238.2081818	8.401818182		3.75S-5.5W	MESA 3	248.6	246.61	237.0422222	9.567777778
				246.61									
	4S-4E	R	265.79	261.14	245.6709091	15.46909091		4S-4E	R	265.79	261.14	246.3708333	14.76916667
	4S-3E	OUTFL	260.52	259.04	245.2390909	13.80909909		4S-3E	OUTFL	260.52	259.04	245.2827273	13.75727273

2008	Well Location	Drainage Area	Pipe Elevation	Average Ground Elevation	Water Elevation	Average Depth to Water Table	2009	Well Location	Drainage Area	Pipe Elevation	Average Ground Elevation	Water Elevation	Average Depth to Water Table
	4S-2E	OUTFL	260.45	258.44	241.4581818	16.98181818		4S-2E	OUTFL	260.45	258.44	241.9109091	16.52909091
	4S-1E	OUTFL	259.23	254.05	239.6081818	14.44181818		4S-1E	OUTFL	259.23	254.05	239.6316667	14.41833333
	4S-0	OUTFL	253.08	251.92	239.6941667	12.22583333		4S-0	OUTFL	253.08	251.92	239.361	12.559
	4S-.5W	OUTFL	253.41	251.47	240.1725	11.2975		4S-.5W	OUTFL	253.41	251.47	239.6475	11.8225
	4S-.75W		253.8	251.76	240.7154545	11.04454545		4S-.75W		254.61	251.76	239.4816667	12.27833333
	4S-2W	OUTFL	250.85	249.2	236.3141667	12.88583333		4S-2W	OUTFL	250.85	249.2	235.7233333	13.47666667
	4S-3W	OUTFL	250.85	249.68	237.933	11.747		4S-3W	OUTFL	250.83	249.68	237.042	12.638
	4S-4W		247.76	247.84	238.5175	9.3225		4S-4W		248.54	247.84	238.768	9.072
	4S-4.5W	OUTFL	248.53	248.16	236.62	11.54		4S-4.5W	OUTFL	248.53	248.16	236.0809091	12.07909091
	4S-5.25W		249.29	246.02	236.8081818	9.211818182		4S-5.25W		249.29	246.02	236.3018182	9.718181818
	4S-5.5W	OUTFL	248.86	246.31	237.2218182	9.088181818		4S-5.5W	OUTFL	248.86	246.31	236.5909091	9.719090909
	4S-5.87W	OUTFL	253.03		237.62	9.04		4S-5.87W	OUTFL	253.03	246.66	237.01	9.65
				245.81									
	4.5S-5.5W		249.47		237.5191667	8.560833333		4.5S-5.5W		249.47	246.08	237.1616667	8.918333333
				246.08									
	4.75S-4.25W		249.14		235.8916667	10.88833333		4.75S-4.25W		249.14	246.78	235.7708333	11.00916667
				246.78									
	5S-3E	R	257.3	256.65	241.6618182	14.98818182		5S-3E	R	257.3	256.65	241.063	15.587
	5S-2.25E	i 2	259.59	257.68	242.8891667	14.79083333		5S-2.25E	i 2	259.59	257.68	242.0775	15.6025
	5S-1E	OUTFL	255.81	253.72	237.8666667	15.85333333		5S-1E	OUTFL	255.81	253.72	237.7263636	15.99363636
	5S-0	OUTFL	253.72	251.27	236.4125	14.8575		5S-0	OUTFL	253.72	251.27	236.0881818	15.18181818
	5S-.75W	OUTFL	248.95	248.5	235.7308333	12.76916667		5S-.75W	OUTFL	248.95	248.5	234.9641667	13.53583333
	5S-2W	OUTFL	245.35	245.45	233.4983333	11.95166667		5S-2W	OUTFL	245.35	245.45	233.3558333	12.09416667
	5S-2.75W	OUTFL	243.86	242.52	231.3827273	11.13727273		5S-2.75W	OUTFL	243.86	242.52	231.3275	11.1925
	5S-3.75W	OUTFL	249.43		236.1244444	11.42555556		5S-3.75W	OUTFL	249.43	247.55	235.416	12.134
				247.55									
	5S-4.75W	OUTFL	246.64	244.38		#VALUE!		5S-4.75W	OUTFL	246.64	244.38	234.8318182	9.548181818
	5S-5.5W	OUTFL	245.46	243.81	235.3154545	8.494545455		5S-5.5W	OUTFL	245.46	243.81	235.082	8.728
	5S-6.18W	OUTFL	246.41	243.91	235.1533333	8.756666667		5S-6.18W	OUTFL	246.41	243.91	235.2681818	8.641818182
	5.5S-.5W		248.06	247.27	235.1527273	12.11727273		5.5S-.5W		248.06	247.27	235.6225	11.6475
	5.5S-1.25W	OUTFL	246.58	245.87	233.2127273	12.65727273		5.5S-1.25W	OUTFL	246.21	245.87	232.427	13.443
	5.5S-4.25W		249.33		237.833	8.417		5.5S-4.25W		249.48	246.25	237.6363636	8.613636364
				246.25									
	5.5S-6.37W		246.66	242.63	234.5188889	8.111111111		5.5S-6.37W		246.66	242.63	234.646	7.984
	5.75S-2W		243.63	242.33	230.665	11.665		5.75S-2W		243.63	242.33	230.5391667	11.79083333
	6S-3E	R	257.88	255.97	239.6454545	16.32454545		6S-3E	R	257.88	255.97	238.9783333	16.99166667
	6S-2E	R	256.02	254.42	240.9372727	13.48272727		6S-2E	R	256.02	254.42	239.846	14.574
	6S-1.12E	i 2	256.31	253.73	240.0808333	13.64916667		6S-1.12E	i 2	256.31	253.73	239.4890909	14.24090909
	6S-2.75W	OUTFL	243.98	241.97	228.4445455	13.52545455		6S-2.75W	OUTFL	243.98	241.97	228.0808333	13.88916667
	6S-4W	OUTFL	244.95	244.34	233.2808333	11.05916667		6S-4W	OUTFL	244.95	244.34	233.5366667	10.80333333
	6S-4.5W	OUTFL	246.86	243.84	233.7	10.14		6S-4.5W	OUTFL	246.86	243.84	233	10.84
	6S-5.5W	OUTFL	246.07	242.52	232.98	9.54		6S-5.5W	OUTFL	246.07	242.52	232.7518182	9.768181818
	6S-6.25W	OUTFL	242.64		232.9763636	7.113636364		6S-6.25W	OUTFL	242.64	240.09	232.5972727	7.492727273
				240.09									
	6.87S-1.87E	R	253.25	253.09	239.5825	13.5075		6.87S-1.87E	R	253.25	253.09	238.485	14.605
	7S-1E	R	254.68	252.62	239.6918182	12.92818182		7S-1E	R	254.68	252.62	239.182	13.438
	7S-0	OUTFL	251.57	249.68	236.8725	12.8075		7S-0	OUTFL	251.57	249.68	236.2509091	13.42909091
	7S-1W	OUTFL	247.1	245.56	233.7672727	11.79272727		7S-1W	OUTFL	247.1	245.56	233.7608333	11.79916667

2008	Well Location	Drainage Area	Pipe Elevation	Average Ground Elevation	Water Elevation	Average Depth to Water Table	2009	Well Location	Drainage Area	Pipe Elevation	Average Ground Elevation	Water Elevation	Average Depth to Water Table
	7S-2W	OUTFL	241.33	241.77	230.22	11.55		7S-2W	OUTFL	241.33	241.77	229.44	12.33
	7S-3W	OUTFL	241.62	240.88	229.0918182	11.78818182		7S-3W	OUTFL	241.62	240.88	228.6527273	12.22727273
	7S-4W	OUTFL	242.84	241.82	231.3572727	10.46272727		7S-4W	OUTFL	242.84	241.82	230.808	11.012
	7S-5W		243.43	241.59	233.7566667	7.833333333		7S-5W		243.43	241.59	233.0275	8.5625
	7S-5.75W	OUTFL	244.57	241.86	232.3308333	9.529166667		7S-5.75W	OUTFL	244.57	241.86	232.0109091	9.849090909
	7S-6.5W	OUTFL	244.09		230.7208333	10.29916667		7S-6.5W	OUTFL	244.09	241.02	230.7863636	10.23363636
				241.02									
	7.75S-0	OUTFL	252.5	248.19	237.4266667	10.76333333		7.75S-0	OUTFL	252.5	248.19	236.9508333	11.23916667
	8S-1E	R	253.78		238.0045455	12.42545455		8S-1E	R	253.78	250.43	238.9090909	11.52090909
				250.43									
	8S-.25W		247.38	244.86	236.383	8.477		8S-.25W		247.38	244.86	235.6591667	9.200833333
	8S-.5W		245.92	243.57	235.8933333	7.676666667		8S-.5W		246.78	243.22	235.937	7.283
	8S-1W	OUTFL	246.95	243.3	235.405	7.895		8S-1W	OUTFL	246.95	243.3	234.8890909	8.410909091
	8S-2W	OUTFL	244.99	242.26	232.5218182	9.738181818		8S-2W	OUTFL	244.99	242.26	232.3518182	9.908181818
	8S-3W	OUTFL	239.43	238.52	228.148	10.372		8S-3W	OUTFL	239.43	238.52	227.5566667	10.96333333
	8S-5W	OUTFL	241.38	239.39	227.73	11.66		8S-5W	OUTFL	241.38	239.39	227.224	12.166
	8S-5.5W	OUTFL	239.17	238.35	231.1036364	7.246363636		8S-5.5W	OUTFL	239.17	238.35	230.03	8.32
	8S-6.5W	OUTFL	242.39	238.67	229.822	8.848		8S-6.5W	OUTFL	242.39	238.67	227.889	10.781
	8.25S-4.25W		240.43	237.34	227.232	10.108		8.25S-4.25W		240.43	237.34	225.925	11.415
	9S-0	OUTFL	250.44	249.51	235.305	14.205		9S-0	OUTFL	250.44	249.51	234.329	15.181
	9S-1.25W	OUTFL	243.23	241.76	232.585	9.175		9S-1.25W	OUTFL	243.23	241.76	232.123	9.637
	9S-2W	OUTFL	244.99	241.32	232.3927273	8.927272727		9S-2W	OUTFL	244.99	241.32	232.1027273	9.217272727
	9S-3W	OUTFL	239.98	237.81	229.1190909	8.690909091		9S-3W	OUTFL	239.98	237.81	229.7733333	8.036666667
	9S-4W	OUTFL	236.84	235.24	225.5608333	9.679166667		9S-4W	OUTFL	236.84	235.24	225.7625	9.4775
	9S-5W	OUTFL	236.66	235.19	226.6781818	8.511818182		9S-5W	OUTFL	236.66	235.19	226.1377778	9.052222222
	9S-5.75W	OUTFL	237.68	235.5	227.5945455	7.905454545		9S-5.75W	OUTFL	237.68	235.5	226.5025	8.9975
	9S-6.5W	OUTFL	238.18	235.01	227.6936364	7.316363636		9S-6.5W	OUTFL	238.18	235.01	226.7716667	8.238333333
	10S-0	R	251.37	249.15	233.3541667	15.79583333		10S-0	R	251.37	249.15	232.6172727	16.53272727
	10S-1W	OUTFL	249.71	248.09	235.314	12.776		10S-1W	OUTFL	249.71	248.09	232.8045455	15.28545455
	10S-2W	OUTFL	242.5	240.12	230.2608333	9.859166667		10S-2W	OUTFL	242.5	240.12	230.1183333	10.00166667
	10S-3W	OUTFL	240.33	237.26	229.1366667	8.123333333		10S-3W	OUTFL	240.33	237.26	228.1181818	9.141818182
	10S-3.87W	OUTFL	238.57	235.16	228.655	6.505		10S-3.87W	OUTFL	238.56	235.16	228.439	6.721
	10S-5W	OUTFL	236.42	233.22	225.15	8.39		10S-5W	OUTFL	236.42	233.54	224.8045455	8.735454545
	10S-6.75W	OUTFL	236.85	233.54	226.597	8.113		10S-6.75W	OUTFL	236.85	234.71	225.256	9.454
	10S-5.75W	OUTFL	235.76	234.71	225.4763636	7.743636364		10S-5.75W	OUTFL	235.76	233.22	224.5681818	8.651818182
	10.75S-4W	OUTFL	236.58	233.4	226.822	6.578		10.75S-4W	OUTFL	236.58	233.4	226.5918182	6.808181818
	11S-1W	OUTFL	244.82	243.45	229.7336364	13.71636364		11S-1W	OUTFL	244.82	243.45	229.5481818	13.90181818
	11S-2W	OUTFL	238.8	237.75	228.3145455	9.435454545		11S-2W	OUTFL	238.8	237.75	228.77	8.98
	11S-3W	OUTFL	237.96	236.02	229.8566667	6.163333333		11S-3W	OUTFL	237.96	236.02	229.0254545	6.994545455
	11S-5W	OUTFL	234.89	232.59	223.913	8.677		11S-5W	OUTFL	234.89	232.59	223.0716667	9.518333333
	11S-5.75W	OUTFL	234.78	232.62	226.9309091	5.689090909		11S-5.75W	OUTFL	234.78	232.62	225.8163636	6.803636364
	11S-6.87W	E PMP	233.32	231.48	224.1418182	7.338181818		11S-6.87W	E PMP	233.32	231.48	223.6009091	7.879090909
	11.75S-6.75W	E PMP	231.3	231	223.191	7.809		11.75S-6.75W	E PMP	231.3	231	222.0536364	8.946363636
	12S-1W	OUTFL	239.28	238.51	228.2190909	10.29090909		12S-1W	OUTFL	238.92	238.68	227.417	11.263
	12S-2W	OUTFL	237.63	237.11	227.1663636	9.943636364		12S-2W	OUTFL	237.63	237.11	226.928	10.182
	12S-3W	OUTFL	242.36	240.04	226.5318182	13.50818182		12S-3W	OUTFL	242.36	240.04	225.504	14.536
	12S-4W	OUTFL	237.71	234.84	223.5091667	11.33083333		12S-4W	OUTFL	237.71	234.84	223.8718182	10.96818182
	12S-5W	OUTFL	236.8	233.16	221.8125	11.3475		12S-5W	OUTFL	236.8	233.16	221.1858333	11.97416667
	12S-6W	OUTFL	233.04	232.37	220.365	12.005		12S-6W	OUTFL	233.04	232.37	220.0663636	12.30363636
	13S-2W	OUTFL	241.14	240.42	228.94	11.48		13S-2W	OUTFL	241.14	240.42	228.5290909	11.89090909

