DOCKET
08-AFC-11
DATE July 31 2009
RECD. July 31 2009

CH2M HILL
2485 Natomas Park Drive
Suite 600
Sacramento, CA 95833-2937
Tel 916.920.0300
Fax 916.920.8463

July 31, 2009

Mr. Rod Jones
Project Manager
California Energy Commission
1516 Ninth Street
Sacramento, CA 95814-5512

Subject: CPV Vaca Station (08-AFC-11)
Response to CEC Staff Data Requests 54 through 57 and 68 through 96

Dear Mr. Jones:

Attached please find one original and 12 copies of CPV Vaca Station, LLC's responses to California Energy Commission Staff Data Requests 54 through 57 and 68 through 96 for the Application for Certification for the CPV Vaca Station Project (08-AFC-11).

If you have any questions about this matter, please contact me at (916) 286-0278 or Sarah Madams at (916) 286-0249.

Sincerely,

CH2M HILL

Douglas M. Davy, Ph.D.
AFC Project Manager

Attachment

cc: A. Welch (CPV)
S. Madams

Application for Certification

Response to CEC Staff Data Requests 54 through 57 and 68 through 96

CPV Vaca Station

Submitted by CPV Vacaville, LLC

Submitted to

California Energy Commission

With Technical Assistance by

CH2MHILL

July 2009

ES122007003SAC

Supplemental Filing

Response to CEC Staff Data Requests 54 through 57 and 68 through 96

In support of the

Application for Certification

for

CPV Vaca Station

Vacaville, California

(08-AFC-11)

Submitted to the:

California Energy Commission

Submitted by:

CPV Vacaville, LLC

CPV Vacaville, LLC

With Technical Assistance by:

CH2MHILL

Sacramento, California

July 2009

Contents

Section Page

Contents iii

Introduction 1

Noise (54–57) 3

Biological Resources (68–74) 11

Soils and Water Resources (75–95) 17

Visual Resources (96) 37

Tables

DR54-1 Summary of Hourly Measurements at Site 1 (dBA)
DR54-2 Summary of Hourly Measurements at Site 2 (dBA)
DR54-3 Summary of Hourly Measurements at Site 3 (dBA)
DR57-1 Distance to Foreseeable Projects
DR72-1 Federally Listed Species
DR72-2 State Listed Species
DR76-1 Mean, Median, Monthly Average High and Low, and Daily Average High and Low Flows for the City of Vacaville's Easterly Wastewater Treatment Plant (January 2006 through December 2008)

Figures

DR54-1 Noise Monitoring Locations
DR54-2 Site 1 Noise Levels (L_{90}) and Wind Speed
DR80-1 Approximate Dilution Ratio of EWTP Effluent in New Alamo Creek Immediately Below Confluence of Old Alamo Creek for Water Years 1998–2006

Attachments

DR69-1 Records of Conversation
DR75-1 Draft Soil Management Plan
DR88-1 Stormwater Calculations
DR88-2 Revised Drainage Plan
DR93-1 Draft Drainage, Erosion, and Sediment Control Plan
DR96-1 Digital Simulations

Introduction

Attached are CPV Vacaville, LLC's (CPV) responses to California Energy Commission (CEC) Staff data requests numbers 54 through 57 and 68 through 96 for the CPV Vaca Station (CPVVS) project (08-AFC-11). The CEC Staff served Data Requests 54 through 57 on May 7, 2009, and CPV requested additional time to respond. Staff served data requests 68 through 96 on June 1, 2009, as part of the discovery process for the CPVVS project.

The responses are grouped by individual discipline or topic area. Within each discipline area, the responses are presented in the same order as CEC Staff presented them and are keyed to the Data Request numbers (54 through 57 and 68 through 96). New or revised graphics or tables are numbered in reference to the Data Request number. For example, the first table used in response to Data Request 15 would be numbered Table DR15-1. The first figure used in response to Data Request 28 would be Figure DR28-1, and so on.

Additional tables, figures, or documents submitted in response to a data request (supporting data, stand-alone documents such as plans, folding graphics, etc.) are found at the end of a discipline-specific section and are not sequentially page-numbered consistently with the remainder of the document, though they may have their own internal page numbering system.

Noise (54–57)

Ambient Noise Survey

54. *Please conduct an ambient noise survey at each of the three residential receptors identified in AFC Section 5.7.2.1 as being located approximately 800 feet to the southeast, 1,900 feet to the north, and 1,600 feet to the east of the project site, near the town of Elmira. These surveys should be conducted during calm weather conditions.*

    a) *The above noise surveys should include measurements of the ambient noise levels at these locations continuously from 10:00 p.m. to 7:00 a.m.*

    b) *These surveys should also include measurements of the ambient noise at these locations during the daytime hours for a period of at least one hour in the late morning and again for a period of at least one hour in the afternoon.*

Response: Noise monitoring was conducted at or near the three residential locations closest to the project. The monitoring locations are depicted in Figure DR54-1.

Larson Davis 824 and Larson Davis 820 ANSI Type 1 (precision), statistical sound level meters were used to conduct the continuous measurements. The sound level meters were field calibrated before and after the measurement with a Larson Davis CAL200 and were factory calibrated within the previous 12 months.

The monitoring data is summarized in Tables DR54-1 through DR54-3. The nighttime levels at Site 1 are generally louder than Sites 2 or 3. This results, in part, from its proximity to the Easterly Wastewater Treatment Plant (EWTP), but it is possible that higher levels of insect and cricket noise also contributed to the levels between 1:00 and 5:00 a.m. Additionally, the 46 dBA level detected at 2:00 a.m. is not wind related.

Other sources of environmental noise include local traffic (including a noticeable number of garbage trucks), trains, and small aircraft (air cargo traffic from Travis Air Force Base was visible but not audible).

TABLE DR54-1
Summary of Hourly Measurements at Site 1 (dBA)

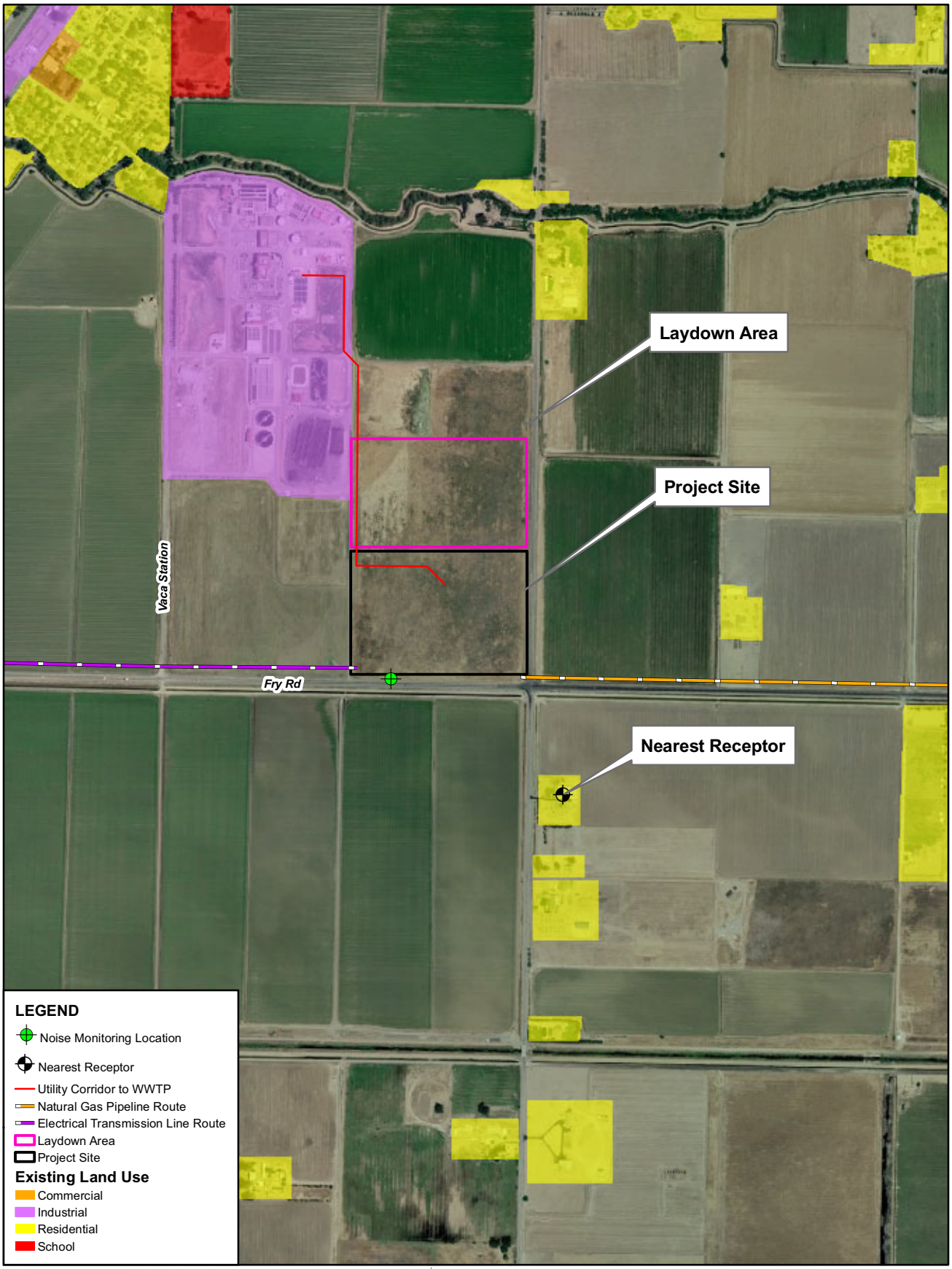
Date and Time	L_{eq}	L_{Min}	L_{Max}	L_{10}	L_{50}	L_{90}
6/2/09 4:00 PM	52	40	74	54	47	43
6/2/09 5:00 PM	47	38	62	49	46	42
6/2/09 6:00 PM	48	39	71	49	45	42
6/2/09 7:00 PM	49	39	68	52	46	43
6/2/09 8:00 PM	53	41	71	55	49	44
6/2/09 9:00 PM	49	40	69	51	46	43
6/2/09 10:00 PM	51	40	73	49	44	42
6/2/09 11:00 PM	46	39	63	47	44	41
6/3/09 12:00 AM	51	39	70	47	43	41

TABLE DR54-1
Summary of Hourly Measurements at Site 1 (dBA)

Date and Time	L_{eq}	L_{Min}	L_{Max}	L_{10}	L_{50}	L_{90}
6/3/09 1:00 AM	51	41	69	53	47	44
6/3/09 2:00 AM	50	42	72	50	48	46
6/3/09 3:00 AM	47	41	55	48	46	44
6/3/09 4:00 AM	47	42	65	48	46	45
6/3/09 5:00 AM	52	39	74	54	47	43
6/3/09 6:00 AM	53	42	73	55	49	46
6/3/09 7:00 AM	50	42	69	51	47	44
6/3/09 8:00 AM	50	40	72	52	46	42
6/3/09 9:00 AM	46	37	69	47	43	39
6/3/09 10:00 AM	45	35	66	46	41	38
6/3/09 11:00 AM	46	34	63	48	42	39
6/3/09 12:00 PM	45	36	60	47	43	40
Nighttime Average (10:00 pm to 7:00 am)	50	41	68	50	46	44

TABLE DR54-2
Summary of Hourly Measurements at Site 2 (dBA)

Date and Time	L_{eq}	L_{Min}	L_{Max}	L_{10}	L_{50}	L_{90}
6/2/09 6:00 PM	48	38	65	50	45	42
6/2/09 7:00 PM	48	40	63	49	45	42
6/2/09 8:00 PM	55	38	71	58	52	41
6/2/09 9:00 PM	57	39	68	58	57	55
6/2/09 10:00 PM	55	38	67	58	55	47
6/2/09 11:00 PM	52	37	63	56	47	40
6/3/09 12:00 AM	51	33	66	55	40	35
6/3/09 1:00 AM	49	36	67	53	44	40
6/3/09 2:00 AM	47	30	69	51	37	32
6/3/09 3:00 AM	43	30	61	47	36	33
6/3/09 4:00 AM	45	31	61	51	38	34
6/3/09 5:00 AM	49	33	68	51	43	37
6/3/09 6:00 AM	54	41	71	58	47	43
6/3/09 7:00 AM	55	40	73	58	49	45
6/3/09 8:00 AM	54	38	70	57	49	41
6/3/09 9:00 AM	51	34	68	53	41	37
6/3/09 10:00 AM	50	33	71	51	41	38
6/3/09 11:00 AM	52	32	73	53	43	38
6/3/09 12:00 PM	52	33	71	53	42	37
6/3/09 1:00 PM	52	34	70	53	42	38
Nighttime Average (10:00 pm to 7:00 am)	51	34	66	53	43	38



N

0 500 1,000
Feet

This map was compiled from various scale source data and maps and is intended for use as only an approximate representation of actual locations.

FIGURE DR54-1
NOISE MONITORING LOCATION

CPV VACA STATION
VACAVILLE, CA

CH2MHILL

SAC \\ZION\SACGIS\PROJ\VACAVILLE_AFC_370668\MAPFILES\NOISEMONITORING.MXD SSCOPES 8/4/2008 11:11:53

TABLE DR54-3
Summary of Hourly Measurements at Site 3 (dBA)

Date and Time	L_{eq}	L_{Min}	L_{Max}	L_{10}	L_{50}	L_{90}
6/2/09 6:00 PM	50	33	65	54	47	39
6/2/09 7:00 PM	51	33	70	54	46	38
6/2/09 8:00 PM	53	34	73	56	47	40
6/2/09 9:00 PM	51	33	73	54	44	36
6/2/09 10:00 PM	51	33	69	54	43	37
6/2/09 11:00 PM	46	33	62	50	40	36
6/3/09 12:00 AM	48	30	65	52	38	34
6/3/09 1:00 AM	49	31	69	51	38	34
6/3/09 2:00 AM	47	31	73	46	38	34
6/3/09 3:00 AM	45	30	66	44	37	32
6/3/09 4:00 AM	50	31	66	55	40	34
6/3/09 5:00 AM	52	34	69	56	48	38
6/3/09 6:00 AM	55	43	73	58	53	47
6/3/09 7:00 AM	54	40	72	57	51	45
6/3/09 8:00 AM	53	39	73	56	50	43
6/3/09 9:00 AM	48	36	66	52	45	39
6/3/09 10:00 AM	45	34	57	48	42	38
6/3/09 11:00 AM	49	33	74	51	43	37
6/3/09 12:00 PM	46	32	60	50	43	36
6/3/09 1:00 PM	47	31	67	50	43	37
6/3/09 2:00 PM	52	33	65	53	43	36
Nighttime Average (10:00 pm to 7:00 am)	50	33	68	52	42	36

Wind speed was monitored at Site 1 in 5-minute increments and is summarized in Figure DR54-2. Measured wind speeds were generally less than 10 miles per hour (mph) and were very low (less than 3 mph) between the hours of 2:00 a.m. and 6:00 a.m. This is consistent with the observation that the winds were decreasing between 1:30 am and 2:30 am to just barely perceptible speeds.

