SECTION 3

Project Description

The site is located in the Southern California inland desert, approximately 10 miles east of Desert Center, eastern Riverside County, California. See Site Vicinity Map Figure 1 (all figures are included in Attachment F). The Project will be located on approximately 3,794 acres of Federal land, Bureau of Land Management (BLM) ROW # CACA 48810, in Townships 5 and 6 South, Range 17 East.

PSEGS will be comprised of two adjacent solar fields and associated facilities with a total combined nominal output of approximately 500 megawatt (MW). PSH proposes to develop PSEGS in two operational phases: each phase will consist of one solar field with approximately 85,000 heliostats, a 750 foot tall solar power tower and receiver, and a power block able to generate approximately 250 MW of electricity. Each phase will also share common facilities, including an approximately 15-acre common facilities area located in the southwestern corner of the site containing an administration building, warehouse, asphalt-paved parking area, two double-lined (with high-density polyethylene) 2-acre evaporation ponds, maintenance complex and a meter/valve station for incoming natural gas service to the site; an on-site switchyard; and a single-circuit 230 kilovolt (kV) generation tie-line to deliver power to the electricity grid. The common facilities area will be used as a temporary laydown area during construction. Other on-site facilities will include access and maintenance roads (either dirt, gravel or paved), perimeter fencing, tortoise fencing and other ancillary security facilities.

An additional 40-acre temporary construction laydown area will be located north and west of the common facilities area. This area will be used for equipment laydown, construction parking, construction trailers, a tire cleaning station, heliostat assembly, a temporary concrete batch plant and other construction support facilities. The surface areas within the temporary construction area that are used frequently will be stabilized and dust suppression maximized with a layer of crushed stone in areas subject to heavy daily traffic.

Southern California Gas (SoCal Gas) will upgrade and extend an existing distribution line from its main transmission gas pipeline located approximately 1.8 miles west and south of the site. The existing distribution facilities will be upgraded from a 4 inch pipeline to an 8 inch pipeline. Additionally, SoCal Gas will permit and construct a new 8 inch gas pipeline extension from the current retail meter point to the new PSEGS meter to be located within the common area. Construction activities related to the on-site metering station and metering sets will include grading a pad and installing above- and belowground gas piping, metering equipment, gas conditioning and pressure regulation equipment, and possibly pigging facilities. A distribution power line for metering station operation lighting, communication equipment, and perimeter chain link fencing for security will also be installed.

Figure 2 shows the overall facility boundaries of the Project including linear features. Figure 3 shows the acreage estimates of the various Project features. Figure 4 shows the Overall Site Plan.

3.1 Project Elements

3.1.1 Solar Plants

Each solar field will have a heliostat array consisting of approximately 85,000 heliostats. The heliostat arrays will be arranged around a single centralized solar power tower. The heliostats will automatically track the sun during the day and reflect the solar energy to the solar receiver steam generator located on top of the solar power tower. Each solar plant will include a power block, which will be connected via underground and overhead generation tie lines to the on-site switchyard in the northern most portion of the site. Each power block will also have a gas metering set. PSEGS will interconnect to the regional transmission grid at Southern California Edison's Red Bluff Substation which is currently under construction.

Permanent parking areas will be provided at each power block for operations and maintenance personnel.

3.1.2 Common Facilities Area

A 15-acre common facilities area will be established in the southwestern corner of the site to accommodate an administration building, warehouse, and maintenance complex; evaporation ponds;asphalt-paved visitor and employee parking area; and landscape areas. The administration complex will occupy approximately 4.8 acres and will be served by power from the local 33-kV distribution system and water from water supply wells located in the common area.

An additional 40-acre temporary construction laydown area will be located north and west of the common facilities area. This area will be used for equipment laydown, construction parking, construction trailers, a tire cleaning station, heliostat assembly, a temporary concrete batch plant and other construction support facilities. The surface areas within the common area that are used for construction will be stabilized and dust suppression maximized with a layer of crushed stone in areas subject to heavy daily traffic.

3.1.3 Access Roads and Drive Zones

Primary access to the site during construction will be by a new1,000-foot, 24-foot wide paved road from Corn Springs Road. The access road will be constructed from a point just north of the I-10 Corn Springs Road entrance/exit ramps east to the Project site entrance. This road will include a 12-foot wide shoulder with gravel surface for truck staging to preclude traffic interferences.