2008	Well Location	Drainage Area	Pipe Elevation	Average Ground Elevation	Water Elevation	Average Depth to Water Table	2009	Well Location	Drainage Area	Pipe Elevation	Average Ground Elevation	Water Elevation	Average Depth to Water Table
	13.12S-2.87W	R 2	243.53	240.58	226.84	13.74		13.12S-2.87W	R 2	243.53	240.58	226.01	14.57
	13S-4.25W	R 2	234.38	234.44	227.02	7.42		13S-4.25W	R 2	234.38	234.44	226.2308333	8.209166667
	13S-5W	OUTFL	235.57	231.38	224.6791667	6.700833333		13S-5W	OUTFL	235.57	231.38	223.9941667	7.385833333
	13S-6W	OUTFL	232.7	231.6	221.9566667	9.643333333		13S-6W	OUTFL	232.7	231.6	221.4	10.2
	13S-6.5W	OUTFL	230.69	228.55	220.6475	7.9025		13S-6.5W	OUTFL	230.69	228.55	220.4918182	8.058181818
	13S-7.12W	OUTFL	233.57	232.23	220.6725	11.5575		13S-7.12W	OUTFL	233.57	232.23	220.6209091	11.60909091
	14.25S-6.5W	OUTFL-2	231.67	228.1	221.1191667	7.340833333		14.25S-6.5W	OUTFL-2	231.67	228.46	220.725	7.735
	15S-6.75W	OUTFL	227.12	226.56	220.1718182	6.388181818		15S-6.75W	OUTFL	227.12	226.56	218.8445455	7.715454545
	15S-6W	R 3	229.73		222.222	6.708		15S-6W	R 3	229.73	228.93	221.0475	7.8825
				228.93									
	16S-6W	OUTFL-2	228.1		#VALUE!	#VALUE!		16S-6W	OUTFL-2	228.1	226.26	220.6944444	5.565555556
				226.26									
	17S-5.75W	OUTFL 2	227.1		220.2922222	5.827777778		17S-5.75W	OUTFL 2	227.1	226.12	218.667	7.453
	6.5N-3.56E	OUTFL	282.44	279.57	270.35	9.22		6.5N-3.56E	OUTFL	282.44	279.57	270.1045455	9.465454545

APPENDIX E

SUMMARY OF PALO VERDE IRRIGATION DISTRICT DIVERSION DATA

APPENDIX E
TABLE E-1
SUMMARY OF PVID DIVERSION AND RETURN DATA
1993 TO 2009
BLYTHE SOLAR POWER PROJECT
RIVERSIDE COUNTY, CALIFORNIA

YEAR[1,2]	UNIT	P.V.I.D. DIVERSION	DELIVERED TO FARMS	SPILL to RIVER	SPILL to DRAINS	TOTAL SPILL	LOSS OR (-) GAIN	OUTFALL DRAIN	OLIVE LAKE DRAIN	SURFACE RETURN TO RIVER	Unmeasured RETURN TO RIVER	DIVERSION LESS RETURNS	DELIVERED TO MESA	DELIVERED TO VALLEY AREA	DELIVERED TO C.R.I.T.	VALLEY LESS DRAIN
2009																
	TOTAL C.F.S.	375,571	311,333	44,356	31,329	75,683	-11,445	163,471	707	208,533	21,020	146,018	8,097	303,236	3,613	135,445
	Acre Feet	744,934	617,520	87,978	62,141	150,115	-22,701	324,240	1,402	413,620	41,693	289,622	16,061	601,459	7,166	268,651
2008																
	TOTAL C.F.S.	442,117	374,895	48,078	34,548	82,626	-15,404	179,279	781	228,138	24,757	189,222	6,661	368,234	4,391	183,783
	Acre Feet	876,926	743,593	95,361	68,524	163,886	-30,553	355,594	1,549	452,505	49,105	375,317	13,213	730,381	8,709	364,529
2007																
	TOTAL C.F.S.	455,220	391,885	50,653	30,408	81,061	-17,726	192,941	5	243,598	25,489	186,133	5,425	386,459	4,054	189,460
	Acre Feet	902,916	777,292	100,468	60,313	160,782	-35,158	382,693	9	483,170	50,557	369,189	10,761	766,531	8,041	375,788
2006																
	TOTAL C.F.S.	432,351	366,186	48,170	31,262	79,431	-13,266	177,834	0	226,004	24,211	182,136	5,146	361,040	3,254	179,952
	Acre Feet	857,556	726,320	95,544	62,007	157,549	-26,313	352,728	0	448,272	48,022	361,262	10,207	716,113	6,455	356,930
2005																
	TOTAL C.F.S.	407,307	322,253	43,638	34,994	78,632	6,422	172,981	9	216,628	22,815	167,864	4,505	317,748	2,433	142,325
	Acre Feet	807,882	639,180	86,555	69,409	155,964	12,737	343,103	18	429,675	45,253	332,953	8,936	630,244	4,826	282,297
1998																
	TOTAL C.F.S.	454,730	411,955	42,490	14,630	57,120	-14,345	203,256	1,513	247,259	--	207,471	5,464	406,491	5,456	196,266
	Acre Feet	901,944	817,101	84,278	29,018	113,296	-28,453	403,152	3,001	490,431	--	411,513	10,838	806,263	10,822	389,288
1997																
	TOTAL C.F.S.	469,673	442,554	43,274	10,837	54,111	-26,992	204,711	1,886	249,871	--	219,802	4,676	437,878	4,564	226,718
	Acre Feet	931,583	877,793	85,834	21,494	107,328	-53,538	406,038	3,741	495,613	--	435,970	9,274	868,519	9,052	449,688
1996																
	TOTAL C.F.S.	485,774	456,089	37,869	10,981	48,850	-19,165	192,342	1,432	231,642	--	254,132	4,256	451,833	5,160	252,900
	Acre Feet	963,519	904,639	75,112	21,780	96,892	-38,013	381,504	2,839	459,456	--	504,063	8,442	896,197	10,234	501,620
1993																
	TOTAL C.F.S.	343,240	291,305	50,512	10,252	60,764	-8,828	134,648	243	185,402	--	157,838	3,939	287,365	2,496	149,978
	Acre Feet	680,807	577,794	100,188	20,335	120,523	-17,511	267,070	483	367,739	--	313,067	7,813	569,981	4,951	297,477

SUMMARY STATISTICS

Average	Acre Feet	**852,007**	**742,359**	**90,146**	**46,113**	**136,259**	**-26,611**	**357,347**	**1,449**	**448,942**	**46,926**	**376,995**	**10,616**	**731,743**	**7,806**	**365,141**
Median	Acre Feet	876,926	743,593	87,978	60,313	150,115	-28,453	355,594	1,402	452,505	48,022	369,189	10,207	730,381	8,041	364,529
Maximum	Acre Feet	963,519	904,639	100,468	69,409	163,886	12,737	406,038	3,741	495,613	50,557	504,063	16,061	896,197	10,822	501,620
Standard Deviation	Acre Feet	91,669	114,594	8,369	22,111	26,363	18,005	43,543	1,447	40,938	3,511	65,943	2,594	115,220	2,141	76,885

DEFINITIONS

CFS	Cubic Feet per Second
Acre-feet	One acre-foot equals 325,829 gallons
PVID	Palo Verde Irrigation District
Delivered to Farms	Delivery to Mesa + Valley + CRIT
Delivered to Valley	Delivered to Farms - Delivery to Mesa - Delivery to CRIT
Spill to River	Sum of the EIGHT spills that discharge directly to the River (See Figure 5)
Spill to Drains	Internal Canals Spills to Drains (Outfall + Olive Lake Drains)
Total Spill	Spill to River + Spill to Drains
Loss or Gain	PVID Diversion - (Delivered to Farms (Valley + Mesa) + Total Spill)
Surface Return to River	Outfall Drain + Olive Lake Drain + Spill to River
Diversion Less Return	PVID Diversion - Surface Return
Valley Delivery less Drain	(Valley Delivery - CRIT) - (Outfall Drain-Olive Lake Drain) = (Field Capacity + Consumptive Use (ET) + Percolation)

NOTES

1 Only those years with complete data sets across all categories were summarized and used in the summary statistics. There was no data available for 2000 to 2004. 1999, 1995 and 1994 did not contain complete date sets.
2 Operational spreadsheets for the years listed follow this summary table in Appendix E.

APPENDIX F

GEOPHYSICAL INVESTIGATION AT THE SOLAR MILLENNIUM PROJECT

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GEOPHYSICAL INVESTIGATION AT THE SOLAR MILLENNIUM PROJECT NORTHWEST OF BLYTHE IN RIVERSIDE COUNTY, CALIFORNIA

August 3, 2010

for

AECOM Incorporated
1220 Avenida Acaso
Camarillo, CA 93012

by

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TABLE OF CONTENTS

LIST OF ILLUSTRATIONS iii

I INTRODUCTION 1

A. Site Conditions 2

II METHODOLOGY 3

A. Instrumentation. 4
B. Data Reduction 4

III RESULTS 6

A. Refraction Profiles 6
B. Depth to Groundwater 8
C. TEM and Well Log Comparisons 8
D. TEM Results 9
E. Depth to Bedrock 9
F. Conclusions 10
H. Limitations 11

IV DRAWINGS

LIST OF ILLUSTRATIONS

Drawing 1 Vicinity Map

Drawing 2 Refraction and Transient Electromagnetic Techniques

Drawing 3 Refraction and TEM Sounding Locations

Drawing 4 Refraction Profiles

Drawing 5 Water Table Elevations

Drawing 6 Well Log and TEM data

Drawing 7 8Hz and 16Hz TEM Results

Drawing 8 Resistivity Averages From 16Hz TEM Data

Drawing 9 Bouguer Residual Gravity Map

Drawing 10 Bedrock Depths From Gravity Data

Drawing 11 Bedrock Elevations

I INTRODUCTION

This report presents the results of a geophysical investigation performed at the Solar Millennium site near Blythe in Riverside County, California. The investigation was performed for AECOM, Incorporated, by J R Associates. The objectives of the investigation were to:

- Measure the depth to the water table.
- Measure the depth to bedrock.
- Look for trends in the unconfined aquifer that suggest changes in clay and sand content that may affect permeability.
- Provide general information regarding site geology, groundwater, and formation thickness.
- Estimate groundwater quality from surface resistivity measurements.

James Rezowalli, Principal Geophysicist, assisted by Garret Rhett, Brian Rezowalli, and Jon Arakaki, Technicians, of J R Associates performed the field work in June and July of 2010.

A. Site Conditions

The Solar Millennium site consists of approximately twelve square miles of open desert northwest of the Blythe Airport (Drawing 1). Highway 10 is on the south side of the site, the McCoy Mountains are on the west side of the site, and Black Creek Road runs north to south through the site. The site gently slopes from elevations between 700 and 800 feet near the McCoy Mountains to elevations between 400 and 500 feet near the McCoy Wash on the site's east side. There are two knobs along the site's southeastern boundary.

Information regarding the site's geology was obtained from a USGS professional paper regarding the geohydrology of the Blythe area[1]. The geology in the area, in descending order from the surface, consists of older alluvium, the Bouse Formation, fanglomerate, and consolidated bedrock. The older alluvium is a result of several broad periods of aggradation and degradation of the Colorado River. The older alluvium consists of moderately consolidated gravel, sand, silt, and clay alluvial fan deposits. The USGS paper divided the older alluvium into five units although the units could not readily be separated. The Bouse Formation is a marine and brackish-water formation that is composed of a basal limestone overlain by interbedded clay, silt, and sand. The Bouse Formation was deposited in an embayment of the Gulf of California and is reported to be at a depth of approximately 600 feet below grade at the site. The fanglomerate that underlies the Bouse Formation is composed mainly of cemented sandy gravel that is probably from a nearby source. The McCoy Mountains on the west side of the site suggest the bedrock beneath the site is composed of metasedimentary rocks. The 1973 USGS report contained water quality data collected from wells east of the site. The sum of solids for these wells ranged from 732 to 1730 mg/l. The depth for the perforated interval for these wells ranged from 150 to 572 feet below grade.

[1]D.G. Metzger, O.J. Loeltz, and Burdge Irelna, *Geohydrology of the Parker-Blythe-Cibola Area, Arizona and California*, USGS Professional Paper 486-G, 1973.

II METHODOLOGY

We used two geophysical methods in our investigation, seismic refraction and transient electromagnetics (TEM). Seismic refraction was used to measure the depth to the water table. For seismic refraction we generated a compressional (sound) wave that traveled through the ground and refracted off geologic layers with different seismic velocities (Drawing 2). Dry unconsolidated alluvium has a compressional (P) wave velocity typically between 1200 to 2500 feet per second (fps). Saturated unconsolidated alluvium has a P-wave velocity of approximately 5500 fps. Bedrock typically has velocities greater than 7500 fps. The contrast between the P-wave velocities makes the top of the water table and rock good refractors.

TEM measures the changes in electrical resistance with depth. The TEM method involves pulsing a magnetic field which induces eddy currents in the ground (Drawing 2). The eddy currents create a secondary magnetic field that decays with time. The rate of decay is related to the resistivities of the formations below. Clay is a good conductor of electricity. Poorly sorted saturated sands and gravels are moderate conductors of electricity. Dry sands, gravels, and consolidated rock are poor conductors of electricity. The resistivity of a formation goes down as the salinity of the pore fluid goes up. Measuring electrical resistance with depth helps to determine if clays or high salinity pore fluids are present.

In addition to the two field techniques, we reviewed geophysical well logs provided by AECOM and reviewed existing gravity data available from the USGS. The USGS collected gravity data throughout the lower Colorado River basin and concatenated it in an Open-File

Report[2]. The Bouguer and isostatic residual gravity map for the Chuckwalla Valley and Palo Verde Mesa were reviewed. The gravity data were used to provide an estimate of the depth to bedrock below the site.

A. Instrumentation

Fifteen 1000-foot long seismic refraction lines were collected at the Solar Millennium site (Drawing 3). Each line contained 24 geophones and three shot points. The shot points were at both ends and in the middle of each line. The shots consisted of small explosive charges 1/3 pound in size. The geophones were connected to a Geometrics 24-channel Geode seismograph which was connected to a laptop for storing and viewing the data. The depth of penetration along the seismic lines was 350 feet below the ground surface.

TEM data were collected at twenty-four locations in the study area (Drawing 3). The TEM soundings used square loops that were 600 feet on a side with the receiver approximately centered in the loop. Data were collected using a Zonge GDP-32/II receiver and a ZT-30 transmitter. Data were acquired at two frequencies, 8 Hz and 16 Hz. Stacking and averaging were used to improve the signal to noise ratio. At each station and for each frequency three TEM measurements were collected to establish repeatability.

[2]Mariano, John, Helferty, M.G., and Gage, T.B., Bouguer and Isostatic Residual Gravity Maps of the Colorado River Region, Including the Kingman, Needles, Salton Sea, and El Centro Quadrangles: US Geological Survey Open-File Report 86-347, 7 Sheets.

B. Data Reduction

Seismic refraction data reduction began by picking the arrival times from the seismograph recordings. An arrival time is the time a P-wave spent traveling from a shot point to geophone. The wave could either travel along the ground surface or be refracted from an interface between materials. For a refraction to occur, the materials below the interface must have a greater P-wave velocity than the materials above the interface. The arrival times were entered into a computer program with elevation, location, and layer control information. The elevation above sea level was determined from a USGS topographic map.