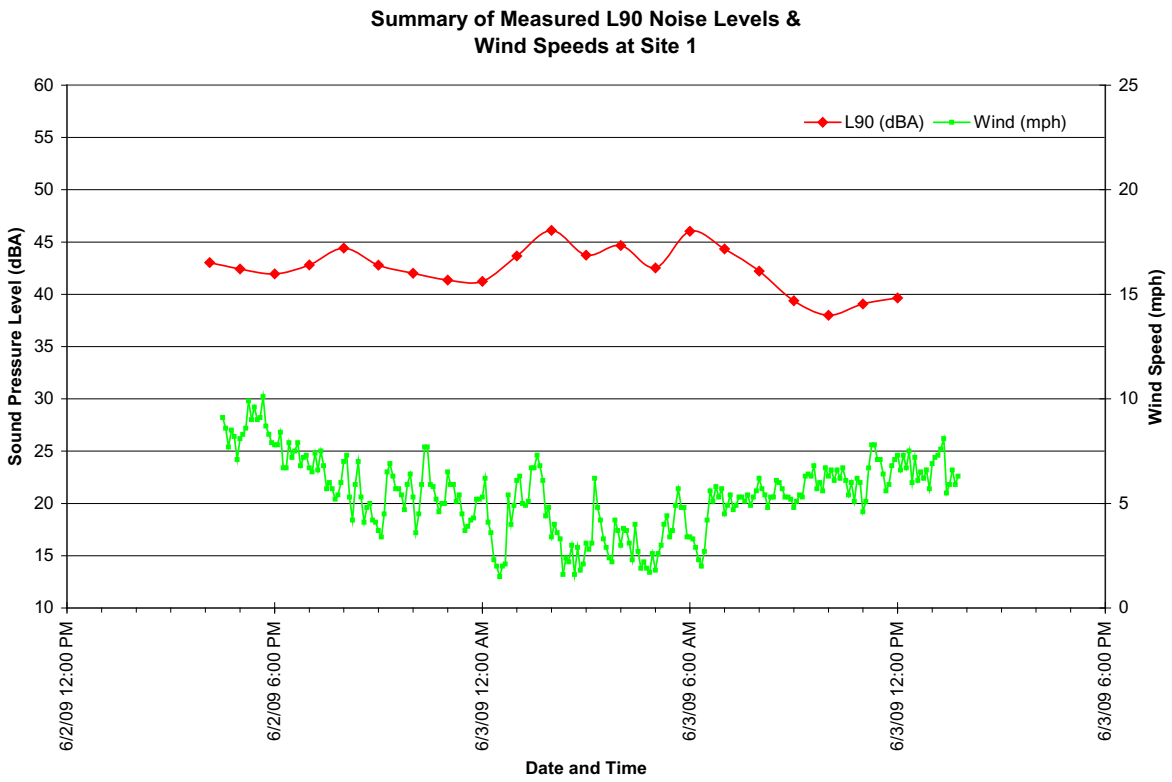


FIGURE DR54-2
Site 1 Noise Levels (L_{90}) and Wind Speed

Survey Noise Level Reporting

55. *Please provide the resultant noise levels in terms of L_{eq}, L_{min}, L_{max}, L_{10}, L_{50}, and L_{90}.*

Response: See response to Data Request #54.

Noise Impacts

56. *Please evaluate the noise impacts of project operation at the receptors identified in AFC Section 5.7.2.1 as being located 1,900 feet to the north and 1,600 feet to the east of the project site, near the town of Elmira. Please provide the results, including the resultant predicted project noise levels at these locations. This evaluation should consider the typical project area ambient conditions, such as the average annual wind speed, wind direction(s), air temperature, and relative humidity.*

Response: The project anticipates incorporating noise control measures to ensure the project noise level does not exceed 44 dBA during the nighttime hours, on average, at any residence as required by state and local laws, ordinances, regulations, and standards (LORS). The effects of wind speed and wind direction, air temperature, and relative humidity on noise and noise transmission and its levels and directionality are highly variable and attempting to model these effects would be speculative. Although generally speaking, wind blowing from a source to receptor would accentuate noise and wind blowing from a receptor to

source would attenuate the noise, wind direction is highly variable in any location, both seasonally and on a daily basis. Standard software used to model power plant noise does not include provisions for modeling ambient air conditions. CPV expects to demonstrate compliance with residential and other LORS.

Cumulative Impacts

57. *Please describe the distances between these foreseeable projects [for cumulative impacts analysis] and the CPV Vaca Station project site.*

Response: As identified in Appendix 5.6A of the AFC, 22 residential subdivision applications have been filed with the City of Vacaville. Table DR57-1, identifies these subdivisions and the distance to the CPVVS site.

TABLE DR57-1
Distance to Foreseeable Projects

Project Name	Site Address	Distance to CPVVS (miles)
Amber Hills	East of Browns Valley Road/McMurtry Lane Intersection	5.6
Brighton Landing	SE Elmira/Leisure Town Road	1.9
Reynolds Ranch	NW of Browns Valley Road/N of McMurtry Road	5.6
Hillview Ranch	Southwest corner of Browns Valley Road/McMurtry Lane	5.6
Ivywood	201 Beard St	4.4
Knoll Creek	West side of Browns Valley Road, South of McMurtry Lane	5.6
Lagoon Valley	E of I-80/S of Lagoon Valley Road	6.2
Meadowood	South side of Fruitvale Avenue, between Stinson Ave and Pintail Drive	5.5
Montessa	1222 California Drive	4.9
North Village	North side of Vaca Valley Parkway between I-505 and Leisure Town Road	4.6
Portofino	West Side of Marshall Road, across from the Three Oaks Community Center	5.0
Portofino Unit 2	West Side of Marshall Road, across from the Three Oaks Community Center	5.0
Rancho Rogelio	7019 Browns Valley Road	5.8
Southtown Commons	East Side Leisure Town Road/South of New Alamo Creek	1.6
Southtown Phase 1	E. of Nut Tree/S. Somerville Drive	2.6
Southtown Phase 1A	West Site of Leisure Town Road/South of New Alamo Creek	1.9
Southtown Phase 2	West Side Vanden Road/South of New Alamo Creek	2.4
Sterling Chateau 2	East side of Ruby Drive, across from Granite Court	3.0
Sterling Chateau 4	SE Corner Alamo/Vanden Road	2.1
Sterling Chateau 5	West side Vanden, North of Southtown	2.1
The Orchards	5790 Vanden Road	2.2
Ventana	NW Corner of Nut Tree Road/Summerfield Dr. Int.	2.6

Biological Resources (68–74)

Acreage of Impacts to Jurisdictional Drainages

68. *Please quantify the acreage of temporary and permanent impacts to each potentially jurisdictional drainage.*

Response: The proposed transmission line towers will avoid drainages, and the natural gas pipeline will be trenched in the shoulder of Fry Road and will be bored beneath culverts. Therefore, there will be no impacts to potentially jurisdictional waters.

Coordination Effort with State Agencies

69. *Please provide an update on coordination efforts with USACE, RWQCB, and CDFG (as applicable) regarding project permits and mitigation for impacts to jurisdictional waters. Provide any supporting documents (letter or record of conversation) that result from communication with these agencies, including impact mitigation, the permits required for the project, the steps the applicant has taken or plans to take, and the schedule for obtaining the permits.*

Response: As described in response to Data Request #68, PG&E will construct in the natural gas line in the shoulder of Fry Road, and will avoid any impact to potentially jurisdictional waters. Therefore permits and mitigation for impacts to potentially jurisdictional waters are not needed. A Record of Conversations with the U.S. Fish and Wildlife Service (USFWS) is provided as Attachment DR69-1.

Acreage for Impacts to Giant Garter Snake Habitat

70. *Please quantify the acreage of temporary and permanent impacts for both upland and aquatic giant garter snake habitat.*

Response: The transmission line towers will avoid drainages and the natural gas pipeline will be trenched in the Fry Road shoulder and will be bored beneath culverts so that there will be no impacts to giant garter snake aquatic habitat. However, one roadside ditch, AD-06 is adjacent to the proposed project site, and is considered giant garter snake upland habitat. Therefore, the project would potentially have a permanent impact on approximately 9.697 acres of giant garter snake upland habitat at the project site. This estimated acreage is conservatively determined by multiplying the length of the ditch potentially impacted by the project (0.4 mile) by the 200-foot-wide distance of the standard giant garter snake upland habitat buffer. A small amount of upland habitat would also be affected by transmission tower bases. Temporary impacts may include the impacts of constructing the natural gas pipeline in Fry Road adjacent to giant garter snake upland habitat. CPV is preparing a Biological Assessment for submittal to USFWS that will address these effects in detail.

Agency Proposed Mitigation

71. *Please provide an update on coordination efforts with USFWS and CDFG regarding required project permits or agency proposed mitigation for impacts to listed species. Provide any supporting documents (letter or record of conversation) that result from communication with these agencies, including impact mitigation measures, the permits required for the project, the steps the applicant has taken or plans to take, and the schedule for obtaining the permits.*

Response: As described in the response to Data Request #70, the project site will disturb approximately 9.7 acres of potential giant garter snake upland habitat and further discussions with USFWS will be required to determine potential impacts and mitigation measures, if needed. Records of Conversation with USFWS are provided as Attachment DR69-1.

Fish Species in Old Alamo Creek and Alamo Creek

72. a. *Please identify resident or migratory fish, avian (or other) species (including any state or federally listed species) that utilize Old Alamo Creek and Alamo Creek.*

Response: There are no state or federally listed fish species using Old Alamo Creek or New Alamo Creek. The fish species known to occur in the creeks are mosquitofish, fathead minnow, threespine stickleback, Sacramento sucker, common carp, and Sacramento pike minnow. In some years, fall-run Chinook salmon have been observed to immigrate opportunistically into New Alamo Creek in small numbers, but their upstream immigration is blocked by the first grade-control structure located between Dally Road and Lewis Road. Fall-run Chinook salmon cannot enter Old Alamo Creek because Old Alamo Creek discharges into New Alamo Creek through flap-gates, which prevent their immigration into Old Alamo Creek (Tetra Tech, Inc. 2004[1]; RBI, unpublished data). Because New Alamo Creek in this reach is not suitable habitat for salmon and this use is opportunistic and does not support spawning, the project would not be likely to adversely affect this species.

Regarding special-status terrestrial species that might use Old Alamo Creek and Alamo Creek, the following species in Tables DR72-1and DR72-2 have been identified based on a review of lists generated by USFWS and the California Department of Fish and Game (CDFG) for the Elmira Quad (498C). The species listed in **bold** are known to occur near the project area.

TABLE DR72-1
Federally Listed Species

Common Name	Scientific Name	Status
California tiger salamander	***Ambystoma californiense***	**Threatened**
California red-legged frog	*Rana aurora draytonii*	Threatened
Giant garter snake	***Thamnophis gigas***	**Threatened**
California clapper rail	*Rallus longirostris obsoletus*	Endangered

[1] Tetra Tech, Inc. 2004. Use Attainability Analysis For Old Alamo Creek. Submitted to Environmental Protection Agency Region 9. EPA Contract No. 68-C-99-249, Work Assignment 2-63. January.

TABLE DR72-2
State Listed Species

Common Name	Scientific Name	Status
Northwestern pond turtle	*Actinemys marmorata*	Species of Concern
Swainson's hawk	***Buteo swainsonii***	**Threatened**
White-tailed kite	*Elanus leucurus*	Fully Protected
Burrowing owl	*Athene cunicularia*	Species of Concern

b. *Please discuss how these species could be impacted by the changes in flow and water quality in Old Alamo Creek resulting from the project's use of EWTP discharge stream.*

Response: Because the primary source of flow to Old Alamo Creek throughout the year is EWTP effluent discharge, the project's use of EWTP effluent (a use assumed to be 5 million gallons per day [mgd] on a daily average basis) would eliminate aquatic habitat within the Old Alamo Creek channel throughout the year, downstream of the EWTP outfall. This reduction in wetted habitat would be expected to reduce the size and diversity of the aquatic communities that could exist within Old Alamo Creek. This would particularly be the case in the 2 miles immediately downstream of the EWTP discharge, which has few other sources of influent water throughout the year. Where Old Alamo Creek makes a right-angle bend to the south (1.4 stream miles downstream of the EWTP), an irrigation canal discharges water into the channel during the irrigation season, which would lessen the reduction in flow in this reach of the creek.

The lower flow rate in Old Alamo Creek may increase creek temperatures, relative to existing conditions, during the summer due to greater heating from solar radiation. The lower flow velocities could lead to increased algae production within the creek as well. These changes may increase the magnitude of the diurnal dissolved oxygen cycle in the creek, possibly leading to lower dissolved oxygen levels at night, relative to existing conditions.