The Project will contain internal roadway and utility corridors for each heliostat field and power block. Each solar plant site will be accessible from a 20-foot-wide paved or hardscape access road from the entrance of the Project site to the power block, and then around the power block.

In addition to the paved or hardscaped access road to the power block of each unit, 12- foot wide unpaved roads will radiate from the power block to provide access through the solar field to the internal perimeter access road. Within the heliostat fields, 10-foot wide "drive zones" will be located concentrically in the field to provide access to the heliostat mirrors for maintenance and cleaning. The drive zones will be located approximately 152 feet apart and will be grubbed to remove vegetation and smoothed.

A 12-foot-wide unpaved path offset from the site fence by 5 feet will be constructed on the inside perimeter of the Project boundary fence for use by PSEGS personnel to monitor and maintain perimeter security and tortoise exclusion fencing. These paths will be grubbed, bladed, and smoothed to facilitate safe use with minimal grading where necessary to cross washes.

3.2 Site Features

3.2.1 Climate

The climate in the Chuckwalla Valley is classified as a "low desert," and is characterized by high aridity and low precipitation. The region experiences a wide variation in temperature, with very hot summer months and cold dry winters. Annual precipitation ranges from 0.02 to 0.47 inches per month for a total annual precipitation of just under four inches per year.

Table 1 presents the average monthly precipitation (rainfall) from 1913 to 2008 collected from the Blythe Airport, which is located approximately 32 miles east of the Project site.

TABLE 1
Average Monthly Rainfall (in Inches) near the Project Site (1913 to 2008)

Precipitation	Total	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Average Monthly	3.59	0.47	0.44	0.36	0.16	0.02	0.02	0.24	0.64	0.37	0.27	0.20	0.39

3.2.2 Watercourses

The Project is located in the alluvial-filled basin of the Chuckwalla Valley in eastern Riverside County. Surface water in the Chuckwalla Valley drains from the surrounding mountains toward Palen or Ford Dry Lakes or playas, the topographic low points within the valley.

The major watercourse in the Project area is Corn Springs Wash, which drains approximately 31 square miles of the Chuckwalla Mountains and flows northeast toward the Project site. Stormwater flows and discharge from springs in the Chuckwalla Mountains travels through Corn Springs Wash and adjacent unnamed washes northeastward before being cut off by I-10. Stormwater flows are intercepted by dikes located south of I-10 and conveyed to three box culverts that cut beneath the roadway of I-10, south (upgradient) of the Project site. These structures were constructed during construction of I-10 and are dikes and culverts that re-concentrate the flows back to three discrete discharge points on the north side of I-10. From these discharge points, stormwater flows continue across the Project

site flowing northeast towards Palen Mountains. After crossing the Project site, stormwater flow continues southeastward (downgradient) along the front of the Palen Mountains where they end in Ford Dry Lake.

The westerly culvert near the Corn Springs Road Interchange conveys flows from Corn Springs Wash to the northwest corner of the Site. The two other culverts convey flows to the center and east side of the Project site, respectively. The elevated freeway roadbed prevents flows from crossing into the Project site from any other locations.

Although the culverts concentrate the flood flows, the flat topography of the area north of I-10 causes the flow to spread back out as the flows continue northeastward. Aerial photography, vegetation patterns and the existing erosion rills indicate that the flows maintain a fairly straight path across the Project site towards Ford Dry Lake. After the flow has completely crossed the site, the runoff flows southeast along the front of the Palen Mountains for approximately 10 miles before reaching Ford Dry Lake.

3.2.3 Groundwater

Groundwater in the area of the Project site is contained within the Colorado River Hydrologic Basin Region that covers about 20,000 square miles of southeastern California. As a part of the Colorado River Hydrologic Basin Region, the Chuckwalla Valley Groundwater Basin (Chuckwalla Hydrologic Unit) is divided into four hydrologic subareas or units: Ford, Palen (which includes the Project site), Pinto and Pleasant subareas. Regionally, the ground surface slopes gently downward in a southeast direction at a gradient of less than one percent toward the Palo Verde Valley and the Colorado River. Locally, topography at the Project site is relatively flat with gentle slopes to the northeast. Site grades typically range from 1.8 percent in the central portion of the site to essentially flat in the northeastern portion of the site. Steeper grades are present at isolated sand dunes along the northern portion of the site (T5S R17E- Section 21). Toward the north and central portions of the site, the ground becomes hummocky as it transitions toward the sand dunes at the toe of the Palen Mountains.