The interpretation program, FSIP, performs a first approximation delineation of the refracting horizons using a delay-time method. The approximation is then tested and improved by the program's ray-tracing procedure in which ray travel times computed for the model are compared against measured travel times. The model is subsequently adjusted iteratively to minimize the discrepancy between the computed and measured travel times. A Bureau of Mines Report of Investigation describes the program[3].

One-dimensional smooth model inversions were generated for each of the 24 TEM soundings obtained during this investigation. Resistivity versus depth profiles were calculated from the measured TEM decay curves using inversion software (1X1D TEM) developed by Interpex, Incorporated. The software uses an iterative process of comparing a predicted TEM decay curve calculated from a starting model to the field data. It then adjusts the model iteratively until a close fit between the predicted data and field data is achieved.

[3]Scott, James H., Computer Analysis of Seismic Refraction Data, BuMines RI 7595, 1972.

III RESULTS

A. Refraction Profiles

The results of the computer analysis of the refraction data are presented in Drawings 4 and 5 and in Table 1. Drawing 4 contains two-dimensional profiles showing the seismic layering and layer velocities measured along the refraction lines. Drawing 5 is a contour map of the top of the third refraction layer. Table 1 is broken into two parts, 1A and 1B. Table 1A summarizes the results of the refraction data collected away from the base of the McCoy Mountains and Table 1B summarizes the results for the refraction lines collected near the base of the McCoy Mountains.

Summary of Refraction Results
Table 1A. Refraction lines away from the base of the McCoy Mountains.

Line	Depth to Layer 2 (feet)	Depth to Layer 3 (feet)	Layer 1 Velocity (fps)	Layer 2 Velocity (fps)	Layer 3 Velocity (fps)
1	52 to 73	213 to 232	2100	3100	5600
2	25 to 51	198 to 226	1800	2700	6000
3	20 to 42	195 to 211	2000	3100	5600
4	50 to 80	190 to 207	2100	3000	6400
5	--	156 to 166	2400	--	6300
7	17 to 27	192 to 208	1800	3200	6300
8	--	166 to 181	2300	--	5500
9	10 to 47	185 to 190	1900	2900	6100
10	8 to 49	169 to 190	1600	2900	6100
11	8 to 26	156 to 166	1600	2700	6200
12	27 to 63	160 to 216	2000	3000	6300
14	8 to 19	193 to 209	1900	3100	6700

Table 1B. Refraction Lines near the McCoy Mountains

Line	Depth to Layer 2 (feet)	Depth to Layer 4 (feet)	Depth to Layer 5 (feet)	Layer 1 Velocity (fps)	Layer 2 Velocity (fps)	Layer 4 Velocity (fps)	Layer 5 Velocity (Fps
6	5 to 38	138 to 152	--	1800	2600	4500	--
13	58 to 88	--	255 to 319	2000	3600	--	11,500
15	--	59 to 163	--	2900	--	4100	--

We found five different seismic layers beneath the site. The layers were distinguished by their P-wave velocities and identified as layers 1, 2, 3, 4, and 5. Layer 1 is shown in grey on Drawing 4. Layer 1 included the ground surface and had a P-wave velocity ranging from of 1600 to 2900 feet per second (fps). The geologic information and the P-wave velocity indicated that Layer 1 consists of dry loose alluvium or fan deposits. Layer 1 was found beneath all of the refraction lines.

Layer 2 is shown in yellow on Drawing 4. This layer was distinguished by a P-wave velocity that ranged from 2600 to 3600 fps. The depth from the ground surface to the top of the second seismic layer ranged from 5 to 88 feet. The geologic information and the P-wave velocity indicated Layer 2 consists of denser dry to partially saturated older alluvium. Layer 2 was found under most of the refraction lines.

Layer 3 is shown in blue on Drawing 4. This layer was distinguished by a P-wave velocity that ranged from 5500 to 6700 fps. The depth from the ground surface to the top of the third seismic layer ranged from 156 to 232 feet. The geologic information and the P-wave velocity indicated that Layer 3 consists of saturated older alluvium and probably coincides with the top of the water table. Layer 3 was found under most of the refraction lines. Layer 3 was not found under the lines near the base of the McCoy Mountains, lines 6, 13, and 15.

A fourth seismic layer was found under refraction lines 6 and 15 which were near the base of the McCoy Mountains. Layer 4 is shown in green in Drawing 4. The fourth seismic layer was distinguished by a P-wave velocity that ranged from 4100 to 4500 fps. The depth from the ground surface to the top of the fourth seismic layer ranged from 59 to 163 feet. The geologic information and P-wave velocity indicated the fourth seismic layer probably consists of partially saturated rocky alluvium or fan deposits.

A fifth seismic layer was found under refraction line 13 which was also near the base of the McCoy Mountains. The depth to the fifth layer ranged from 255 to 319 feet below the ground surface. The high P-wave velocity of 11,500 fps suggests the fifth seismic layer consists of bedrock.

B. Depth to Groundwater

Drawing 5 is a contour map of the groundwater table elevations based on the refraction data. The contours represent the average depth to the third refracting layer found under lines 1, 2, 3, 4, 5, 7, 8, 9, 10, 11, 12 and 14. The data suggest the water table slopes from the west and the north toward the southeast. The data suggest that water migrates from west and north of the site to the southeast between the two knobs.

C. TEM and Well Log Comparisons

Drawing 6 compares the geophysical test well log to the two closest TEM soundings. Both the TEM soundings and the geophysical well log indicate the saturated alluvium at a depth of approximately 200 feet below grade is electrically conductive. The well log indicates a range of 10 to 12 Ohm-m and the TEM soundings show a range of 5 to 23 Ohm-m. The low resistivities indicate the saturated older alluvium will likely have a significant amount of clay and it is likely the groundwater will have a high amount of total dissolved solids, in the 1500 mg/l and higher range.

D. TEM Results

Drawings 7 and 8 show the results of the TEM soundings. Drawing 7 shows the TEM soundings and the variation of resistivity with depth and Drawing 8 is a contour map of the average resistivity for the saturated older alluvium between a depth of 200 and 700 feet below grade. There are two sets of decay curves and resistivity profiles for each sounding, one for the data collected at 8 Hz and one for the data collected at 16 Hz (Drawing 7). In general, the TEM data shows the near surface dry alluvium is electrically resistive. Typically, there is a sharp decrease in resistivity when the groundwater table is reached and the resistivity tends to go down with depth. A comparison between the 8 Hz data, the 16 Hz data, and the well log suggest the smaller variations in resistivity in the TEM models with depth are not significant since they are not consistently repeated. Except for TEM lines near the base of the McCoy Maintains, the TEM data suggest the geology at the site is fairly uniform with a slight increase in resistivity (corresponding to a slight decrease in clay content) to the southeast between the knobs (Drawing 8). The resistivity increases significantly as the base of the McCoy Mountains is approached indicating rocky dry soils. Based on the resistivity data, with respect to groundwater, the most productive areas of the site will be the areas with resistivities between 8 and 14 Ohm-m on the eastern half of the site. The areas west of Black Creek Road to the base of the McCoy Mountains may not be very productive.

E. Depth to Bedrock

To help determine depth to bedrock we reviewed gravity data collected by the USGS[4]. Drawing 9 shows the USGS Bouguer residual anomaly data superimposed on the vicinity map of the study area. Gravity data are somewhat like a contour map of the bedrock. Gravity lows occur over deep basins and gravity highs occur over the mountains. Individual residual gravity

[4]Mariano, John, Helferty, M.G., and Gage, T.B., Bouguer and Isostatic Residual Gravity Maps of the Colorado River Region, Including the Kingman, Needles, Salton Sea, and El Centro Quadrangles: US Geological Survey Open-File Report 86-347, 7 Sheets.

data points were obtained from the USGS data along five profile lines crossing from the McCoy Mountains on the west through the site to the Big Maria Mountains on the east. The residual gravity data were digitized at half kilometer intervals along the lines and the resulting profiles were inverted using the program GravMod V3.1 developed at Lancaster University in the UK. For the inversion we assumed a two layer model of alluvium over bedrock, that the bedrock outcrops at the McCoy and Big Maria Mountains, a density difference of 1000 Kg/m3 between the alluvium and bedrock, and that the bedrock would be deeper than the deepest well drilled in the area, well 28C1. The results of the inversion are shown on Drawings 10 and 11. Drawing 10 shows the depth to bedrock across the five profile lines and Drawing 11 is a contour map of the top of bedrock beneath the site. The bedrock contours indicate the bedrock generally slopes from the west to the east with a local high under the knob nearest the northeast corner of the site. The deepest section of bedrock beneath the site is between the two knobs.

F. Conclusions

The geophysical data indicates the water table elevations below the site varies from 350 feet near Black Creek Road to 240 feet between the two knobs on the eastern side of the site (Drawing 5). The data suggest groundwater flows from the west and from the north toward the southeast between the two knobs. The TEM data indicates the geology from Black Creek Road to the eastern side of the site is fairly uniform with a slight increase in resistivity to the southeast and a slight decrease in resistivity with depth (Drawings 7 and 8). The TEM and refraction data indicate the soil becomes more rocky and dryer west of Black Creek Road. The data also indicate that shallow bedrock occurs at the base of the McCoy Mountains. Bedrock outcrops at the McCoy Mountains and the gravity data suggest the bedrock reaches a depth of -2000 feet between the two knobs on the eastern side of the site (Drawing 11). The geophysical

data suggest that the best locations for groundwater production will be between Black Creek Road and the site's southeastern boundary between the two knobs.

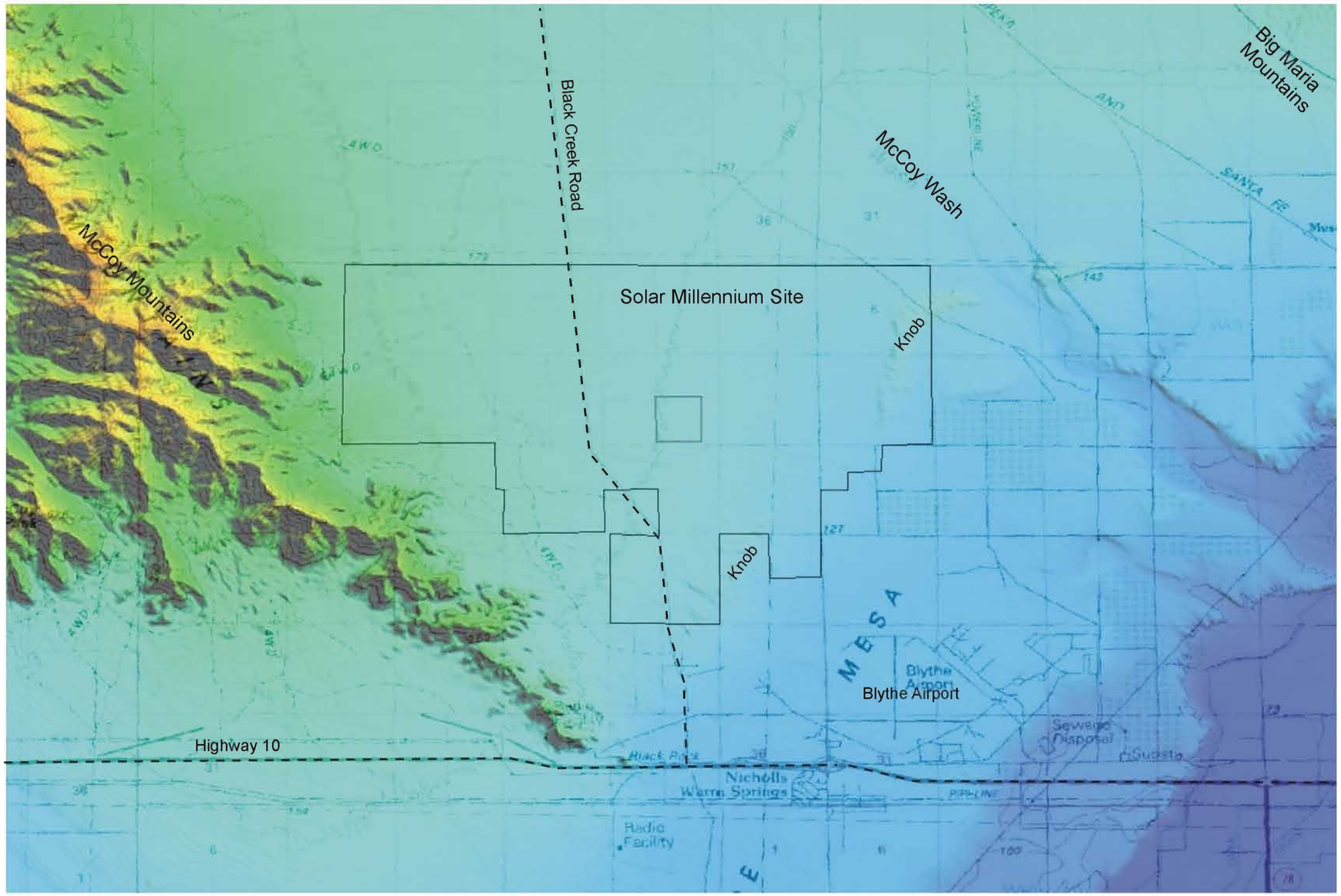
G. Limitations

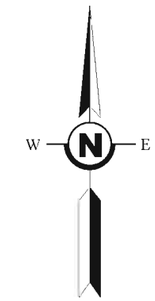
Many factors contribute to soil resistivity. Each soil type, sand, silt, or clay has a range of resistivity associated with it and there is overlap between the ranges. Trends in the resistivity data should be correlated to other data regarding the site's geology, hydrology, and history before conclusions are made.

Seismic layers do not always correspond directly to lithologic changes that might be found in borehole or trenching data. A seismic layer is an interface between materials with different P-wave velocities. Factors such as weathering, cementation, induration, and saturation as well as lithologic changes can create changes in seismic velocities. Also, there can be lithologic changes without velocity changes. However, our field experience indicates that seismic layers often correspond to major changes in lithology or saturation to within ±10% of the depth to the interface.

No gravity data were collect for this study. The results based on gravity data were obtained from existing USGS gravity data available online through the USGS. The geophysical interpretations should be reviewed and updated as more data becomes available.