The flow and water quality changes that would occur under the project would not significantly impact any state or federally listed species because no such species utilize Old Alamo Creek and the changes to flows in New Alamo Creek are not expected to significantly affect such species. If, however, consultation with the USFWS, CDFG, and the Regional Water Quality Control Board (RWQCB) identifies potentially significant impacts to state or federally listed species using Old Alamo Creek, and possibly New Alamo Creek, appropriate mitigation measures would be developed. EWTP

State and Federal Listed Species in Old Alamo Creek and Alamo Creek

73. a. *Please provide information on all state or federally listed species that could utilize Old Alamo Creek and Alamo Creek including the migratory windows for transient species that could utilize these waters during migration.*

Response: Please see response to Data Request #72a, which includes all state and federally listed species known to occur in the Elmira Quad (498C). Further assessment based on the agency consultation discussed in the response to Data Request #72 is required to determine

whether any of theses species actually make use of Old Alamo Creek or New Alamo Creek.

b. *Please discuss how these species could be impacted by the changes in flow and water quality in Old Alamo Creek resulting from the project's use of EWTP discharge stream.*

Response: Since no state or federally listed fish species occur in Old Alamo Creek, none could be impacted by changes in flow and water quality in Old Alamo Creek resulting from the project's use of EWTP discharge stream.

Further assessment would be required to determine whether any of the state or federally listed terrestrial species known to occur in the Elmira Quad (498C) actually make use of Old Alamo Creek and, if so, how changes in flow and water quality in Old Alamo Creek resulting from the project's use of EWTP discharge stream would affect these species.

Correspondence Related to Reduction in Flows for Old Alamo Creek and Alamo Creek

74. *Please provide copies of any correspondence and discuss any contacts that CPPV has had with California Department of Fish and Game, U.S. Fish and Wildlife Service, and/or National Marine Fisheries Service regarding the planned reduction in flows in Old Alamo Creek and Alamo Creek.*

Response: Michelle Tovar with USFWS has been contacted regarding the reduction of flow in Old Alamo Creek and Alamo Creek. The record of conversation may be found as Attachment DR69-1.

Attachment DR69-1
Records of Conversation

CH2MHILL TELEPHONE CONVERSATION RECORD

Call To:	US Fish and Wildlife Service Sacramento Office		
Phone No.:	(916) 414-6645	**Date:**	July 7, 2008
Call From:	Michael Clary/SAC	**Time:**	9:00 AM
Message Taken By:	CH2M HILL		
Subject:	Vacaville Energy Center		

6/23/2008 Call to John Cleckler, Biologist with CH2M HILL assigned to the US Fish and Wildlife Service Sacramento Office to determine appropriate avoidance measures related to potential federally listed vernal pool branchiopod habitat near the VEC site. On June 25 I sent photographs of the basin and a narrative description of the basin to Mr. Cleckler, who relayed my request to Michelle Tovar of the USFWS Sacramento Office.

7/1/2008 Mr. Cleckler called to report that he had been in contact with Ms. Tovar, who advised that the USFWS would require a request for technical assistance.

4/6/2009, 6/18/2009, 6/23/2009, 7/2/2009 left messages with Michelle Tovar/USFWS (916) 414-6646 requesting guidance on need to consult on giant garter snake (GGS) issues.

7/7/2009 Call from Michelle Tovar. Based on her prior experience with CEC she advises that the project should prepare a BA (probably a not likely to adversely affect) for GGS, so we have take authorization.

COPYRIGHT 2009 BY CH2M HILL, INC. • COMPANY CONFIDENTIAL

Soils and Water Resources (75–95)

Draft Soil Management Plan

75. *Please provide a draft Soil Management Plan including planning level discussion of soil handling plans for removal of existing soils including the planned disposal location for the excavated materials. The draft Soil Management Plan should include sufficient detail for Waste Management staff to review the adequacy of the plan related to soil handling and disposal and for Soil and Water Resources staff to confirm that Best Management Practices will be employed to limit the potential impacts related to wind or water borne erosion of existing soils.*

Response: A draft soil management plan is provided as Attachment DR75-1.

Range of Production Rates from EWTP

76. *Please provide the range of production rates of secondary-treated recycled water from EWTP that result in an average production of 6.5 mgd. Additionally, provide discussion showing the seasonal variation of discharges to verify that the EWTP summer discharges will meet the peak demands of the CPVVS, which are most likely to occur during the hot summer months.*

Response: The range of production rates and seasonal variation in EWTP discharges are provided in Table DR76-1.

TABLE DR76-1
Mean, Median, Monthly Average High and Low, and Daily Average High and Low Flows for the City of Vacaville's Easterly Wastewater Treatment Plant (January 2006 through December 2008)

	Discharge Rate (mgd)			
Month	**3-year Mean**	**3-year Median**	**High (Daily Average)**	**Low (Daily Average)**
January	10.2	9.6	23.3	7.4
February	9.6	9.3	15.5	7.3
March	10.2	10.2	18.5	7.5
April	10.0	10.0	18.9	6.7
May	8.8	8.8	10.9	6.8
June	8.5	8.5	10.9	6.8
July	8.2	8.2	9.1	6.7
August	8.0	8.0	9.3	6.5
September	7.9	8.0	9.0	6.7
October	7.9	8.0	9.2	6.3
November	7.8	7.8	9.9	4.9
December	8.1	8.0	12.3	6.0

Source: City of Vacaville, personal communication

The average annual water use of CPVVS will be 3,636 acre-feet per year (afy), or 3.2 mgd. The maximum daily use will be 4,363 gallons per minute (gpm), or 6.3 mgd. Thus, the

maximum daily use would be higher than or equal to the EWTP's average low discharge rate for every month except November and December, and is well below the mean discharge rates for all months.

In addition to seasonal variation, it is important to understand the diurnal variation in discharge over the daily 24-hour cycle for the EWTP. Although the summer average dry weather flow for the EWTP is currently between 8 and 9 mgd, the flow between 1:00 and 4:00 a.m. during the summer period may be as low as 3 to 4 mgd with flows at 11:00 a.m. being as high as approximately 10 mgd. CPV will construct and operate a 24-hour flow equalization basin along with the tertiary-treatment facilities to make use of up to 5 mgd of EWTP effluent, on a daily average basis.

Recycled Water Storage Capacity at the EWTP

77. *Please provide a discussion of the recycled water storage capacity at the EWTP. This storage capacity is critical to provide the reliability of supply for CPVVS and subsequently precludes the need for any backup supplies for cooling water. Please include in the discussion, if there are any options for alternative sources of cooling water if EWTP is not capable of meeting peak water demands. Ideally, the applicant should provide a water balance illustrating that there is sufficient storage capacity at EWTP to dampen variations in effluent production and water demand at CPVVS.*

Response: The EWTP has limited onsite storage capacity and, as a result, CPVVS plans to have onsite storage to account for potential limited outages at the EWTP as well as to trim the diurnal fluctuations. There is no backup source for cooling water makeup, so a filtered water storage tank is planned to: (a) provide emergency makeup water storage in the event of an outage at EWTP, (b) dampen potential low flow effluent conditions, and (c) serve as the facility's firewater storage tank. (Please see the response to Data Request #79.) Each of these three functions has been carefully considered in the sizing of a 2-million-gallon filtered water storage tank. This 2-million-gallon storage tank includes approximately 500,000 gallons reserved for firewater. (The firewater considerations are discussed further in the response to Data Request #79.)

The EWTP's record of reliability is excellent. Outages are rare and those that have occurred have been of very limited duration. For a total outage, the 1.5 million gallons of filtered water storage available for cooling water makeup would last about 6 hours based on summer conditions with full duct firing. Based on discussions with the City of Vacaville, the few times that total outages have occurred, the facility has been back in operation within 2 to 4 hours.

The diurnal characteristics of the EWTP's effluent discharges have also been considered. The flow information provided by the City in the response to Data Request #76 shows that there is adequate supply, on a daily average basis. Even considering the low summertime flow ranges of 3 to 4 mgd from 1:00 to 4:00 a.m., the 1.5-million-gallon storage tank provides adequate storage. This is particularly true considering the overnight dispatch probabilities of the CPVVS (lower loads are expected as well as lower ambient temperatures, reducing the evaporative losses in the cooling tower). The pump station at EWTP and piping to CPVVS will also be designed to take advantage of the EWTP's peak effluent periods to replenish the filtered water storage tank, should it be drawn down by low flow diurnal conditions.

Anticipated Uses for Potable Water

78. *Please provide a discussion of the anticipated uses and requirements for potable water. Please confirm if the 12-inch potable water line is required to supply water for fire protection and/or to utilize potable water as a backup supply.*

Response: The potable water supply from EWTP will only be used for domestic uses such as sinks, showers, and toilets. Potable water will not be used for fire water. Secondary treated water will be used for this purpose (see the response to Data Request #79). The 12 inch sizing was larger than necessary for this purpose and it is certain that a small-bore line 1 to 2 inches in diameter will be sufficient. The City and CPV have an agreement that the City will provide CPVVS with potable water at a rate not to exceed 840 gallons per day at a maximum flow rate of 5 gpm. The City will only allow a 1-inch connection to its potable water source. The City will not supply potable water for fire protection or as a backup supply. Both of those water supply needs will be addressed by CPV with the use of recycled water and water storage facilities provided on the CPVVS site.

Planned Source of Water for Fire Protection

79. *Please confirm the planned source of water for fire protection. Please clarify if CPVVS is planning to utilize potable water, the EWTP fire loop, or both for fire protection.*

Response: Potable water will not be used for fire protection and CPVVS will not be connected to the EWTP fire loop. The planned source of water for fire protection is from the allocation of recycled water the City has agreed to provide CPVVS for the project, coupled with storage facilities and pumps on the CPVVS project site. This water will be stored in a reserved portion of the filtered water storage tank. This will be accomplished by having the supply pipe connection for cooling tower supply at an elevation that prevents drawing from the bottom portion of the tank. The volume of storage dedicated for firewater will be in the range of 300,000 to 500,000 gallons.

Average Monthly Flow Data for Old Alamo Creek

80. *Please provide average monthly flow data for Old Alamo Creek upstream and downstream of the point of discharge from EWTP and for Alamo Creek downstream of the confluence with Old Alamo Creek. Please provide an estimate of the percentage of the average monthly flow in Old Alamo Creek and subsequently Alamo Creek that is made up of effluent discharged from EWTP.*

Response: The average monthly flow in Old Alamo Creek, upstream of the EWTP, is zero or near zero for all months of the year. Old Alamo Creek has been disconnected from its watershed in the Vacaville City Park, where New Alamo Creek diverges from the Old Alamo Creek Channel. Nearly all watershed runoff is now conveyed by New Alamo Creek.

New Alamo Creek, upstream of its confluence with Old Alamo Creek, does not receive watershed runoff during the summer months—it is an ephemeral system. Thus, New Alamo Creek conveys only agricultural return and conveyance flows and urban runoff from about June through November, annually.

During the precipitation season (i.e., primarily November through April), the water in lower New Alamo Creek is composed of runoff from the upper watershed, urban runoff, runoff

from agricultural lands, and EWTP effluent (RBI, 2007[2]). The relative fraction of effluent throughout the precipitation season varies depending on the size of each storm event and the frequency and size of antecedent storms. A dilution study found the portion of EWTP effluent present in March 2004 to be approximately 50 percent of the flow in New Alamo Creek (Flow Science, 2005[3]). Figure DR80-1 demonstrates that there are periods when the flow in New Alamo Creek is largely runoff from the watershed lands, and that there are periods when very little flow is contributed by the watershed and most of the flow is EWTP effluent. For the period 1998–2006, the dilution ratio (New Alamo Creek flow:EWTP flow) was 5:1 or less approximately 90 percent of the time (Figure DR80-1).

During the non-precipitation period of the year, natural base flow in New Alamo Creek annually goes to zero, typically in June, and remains in a zero-flow condition until adequate rains have occurred, typically in November (RBI, 2007). During the irrigation season (mid-April through October), significant inflows of agricultural drainage and irrigation water enter lower New Alamo Creek, and significant volumes are pumped out of the creek. Additional inputs to the creek include urban runoff and EWTP effluent. On a day in late July 2004, which is typical of operations throughout the irrigation season, there was no flow input to New Alamo Creek from the upper watershed. Of the 35 cubic feet per second (cfs) of flow in New Alamo Creek downstream of the Old Alamo Creek confluence, 11 cfs (31%) came from the EWTP, 23.5 cfs (67%) came from agricultural drainage water, and 0.5 cfs (2%) came from urban runoff (RBI, 2007).

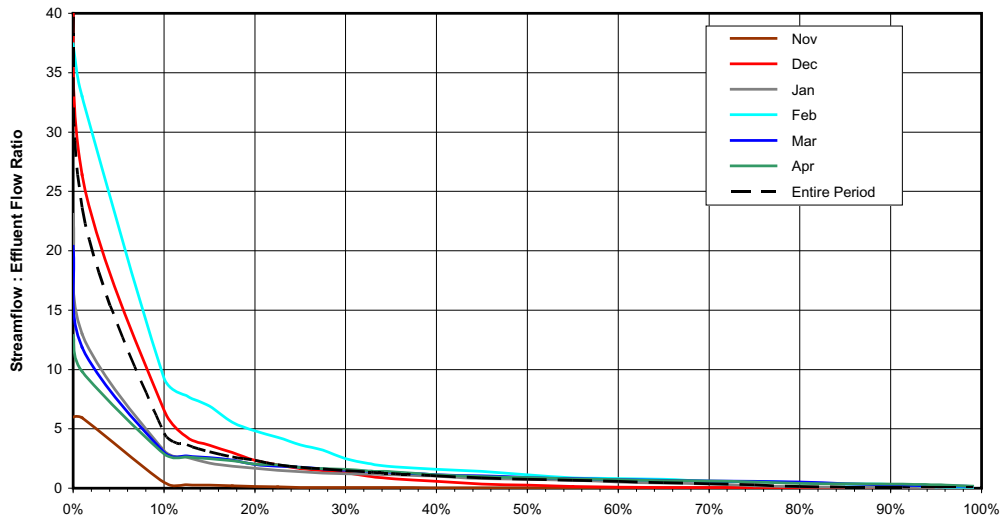


FIGURE DR80-1
Approximate Dilution Ratio of EWTP Effluent In New Alamo Creek
Immediately Below Confluence of Old Alamo Creek for Water Years 1998–2006.
Source: RBI, 2007

[2] RBI (Robertson-Bryan, Inc.). 2007. Use Attainability Analysis for Municipal and Domestic Supply (Mun) Use in Segments of New Alamo Creek and Ulatis Creek, Solano County, California – Final Report. Prepared by RBI for the Central Valley Regional Water Quality Control Board on Behalf of the City of Vacaville. December 2007. 52 Pp.