Groundwater flows to the east-southeast below the Project site. The depth to groundwater below the site, measured in well 5/17-33N1 on May 22, 2009, was 180 feet below ground surface (bgs). In addition, in 2009 groundwater was encountered within two soil borings at depths of 68 and 73 feet bgs (Kleinfelder, 2009). Groundwater is not anticipated to be encountered during Project construction activities.

3.2.4 Other Critical Areas

The Project disturbance area is relatively undisturbed at present and is dominated by Sonoran creosote brush scrub. Other communities in the disturbance area include desert dry wash woodland, unvegetated ephemeral dry wash, active dunes and stabilized and partially stabilized desert dunes. Harwoods' milkvetch, a California Native Plant Society-listed and BLM-listed species, was the only Federal or State special-status plant species observed within the disturbance area.

Jurisdictional waters delineations indicate that it is unlikely that waters on the site be considered jurisdictional by the U.S. Army Corps of Engineers. However, 256.7 acres of

desert washes are considered State jurisdictional waters under California Department of Fish and Wildlife (CDFW) jurisdiction. Although all the ephemeral washes occurring within the disturbance area flow toward Palen Dry Lake; none directly flow into it, as all washes begin to flow in a dispersed pattern as sheet flow.

The Project site is considered suitable habitat for desert tortoise and Mojave fringe-toed lizard. In addition, Western burrowing owl pairs and associated active burrows have been observed within the disturbance area.

Mitigation (or protective) measures for biological resources, including special-status species that could be affected by Project construction activities, will be taken from existing guidelines developed with the United States Fish and Wildlife and CDFW and those required by the CEC Biological Resources Mitigation Implementation and Monitoring Plan (BRMIMP). The BRMIMP comprehensively describes avoidance, minimization, and mitigation measures, and provides a matrix to document their implementation and monitor their effectiveness.

In addition to preconstruction surveys, qualified biologists will conduct employee environmental awareness training and monitor construction activities in accordance with agency requirements.

3.3 Soils

Soils on site were described as consisting of sandy material and classified as poorly graded sand with silt. Typical fines content in these soils would be expected to be in the range of 5 to 35 percent.

There are three mapped geologic units within the Project limits. These units are dune sand (Qs), alluvium (Qal), and lake deposits (Ql).

Dune sand consists of fine sand and silt that has been deposited as wind-blown deposits. At the Project site the surface deposits are very loose and the buried unit medium dense. Because of the nature of dune sand occurrence, there is the potential for discontinuous buried dune sand deposits throughout the site at any depth.

Alluvium is generally sand and silty sand and ranged from loose to very dense at the site. The alluvium contains gravel and cobbles. In several locations the alluvium is moderately to strongly cemented with calcium carbonate. Alluvium is anticipated to be the dominant material type above the elevation of 423 feet above mean sea level and interfinger with lake deposits at lower elevations.

Lake deposits (mixtures of silts, clays, and fine sands) are at the ground surface in the northeast part of the site (Kleinfelder 2009).

3.3.1 Historical Use

A Phase I Environmental Site Assessment for the Project area (AECOM, 2009a) concluded that no recognized environmental conditions were associated with the Project site.

3.4 Drainage

3.4.1 Preconstruction

The major watercourse in the Project area is Corn Springs Wash, which drains approximately 31 square miles of the Chuckwalla Mountains and flows northeast toward the Project site. Stormwater flows and discharge from springs in the Chuckwalla Mountains travels through Corn Springs Wash and adjacent unnamed washes northeastward before being cut off by I-10. Stormwater flows are intercepted by dikes located south of I-10 and conveyed to three box culverts that cut beneath the roadway of I-10, south (upgradient) of the Project site. These structures were constructed during construction of I-10 and are dikes and culverts that re-concentrate the flows back to three discrete discharge points on the north side of I-10. The westerly culvert near the Corn Springs Road Interchange conveys flows from Corn Springs Wash to the northwest corner of the Site. The two other culverts convey flows to the center and east side of the Project site, respectively. The elevated freeway roadbed prevents flows from crossing into the Project site from any other locations. Although the culverts concentrate the flood flows, the flat topography of the area north of I-10 causes the flow to spread back out as the flows continue northeastward. From these discharge points, surface water flows in a northeasterly direction across the Project site then turns southeast and east along the toe of the Palen Mountains for approximately 10 miles before reaching Ford Dry Lake. There are no perennial streams in the Chuckwalla Valley.