IV DRAWINGS





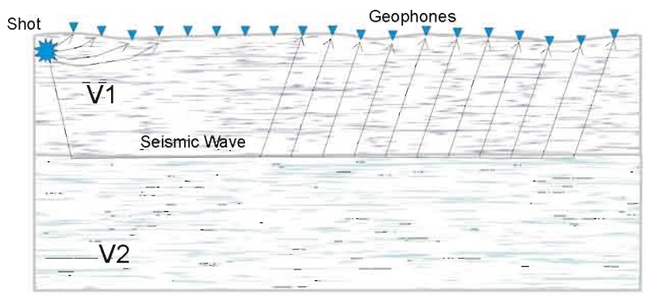
Vicinity Map- Solar Millennium Project
Northwest of the Blythe Airport
Riverside County, California

SCALE:	No Scale		DRAWN BY: J.J.R.
DATE:	7-20-2010	JOB NUMBER: 120-275-10	REVISED:

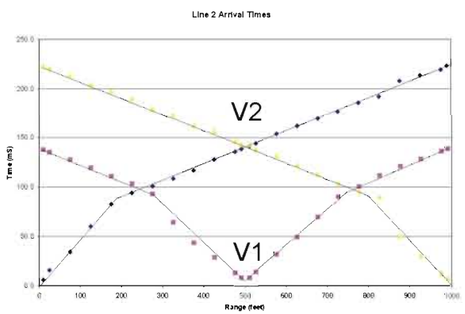
J R ASSOCIATES Civil and Environmental Geophysics
1886 Emory Street, San Jose, CA (408) 293-7390

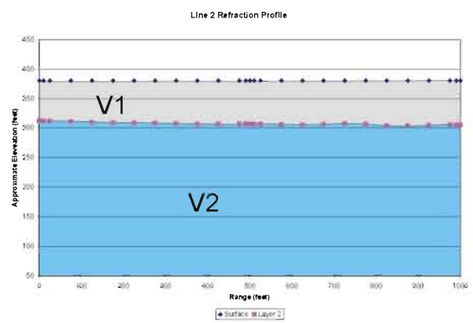
DRAWING NUMBER: 1

Refraction Field Setup

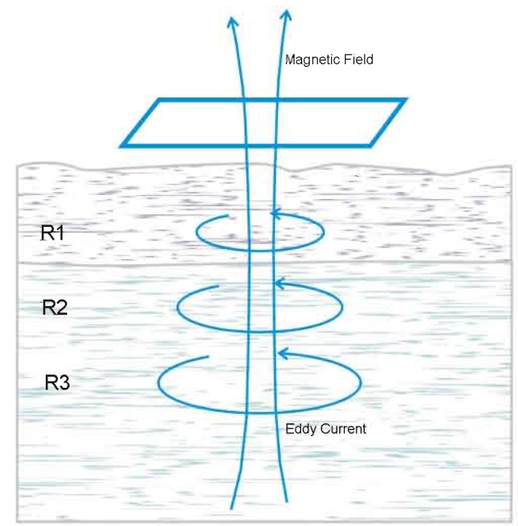


Refraction Data





TEM Field Setup



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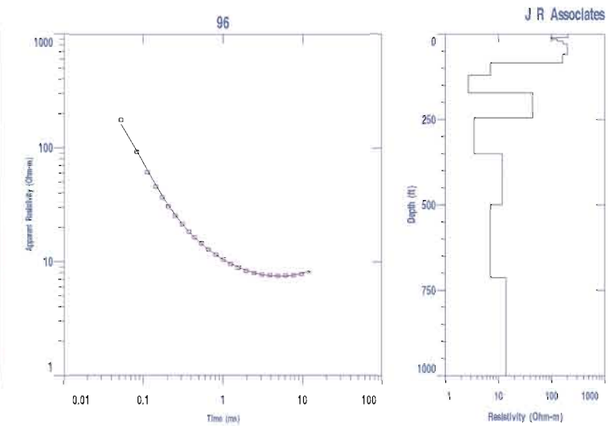

Refraction and Transient Electromagnetic Techniques
Northwest of the Blythe Airport
Riverside County, California

SCALE: See Diagrams		DRAWN BY:	J.J.R.
DATE: 7-20-2010	JOB NUMBER: 120-275-10	REVISED:	

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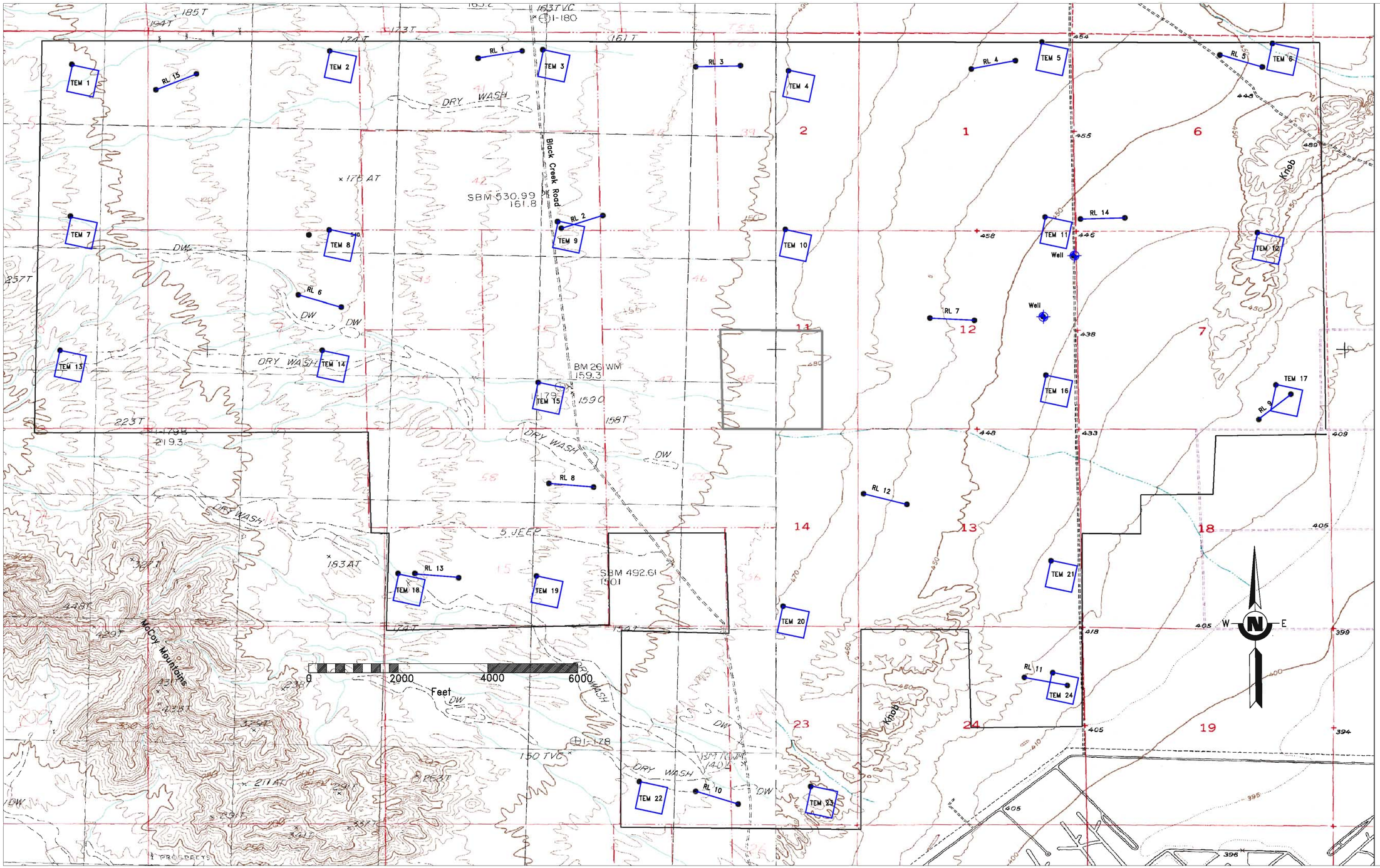
DRAWING NUMBER: 2



EXPLANATION:

Refraction Line

TEM Sounding

Refraction and TEM Sounding Locations- Solar Millenium Project
Northwest of the Blythe Airport
Riverside County, California

SCALE: See Diagram		DRAWN BY:	J.J.R.
DATE: 7-20-2010	JOB NUMBER: 120-275-10	REVISED:	

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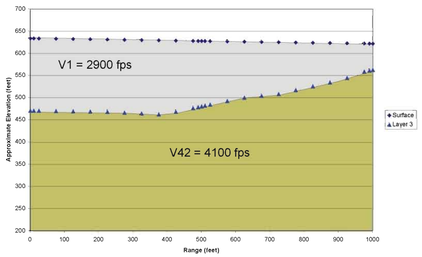
DRAWING NUMBER: 3

Refraction Line 15



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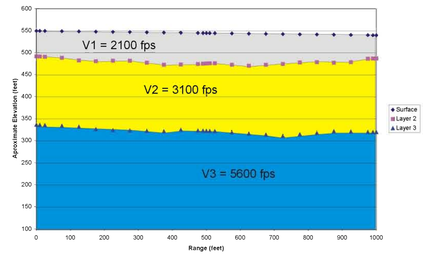

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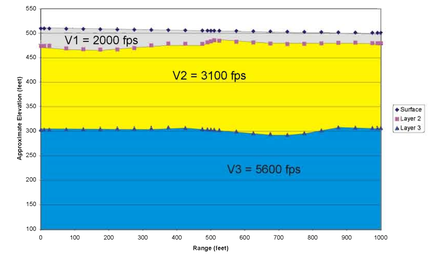

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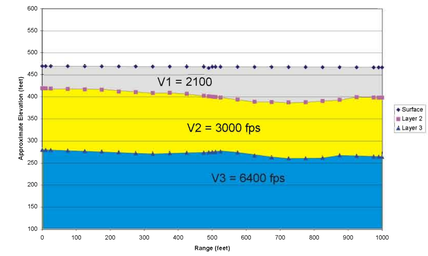

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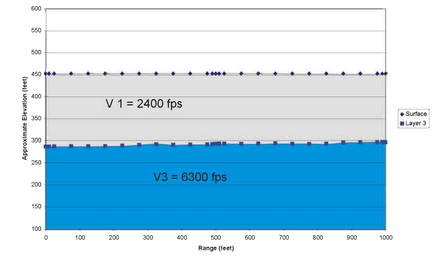

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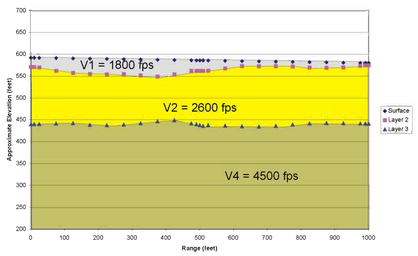

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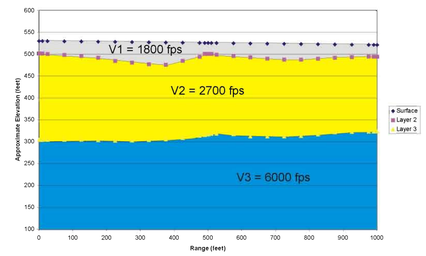

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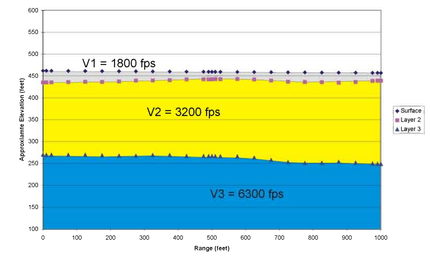

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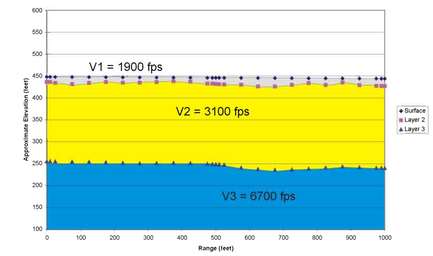

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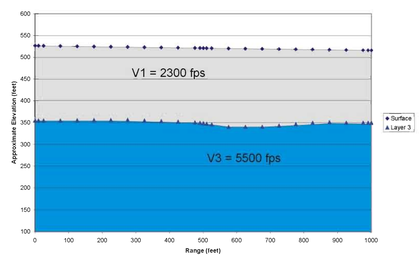

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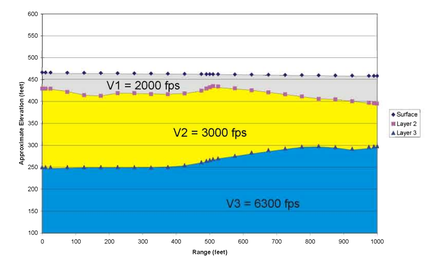

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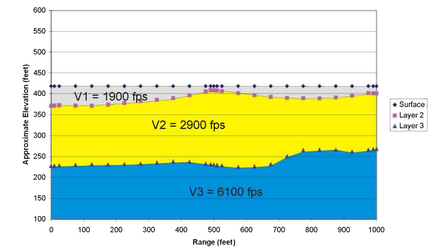

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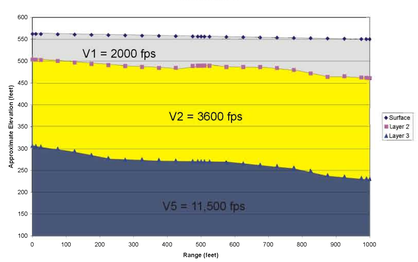

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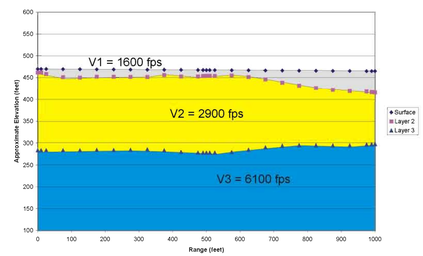

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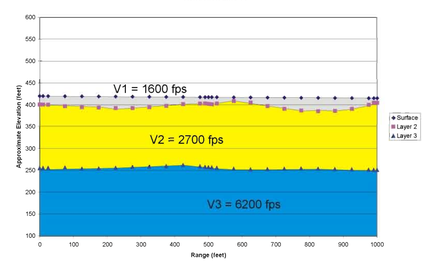

EXPLANATION:

1	Dry Loose Alluvium
2	Dry Denser Alluvium
3	Saturated Alluvium
4	Dry to Partially Saturated Rocky Alluvium
5	Bedrock

Refraction Profiles- Solar Millennium Project
Northwest of the Blythe Airport
Riverside County, California

SCALE: See Diagrams		DRAWN BY:	J.J.R.
DATE: 7-20-2010	JOB NUMBER: 120-275-10	REVISED:	