[3] Flow Science. 2005. Technical Memorandum No. 3, Easterly Wastewater Treatment Plant Effluent Dilution Analysis In Support of Potential Basin Plan Amendments For Defined Reaches of New Alamo Creek, Ulatis Creek and Cache Slough, Solano County, California. Pasadena, Ca. Prepared for Robertson-Bryan, Inc. on Behalf of the City of Vacaville. 49 Pp. Plus Appendices.

Impacts to Average Monthly Flow Rates

81. *Please provide a discussion of the anticipated impacts to average monthly flow rates, water quality, salinity, and temperature in Old Alamo Creek and Alamo Creek if all or most of the EWTP effluent is diverted to the CPVVS.*

Response: On an average daily or monthly basis, the project will not require "all or most of the EWTP effluent." Table DR76-1 shows that the EWTP's effluent averages between 7.8 and 10.2 mgd on a monthly basis. As discussed in the response to Data Request #76, the average annual water use of CPVVS would be 3.2 mgd and its maximum daily use would be 6.3 mgd.

If all or most of the EWTP effluent were to be diverted to the CPVVS facility, substantial reaches of Old Alamo Creek downstream of the EWTP outfall would change from its current hydrologic condition of perennial flow, to one of substantially lower flow or zero flow. Because the majority of Old Alamo Creek water is currently EWTP effluent, most water quality parameters would change little, as long as effluent-dominated flow remained. However, during the summer period, one would expect higher creek average and maximum water temperatures, and possibly lower average and daily low dissolved oxygen levels under lower flow conditions.

As for New Alamo Creek, effects on flows would be notable about 90 to 95 percent of the time in November, and about 75 to 80 percent of the time during the December through April period (see Figure DR80-1). Effects on hydrology in New Alamo Creek would be notable, but often somewhat less during the irrigation season (May through October) due to substantial volumes of agricultural drainage and conveyance water routed down New Alamo Creek during these months. Water quality parameter concentrations or levels in New Alamo Creek driven primarily by EWTP would be reduced (e.g., salinity), with many other parameters changing by lesser degrees. During the late October through November period, when irrigation flows have ceased and natural precipitation-driven flows have not yet started and thus the majority of flow in New Alamo Creek downstream of Old Alamo Creek is EWTP effluent, flow reduction would be notable, but most water quality parameters would change little, with the possible exceptions of temperature and dissolved oxygen, which may show greater changes under the lower flow regime.

Correspondence with RWQCB

82. *Please provide copies of any correspondence and discuss any contacts that CPV has had with the local RWQCB regarding the planned reduction in flows in Old Alamo Creek and Alamo Creek.*

Response: The City has shared with RWQCB staff that the potential siting, construction, and operation of a power plant that will use EWTP effluent is being explored and assessed, but neither the City nor CPV has had detailed discussions with RWQCB staff regarding planned flow reductions in downstream water bodies as a result of constructing and operating a power plant.

Alternatives to Evaporative Cooling

83. *Please provide a discussion of project alternatives including utilizing dry cooling technology as an alternative to evaporative cooling at CPVVS. Please provide a planning level economic analysis and water supply estimates comparing the use of dry cooling, wet/dry cooling, vs. the proposed wet cooling approach.*

Response: Dry cooling and hybrid wet/dry cooling alternatives were briefly considered and rejected for several reasons including cost, space constraints, the proximity and availability of reclaimed water from the City of Vacaville, and plant thermal efficiency loss with the resultant higher air emissions per kilowatt-hour of generation that would be associated with dry and hybrid cooling systems.

The cost increase to apply an air-cooled condenser system in lieu of mechanical draft cooling tower for the CPVVS would be approximately $30-35 million dollars. The budgetary cost for the cooling tower for the CPVVS is approximately $8 million, including erection. The corresponding budgetary cost for an air-cooled condenser is in the range of $32-35 million, not including erection.

An air-cooled condenser would also not be practical for the CPVVS because of limited space available on the site. As can be seen from the general arrangement drawing submitted in the AFC (Figure 2.1-2 in the Project Description), the available space on the eastern end of the site is prohibitively small for siting an air-cooled condenser, considering the property line, setbacks, landscape buffers, stormwater detention pond, and other project design needs. The relatively narrow width of the cooling tower lends itself well to the limited space available on the site's eastern boundary. The air-cooled condenser is nearly 5 times as wide as the cooling tower.

A significant consideration in evaluating the air-cooled condenser is the loss of thermal efficiency. The performance of an air-cooled condenser is driven by the ambient dry bulb temperature, as well as the size of the unit. With an air-cooled condenser instead of a cooling tower the steam turbine output for the rated summer case would drop by about 15 to 18 MW because of the increased backpressure. The auxiliary load increase due to extra horsepower needed for the fans would further decrease the net plant output by another 2.5 to 3 MW. The resultant thermal efficiency loss due to the approximately 20 MW decrease in net plant output with the same heat input is roughly 3 percent. A consequence of this poor thermal efficiency would be a higher air pollutant loading on a mass flow per kilowatt-hour basis.

The most important factor, however, in selecting wet cooling for the CPVVS was the proximity of the EWTP and the availability of ample reclaimed water usable for cooling water makeup. In summary, the wet cooling configuration represents the best solution from a space utilization/availability standpoint and results in the lowest cost, lowest visual impacts, highest thermal efficiency, and lowest emissions per kilowatt-hour over both dry and hybrid wet/dry cooling systems.

Records of Conversation with DHS and RWQCB

84. *Please provide documentation showing the applicant has established contact with DHS and RWQCB notifying them that they propose to treat and use recycled water for project operation. If the applicant has already contacted these agencies regarding their proposed treatment and use, please provide copies of any correspondence.*

Response: DHS and RWQCB have not yet been contacted, but will be contacted as the project moves forward.

Status Report on Filter Backwash Wastewater

85. *Please provide a status report on the discussions with EWTP to return the filter backwash wastewater stream to the EWTP headworks.*

Response: CPV is exploring options to dispose of the filter backwash water and this discussion is ongoing. The City of Vacaville is willing to consider accepting the filter backwash water stream at the EWTP headworks if CPVVS reduces the salinity of the filter backwash wastewater consistent with the requirements of the discharge requirements of the EWTP. Return water from CPVVS would not be allowed to compromise the future discharge level.

Alternative Treatment Plans for Filter Backwash Water

86. *Please provide a discussion of alternate plans for treatment of the filter backwash if the water quality of the wastewater stream does not allow for direct delivery to the EWTP headworks.*

Response: The alternate plan for treatment of the filter backwash if the water quality of the wastewater stream does not allow for direct delivery to the EWTP headworks is as follows:

a. Collect backwash waters in a sump or tank (with duplex forwarding pumps).

b. Process this wastewater through a lamella-type clarification/thickener system (including a coagulant chemical feed system, sludge holding/transfer tank, sludge forwarding pumps, and a complete control system).

c. Recover the treated lamella effluent to the feed of the tertiary treatment system.

d. Treat the lamella-produced sludge via the existing gravity thickener/filter press in the ZLD system. This results in an increase in size of the gravity thickener and the filter press, but will not cause any size increases in the reverse osmosis and brine concentrator/ crystallizer systems.

Intended Function of Retention Pond

87. *Please provide a discussion clarifying the intended function of the retention pond, indicating if stormwater will be released from the site during events equal or below a 100-year event.*

Response: The onsite detention pond is intended to temporarily capture and continuously release onsite stormwater runoff into the existing downstream drainage facilities. The detention pond will mitigate the 100-year peak flow rates over the pre-developed site. The detention pond will gravity-drain to the 48-inch-diameter standpipe and culvert outfall structure in the southeastern corner of the pond. Standing water is not anticipated in the pond during non-storm times.

Hydrologic Design Calculations

88. *Please provide hydrologic design calculations for the proposed stormwater retention basin, demonstrating that the basin can handle a 100-year 24-hour runoff volume based on the retention basin stage-volume relationship and the planned outlet structure.*

Response: The revised calculations are included here as Attachment DR88-1 and include the 24-hour 100-year storm event as requested. The pond has been re-sized to accommodate this criterion.

Riser Pipe Function

89. *Please clarify if the 48-inch riser pipe is intended to serve as an emergency outlet for the retention pond for events greater than the 100-year event, and if so, provide discussion and calculations for sizing the structure. If this is not the case, provide a discussion and/or figures to clearly demonstrate the design intent and include an emergency outlet for the retention pond.*

Response: The 15-inch-diameter culvert will meter the out-flowing runoff during storm events. The 48-inch-diameter riser pipe is intended to serve as an emergency outlet in the event that the 15-inch culvert becomes plugged. The elevation of the top of the 48-inch riser pipe will be designed such that, in the event of a failure of the 15-inch-diameter culvert, the site will sustain minimal flooding and the pond walls will not be overtopped.

An additional set of calculations making use of the 48-inch-diameter emergency riser pipe has also been prepared. In this hypothetical design, to simulate plugging of the 15-inch gravity outlet, this was eliminated from the modeling calculations. Such that the only pond outlet would be the top of the 48-inch riser pipe. These calculations showed that the 48-inch riser pipe would have sufficient capacity to act as an emergency outlet for the pond in the event that the 15-inch culvert were to become plugged.

Waterways Receiving Stormwater Runoff

90. *Please provide a discussion of the waterways and water bodies downstream of the connection to the culvert at Fry and Lewis roads that will receive stormwater runoff discharged from the retention pond if this is to occur as shown on the site drainage plan.*

Response: The waterways downstream of the project consist of manmade channels, ditches, culverts, and natural waterways. These ditches, culverts, and channels generally drain to the east toward the Sacramento River. The project site sheet drains storm runoff to the east into a roadside ditch along Lewis Road. Drainage in the ditch is directed south along Lewis Road for approximately 0.5 mile into New Alamo Creek. Runoff in New Alamo Creek drains east for approximately 5 miles to Ulatis Creek. Ulatis Creek is tributary to Cache Slough, the Sacramento River, and the Sacramento-San Joaquin Delta.

The roadside ditch along Lewis Road is an unlined earthen ditch maintained by Solano County. New Alamo Creek and Ulatis Creek are unlined earth flood-control channels that are maintained by Solano County Water Agency. These flood control channels were constructed from 1962 to 1972 to alleviate recurring floods in the Ulatis watershed area. Cache Slough is a natural waterway that drains to the east into the Sacramento River and then into the Sacramento-San Joaquin Delta.

The proposed project will make use of the same downstream drainage course. The onsite detention pond will be sized such that the post-developed site peak runoff from the 100-year storm event will be less than the pre-development flow. Storm runoff from the project site will leave the detention pond through a culvert and enter into the Lewis Road roadside ditch.

CASQA Water Quality Volume

91. *Please provide documentation demonstrating that the CASQA Water Quality Volume can infiltrate into the subsurface within 3 to 5 days given the low permeability soil conditions that exist at the CPVVS site.*

Response: The pond is being designed as a detention pond and will have a gravity outlet through a culvert. No infiltration into the soil or evaporation has been taken into account in the model calculations.

The two onsite vegetated bio-swales will be used as a water quality treatment device (see Attachment DR88-2). Calculations included here as Attachment DR88-1 show that a residence time greater than 10 minutes is achieved in both the northern and southern swale. This will allow treatment of the site runoff prior to entering the detention pond. Although the detention pond is not taking credit as a water quality treatment facility, a 2-foot-high sediment berm around the outfall riser structure has been included. This will help prevent sediment from leaving the project site.

Preliminary Size of Retention Pond

92. *Please clarify the discrepancy related to the preliminary size of the retention pond.*

Response: The pond will store 137,390 cubic feet (ft^3) in the 100-year, 24-hour design storm with a water surface elevation of 62.6 feet. The pond storage is 143,128 ft^3 at the top of riser elevation of 62.7 feet. The pond storage is 173,008 ft^3 at the spillway elevation of 63.2 feet. The total pond storage is 223,663 ft^3 at the top of bank elevation of 64.0 feet.

Draft Drainage Erosion and Sediment Control Plan

93. *Please provide a draft Drainage Erosion and Sediment Control Plan (DESCP) containing elements A through I below outlining site management activities and erosion/sediment control BMPs to be implemented during site mobilization, excavation/demolition, construction, and post-construction activities. The level of detail in the draft DESCP should be commensurate with the current level of planning for site grading and drainage. Please provide all conceptual erosion control information for those phases of construction and post-construction that have been developed or provide a statement when such information will be available. The DESCP may be combined with the Stormwater Pollution Prevention Plan (SWPPP) required by the Regional Water Quality Control Board to limit the need for the project to develop separate stormwater management plans.*

    A. ***Vicinity Map*** *– A map(s) at a minimum scale 1"=100' will be provided indicating the location of all project elements (construction site, laydown area, pipelines, etc.) with depictions of all significant geographic features including swales, storm drains, and sensitive areas.*

B. ***Site Delineation*** *– All areas subject to soil disturbance for the CPVVS (project site, laydown area, all linear facilities, landscaping areas, and any other project elements) shall be delineated showing boundary lines of all construction/demolition areas and the location of all existing and proposed structures, pipelines, roads, and drainage facilities.*

C. ***Watercourses and Critical Areas*** *– The DESCP shall show the location of all nearby watercourses including swales, storm drains, and drainage ditches. Indicate the proximity of those features to the CPVVS construction, laydown, and landscape areas and all transmission and pipeline construction corridors.*

D. ***Drainage Map*** *– The DESCP shall provide a topographic site map(s) at a minimum scale 1"=100' showing all existing, interim and proposed drainage systems and drainage area boundaries. On the map, spot elevations are required where relatively flat conditions exist. The spot elevations and contours shall be extended off-site for a minimum distance of 100 feet in flat terrain.*

E. ***Narrative of Project Site Drainage*** *– The DESCP shall include a narrative of the drainage measures to be taken to protect the site and downstream facilities. The narrative should include the summary pages from the hydraulic analysis prepared by a professional engineer/erosion control specialist. The narrative shall state the watershed size(s) in acres that was used in the calculation of drainage measures. The hydraulic analysis should be used to support the selection of BMPs and structural controls to divert off-site and on-site drainage around or through the CPVVS construction and laydown areas.*

F. ***Clearing and Grading Plans*** *– The DESCP shall provide a delineation of all areas to be cleared of vegetation and areas to be preserved. The plan shall provide elevations, slopes, locations, and extent of all proposed grading as shown by contours, cross sections or other means. The locations of any disposal areas, fills, or other special features will also be shown. Illustrate existing and proposed topography tying in proposed contours with existing topography.*

G. ***Clearing and Grading Narrative*** *– The DESCP shall include a table with the quantities of material excavated or filled for the site and all project elements of the CPVVS project (project site, lay down area, transmission corridors, and pipeline corridors) whether such excavations or fill is temporary or permanent, and the amount of such material to be imported or exported.*

H. ***Best Management Practices Plan*** *– The DESCP shall identify on the topographic site map(s) the location of the site specific BMPs to be employed during each phase of construction (initial grading/demolition, project element excavation and construction, and final grading/stabilization). BMPs shall include measures designed to prevent wind and water erosion.*

I. ***Best Management Practices Narrative*** *– The DESCP shall show the location (as identified in H above), timing, and maintenance schedule of all erosion and sediment control BMPs to be used prior to initial grading, during all project element (site, pipelines, etc.) excavations and construction, final grading/stabilization, and post-construction. Separate BMP implementation schedules shall be provided for each project element for each phase of construction. The maintenance schedule should*

include post-construction maintenance of structural control BMPs, or a statement provided when such information will be available.