Preconstruction Project site topography, drainage at the Project site, and site hydrology calculations are provided in Attachment G.

3.4.2 During Construction

Protection of soil resources will be an important factor in the design of the erosion and sedimentation controls. To minimize wind and water erosion, open spaces will be preserved and left undisturbed, maintaining existing vegetation to the extent possible with respect to site topography and access requirements.

During construction, portions of the Project site, including portions along the ephemeral washes on the site, will be graded. Grading is not intended to level the site, but rather to prepare the site for installation of the heliostats and ease future maintenance activities. As such, the existing depressions for the drainages will remain, and natural drainage waters are expected to continue to occupy these ephemeral washes. Any grading required will be designed to promote sheet flow where possible.

If needed, stone filters and check dams will be strategically placed throughout the Project site to provide areas for sediment deposition and to promote the sheet flow of stormwater prior to leaving the Project site boundary. Where available, native materials (rock and gravel) will be used for the construction of the stone filter and check dams. Diversion berms will be used to redirect stormwater around critical facilities, as required. Periodic maintenance will be conducted as required after major storm events and when the volume of material behind the check dams exceeds 50 percent of the original volume. Stone filters and check dams are not intended to alter drainage patterns but to minimize soil erosion and promote sheet flow.

Areas compacted during construction activities will be restored, as appropriate, to approximate preconstruction compaction levels to minimize the opportunity for any increase in surface runoff.

3.4.3 Post-construction

The majority of the Project site will maintain the original grades and natural drainage features and, therefore, will require no added storm drainage control. In limited areas, such as the power blocks, switchyard, heliostat assembly area and administrative areas, the stormwater management system will include diversion channels, bypass channels, or swales to direct run-on flow from up-slope areas and run-off flow through and around each facility. Diversion channels will be designed so that a minimum ground surface slope of 0.5 percent will be provided to allow positive, puddle-free drainage. To reduce erosion, storm drainage channels may be lined with a nonerodible material such as compacted rip-rap, geo-synthetic matting, or engineered vegetation.

Grading and mowing during construction may directly result in a permanent loss of a large portion of the ephemeral drainages that are present due to their shallow depths; however, affected drainages would be expected to reform naturally in this landscape where flow patterns are highly variable, both temporally and spatially.

Paved access roads will be designed to allow stormwater to flow unimpeded across the roadways in order to maintain the existing sheet flow pattern.

The design will be developed for sheet flow for all storm events less than or equal to a 100-year, 24-hour storm event. The Project site is in close proximity to the I-10 Freeway. The stormwater management design for the freeway includes three drainage culverts to allow rain to flow from south to north underneath the freeway. The design of the site encompasses a worst-case conservative approach with respect to stormwater runoff and reflects a situation where some of the runoff south of the freeway will overtop the freeway and run on the site.

Based upon the runoff volume calculated in the post-construction condition (100-Yr storm event), the difference in post-construction runoff volume (13979.2 ac-ft) and existing condition runoff volume (13713.9 ac-ft) is 265.3 ac-ft. This computes to a 1.93 percent difference in runoff between the post-construction and the existing condition. This flow increase is spread out along the northern boundary of the site and is not concentrated in any isolated location. Based on the minor increase in runoff, the development of this site should not have a negative impact on any downstream properties.

Development of the Project will result in an increase of 830 acres of impervious surfaces (21.9 percent of total Project area) for the mirror area, paved roadways, power blocks, parking lots, and buildings.

Post-construction drainage at the Project site and site hydrology calculations are provided in Attachment H.

3.5 Clearing and Grading Narrative

The surface soil grade of each area will be designed to provide the minimum requirements for access of installation equipment and materials during site construction and operations. Most of the natural drainage features will be maintained and any grading required will be designed to promote sheet flow where possible. Advantage of the natural permeability of the alluvium at the site will be utilized by minimizing compaction and decompacting soils where necessary.

Cut and fill for grading will occur from within the site. There will be no borrow sites outside of the Project site. Two hundred thousand (0.2 million) cubic yards of cut and fill is planned for the Project.

A preliminary grading plan is depicted on Figures 5a-d.