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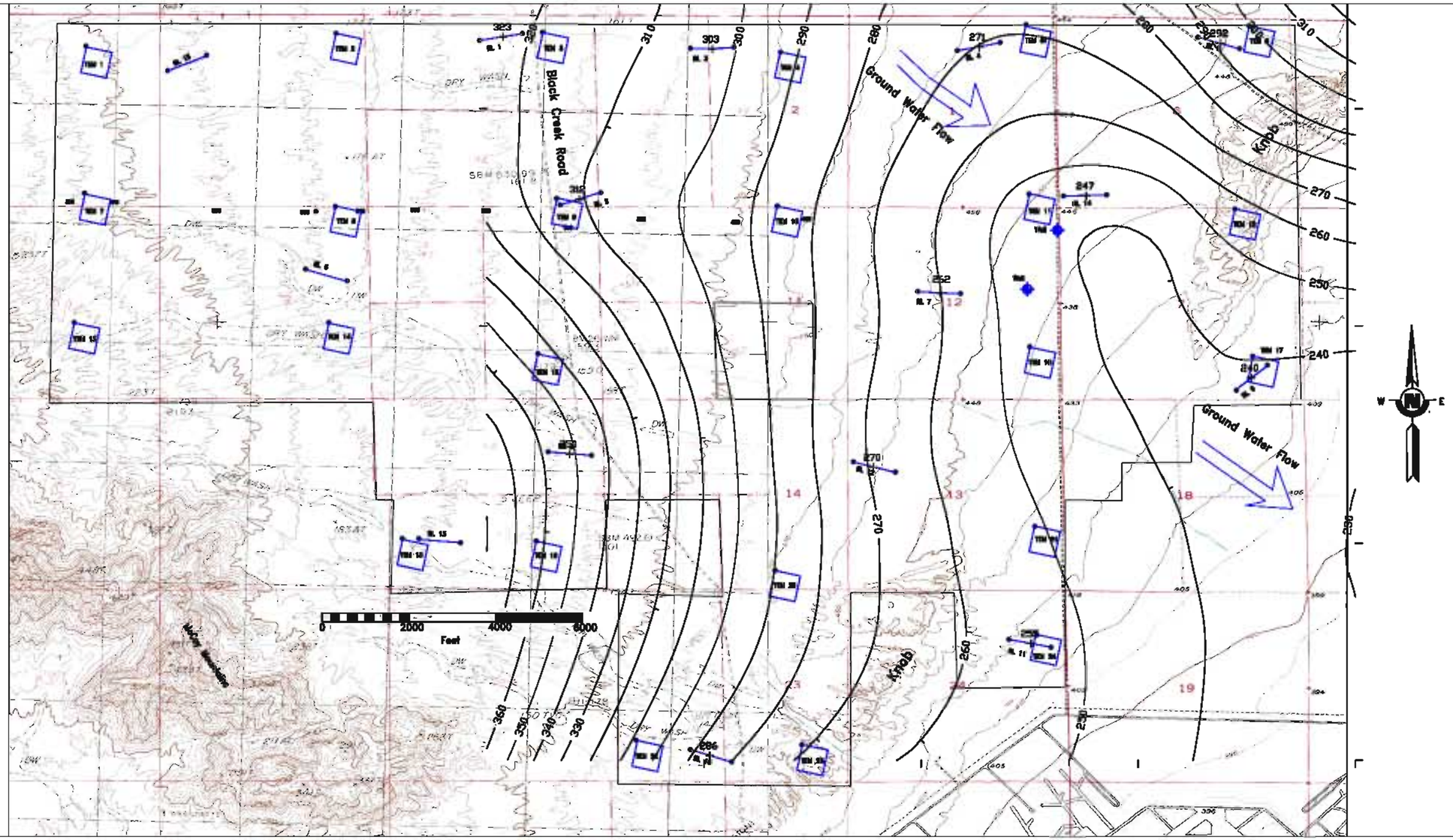
DRAWING NUMBER: 4



EXPLANATION:

10-foot Contour Interval

Refraction Line

TEM Sounding

Water Table Elevations And Flow Direction Based on Third Seismic Layer Depths

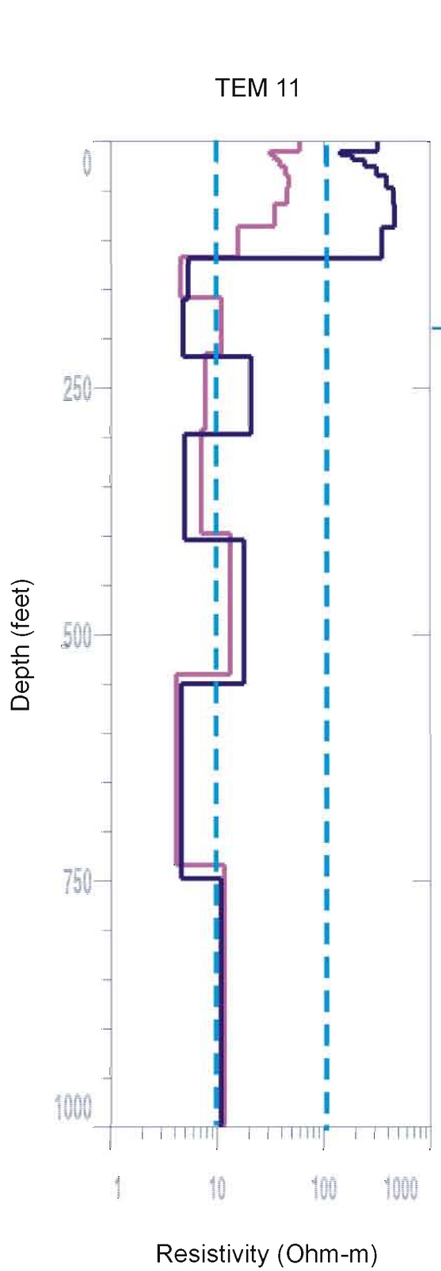
Water Table Elevations- Solar Millennium Project
Northwest of the Blythe Airport
Riverside County, California

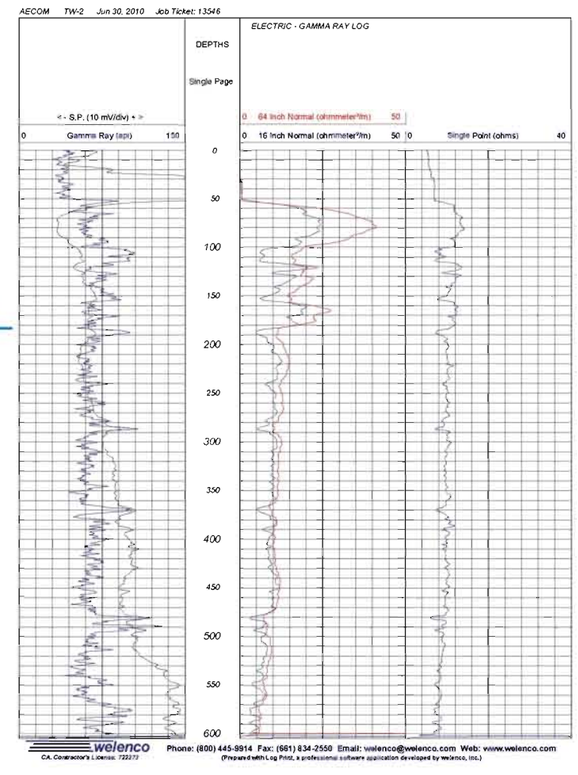
SCALE: See Diagram		DRAWN BY:	J.J.R.
DATE: 7-20-2010	JOB NUMBER: 120-275-10	REVISED:	

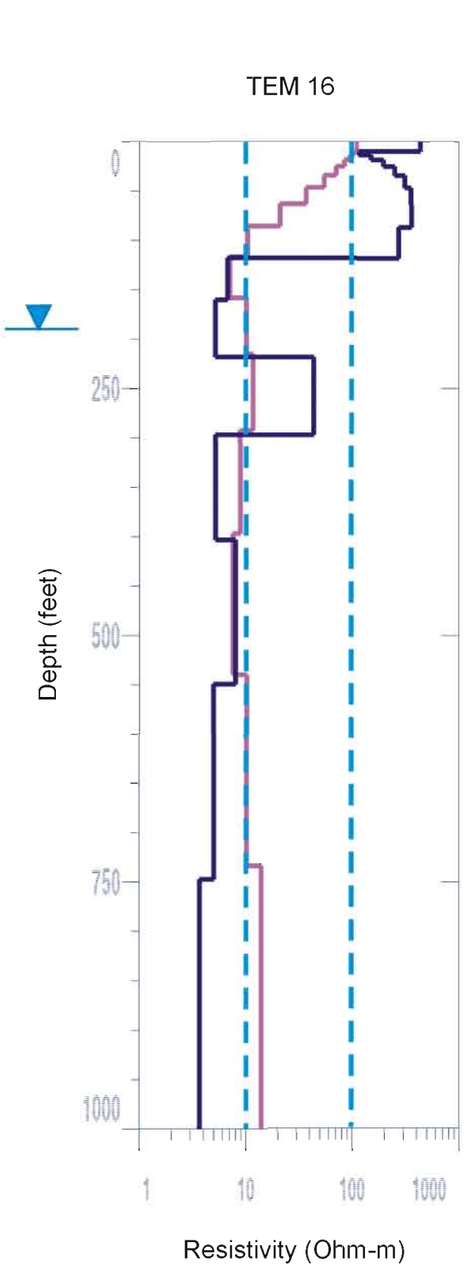
J R Associates Civil and Environmental Geophysics
1886 Emory Street, San Jose, CA (408) 293-7390

DRAWING NUMBER: 5

TW-2 Well Log





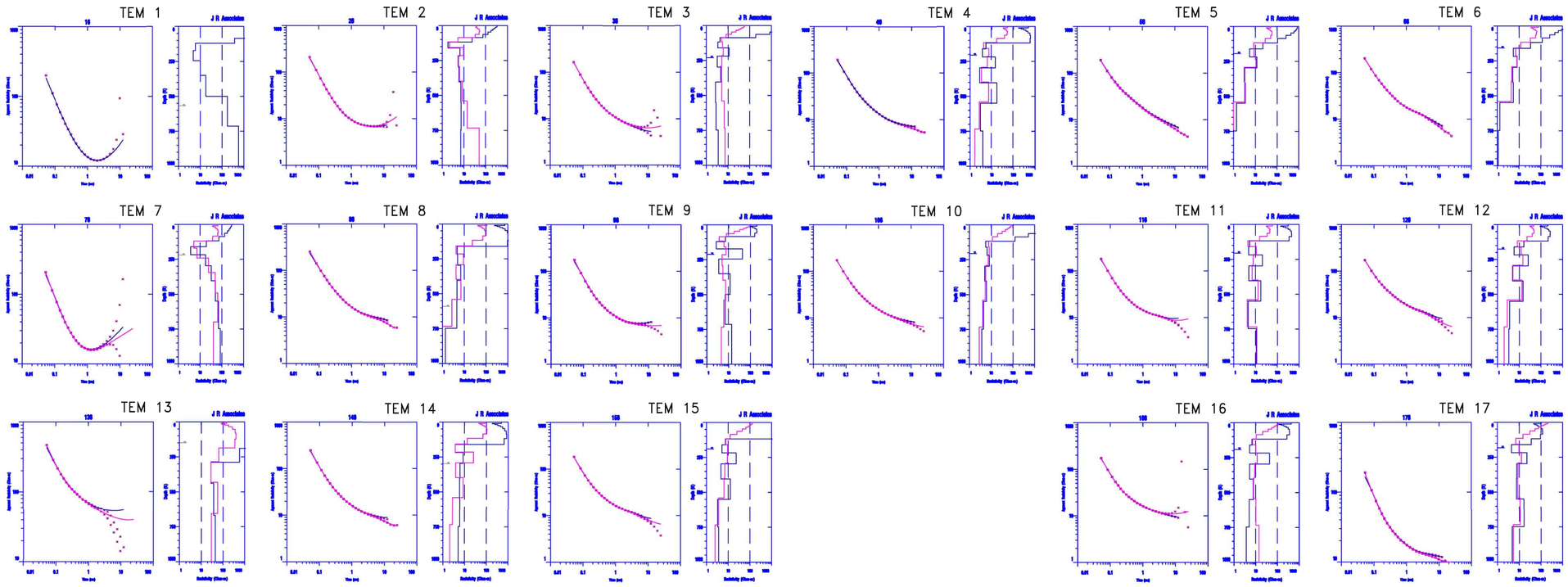


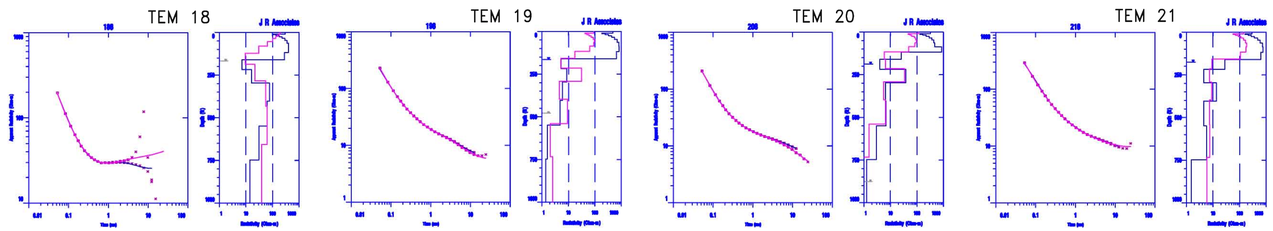
Well Log and TEM Data- Solar Millennium Project
Northwest of the Blythe Airport
Riverside County, California

See Diagrams		DRAWN BY: J.J.R.
7-20-2010	JOB NUMBER: 120-275-10	REVISED:

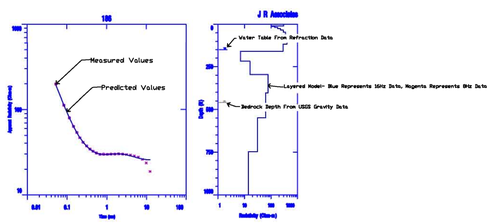
J R ASSOCIATES Civil and Environmental Geophysics
1886 Emory Street, San Jose, CA (408) 293-7390

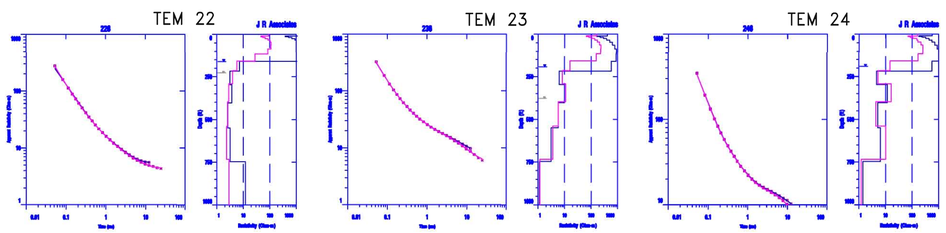
DRAWING NUMBER: 6





EXPLANATION:



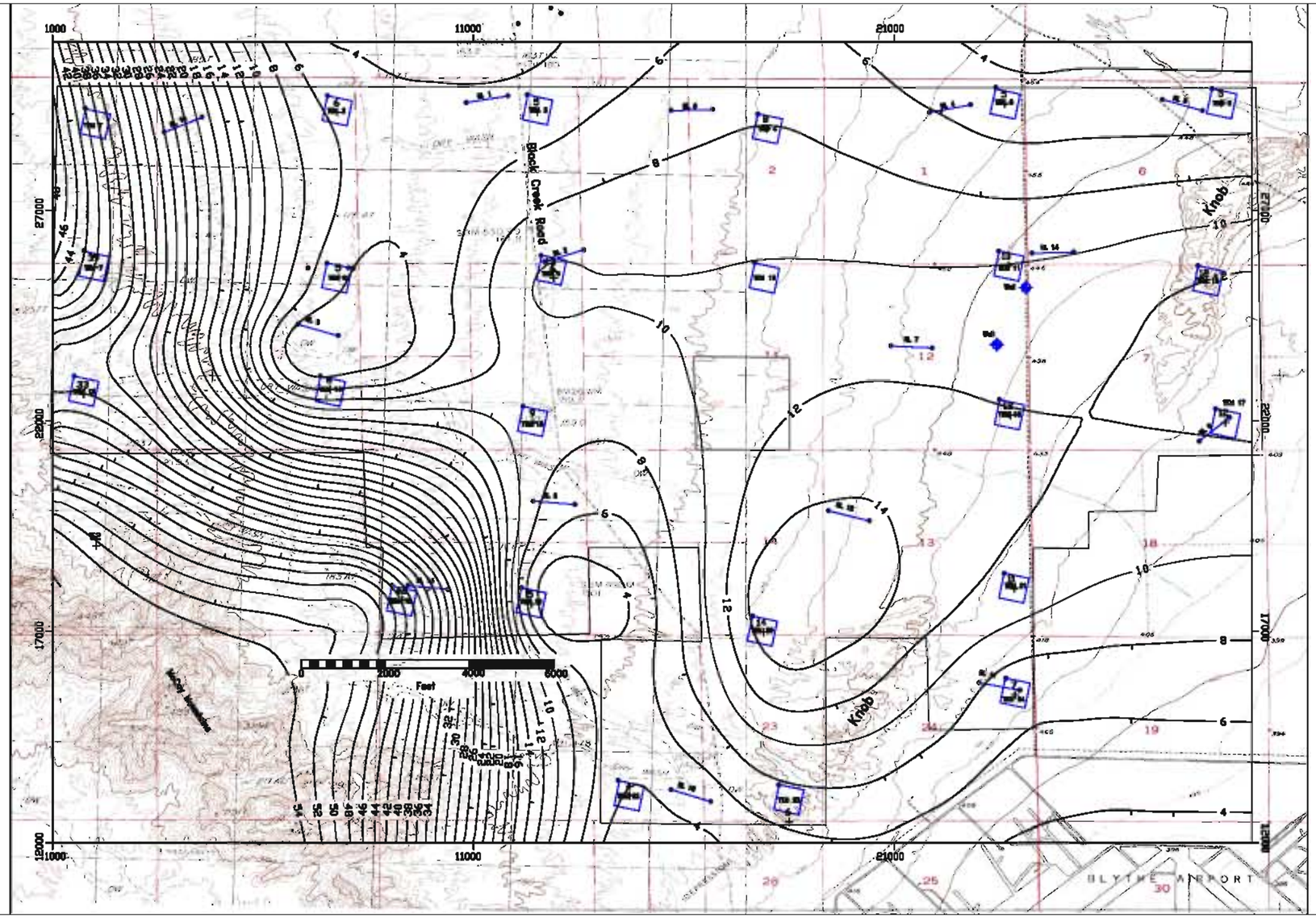


8Hz & 16Hz TEM Results- Solar Millennium Project
Northwest of the Blythe Airport
Riverside County, California

SCALE: See Diagrams		DRAWN BY:	J.J.R.
DATE: 7-20-2010	JOB NUMBER: 120-275-10	REVISED:	

J R Associates Civil and Environmental Geophysics
1886 Emory Street, San Jose, CA (408) 293-7390

DRAWING NUMBER: 7



EXPLANATION:

Refraction Line

TEM Sounding

Average Resistivity in Ohm-meters For Depths Between -200' and -700'

2 Ohm-meter Contour Interval

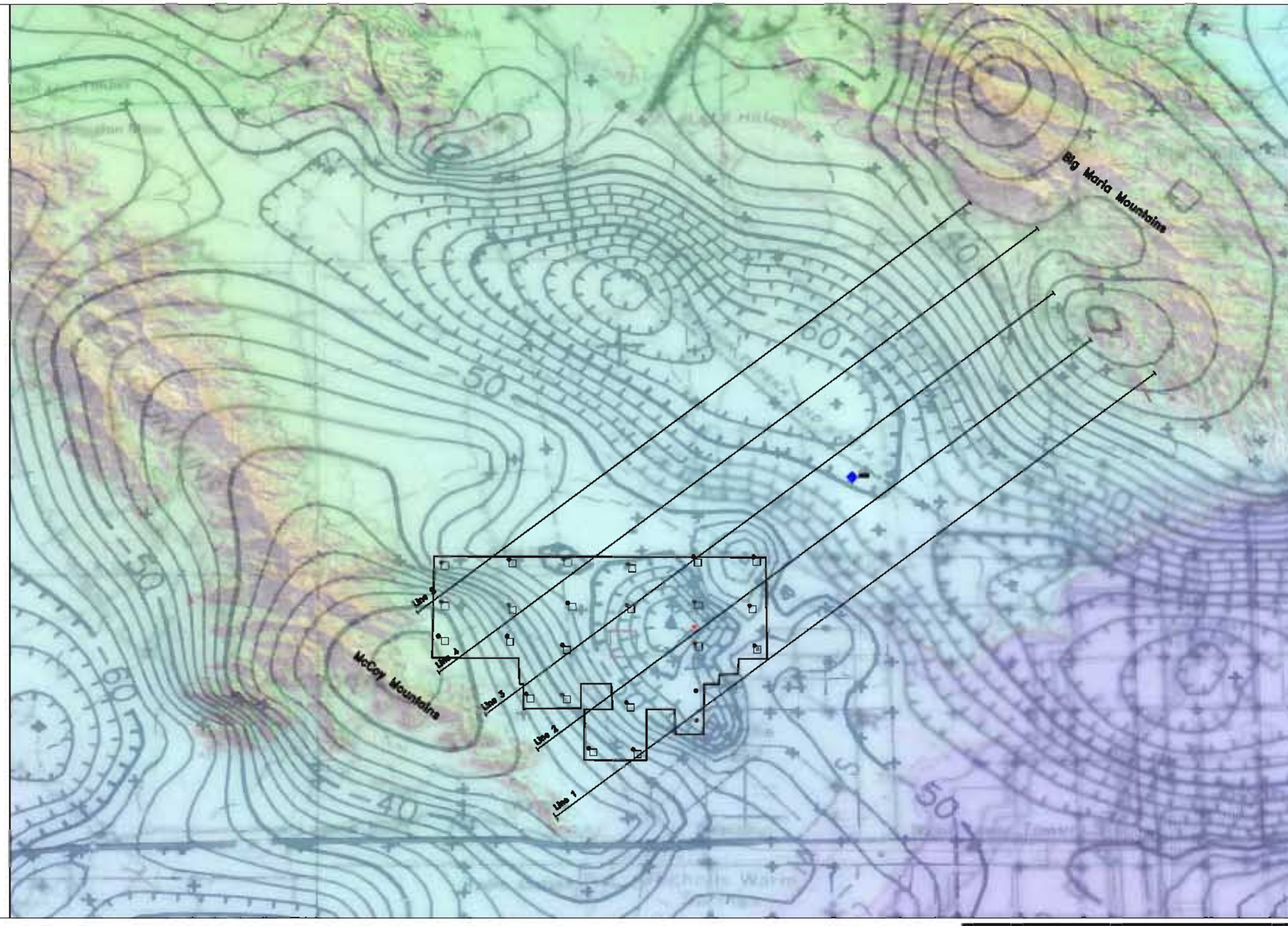
Base contour map obtained from DRG USGS Digital Raster Graphics (MSMAPS.COM) online data base.
Surface elevations obtained from United States Elevation Data (NED) (30m Resolution) online data base.

Resistivity Averages From 16Hz TEM Data- Solar Millennium Project
Northwest of the Blythe Airport
Riverside County, California

SCALE: See Diagram		DRAWN BY:	J.J.R.
DATE: 7-20-2010	JOB NUMBER: 120-275-10	REVISED:	

J R Associates Civil and Environmental Geophysics
1886 Emory Street, San Jose, CA (408) 293-7390

DRAWING NUMBER: 8



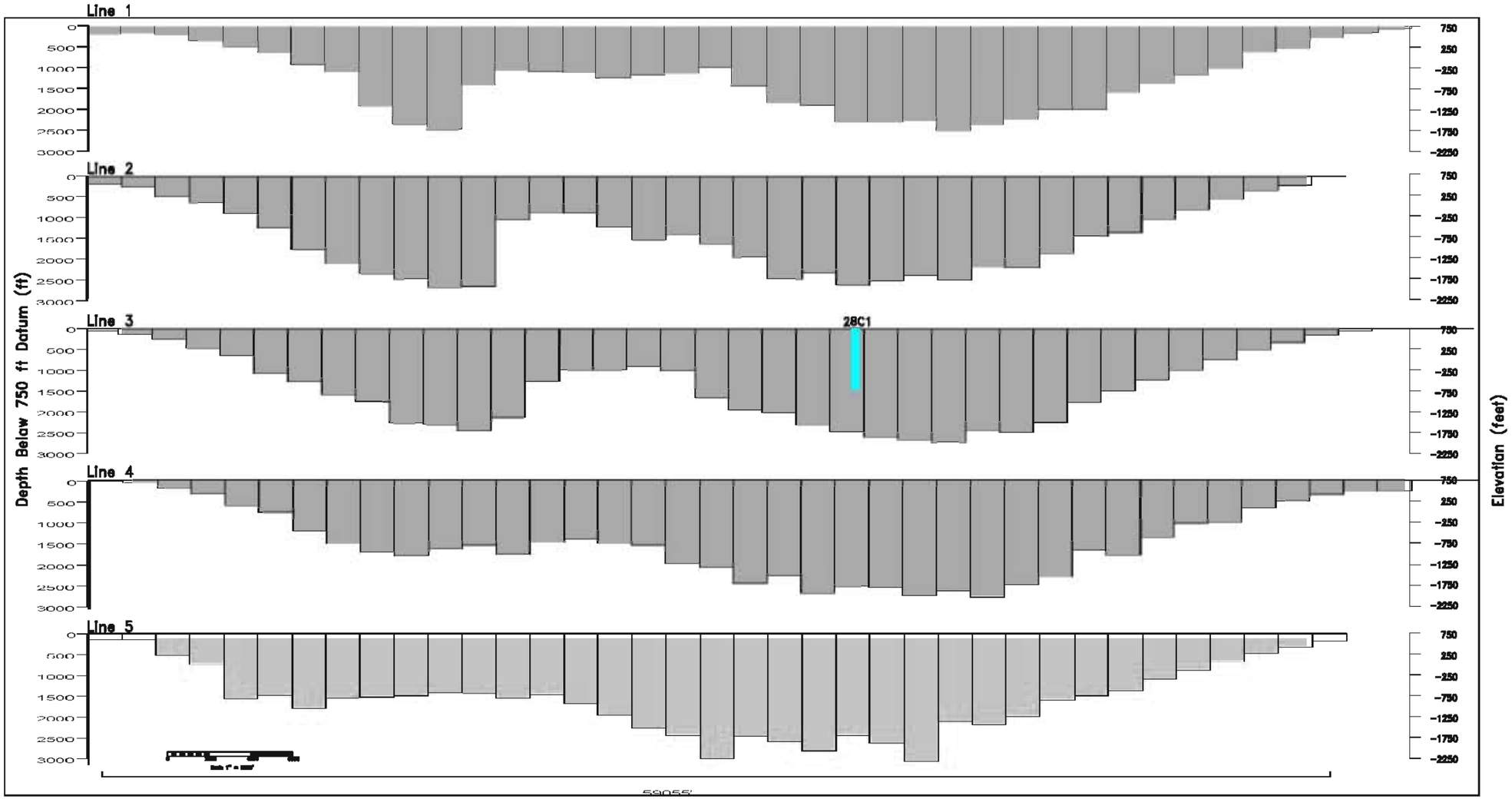
Bouguer residual gravity map obtained from the USGS open file report 86–347.

Bouguer Residual Gravity Map- Solar Millennium Project
Northwest of the Blythe Airport
Riverside County, California

SCALE: See Diagram		DRAWN BY:	J.J.R.
DATE: 7-20-2010	JOB NUMBER: 120-275-10	REVISED:	

J R Associates Civil and Environmental Geophysics
1886 Emory Street, San Jose, CA (408) 293-7390

DRAWING NUMBER: 9



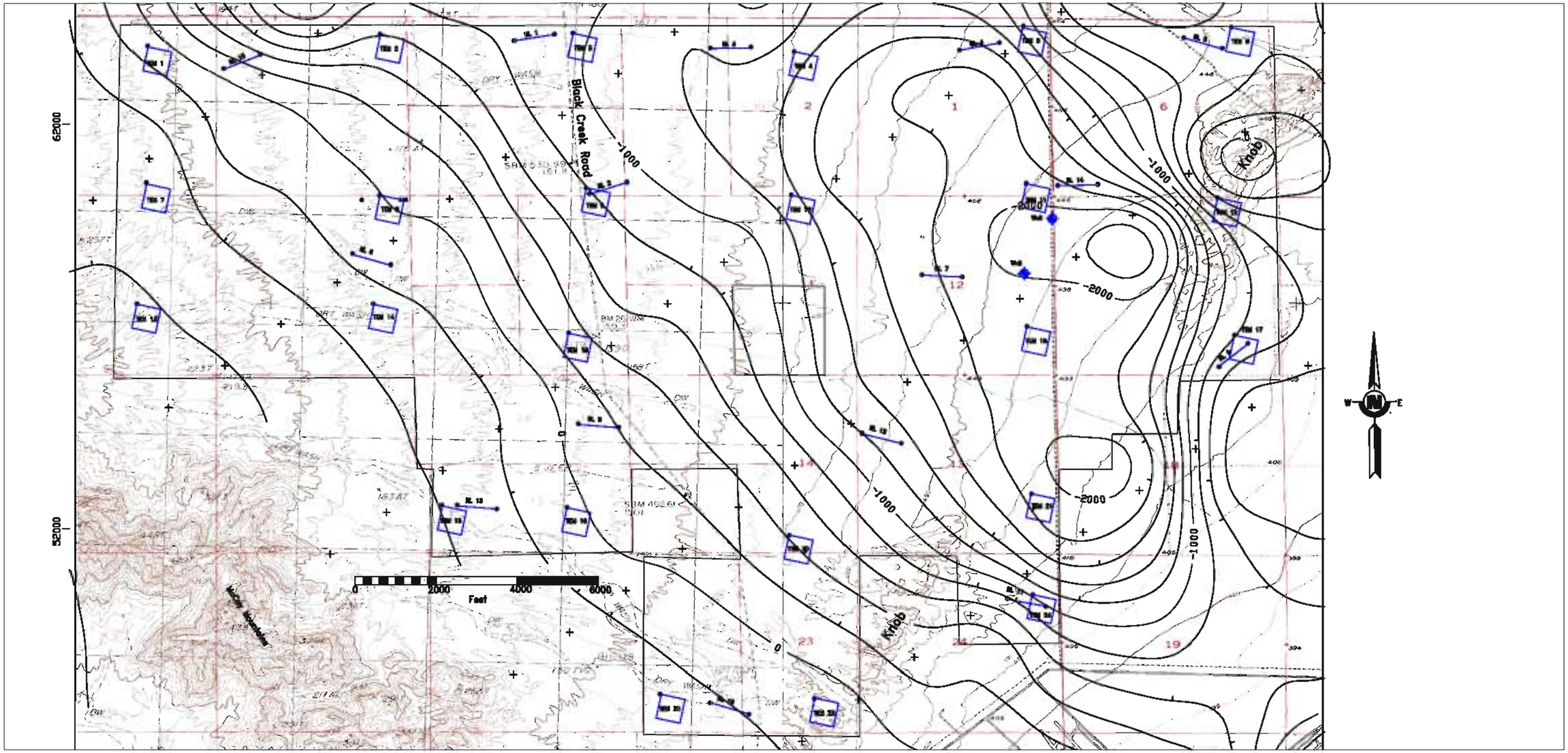
Note: Profiles obtained from an inversion of Bouguer residual gravity data obtained from the USGS open file report 86–347.