Response: A draft drainage, erosion, and sediment control plan (DESCP) is provided as Attachment DR93-1.

Construction Dewatering Plan

94. *Please provide a detailed discussion of the construction dewatering plan. Include discussion of how materials will be handled on site, where the groundwater will be discharged, whether water treatment required and whether a RWQCB Waste Discharge permit will be required.*

Response: Discharge from construction dewatering will be routed to the stormwater detention pond located on the east side of the project site. An RWQCB Report of Waste Discharge will therefore not be required.

Report of Waste Discharge

95. *If a RWQCB waste discharge permit is required please provide a draft Report of Waste Discharge that has also been submitted to the RWQCB for review and comment.*

Response: Please see response to Data Request #94.

Attachment DR75-1
Draft Soil Management Plan

CPV Vaca Station Project Soil Management Plan

PREPARED FOR: Competitive Power Ventures Vacaville, LLC

PREPARED BY: Jenny Krenz/CH2M HILL

DATE: July 10, 2009

Introduction

CH2M HILL has prepared this Soil Management Plan (SMP) on behalf of Competitive Power Ventures Vacaville, LLC (CPV) for the proposed development of a gas-fired electrical generating station identified as CPV Vaca Station (CPVVS). The proposed site is located north and west of the intersection of Fry Road and Lewis Road in Vacaville, Solano County, California (Figure 1). The 25-acre site would be leased from the City of Vacaville lies and within a larger 143.5-acre City-owned parcel.

Background

Review of historic aerial photographs revealed that the property was used as an agricultural field from prior to 1937 up to the early 2000s. In 1999, the City of Vacaville purchased the 143.5-acre parcel, which includes the proposed project site. It was used for 4 or 5 years for the application of biosolids (i.e., municipal wastewater treatment sludge; CH2M HILL, 2008). Historical groundwater impacts at the site have been attributed to agricultural practices rather than the program of biosolids application (Luhdorff and Scalmanini, 2005).

Because of the long-term use of the subject property for agricultural production (row crops), it was recommended in the Phase I report that a limited program of soil sampling and laboratory analysis be completed to determine if metals or organochlorine pesticide residues remained that could pose a potential future health risk to construction workers or other workers on the property. While the proposed CPVVS would not use groundwater or create discharges that would affect groundwater resources, it was also recommended that baseline groundwater conditions be assessed prior to CPVVS construction or operation as a due diligence measure to protect CPVVS against future environmental liability. The findings of these investigations are available in the Phase II report (CH2M HILL, 2008) and are summarized below.

Site Description

The 25-acre subject property lies within a 143.5-acre parcel that is owned by the City of Vacaville (APN 142-200-040). The site topography is relatively flat and slopes slightly toward the east and southeast. Rainfall is expected to infiltrate or flow overland to a roadside ditch located along the east side of the property. The nearest surface water bodies are unlined canals, operated by Solano Irrigation District, located just south of Fry Road

(approx. 120 ft from the southern boundary of the site). The nearest natural water body is Alamo Creek, located approximately 0.4 mile north of the subject property (Figure 1). The subject property is located in an area used primarily for agricultural production of corn and other row crops. The site has been fallow for a few years but had been mowed and disked at the time of the September 2008 field investigation. Other property owned by the City of Vacaville to the west and north of the proposed CPVVS site was also fallow during site visits in 2008.

The only structures located on the proposed CPVVS site are a utility pole with a transformer and a utility box, both located near the southeast corner. A groundwater monitoring well (MW-5) is also located near the southeast corner of the site (Figure 1). This monitoring well was part of a shallow groundwater study conducted for the City of Vacaville Easterly Wastewater Treatment Plant (EWTP) (Luhdorff and Scalmanini, 2005). This study showed that the flow direction of the unconfined shallow groundwater is toward the southeast.

The EWTP is located approximately 500 feet northwest of the proposed CPVVS site (Figure 1). A gravel access road for the EWTP (sludge haul road) is located along the west side of the subject property and was elevated approximately 2 to 4 feet in the northwest corner of the site.

Soils at the subject site are mapped almost entirely as Capay silty clay loam (Ca), with a very limited portion in the north central margin of the subject site mapped as San Ysidro sandy loam, 0 to 2 percent slopes (SeA). Both of these moderately well drained, deep soils are formed on basin rims in alluvium derived from sedimentary rocks. The Capay silty clay loam soils are described as nearly level to level with a silty clay loam texture throughout the profile. The San Ysidro sandy loam has a sandy loam surface layer with a clay loam subsurface (NRCS, 1977).

Phase II Site Investigation

A preliminary Phase II ESA, comprised of soil and groundwater sampling and chemical laboratory analysis, was conducted for the proposed CPVVS site near Vacaville, California (CH2M HILL, 2008). The results of the assessment, as summarized in this report, indicate that inorganic and organochlorine constituents exist in surface and subsurface soils at levels that warrant consideration in the plans to develop the proposed CPVVS.

Sampling and Analysis

Surface (0- to 6-inch-bgs) and near surface (3-foot-bgs) soil samples were collected at 20 locations on the 25-acre proposed CPVVS site. Of these 20 locations, five locations received additional sampling at the 5-foot-bgs depth. Surface and subsurface soils were also sampled at five nearby off-site locations in areas that did not receive biosolids to provide a way to assess ambient (background) metals concentrations. A total of 59 soil samples were collected, with five additional samples collected as field duplicates.

Grab samples of shallow groundwater were collected from 3 of the 20 locations to supplement the groundwater sample from the monitoring well in the southeastern corner of the site. The intent of the groundwater sampling program was to document baseline shallow groundwater conditions prior to CPVVS construction or operations.

Soil and groundwater samples were sent to Applied Sciences Laboratory (ASL) in Corvallis, OR for analysis. Both types of samples were analyzed for CAM 17 metals and for organochlorine pesticides.

Results

CAM-17 metals were the most widely detected contaminant in the soil samples. In the surface samples, antimony, cadmium, molybdenum, and thallium were either not detected or were detected in relatively few samples (CH2M HILL, 2008). In the subsurface soils, antimony and thallium were detected in only one or two samples, while cadmium and molybdenum were detected in 92 percent and 76 percent of subsurface soils, respectively. Most of the CAM-17 metals were detected in nearly all surface and subsurface samples, including arsenic, barium, beryllium, chromium, cobalt, copper, lead, mercury, nickel, silver, vanadium, and zinc (CH2M HILL, 2008).

The mean metals concentrations in surface soils at the site are higher than those in background surface soils for beryllium, chromium, copper, lead, mercury, selenium, silver, vanadium, and zinc. However, only three of these constituents—copper, silver, and zinc—were significantly higher at the $p \leq 0.05$ level. According to the Phase II report (CH2M HILL, 2008), it is possible that the metals are found at higher concentrations within the field due to historical agricultural practices that included the applications of biosolids. However, it was also noted that mean concentrations of other metals are higher in the background surface samples than in the in-field samples. These metals included arsenic, barium, cobalt, and nickel. Among these metals, only the nickel concentration was statistically different than background concentrations in surface soils.

The mean concentrations of metals in surface soils are higher than those of subsurface soils for chromium, copper, lead, mercury, silver, vanadium, and zinc. Differences are statistically significant except for chromium and vanadium. These elevated metals in the surface soils could be explained by agricultural practices and the application of biosolids. However, it should also be noted that mean concentrations of arsenic, barium, beryllium, cobalt, nickel, and selenium are higher in the subsurface soils than in the surface soils. Of these, all were statistically significant except for selenium (CH2M HILL, 2008).

The concentrations of several metals (copper, cobalt, nickel, selenium, and zinc) were lower in surface soils when compared to surface background or subsurface soils. It was hypothesized that, given the agricultural background of the site, accumulation of these metals in plant biomass and subsequent harvesting could explain this difference.

The organochlorine pesticide results for the soils indicated that these constituents were detected almost exclusively in the surface soil samples. All subsurface samples were non-detect for organochlorine pesticides except for a single estimated (J-flagged) result for Endosulfan II that was detected in a field duplicate of a 3-foot sample. With only two exceptions (alpha-chlordane and 4,4-DDE), organochlorine pesticides in the surface soil samples were estimated at levels that were between the method detection limit and the report limit (that is, J-flagged). Alpha-chlordane was detected above the reporting limit in three surface samples at concentrations ranging from 0.5 to 0.87 mg/kg dw. 4,4-DDE was detected above the reporting limit in the surface soil samples in all but one of the in-field samples (ranging from 0.5 to 1.6 mg/kg dw) and in three of four of the background samples

(ranging from 0.48 to 1.3 mg/kg dw). Because organochlorine compounds are not water soluble, they tend to adsorb to particulates in near-surface soils or within the plowed depth of the soil, and are not readily transported to groundwater (ATSDR, 2002).

Other organochlorine pesticides that were detected at levels below the reporting limit in surface samples include gamma-BHC (Lindane), beta-BHC, delta-BHC, alpha-chlordane, 4-4'-DDE, 4,4'-DDT, dieldrin, Endosulfan I, Endosulfan II, Endosulfan sulfate, Heptachlor and Heptachlor epoxide. Summary statistics and statistical comparisons were not conducted, due to the limited occurrence of organochlorine pesticide compounds in the surface soils and the relatively low number of detections.

Table 1, attached, contains an abbreviated version of the Phase II soils results. Only those samples & locations with results above the screening levels are reported. Refer to the Phase II Environmental Site Assessment (CH2M HILL, 2008) for the complete results.

The results from the groundwater sampling indicated few samples with relatively low concentrations of metals and organochlorine pesticides in the shallow groundwater beneath the proposed CPVVS site. The analytical data did not indicate any exceedances of human health risk-based criteria (tap water PRGs) for metals, although it should be noted that the method detection limits were too high to assess the relatively low risk criteria for tap water for arsenic (0.045 µg/L) and thallium (2.4 µg/L). There was a single exceedance of the health risk-based criteria for the organchlorine pesticide heptachlor epoxide. This compound was detected at 0.026 µg/L, which exceeded the tap water PRG (based on heptachlor) of 0.015 µg/L. Because groundwater will not be used for potable water at the proposed CPVVS project, it is not anticipated that these results pose a significant threat to human health during construction or operation of the CPVVS. These data will serve to provide a baseline of shallow groundwater conditions during the late dry season (September) prior to CPVVS construction or operation.

Risk Assessment (based on Phase II Results)

The Phase II sampling of the proposed CPVVS site found that arsenic concentrations exist at levels above the comparative health risk-based thresholds, including Preliminary Remediation Goals (PRGs) and California Human Health Screening Levels (CHHSLs) in surface and subsurface soils at the site (CH2M HILL, 2008). Chromium was also detected above the risk-based values for chromium VI; however, it is expected that the total chromium levels detected in surface and subsurface soils are associated with the less toxic form (chromium III) due to the unsaturated (oxidizing) conditions in surface soils at the site. Based on these conditions, it was concluded that the actual chromium levels are below the risk-based values (i.e., those for chromium III).

Arsenic was detected at concentrations that were similar to those of the background soil samples collected from around the site. They were also comparable with arsenic levels documented in a state-wide assessment of background concentrations of metals (Kearney Foundation, 1996). While arsenic is a known carcinogen and represents a potential risk for human health under an industrial/commercial worker exposure scenario to surface soils, the implementation of normal dust-control and erosion mitigation measures (as part of the

construction BMPs) would be sufficient to avoid potential health risks for construction workers and offsite receptors during the CPVVS construction activities.

Residual organochlorine pesticide (4,4′-DDE) concentrations were noted in several surface samples at levels near the hazardous waste TTLC criterion (CH2M HILL, 2008); however, these were below human health risk-based screening levels (PRGs and CHHSLs). With only a few exceptions, organochlorine pesticides were not detected in subsurface soils. DDE is one of the breakdown products of DDT, a historically used agricultural pesticide banned in the United States in 1973. As such, DDE is commonly found in agricultural areas where DDT was historically used. The presence of DDE in several of the sampled locations confirms that DDT was historically utilized during farming operations at this location. Although the concentration of DDE at the locations sampled were below the human health risk-based screening levels, the imperfect nature of farming leaves the possibility for areas of higher concentrations to exist on the site. The BMPs discussed for arsenic are sufficient to avoid potential health risks for construction workers and offsite receptors during construction, should this situation exist.

The concentrations of both DDE and arsenic are above the NOAA Ecological Soil Screening Levels (Eco-SSLs). The Eco-SSLs are concentrations of contaminants in soil that are protective of ecological receptors that commonly come into contact with and/or consume biota that live in the or on the soil (USEPA, 2005). The main concern for the site is erosion; erosion of soil from the project area into local water bodies could result in toxicity to benthic organisms, plants, and animals living nearby. Employment of the construction BMPs mentioned above and outlined in the Stormwater Pollution Prevention Plan (SWPPP) should be sufficient to prevent erosion and subsequent toxicity from occurring.