3.5.1 General Grading and Leveling

Heavy to medium grading will be performed within each plant's solar power tower and power block areas, for the switchyard, within the administration complex area, and for the heliostat assembly area. The deepest excavations will be restricted to foundations and sumps. Within each of these individual areas, earthwork cuts and fills will be balanced to the greatest degree possible. The earthwork within the power blocks and common area will be excavated and compacted to the recommendations of the associated geotechnical report.

At some washes, limited grading may be required. Surface rocks and boulders will need to be relocated to allow proper installation of heliostats and facilities when they cannot be avoided.

3.5.2 Vegetation Clearing and Cutting

To construct the heliostat array fields located within these sites, some vegetation clearing will occur—but only where necessary to allow for equipment access and stormwater management. In areas where general site grading is not required, vegetation clearing will not occur, except for the drive zones, which will be grubbed, bladed, and smoothed.

An approximate 8- to 12-foot-wide linear swath of vegetation along the entire outer edge of the area to be developed will be cleared and grubbed (but not graded except as required for safe passage of vehicles) to create an internal perimeter path for installation of the tortoise and security fencing.

Vegetation clearing, with leveling or grading limited to arroyo walls, will be performed throughout the sites beneath the heliostats where the existing vegetative cover will not permit access of installation equipment and materials. Other than access roads and drive zones, when necessary, vegetation will be cut with a mower to a height of approximately 12 to 18 inches to allow clearance for heliostat function and at the same time leave the soil surface and root structures intact.

Clearing and grubbing, where shrubs including roots are removed, will be performed for maintenance roads for each solar plant, drive zone paths, the power blocks, in the common area where existing topography must be modified to make suitable parking, building pads and laydown areas; in areas to be graded at the solar plant sites; and to provide access for

installation equipment and materials during construction (areas requiring leveling by grading). For all other areas, existing vegetation (and root systems) will be maintained to anchor the soil and reduce the potential for erosion. Where existing site topography is favorable, the natural drainage features will be maintained.

3.5.3 Common Area

The common area will also be used for temporary construction parking areas, construction trailers, a tire cleaning station, and other construction support facilities. The surface areas within the common area that are used for construction will be stabilized and dust suppression maximized with a layer of crushed stone in areas subject to heavy daily traffic.

3.5.4 Heliostat Field Preparation

Vegetation clearing, grubbing, and contour smoothing in the heliostat fields will occur where necessary to allow for equipment access and stormwater management. In areas where these activities are not required for access or construction, the vegetation will not be removed but will be mowed (if needed) to a height of approximately 12 to 18 inches.

A linear swath of vegetation along the outer edge of each heliostat field will be cleared, grubbed, and smoothed to create a 12-foot wide external perimeter path for installation and maintenance of the tortoise and security fence and associated external perimeter inspection roads.

Grading of the roads will be performed in limited areas to afford safe passage of vehicles. To allow for external roads, the setback area from the property line will be a minimum of 5 between the edge of the roadway and the property line. Additional setbacks may be required for installation of gas and electric utilities. Elsewhere, vegetation will remain but will be cut (when necessary) to a height that will allow clearance for heliostat function while leaving the root structures intact. Occasional cutting of the vegetation will be performed as needed to permit unobstructed heliostat mirror movement.

3.5.4.1 Installation of Heliostats

The heliostats will be installed in two steps. Initially, the support pylons will be installed using vibratory technology to insert the pylons into the ground (pre-augering prior to the installation of the pylon may be required). Depths are not expected to be greater than 12 feet. Then, the heliostat assembly (mirrors, support structure and aiming system) will be mounted on the pylon.

The majority of the Project site will maintain the original grades and natural drainage features, and therefore, construction will require machines that are maneuverable and can negotiate the terrain. The siting of pylons will be guided by global positioning system technology. Pylons will be delivered to their locations by an all-terrain vehicle. Installation of the heliostat assemblies will be accomplished with a rough terrain crane. The crane will be able to mount heliostat assemblies on several pylons before moving to the next location.

3.5.5 Construction of Power Blocks

Project construction will commence with the building of site roads and the installation of temporary construction facilities including office trailers, parking areas, material laydown areas, a concrete batch plant, and a heliostat assembly facility.