Bedrock Depths From Gravity Data Solar Millennium Project
Northwest of the Blythe Airport
Riverside County, CA

SCALE: See Diagrams		DRAWN BY:	J.J.R.
DATE: 7-10-2010	JOB NUMBER: 120-275-10	REVISED:	

J R Associates Civil and Environmental Geophysics
1886 Emory Street, San Jose, CA (408) 293-7390

DRAWING NUMBER: 10



EXPLANATION:

Refraction Line

TEM Sounding

200-foot Contour Interval

Base contour map obtained from DRG USGS Digital Raster Graphics (MSMAPS.COM) online data base.
Surface elevations obtained from United States Elevation Data (NED) (30m Resolution) online data base.

Note: Bedrock contours based on existing Bouguer residual gravity data obtained from the USGS open file report 86–347.

Bedrock Elevations- Solar Millennium Project
Northwest of the Blythe Airport
Riverside County, California

SCALE: See Diagram			DRAWN BY: J.J.R.
DATE: 7-20-2010	JOB NUMBER:	120-275-10	REVISED:

J R Associates Civil and Environmental Geophysics
1886 Emory Street, San Jose, CA (408) 293-7390

DRAWING NUMBER: 11

APPENDIX G

ANALYSIS OF THE DEPTH OF BEDROCK IN THE LOWER COLORADO RIVER VALLEY

J R ASSOCIATES

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ANALYSIS OF THE DEPTH TO BEDROCK IN THE LOWER COLORADO RIVER VALLEY RIVERSIDE COUNTY, CALIFORNIA

August 23, 2010

for

AECOM Incorporated
1220 Avenida Acaso
Camarillo, CA 93012

by

James Rezowalli
California Registered Geophysicist, GP-921

TABLE OF CONTENTS

LIST OF ILLUSTRATIONS iii

I INTRODUCTION 1

A. Site Conditions 1

II METHODOLOGY 3

A. USGS Gravity Data 3
B. Digitizing the Data 3
C. Data Inversion 4

III RESULTS 5

A. Inversion Results 5
B. Accuracy and Limitations 5

IV DRAWINGS

LIST OF ILLUSTRATIONS

Drawing 1 Vicinity Map

Drawing 2 Bouguer and Isostatic Residual Gravity Map

Drawing 3 Gravity Profiles

Drawing 4 Depth to Bedrock Contour Map

I INTRODUCTION

This report presents the results of an analysis of the depth to bedrock in the lower Colorado River Valley near Blythe in Riverside County, California. The investigation was performed for AECOM, Incorporated, by J R Associates. The purpose on the investigation was to use existing publicly available gravity data obtained from the United States Geological Survey (USGS) to determine the depth to bedrock. AECOM is evaluating the groundwater resources in the area and the depth to the bedrock beneath the river valley was needed for the evaluation. James Rezowalli, Principal Geophysicist, performed the analysis in August of 2010.

A. Site Conditions

The study area consists of Palo Verde Valley and Parker Valley (Drawing 1). It extends approximately 40 miles to the north and approximately 20 miles to the south of Blythe, California. The Colorado River runs from the north to the south through the middle of the valley. Information regarding the site's geology was obtained from a USGS professional paper regarding the geohydrology of the Blythe area[1]. The geology in the area, in descending order from the surface, consists of younger alluvium, older alluvium, the Bouse Formation, fanglomerate, and consolidated bedrock. The younger alluvium is from the most recent

[1] D.G. Metzger, O.J. Loeltz, and Burdge Irelna, *Geohydrology of the Parker-Blythe-Cibola Area, Arizona and California*, USGS Professional Paper 486-G, 1973.

degradation of the Colorado River. The older alluvium is a result of several broad periods of aggradation and degradation of the Colorado River. The older alluvium consists of moderately consolidated gravel, sand, silt, and clay alluvial fan deposits. The USGS paper divided the older alluvium into five units although the units could not readily be separated. The Bouse Formation is a marine and brackish-water formation that is composed of a basal limestone overlain by interbedded clay, silt, and sand. The Bouse Formation was deposited in an embayment of the Gulf of California. The fanglomerate that underlies the Bouse Formation is composed mainly of cemented sandy gravel that is probably from a nearby source. The bedrock consists of sedimentary, igneous, and metamorphic rocks. The USGS geohydrology study contained depth and other information from wells drilled throughout the area.

II METHODOLOGY

A. USGS Gravity Data

The gravity data we reviewed was from a USGS Open File Report[2] obtained through an online search. The gravity data consisted of seven plates showing contours of the Bouguer gravity anomalies superimposed on USGS topographic maps. The report's gravity data set was compiled from various projects of the USGS. It was supplemented with data from the Defense Mapping Agency Gravity Library. The observed gravity data were reduced to free air gravity anomalies using the Geodetic Reference System 1967 formula for the theoretical value of gravity at sea level. Bouguer, curvature, and terrain corrections at a standard reduction density of 2.67 g/cm3 were added to the free air anomaly at each station to complete the Bouguer gravity anomalies. Drawing 2 shows the gravity anomaly contours in our study area.

B. Digitizing the Data

In order to invert the data, the raster image showing the locations where data were collected and the residual gravity contours had to be converted to a series of evenly spaced data points in a digital format. The first step involved converting the original DjVu browser format into a jpeg image. The jpeg was then rectified to add north and east coordinates. The State Plane Coordinate system, California Zones 6, NAD 83 (feet) was used when adding northing and easting information to the jpeg. Once the coordinate system was added to the gravity map, the residual gravity values were digitized at the original station locations.

---

[2] Bouguer and Isostatic Residual Gravity Maps of the Colorado River region, Including the Kingman, Needles, Salton Sea, and El Centro Quadrangle, USGS Open File Report 86-347.

The left half of Drawing 3 shows the locations of individual stations where gravity readings were obtained from the USGS data. From the drawing it can be seen that data were densely collected in some areas and data were sparsely collected in others. Once the gravity data from the original stations was digitized, the data was extrapolated into 42 evenly spaced west to east profiles and four south to north profiles. The data along the profiles were at one kilometer intervals and the profiles were three kilometers apart (Drawing 3, right side).

C. Data Inversion

Once the data were in an evenly spaced digital format, we inverted the data using the program GravMod V3.1 developed at Lancaster University in the UK. For the inversion we assumed a two-layer model of alluvium over bedrock. The younger and older alluvium, the Bouse Formation, and the fanglomerate were considered as the alluvial layer. We also assumed the bedrock outcrops near the base of the mountains, a density difference of 700 kg/m3 between the alluvium and bedrock, and that the bedrock would be as deep or deeper than the deepest wells drilled in the area. The well depths were obtained from the USGS professional paper regarding the geohydrology of the Blythe area.

III RESULTS

A. Inversion Results

Drawing 4 illustrates the results of the inversion of the USGS residual gravity data. The drawing shows contours of the depth to bedrock superimposed on a colored relief map. The inversion indicates the bedrock outcrops at the mountains and reaches a maximum depth of 3426 feet beneath Blythe. The average depth was 674 feet beneath the ground surface.

B. Accuracy and Limitations

There is little information regarding the depth to bedrock in the study area to compare the inversion results with. Bedrock outcrops occur at the base of the mountains but we found only a few well logs where bedrock was noted. Drawing 4 includes the locations and depths of fourteen deep wells for which we have partial information. Table 1 lists the wells' identification, the formation found at the bottom of the well if available, the wells' depth, and the calculated depth to bedrock. The table also includes the percent difference between the depth to bedrock noted in a well's log (or the well's total depth if bedrock was not reached) and calculated depth to bedrock. If the well did not reach bedrock and the calculated bedrock was deeper than the well then no difference was noted.

Table 1. Well data from the USGS hydrological study.

Well ID	Deepest noted Formation	Well Depth	Bedrock Depth	Difference
15b2	Fanglomerate	1386'	1250'	10%
1a1	---	685'	1380'	--
5ddd	Fanglomerate	520'	350'	33%
1dbc2	Fanglomerate	400'	430'	--
5bba	Sedimentary Bedrock	800'	1420'	-55%
29baa	Fanglomerate	763'	600'	21%

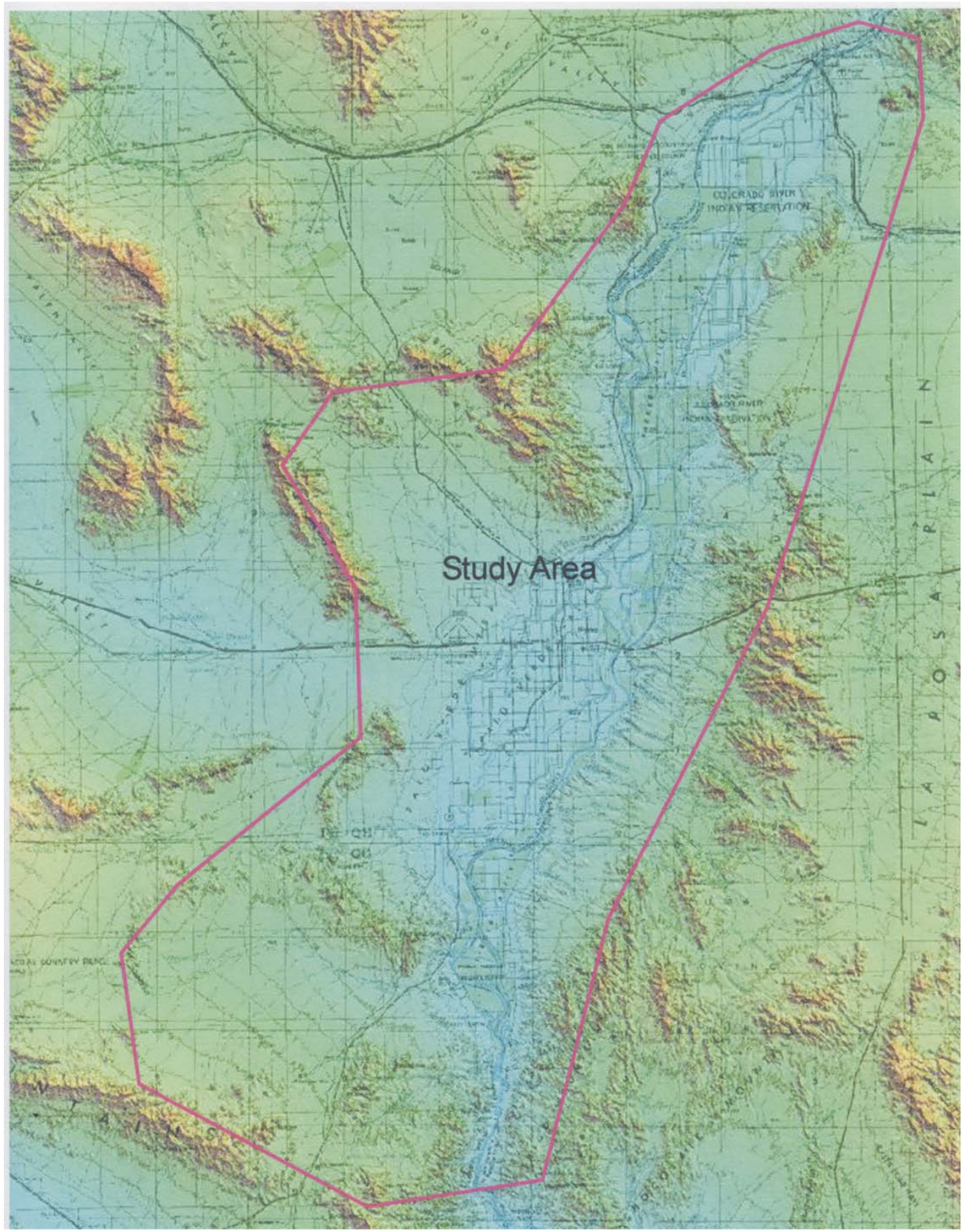
Table 1 (continued). Well data from the USGS hydrological study.

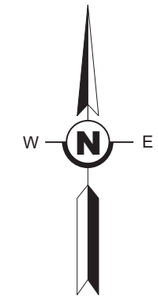
Well ID	Deepest noted Formation	Well Depth	Bedrock Depth	Difference
31aaa	Sedimentary Bedrock	903'	1310'	-45%
28c1	Bouse	1118'	2400'	--
32e1	Bouse	725'	1650'	--
15bcc	---	600'	1380'	--
14h1	Fanglomerate	1368'	1400'	--
13a1	Bouse	800'	800'	--
16bba	Fanglomerate	998'	880'	20%
28abb	---	1009'	-2000'	--

At most of the wells the calculated depth to bedrock was deeper than the well, as would be expected. At six of the wells the bedrock was either too shallow or too deep when compared to the deepest formation noted in the wells' logs. When compared to the information from the six well logs, the calculated depths to bedrock ranged from 33% too shallow to 55% too deep. The average difference was 31%.

The differences between the well logs and the calculated depths to bedrock arose from limitations in gravity surveys. The two main limitations are the limited knowledge of formation densities and extrapolation of data into areas with sparse gravity information. We assumed one density for the overlying alluvium and another for the underlying bedrock when making the depth calculations. The density of geologic materials is more complex than this. In alluvium density can change with grain types, size, angularity, and with saturation and induration. In bedrock density can change with rock types. metamorphic activity, and weathering. Densities also will change across intrusions like dikes or sills. In some areas the USGS gravity data were sparse and the data had to be extrapolated over large distances. This was particularly problematic near the base of the mountains where bedrock outcropped and the extrapolated residual gravity values were used to calibrate the gravity inversion. Based on the available well data we estimate that the accuracy of the calculated depths is ±31% of the true depth on average and could be off up to ±55% at any particular location. These estimates should be adjusted if more data become available.