It is important to note that the concentrations of these contaminants are not severe enough to warrant soil removal. While a few sampling points had DDE concentrations above the hazardous waste level, soil concentrations are below those that would constitute a human health risk. In addition, construction activities will mix surface soils with underlying subsoil materials, thereby reducing concentrations to levels that are below those of hazardous waste.

Soil Management Plan

Objectives

The soil contaminant levels observed at the proposed CPVVS site are such that, without mitigation, construction worker risks would be expected to be higher than the commercial/industrial worker CHHSLs scenario, given the potential for increased direct exposure via accidental ingestion or inhalation. This elevated risk to workers is primarily due to exposure to the naturally occurring soil arsenic and, to a lesser degree, organochlorine pesticides (especially 4,4′-DDE) which were detected near the hazardous waste TTLC (although below the CHHSLs). Exposure mitigation for construction workers should therefore include soil handling best management practices (BMPs) aimed at minimizing soil contact and fugitive dust generation during construction.

Soil contaminant levels also present a potential threat to organisms living off-site. Erosion of soil from the project area into local water bodies could result in toxicity to benthic

organisms, plants, and animals living nearby. Because organochlorine pesticides (such as DDE), adsorb strongly to fine soil particles, soil erosion will be a main source of transport offsite. Prevention of wind and water erosion will be essential to prevent potential off-site contamination. BMPs will therefore be directed at preventing and controlling erosion and off-site contamination.

The objectives of the SMP are to:

- provide instructions for soil handling, stockpiling, and dust and erosion minimization during site construction activities for the proposed CPVVS; and,
- describe procedures for soil management following site construction until the site is stabilized and vegetation is fully established onsite.

Worker Risks and Exposure Pathways

As mentioned above, the elevated risk to workers is primarily due to exposure to soil arsenic and, to a lesser degree, organochlorine pesticides (especially 4,4'-DDE). This section gives more information about these contaminants, and describes pathways for worker exposure. Appendix A contains the Department of Health and Human Services Public Health Statements for both of these contaminants.

Arsenic

Arsenic was found in all of the depths and locations sampled. Arsenic is a naturally occurring element; because it was found in both the site and background samples, it is assumed that much of the concentration is due to local, natural sources. The main exposure pathways for arsenic are by eating food (found in fish, plants, etc), drinking water, breathing air, or ingesting soil (ATSDR, 2007). On the CPVVS site, the main exposure pathways will be ingestion and inhalation.

4,4'-DDE

DDE is one of the breakdown products of DDT, a historically used agricultural pesticide banned in the United States in 1973. As such, DDE is commonly found in agricultural areas where DDT was historically used. DDT and DDE chemicals stick strongly to soil particles, and therefore generally remain in the surface layers of the soil (ATSDR, 2002). The main exposure pathways for DDE are by eating food (found in fish, leafy vegetables, etc), skin exposure (minimal unless in high concentrations), or breathing in dust (ATSDR, 2002). On the CPVVS site, the main exposure pathway will be inhalation.

General Guidelines

Construction worker training regarding best management practices should include a discussion of the naturally-occurring presence of arsenic in the soil and common-sense practices to reduce worker exposure. Erosion and sediment control BMPs are expected to effectively attenuate any adverse effects due to presence of soil contaminants.

Onsite Facilities

Because ingestion is one of the main worker exposure pathways, washing facilities should be made readily available onsite. The facility should allow for the washing of the hands,

face, and neck. In addition, an area for boot rinsing should be established to avoid the tracking of soil offsite.

If possible, an area should be designated for eating, drinking, and smoking to reduce the potential for ingestion.

Tracking control BMPs, such as providing truck tire washing facilities (with containment berms to keep wash water onsite) will be established at exit points to the site.

Workers

Workers should follow good hygiene and exposure-reducing practices, such as:

- Wash hands and face before eating, drinking, or smoking.
- Wear gloves while working to prevent accidental ingestion.
- If airborne dust is present, wear a dust mask to prevent inhalation.

Soil Management during Site Construction

The following procedures will be implemented during site preparation and construction activities to minimize fugitive dust and to control erosion. Refer to the SWPPP and Drainage, Erosion, and Sedimentation Control Plan (DESCP) for more detailed information.

Dust Control

During construction of the project, dust control measures will be implemented to minimize the wind-blown loss of soil from the site, and to reduce worker exposure via inhalation.

Dust control measures to be implemented at the proposed CPVVS site correspond to the PM_{10} control measures recommended by the Bay Area Air Quality Management District (BAAQMD) and the South Coast Air Quality Management District (SCAQMD) incompliance with the California Environmental Quality Act (CEQA). These measures include:

- Water all active construction areas at least twice daily,
- Enclose, cover, water twice daily, or apply non-toxic soil binders to exposed piles of soil,
- Mist or spray water while loading transportation vehicles,
- Minimize drop heights when loading transportation vehicles,
- Use tarps or other effective covers for trucks carrying soil on roads offsite, and
- Pave, gravel, or water thrice daily, all unpaved access roads, parking areas, and staging areas.

These dust control measures will continue until project completion, or until establishment of permanent control measures.

Air quality should be monitored periodically throughout the duration of the construction activities to ensure BMP's are adequately controlling dust emissions. Monitoring should take place both onsite, and off site.

Erosion Control

A SWPPP and a DESCP have been developed for this project. These documents include identification of Best Management Practices (BMPs) that are required under the National Pollutant Discharge Elimination System (NPDES) permit. These erosion-control measures are required to help maintain water quality, protect property from erosion damage, and prevent accelerated soil erosion or dust generation that destroys soil productivity and soil capacity. Please refer to the SWPPP and DESCP for project specific requirements.

Temporary erosion control measures required by the SWPPP and DESCP will be implemented before construction begins, and will be evaluated and maintained during construction. These measures will likely include but are not limited to revegetation, mulching, physical stabilization, dust suppression, berms, ditches, and sediment barriers. These measures will be removed from the site after the completion of construction.

Sediment barriers, which slow runoff and trap sediment, will also be incorporated. Sediment barriers include straw bales, sand bags, straw wattles, and silt levees. They are generally placed below disturbed areas, at the base of exposed slopes, and along streets and property lines below the disturbed area. Sediment barriers are often placed around sensitive areas to prevent sediment discharge into wetlands, creeks, or storm drains.

The site will be constructed on relatively level ground; therefore, it is not considered necessary to place sediment barriers around the entire property boundary. However, barriers will be placed in locations where offsite drainage could occur to prevent sediment from leaving the site. If used, sediment barriers will be properly installed (staked and keyed), then removed or used as mulch after construction. Runoff detention basins, drainage diversions, and other large-scale sediment traps are not considered necessary because of the site's small size, level topography, and surrounding paved areas. Any soil stockpiles, including sediment barriers around the base of the stockpiles, will be stabilized and covered, as described in the following section.

Permanent erosion-control measures on the site will include establishment of permanent vegetation, gravel, paving, and drainage systems.

All installed BMP's should be inspected frequently, at least once weekly during the rainy season and at least once every two weeks during the non-rainy season, or as specified by the permit, to verify continued BMP implementation.

Soil Stockpile Management

Temporary stockpiling of excavated soil may be necessary throughout site construction. Soil stockpiles at the site will be lightly sprayed with water twice daily (or as needed) to minimize dust. To the extent practical, the soil stockpiles will be covered with tarps or other similar material during times when the material is not in active use. If a soil stockpile is uncovered during the rainy season, it will be surrounded by hay bales, silt traps, or a berm prior to uncovering to prevent sediment runoff. Soil stockpiles should not be made in or near storm drains or watercourses.

Erosion Pathways - Off Site Concerns

Wind erosion (dust) should be prevented to prevent the possibility for off site inhalation risk. This risk is mainly to humans living and working in the vicinity of the project area.

The concentrations of arsenic and DDE in the soil are above the NOAA Ecological Soil Screening Levels (Eco-SSLs). Erosion of soil from the project area into local water bodies could result in toxicity to benthic organisms, plants, and animals living nearby. Because organochlorine pesticides (such as DDE), adsorb strongly to fine soil particles, soil erosion will be a main source of transport offsite. Prevention of wind and water erosion will be essential to prevent potential offsite contamination.

Water erosion should be prevented to reduce the possibility of contamination of offsite water bodies. The irrigation canal just south of Fry Rd is within two hundred feet of the project site, making it the most likely site for sedimentation and contamination.

Soil Disposal

Generation of excess soil at the proposed CPVVS site is not anticipated at this time. If excess soil is generated from the site, the excess soil will be profiled to determine appropriate disposal options.

Site Access Control

The construction site will be fenced to control unauthorized entry. Controlled entry points (gates) will be staffed during working hours to provide access control. No trespassing signs will be posted every 500 feet along the fencing to prevent unauthorized entry.

Soil Management Following Site Development

General

After construction is completed, site cover should be established and maintained to prevent future losses of soil from the site. Access to the site should be restricted until the site cover is fully installed or established. Site covering options, including paving, graveling, or restoring close growing vegetation (such as well maintained grass) will help to ensure that the soil remains in place, and will reduce opportunities for off-site soil transport.

Future soil disturbing activities on the site should be held to the same or greater standards as described in this plan to ensure worker safety and prevent off-site soil transport.

Exposed Soil Areas

Prior to landscaping, surface soils will be mulched or compost applied. This additional organic matter will assist with soil stabilization, facilitate plant growth, and will assist in binding potential contaminants. In addition, the cover will reduce post-project soil exposure and erosion. Areas under shrubs or trees that are unable to grow close growing vegetation (such as grass) should be maintained with a mulch cover to reduce the potential for soil exposure and erosion.

Health and Safety Guidelines

A Health and Safety Plan (HASP) will be developed for this project before the initiation of construction activities. The soil contaminant levels of arsenic observed at the proposed CPVVS site are above applicable human health screening values. Therefore, without mitigation, construction worker risks may be greater than an industrial/commercial scenario, given the potential for increased direct exposure via dermal contact, ingestion, and inhalation. The health and safety plan should address the potential for exposure to this naturally-occurring soil constituent.

References

ATSDR, 2007. Public Health Statement - Arsenic [Online]. Available at: http://www.atsdr.cdc.gov/toxprofiles/tp2-c1-b.pdf (accessed 2 July 2009).

ATSDR, 2002. Public Health Statement - DDT, DDE, and DDD [Online]. Available at: http://www.atsdr.cdc.gov/toxprofiles/tp35-c1-b.pdf (accessed 2 July 2009).

CH2M HILL, 2008. Preliminary Phase II Environmental Site Assessment for the Competitive Power Ventures Vaca Station Project, Solano County, California. Prepared for Competitive Power Ventures Vacaville, Inc. 8 Dec 2008.

Kearney Foundation of Soil Science. 1996. Background Concentrations of Trace and Major Elements in California Soil. March.

Luhdorff and Scalmanini. 2005. Shallow Groundwater Quality in the Vicinity of the Easterly Wastewater Treatment Plant, Solano County, California. August 23.

Natural Resource Conservation Service (NRCS [formerly Soil Conservation Service]). 1977. Soil Survey of Solano County, California. U.S. Department of Agriculture in cooperation with University of California Agricultural Experiment Station.

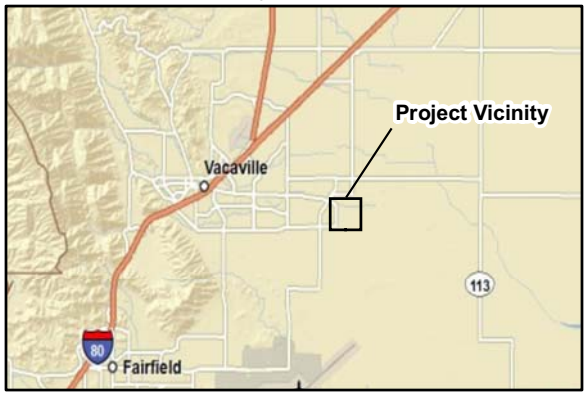
USEPA, 2005. Ecological Soil Screening Levels for Arsenic [Online]. Available at: http://www.epa.gov/ecotox/ecossl/pdf/eco-ssl_arsenic.pdf (accessed 10 July 2009).

Figure

LEGEND

- Monitoring Well
- Transformer and Utility Box
- Project Site

VICINITY MAP



N

0 375 750

Feet

This map was compiled from various scale source data and maps and is intended for use as only an approximate representation of actual locations.

FIGURE 1
SITE MAP
SOIL MANAGEMENT PLAN
CPV VACA STATION, VACAVILLE, CA

CH2MHILL

SAC\\ZION\SACGIS\PROJ\VACAVILLE_AFC_370668\MAPFILES\SOILMANGTPLAN.MXD MHASKELL 6/22/2009 10:27:17

Table 1

Table 1. Summary of Soil Samples with Concentrations Above Screening Levels

Sample ID	PRGs[1] Industrial Soil (mg/kg)	CHHSL's[2] Industrial Soil (mg/kg)	TTLC[3] Wet wt basis (mg/kg)	A1-06SB	A1-03SB	A1-05SB	A1-10SB A1-05SB-FD	A2-06SB	A2-03SB	A3-06SB	A3-03SB	A3-10SB A3-03SB-FD	A4-06SB	A4-03SB	B1-06SB	B1-03SB	B2-06SB	B2-03SB	B3-06SB	B3-03SB	B2-10SB B3-03SB-FD	B3-05SB	B4-06SB	B4-03SB	C1-06SB	C1-03SB	C2-06SB	C2-03SB	C3-06SB
% Moisture (SW3550)				4	17	17	16	3	18	3	11	14	5	16	3	17	4	12	4	17	13	17	5	11	3	13	4	18	4
Total Metals (SW6010B)																													
Arsenic	1.6 c	0.24	500	**6.7**	**9.55**	**13.8**	**8.96**	**7.3**	**11.3**	**8.8**	**8.56**	**11.2**	**11.1**	**10.7**	**7.6**	**10.4**	**7.6**	**9.89**	**7.1**	**11.3**	**8.98**	**10.9**	**8.3**	**10.4**	**10.5**	**10.6**	**7.6**	**10.6**	**7.5**
Chromium *(based on VI)*	200 c*	37	500	**45.9**	**41.5**	**35.4**	**35.8**	**39.2**	**33.4**	**40.4**	**36.7**	**39.4**	**39.7**	**37.1**	**44.5**	**38.8**	**41.5**	**39.7**	**38.4**	**35.4**	**35.6**	**25.5**	**44.2**	**41.2**	**43.7**	**41.3**	**45.4**	**42.3**	**40.1**
Pesticide Organics (SW8081A)																													
4,4'-DDE	5.1	6.3	1.0							**1.2**			**1.6**										**1.1**						

Notes:

All analytical results for soil given in mg/kg on a dry weight basis.