The construction of each plant will begin with grading and construction of earthen berms around the power block areas to divert stormwater followed by the excavation and placement of foundations and other underground facilities. Superstructures and equipment will then be placed on the foundations. Major items include the 750-foot-tall solar power tower and solar receiver steam generator construction, the steam turbine-generator (STG) pedestal and STG, and construction of the air-cooled condenser. Once the mechanical equipment is in place, construction will continue with the installation of the piping, electrical equipment, and cables necessary to connect and power the equipment. Upon completion of construction, the checkout, testing, startup and commissioning of the various plant systems will begin resulting in a fully operational solar plant.

3.6 Stormwater Run-on from Off Site Areas

Calculations of stormwater run-on from off site areas and design details are included in Attachment G.

3.7 Construction Site Estimate Summary

Construction site total area:	3,794 acres
Percentage impervious area before construction:	0%
Percentage impervious area after construction:	21.9%

Information on stormwater flow and runoff coefficients is provided in Attachment H.

3.8 Findings of the Construction Site Sediment and Receiving Water Risk Determination

3.8.1 Sediment Risk

EPA's *Stormwater Phase II Final Rule: Construction Rainfall Erosivity Waiver Fact 2012 Sheet 3.1* was used to determine the Project's R value. The SMARTS system was used to obtain the Project site's K and LS values.

Soil erosivity factor (R) = 24.9
Soil erodibility factor (K) = 0.2
Length-slope factor (LS) = 1.2

The rate of sheet and rill erosion is 6.0 tons per acre, which is considered a low sediment risk.

3.8.2 Receiving Water Risk

The SWRCB 2010 Integrated Report (Clean Water Act Section 303(d) List / 305(b) Report) was used to determine the Project's Receiving Water Risk. Ford Dry Lake was not listed on the Section 303(d) list of impaired water bodies.

Ford Dry Lake is a dry lakebed and does not have the designated beneficial uses of "Spawn," "Cold," and "Migratory.

A low risk factor to the receiving water was calculated.

3.8.3 Site Risk Level

The Site Sediment Risk Factor is low.

The Receiving Water Risk is low.

Therefore, the Site Risk Level is 1. This DESCP/SWPPP has been prepared to comply with Risk Level 1 (Attachment C of the General Permit).

3.9 Construction Schedule

Construction on the PSEGS is anticipated to begin immediately after the Fall 2013 Desert Tortoise Survey Window. Construction of PSEGS, from perimeter fencing installation to site preparation and grading to commercial operation, is expected to take place from the fourth quarter of 2013 to commercial operation in June 2016. The first phase of construction would include the generation tie-line and the first solar field/power block. The second phase of construction would begin shortly after start of construction of the first phase and would continue to support the commercial operation dates of both units by the end of June 2016. Construction of the common area facilities would occur concurrently with the construction of the first solar plant.

A more detailed construction schedule that includes the phases of significant grading activities, work near drainages, and BMP implementation will be included by the construction contractor in Attachment I.

3.10 Potential Construction Site Pollutant Sources

Following is a list of construction materials that will be used, or are expected to be used, and activities to be performed that have the potential to contribute pollutants other than sediment to stormwater runoff. These pollutants and potential pathways were considered when developing BMPs in accordance with General Permit requirements to reduce or prevent pollutants in discharges. The list will be reviewed by the construction contractor, once selected, and will be revised as necessary when the final construction materials inventory for the site has been developed.

Materials:

- Vehicle fluids, including oil, grease, petroleum, and coolants
- Asphaltic emulsions
- Cement materials
- Base and sub-base material
- Joint and curing compounds
- Concrete curing compounds
- Paints
- Solvents, thinners, and acids
- BMP materials
- Treated lumber (materials and waste)
- Portland cement concrete (PCC); masonry rubble
- Adhesives
- General litter

Activities:
- The storage, transport, and/or use of materials listed above
- Clearing and grubbing operations
- Grading operations
- Trenching operations
- Boring operations
- Paving operations
- Delivery/transportation operations
- Utility excavation and installation operations
- Foundation/structure construction operations
- Vehicle and equipment cleaning, fueling, and maintenance
- Painting

3.11 Identification of Non-stormwater Discharges

Following is a list of non-stormwater discharges that apply to the site. The list will be reviewed by the construction contractor, once selected, and will be revised as needed. Non-stormwater discharges will be eliminated, controlled, or treated in accordance with General Permit requirements to minimize or eliminate the release of pollutants in stormwater.

Non-stormwater Discharges:
- Wash water
- Sanitary wastes
- Concrete washout water
- Paint wash water
- Drilling slurries and drilling fluids
- Pipe testing water