IV DRAWINGS



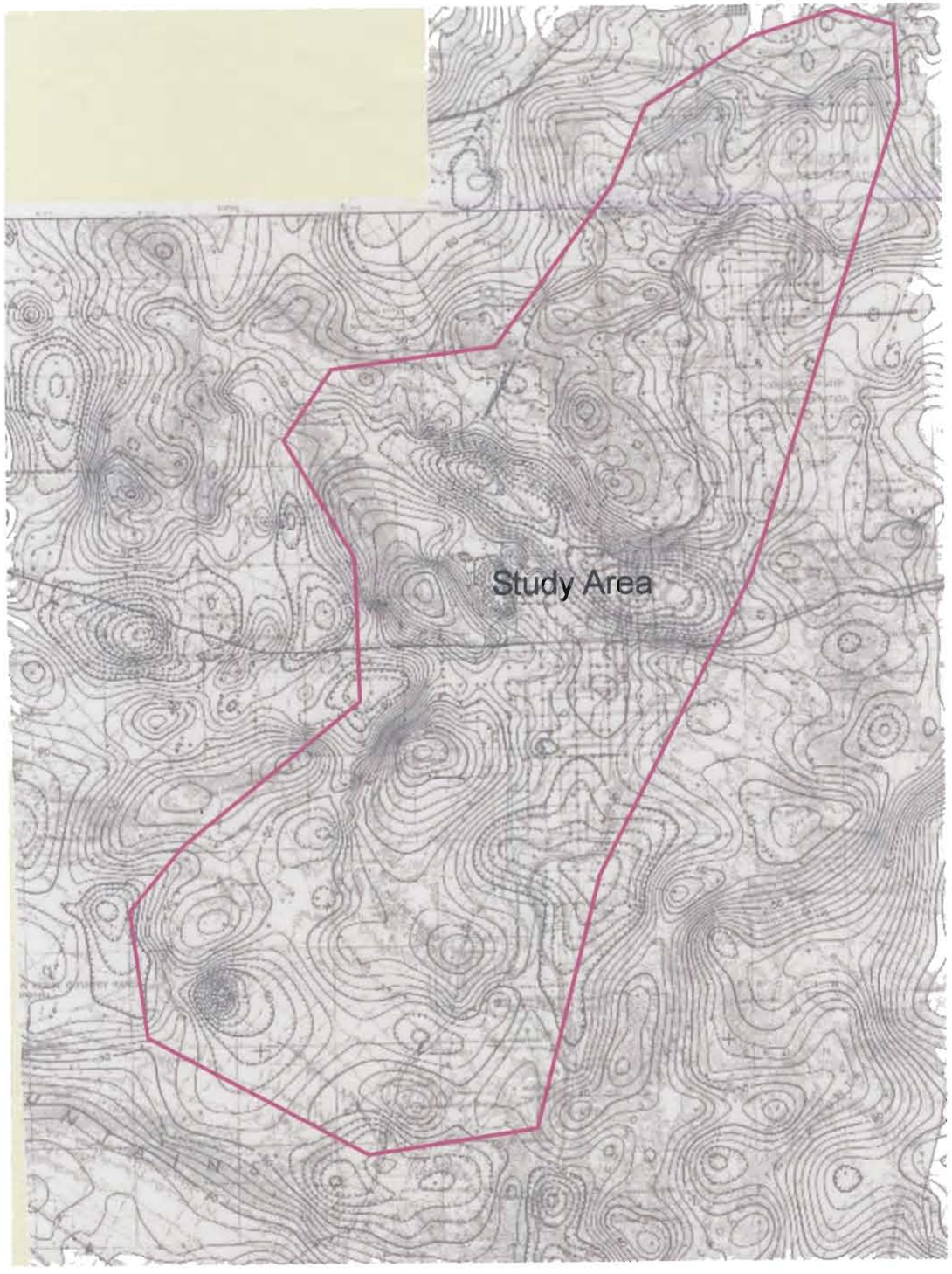


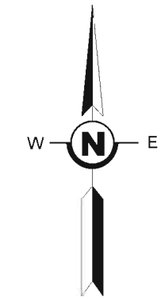
Vicinity Map- Gravity Data Review
Lower Colorado River Valley
Riverside County, California

SCALE:	No Scale		DRAWN BY: J.J.R.
DATE:	8-20-2010	JOB NUMBER: 125-275-10	REVISED:

J R ASSOCIATES Civil and Environmental Geophysics
1886 Emory Street, San Jose, CA (408) 293-7390

DRAWING NUMBER: 1





Bouguer and isostatic residual gravity map obtained from USGS open file report 86-347 sheets 4 and 5. See report for details,

Bouguer and Isostatic Residual Gravity Map- Gravity Data Review
Lower Colorado River Valley
Riverside County, California

SCALE:	No Scale		DRAWN BY: J.J.R.
DATE:	8-20-2010	JOB NUMBER: 125-275-10	REVISED:

J R ASSOCIATES Civil and Environmental Geophysics
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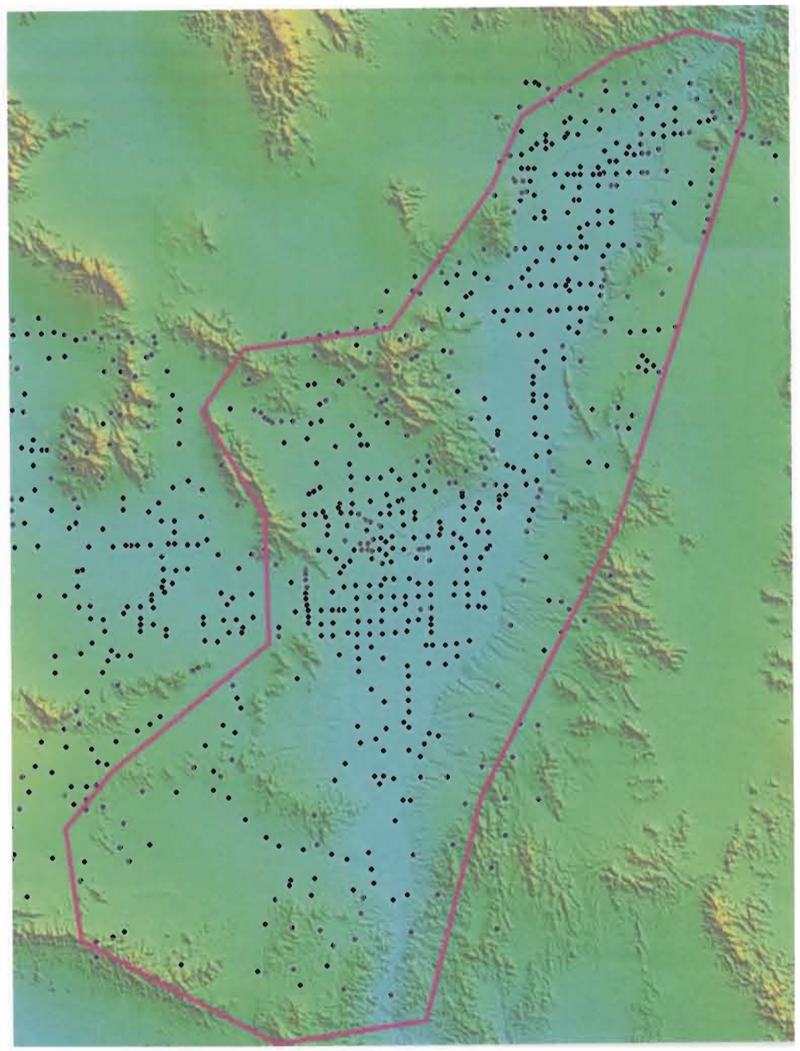
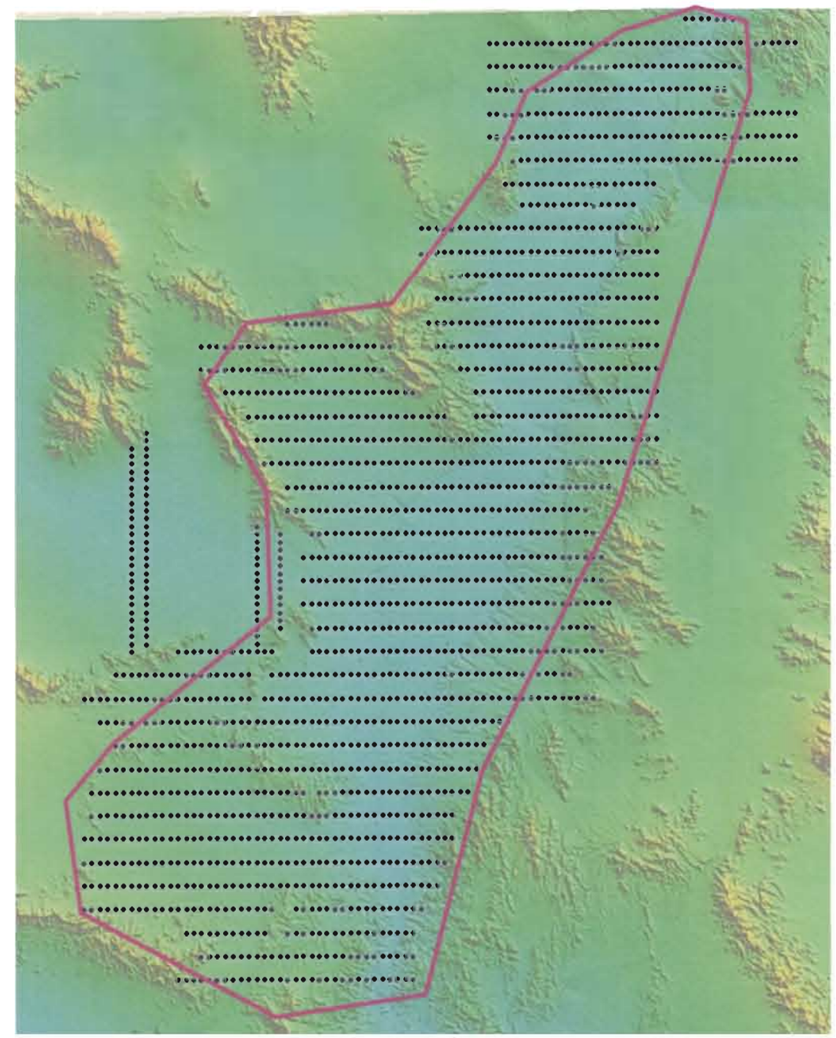
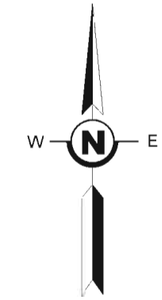
DRAWING NUMBER: 2

Original Observed Gravity Stations



Extrapolated Gravity Profiles





Gravity Profiles- Gravity Data Review
Lower Colorado River Valley
Riverside County, California

SCALE:	No Scale		DRAWN BY: J.J.R.
DATE:	8-20-2010	JOB NUMBER: 125-275-10	REVISED:

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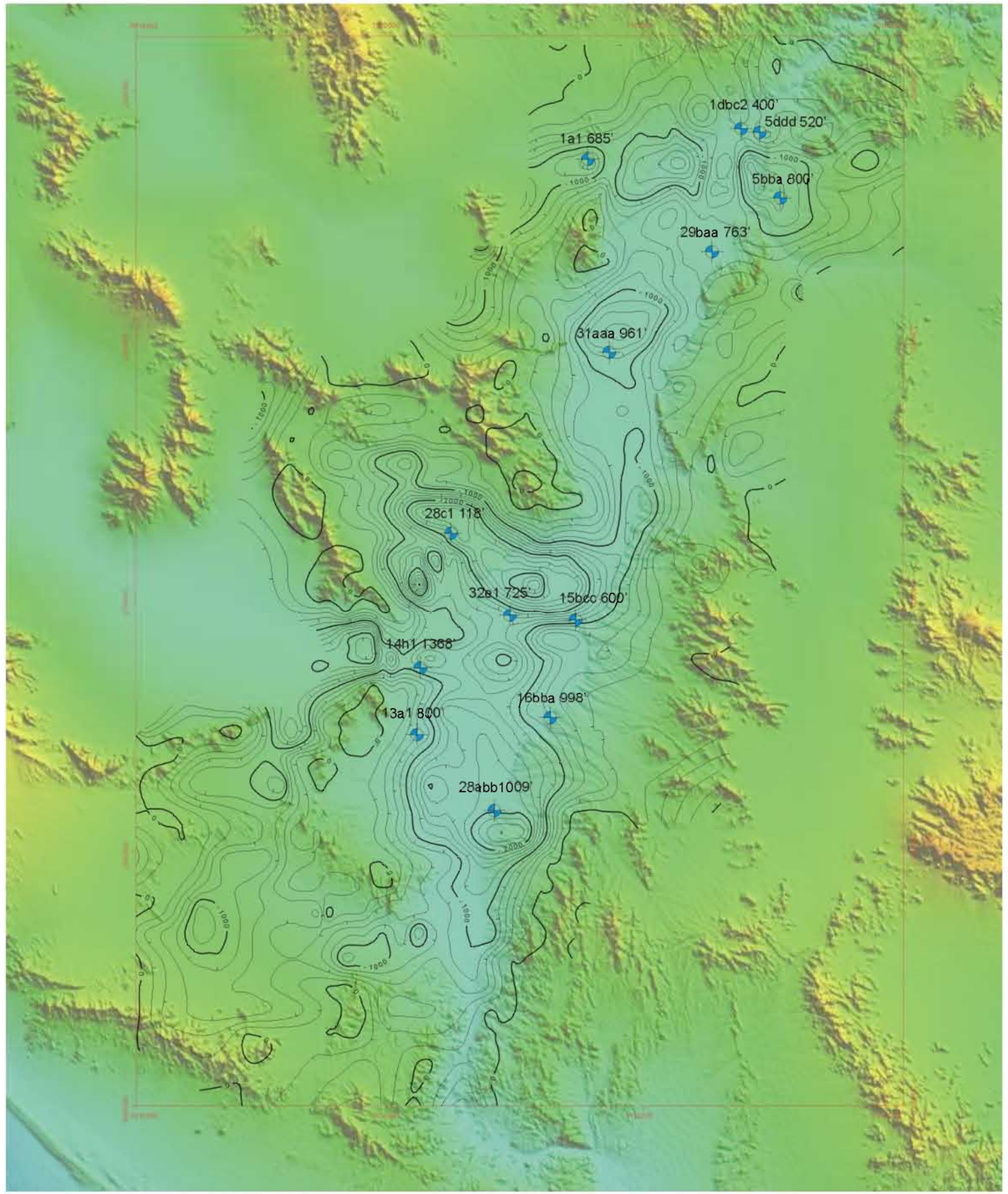
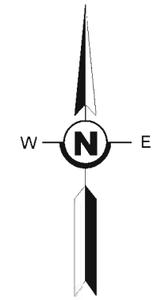
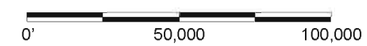
DRAWING NUMBER: 3







Horizontal Scale in Feet

Major Contours Every 100'
Minor Contours Every 200'

16bba 998'

Well With ID and Depth

Depth to Bedrock Contour Map- Gravity Data Review
Lower Colorado River Valley
Riverside County, California

SCALE:	See Diagram,		DRAWN BY: J.J.R.
DATE:	8-20-2010	JOB NUMBER: 125-275-10	REVISED:

J R ASSOCIATES Civil and Environmental Geophysics
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DRAWING NUMBER: 4

APPENDIX H

ELECTRONIC GROUNDWATER MODELING FILES (CD)