-06SB Samples were collected in the 0 to 6 inch bgs depth interval
-03SB, -05SB, -10SB Samples were collected in the 3-foot, 5-foot, or 10-foot bgs depth interval, respectively

U = Not detected at specified reporting limit
J = Estimated value below reporting limit

Boldface entries indicate detected constituents/compounds (including those detected between MDL and RL - 'J' flagged)

Exceeds Title 22 Hazardous Waste Criteria

Exceeds one or more of the risk-based criteria (PRGs or CHHSLs)

Exceeds the corresponding 95% Upper Confidence Limit on the geometric mean for Background Soils (using samples from all depths)

c = Cancer PRG
n = Noncancer PRG
c* = where: n screening level < 100x cancer screening level
m = concentration may exceed ceiling limit
^ = MDL's for this method are less than or equal to the screening level.

1 = USEPA Region IX Preliminary Remediation Goals (PRGs) 2008
2 = California Human Health Screening levels
3 = Total Threshold Limit Concentration (wet weight basis) that is hazardous waste criteria under California Code of Regulation, Title 22, Division 4.5, Chapter 11, Section 66261.24.

Table 1. Summary of Soil Samples with Concentrations Above Screening Levels

Sample ID	PRGs[1] Industrial Soil (mg/kg)	CHHSL's[2] Industrial Soil (mg/kg)	TTLC[3] Wet wt basis (mg/kg)	C3-03SB	C4-06SB	C4-03SB	C4-05SB	C4-10SB C4-05SB-FD	D1-06SB	D1-03SB	D2-06SB	D2-03SB	D2-05SB	D3-06SB	D3-03SB	D4-06SB	D4-03SB	E1-06SB	E1-03SB	E1-05SB	E1-10SB E1-05SB-FD	E2-06SB	E2-03SB	E3-06SB	E3-03SB	E4-06SB	E4-03SB
% Moisture (SW3550)				17	4	14	19	18	2	18	2	19	19	2	16	3	11	2	17	17	16	2	17	3	20	3	16
Total Metals (SW6010B)																											
Arsenic	1.6 c	0.24	500	**7.96**	**8.9**	**6.74**	**12.4**	**19.0**	**8.3**	**12.5**	**8.4**	**11.4**	**11.8**	**10.1**	**10.1**	**6.5**	**9.09**	**6.2**	**10.8**	**14.1**	**13.2**	**8.5**	**11.9**	**7.4**	**11.3**	**8.5**	**9.94**
Chromium *(based on VI)*	200 c*	37	500	**36.8**	**44.2**	**36.1**	**38.0**	**37.2**	**43.3**	**42.4**	**42.2**	**36.0**	**27.5**	**37.9**	**37.8**	**34.3**	**40.7**	**33.4**	**48.0**	**40.3**	**36.9**	**30.8**	**39.4**	**38.9**	**43.3**	**33.7**	**32.0**
Pesticide Organics (SW8081A)																											
4,4'-DDE	5.1	6.3	1.0		**1.3**									**1.2**		**1.2**											

Notes:

All analytical results for soil given in mg/kg on a dry weight basis.

-06SB Samples were collected in the 0 to 6 inch bgs depth interval
-03SB, -05SB, -10SB Samples were collected in the 3-foot, 5-foot, or 10-foot bgs depth interval, respectively

U = Not detected at specified reporting limit
J = Estimated value below reporting limit

Boldface entries indicate detected constituents/compounds (including those detected between MDL and RL - 'J' flagged)

Exceeds Title 22 Hazardous Waste Criteria

Exceeds one or more of the risk-based criteria (PRGs or CHHSL

Exceeds the corresponding 95% Upper Confidence Limit on the geometric mean for Background Soils (using samples from all de

c = Cancer PRG
n = Noncancer PRG
c* = where: n screening level < 100x cancer screening level
m = concentration may exceed ceiling limit
^ = MDL's for this method are less than or equal to the screening level.

1 = USEPA Region IX Preliminary Remediation Goals (PRGs) 2008
2 = California Human Health Screening levels
3 = Total Threshold Limit Concentration (wet weight basis) that is hazardous waste criteria under Calif Code of Regulation, Title 22, Division 4.5, Chapter 11, Section 66261.24.

Table 1. Summary of Soil Samples with Concentrations Above Screening Levels

Sample ID	PRGs[1] Industrial Soil (mg/kg)	CHHSL's[2] Industrial Soil (mg/kg)	TTLC[3] Wet wt basis (mg/kg)	BG1-06SB	BG1-06.5SB	BG1-09.5SB	BG2-06SB	BG2-05SB	BG2-08SB	BG3-06SB	BG3-04SB	BG3-07SB	BG4-06SB	BG4-03SB	BG4-05SB	BG5-06SB	BG5-03SB	BG5-05SB
% Moisture (SW3550)				2	16	17	2	22	17	Not collected	17	17	3	17	22	2	17	16
Total Metals (SW6010B)																		
Arsenic	1.6 c	0.24	500	**9.0**	**9.51**	**13.0**	**7.4**	**9.79**	**12.0**		**11.2**	**7.06**	**9.0**	**10.4**	**11.5**	**9.8**	**9.52**	**11.7**
Chromium *(based on VI)*	200 c*	37	500	**38.1**	**39.5**	**44.0**	**36.6**	**37.7**	**40.5**		**38.0**	**39.0**	**34.8**	**40.1**	**44.9**	**38.4**	**41.3**	**39.3**
Pesticide Organics (SW8081A)																		
4,4'-DDE	5.1	6.3	1.0													**1.3**		

Notes:

All analytical results for soil given in mg/kg on a dry weight basis.

-06SB Samples were collected in the 0 to 6 inch bgs depth interval
-03SB, -05SB, -10SB Samples were collected in the 3-foot, 5-foot, or 10-foot bgs depth interval, respectively

U = Not detected at specified reporting limit
J = Estimated value below reporting limit

Boldface entries indicate detected constituents/compounds (including those detected between MDL and RL - 'J' flagged)

Exceeds Title 22 Hazardous Waste Criteria

Exceeds one or more of the risk-based criteria (PRGs or CHHSL

Exceeds the corresponding 95% Upper Confidence Limit on the geometric mean for Background Soils (using samples from all de

c = Cancer PRG
n = Noncancer PRG
c* = where: n screening level < 100x cancer screening level
m = concentration may exceed ceiling limit
^ = MDL's for this method are less than or equal to the screening level.

1 = USEPA Region IX Preliminary Remediation Goals (PRGs) 2008
2 = California Human Health Screening levels
3 = Total Threshold Limit Concentration (wet weight basis) that is hazardous waste criteria under Calif Code of Regulation, Title 22, Division 4.5, Chapter 11, Section 66261.24.

APPENDIX A

ATSDR Public Health Statement for Arsenic and DDT, DDE, and DDD

PUBLIC HEALTH STATEMENT
Arsenic
CAS#: 7440-38-2

Division of Toxicology and Environmental Medicine **August 2007**

This Public Health Statement is the summary chapter from the Toxicological Profile for Arsenic. It is one in a series of Public Health Statements about hazardous substances and their health effects. A shorter version, the ToxFAQs™, is also available. This information is important because this substance may harm you. The effects of exposure to any hazardous substance depend on the dose, the duration, how you are exposed, personal traits and habits, and whether other chemicals are present. For more information, call the ATSDR Information Center at 1-800-232-4636.

This public health statement tells you about arsenic and the effects of exposure to it.

The Environmental Protection Agency (EPA) identifies the most serious hazardous waste sites in the nation. These sites are then placed on the National Priorities List (NPL) and are targeted for long-term federal clean-up activities. Arsenic has been found in at least 1,149 of the 1,684 current or former NPL sites. Although the total number of NPL sites evaluated for this substance is not known, the possibility exists that the number of sites at which arsenic is found may increase in the future as more sites are evaluated. This information is important because these sites may be sources of exposure and exposure to this substance may harm you.

When a substance is released either from a large area, such as an industrial plant, or from a container, such as a drum or bottle, it enters the environment. Such a release does not always lead to exposure. You can be exposed to a substance only when you come in contact with it. You may be exposed by breathing, eating, or drinking the substance, or by skin contact.

If you are exposed to arsenic, many factors will determine whether you will be harmed. These factors include the dose (how much), the duration (how long), and how you come in contact with it. You must also consider any other chemicals you are exposed to and your age, sex, diet, family traits, lifestyle, and state of health.

1.1 WHAT IS ARSENIC?

Arsenic is a naturally occurring element that is widely distributed in the Earth's crust. Arsenic is classified chemically as a metalloid, having both properties of a metal and a nonmetal; however, it is frequently referred to as a metal. Elemental arsenic (sometimes referred to as metallic arsenic) is a steel grey solid material. However, arsenic is usually found in the environment combined with other elements such as oxygen, chlorine, and sulfur. Arsenic combined with these elements is called inorganic arsenic. Arsenic combined with carbon and hydrogen is referred to as organic arsenic.

Most inorganic and organic arsenic compounds are white or colorless powders that do not evaporate. They have no smell, and most have no special taste. Thus, you usually cannot tell if arsenic is present in your food, water, or air.

Inorganic arsenic occurs naturally in soil and in many kinds of rock, especially in minerals and ores that contain copper or lead. When these ores are heated in smelters, most of the arsenic goes up the stack and enters the air as a fine dust. Smelters may collect this dust and take out the arsenic as a compound called arsenic trioxide (As_2O_3).

However, arsenic is no longer produced in the United States; all of the arsenic used in the United States is imported.

Presently, about 90% of all arsenic produced is used as a preservative for wood to make it resistant to rotting and decay. The preservative is copper chromated arsenate (CCA) and the treated wood is referred to as "pressure-treated." In 2003, U.S. manufacturers of wood preservatives containing arsenic began a voluntary transition from CCA to other wood preservatives that do not contain arsenic in wood products for certain residential uses, such as play structures, picnic tables, decks, fencing, and boardwalks. This phase out was completed on December 31, 2003; however, wood treated prior to this date could still be used and existing structures made with CCA-treated wood would not be affected. CCA-treated wood products continue to be used in industrial applications. It is not known whether, or to what extent, CCA-treated wood products may contribute to exposure of people to arsenic.

In the past, inorganic arsenic compounds were predominantly used as pesticides, primarily on cotton fields and in orchards. Inorganic arsenic compounds can no longer be used in agriculture. However, organic arsenic compounds, namely cacodylic acid, disodium methylarsenate (DSMA), and monosodium methylarsenate (MSMA), are still used as pesticides, principally on cotton. Some organic arsenic compounds are used as additives in animal feed. Small quantities of elemental arsenic are added to other metals to form metal mixtures or alloys with improved properties. The greatest use of arsenic in alloys is in lead-acid batteries for automobiles. Another important use of arsenic compounds is in semiconductors and light-emitting diodes.

1.2 WHAT HAPPENS TO ARSENIC WHEN IT ENTERS THE ENVIRONMENT?

Arsenic occurs naturally in soil and minerals and it therefore may enter the air, water, and land from wind-blown dust and may get into water from runoff and leaching. Volcanic eruptions are another source of arsenic. Arsenic is associated with ores containing metals, such as copper and lead. Arsenic may enter the environment during the mining and smelting of these ores. Small amounts of arsenic also may be released into the atmosphere from coal-fired power plants and incinerators because coal and waste products often contain some arsenic.

Arsenic cannot be destroyed in the environment. It can only change its form, or become attached to or separated from particles. It may change its form by reacting with oxygen or other molecules present in air, water, or soil, or by the action of bacteria that live in soil or sediment. Arsenic released from power plants and other combustion processes is usually attached to very small particles. Arsenic contained in wind-borne soil is generally found in larger particles. These particles settle to the ground or are washed out of the air by rain. Arsenic that is attached to very small particles may stay in the air for many days and travel long distances. Many common arsenic compounds can dissolve in water. Thus, arsenic can get into lakes, rivers, or underground water by dissolving in rain or snow or through the discharge of industrial wastes. Some of the arsenic will stick to particles in the water or sediment on the bottom of lakes or rivers, and some

will be carried along by the water. Ultimately, most arsenic ends up in the soil or sediment. Although some fish and shellfish take in arsenic, which may build up in tissues, most of this arsenic is in an organic form called arsenobetaine (commonly called "fish arsenic") that is much less harmful.

1.3 HOW MIGHT I BE EXPOSED TO ARSENIC?

Since arsenic is found naturally in the environment, you will be exposed to some arsenic by eating food, drinking water, or breathing air. Children may also be exposed to arsenic by eating soil. Analytical methods used by scientists to determine the levels of arsenic in the environment generally do not determine the specific form of arsenic present. Therefore, we do not always know the form of arsenic a person may be exposed to. Similarly, we often do not know what forms of arsenic are present at hazardous waste sites. Some forms of arsenic may be so tightly attached to particles or embedded in minerals that they are not taken up by plants and animals.

The concentration of arsenic in soil varies widely, generally ranging from about 1 to 40 parts of arsenic to a million parts of soil (ppm) with an average level of 3–4 ppm. However, soils in the vicinity of arsenic-rich geological deposits, some mining and smelting sites, or agricultural areas where arsenic pesticides had been applied in the past may contain much higher levels of arsenic. The concentration of arsenic in natural surface and groundwater is generally about 1 part in a billion parts of water (1 ppb), but may exceed 1,000 ppb in contaminated areas or where arsenic levels in soil are high. Groundwater is far more likely to contain high levels of arsenic than surface water. Surveys of U.S. drinking water indicate that about 80% of water supplies have less than 2 ppb of arsenic, but 2% of supplies exceed 20 ppb of arsenic. Levels of arsenic in food range from about 20 to 140 ppb. However, levels of inorganic arsenic, the form of most concern, are far lower. Levels of arsenic in the air generally range from less than 1 to about 2,000 nanograms (1 nanogram equals a billionth of a gram) of arsenic per cubic meter of air (less than 1–2,000 ng/m^3), depending on location, weather conditions, and the level of industrial activity in the area. However, urban areas generally have mean arsenic levels in air ranging from 20 to 30 ng/m^3.

You normally take in small amounts of arsenic in the air you breathe, the water you drink, and the food you eat. Of these, food is usually the largest source of arsenic. The predominant dietary source of arsenic is seafood, followed by rice/rice cereal, mushrooms, and poultry. While seafood contains the greatest amounts of arsenic, for fish and shellfish, this is mostly in an organic form of arsenic called arsenobetaine that is much less harmful. Some seaweeds may contain arsenic in inorganic forms that may be more harmful. Children are likely to eat small amounts of dust or soil each day, so this is another way they may be exposed to arsenic. The total amount of arsenic you take in from these sources is generally about 50 micrograms (1 microgram equals one-millionth of a gram) each day. The level of inorganic arsenic (the form of most concern) you take in from these sources is generally about 3.5 microgram/day. Children may be exposed to small amounts of arsenic from hand-to-mouth activities from playing on play structures or decks constructed out of CCA-treated wood. The potential exposure that children

may receive from playing in play structures constructed from CCA-treated wood is generally smaller than that they would receive from food and water.

In addition to the normal levels of arsenic in air, water, soil, and food, you could be exposed to higher levels in several ways, such as the following:

- Some areas of the United States contain unusually high natural levels of arsenic in rock, and this can lead to unusually high levels of arsenic in soil or water. If you live in an area like this, you could take in elevated amounts of arsenic in drinking water. Children may be taking in higher amounts of arsenic because of hand-to-mouth contact or eating soil in areas with higher than usual arsenic concentrations.

- Some hazardous waste sites contain large quantities of arsenic. If the material is not properly disposed of, it can get into surrounding water, air, or soil. If you live near such a site, you could be exposed to elevated levels of arsenic from these media.

- If you work in an occupation that involves arsenic production or use (for example, copper or lead smelting, wood treating, or pesticide application), you could be exposed to elevated levels of arsenic during your work.

- If you saw or sand arsenic-treated wood, you could inhale some of the sawdust into your nose or throat. Similarly, if you burn arsenic-treated wood, you could inhale arsenic in the smoke.

- If you live in a former agricultural area where arsenic was used on crops, the soil could contain high levels of arsenic.

- In the past, several kinds of products used in the home (rat poison, ant poison, weed killer, some types of medicines) had arsenic in them. However, most of these uses of arsenic have ended, so you are not likely to be exposed from home products any longer.

1.4 HOW CAN ARSENIC ENTER AND LEAVE MY BODY?

If you swallow arsenic in water, soil, or food, most of the arsenic may quickly enter into your body. The amount that enters your body will depend on how much you swallow and the kind of arsenic that you swallow. This is the most likely way for you to be exposed near a waste site. If you breathe air that contains arsenic dusts, many of the dust particles settle onto the lining of the lungs. Most of the arsenic in these particles is then taken up from the lungs into the body. You might be exposed in this way near waste sites where arsenic-contaminated soils are allowed to blow into the air, or if you work with arsenic-containing soil or products. If you get arsenic-contaminated soil or water on your skin, only a small amount will go through your skin into your body, so this is usually not of concern.

Both inorganic and organic forms leave your body in your urine. Most of the inorganic arsenic will be gone within several days, although some will remain in your body for several months or even longer. If you are exposed to organic arsenic, most of it will leave your body within several days.

1.5 HOW CAN ARSENIC AFFECT MY HEALTH?

Scientists use many tests to protect the public from harmful effects of toxic chemicals and to find ways for treating persons who have been harmed.

One way to learn whether a chemical will harm people is to determine how the body absorbs, uses, and releases the chemical. For some chemicals, animal testing may be necessary. Animal testing may also help identify health effects such as cancer or birth defects. Without laboratory animals, scientists would lose a basic method for getting information needed to make wise decisions that protect public health. Scientists have the responsibility to treat research animals with care and compassion. Scientists must comply with strict animal care guidelines because laws today protect the welfare of research animals.

Inorganic arsenic has been recognized as a human poison since ancient times, and large oral doses (above 60,000 ppb in water which is 10,000 times higher than 80% of U.S. drinking water arsenic levels) can result in death. If you swallow lower levels of inorganic arsenic (ranging from about 300 to 30,000 ppb in water; 100–10,000 times higher than most U.S. drinking water levels), you may experience irritation of your stomach and intestines, with symptoms such as stomachache, nausea, vomiting, and diarrhea. Other effects you might experience from swallowing inorganic arsenic include decreased production of red and white blood cells, which may cause fatigue, abnormal heart rhythm, blood-vessel damage resulting in bruising, and impaired nerve function causing a "pins and needles" sensation in your hands and feet.

Perhaps the single-most characteristic effect of long-term oral exposure to inorganic arsenic is a pattern of skin changes. These include patches of darkened skin and the appearance of small "corns" or "warts" on the palms, soles, and torso, and are often associated with changes in the blood vessels of the skin. Skin cancer may also develop. Swallowing arsenic has also been reported to increase the risk of cancer in the liver, bladder, and lungs. The Department of Health and Human Services (DHHS) has determined that inorganic arsenic is known to be a human carcinogen (a chemical that causes cancer). The International Agency for Research on Cancer (IARC) has determined that inorganic arsenic is carcinogenic to humans. EPA also has classified inorganic arsenic as a known human carcinogen.

If you breathe high levels of inorganic arsenic, then you are likely to experience a sore throat and irritated lungs. You may also develop some of the skin effects mentioned above. The exposure level that produces these effects is uncertain, but it is probably above 100 micrograms of arsenic per cubic meter ($\mu g/m^3$) for a brief exposure. Longer exposure at lower concentrations can lead to skin effects, and also to circulatory and peripheral nervous disorders. There are some data suggesting that inhalation of inorganic arsenic may also

interfere with normal fetal development, although this is not certain. An important concern is the ability of inhaled inorganic arsenic to increase the risk of lung cancer. This has been seen mostly in workers exposed to arsenic at smelters, mines, and chemical factories, but also in residents living near smelters and arsenical chemical factories. People who live near waste sites with arsenic may have an increased risk of lung cancer as well.

If you have direct skin contact with high concentrations of inorganic arsenic compounds, your skin may become irritated, with some redness and swelling. However, it does not appear that skin contact is likely to lead to any serious internal effects.

Almost no information is available on the effects of organic arsenic compounds in humans. Studies in animals show that most simple organic arsenic compounds (such as methyl and dimethyl compounds) are less toxic than the inorganic forms. In animals, ingestion of methyl compounds can result in diarrhea, and lifetime exposure can damage the kidneys. Lifetime exposure to dimethyl compounds can damage the urinary bladder and the kidneys.

1.6 HOW CAN ARSENIC AFFECT CHILDREN?

This section discusses potential health effects in humans from exposures during the period from conception to maturity at 18 years of age.

Children are exposed to arsenic in many of the same ways that adults are. Since arsenic is found in the soil, water, food, and air, children may take in arsenic in the air they breathe, the water they drink, and the food they eat. Since children tend to eat or drink less of a variety of foods and beverages than do adults, ingestion of contaminated food or juice or infant formula made with arsenic-contaminated water may represent a significant source of exposure. In addition, since children often play in the soil and put their hands in their mouths and sometimes intentionally eat soil, ingestion of contaminated soil may be a more important source of arsenic exposure for children than for adults. In areas of the United States where natural levels of arsenic in the soil and water are high, or in areas in and around contaminated waste sites, exposure of children to arsenic through ingestion of soil and water may be significant. In addition, contact with adults who are wearing clothes contaminated with arsenic (e.g., with dust from copper- or lead-smelting factories, from wood-treating or pesticide application, or from arsenic-treated wood) could be a source of exposure. Because of the tendency of children to taste things that they find, accidental poisoning from ingestion of pesticides is also a possibility. Thus, although most of the exposure pathways for children are the same as those for adults, children may be at a higher risk of exposure because of normal hand-to-mouth activity.

Children who are exposed to inorganic arsenic may have many of the same effects as adults, including irritation of the stomach and intestines, blood vessel damage, skin changes, and reduced nerve function. Thus, all health effects observed in adults are of potential concern in children. There is also some evidence that suggests that long-term exposure to inorganic arsenic in children may result in lower IQ scores. We do not know if absorption of inorganic arsenic from the gut in children differs from adults.

There is some evidence that exposure to arsenic in early life (including gestation and early childhood) may increase mortality in young adults.

There is some evidence that inhaled or ingested inorganic arsenic can injure pregnant women or their unborn babies, although the studies are not definitive. Studies in animals show that large doses of inorganic arsenic that cause illness in pregnant females can also cause low birth weight, fetal malformations, and even fetal death. Arsenic can cross the placenta and has been found in fetal tissues. Arsenic is found at low levels in breast milk.

In animals, exposure to organic arsenic compounds can cause low birth weight, fetal malformations, and fetal deaths. The dose levels that cause these effects also result in effects in the mothers.

1.7 HOW CAN FAMILIES REDUCE THE RISK OF EXPOSURE TO ARSENIC?

If your doctor finds that you have been exposed to substantial amounts of arsenic, ask whether your children might also have been exposed. Your doctor might need to ask your state health department to investigate.

Many communities may have high levels of arsenic in their drinking water, particularly from private wells, because of contamination or as a result of the geology of the area. The north central region and the western region of the United States have the highest arsenic levels in surface water and groundwater sources, respectively. Wells used to provide water for drinking and cooking should be tested for arsenic. As of January 2006, EPA's Maximum Contaminant Level (MCL) for arsenic in drinking water is 10 ppb. If you have arsenic in your drinking water at levels higher that the EPA's MCL, an alternative source of water should be used for drinking and cooking should be considered.

If you use arsenic-treated wood in home projects, personal protection from exposure to arsenic-containing sawdust may be helpful in limiting exposure of family members. These measures may include dust masks, gloves, and protective clothing. Arsenic-treated wood should never be burned in open fires, or in stoves, residential boilers, or fire places, and should not be composted or used as mulch. EPA's Consumer Awareness Program (CAP) for CCA is a voluntary program established by the manufacturers of CCA products to inform consumers about the proper handling, use, and disposal of CCA-treated wood. You can find more information about this program in Section 6.5. Hand washing can reduce the potential exposure of children to arsenic after playing on play structures constructed with CCA-treated wood, since most of the arsenic on the children's hands was removed with water.

If you live in an area with a high level of arsenic in the water or soil, substituting cleaner sources of water and limiting contact with soil (for example, through use of a dense groundcover or thick lawn) would reduce family exposure to arsenic. By paying careful attention to dust and soil control in the home (air filters, frequent cleaning), you can reduce family exposure to contaminated soil. Some children eat a lot of soil. You should prevent your children from eating soil. You should discourage your children from putting objects in their mouths. Make sure they wash their hands frequently and

before eating. Discourage your children from putting their hands in their mouths or engaging in other hand-to-mouth activities. Since arsenic may be found in the home as a pesticide, household chemicals containing arsenic should be stored out of reach of young children to prevent accidental poisonings. Always store household chemicals in their original labeled containers; never store household chemicals in containers that children would find attractive to eat or drink from, such as old soda bottles. Keep your Poison Control Center's number by the phone.

It is sometimes possible to carry arsenic from work on your clothing, skin, hair, tools, or other objects removed from the workplace. This is particularly likely if you work in the fertilizer, pesticide, glass, or copper/lead smelting industries. You may contaminate your car, home, or other locations outside work where children might be exposed to arsenic. You should know about this possibility if you work with arsenic.

Your occupational health and safety officer at work can and should tell you whether chemicals you work with are dangerous and likely to be carried home on your clothes, body, or tools and whether you should be showering and changing clothes before you leave work, storing your street clothes in a separate area of the workplace, or laundering your work clothes at home separately from other clothes. Material safety data sheets (MSDS) for many chemicals used should be found at your place of work, as required by the Occupational Safety and Health Administration (OSHA) in the U.S. Department of Labor. MSDS information should include chemical names and hazardous ingredients, and important properties, such as fire and explosion data, potential health effects, how you get the chemical(s) in your body, how to properly handle the materials, and what to do in the case of emergencies. Your employer is legally responsible for providing a safe workplace and should freely answer your questions about hazardous chemicals. Your state OSHA-approved occupational safety and health program or OSHA can answer any further questions and help your employer identify and correct problems with hazardous substances. Your state OSHA-approved occupational safety and health program or OSHA will listen to your formal complaints about workplace health hazards and inspect your workplace when necessary. Employees have a right to seek safety and health on the job without fear of punishment.

1.8 IS THERE A MEDICAL TEST TO DETERMINE WHETHER I HAVE BEEN EXPOSED TO ARSENIC?

Several sensitive and specific tests can measure arsenic in your blood, urine, hair, or fingernails, and these tests are often helpful in determining if you have been exposed to above-average levels of arsenic in the past. These tests are not usually performed in a doctor's office. They require sending the sample to a testing laboratory.

Measurement of arsenic in your urine is the most reliable means of detecting arsenic exposures that you experienced within the last several days. Most tests measure the total amount of arsenic present in your urine. This can sometimes be misleading, because the nonharmful forms of arsenic in fish and shellfish can give a high reading even if you have not been exposed to a toxic form of arsenic. For this reason, laboratories sometimes use a more

complicated test to separate "fish arsenic" from other forms. Because most arsenic leaves your body within a few days, analysis of your urine cannot detect if you were exposed to arsenic in the past. Tests of your hair or fingernails can tell if you were exposed to high levels over the past 6–12 months, but these tests are not very useful in detecting low-level exposures. If high levels of arsenic are detected, this shows that you have been exposed, but unless more is known about when you were exposed and for how long, it is usually not possible to predict whether you will have any harmful health effects.

1.9 WHAT RECOMMENDATIONS HAS THE FEDERAL GOVERNMENT MADE TO PROTECT HUMAN HEALTH?

The federal government develops regulations and recommendations to protect public health. Regulations *can* be enforced by law. The EPA, the Occupational Safety and Health Administration (OSHA), and the Food and Drug Administration (FDA) are some federal agencies that develop regulations for toxic substances. Recommendations provide valuable guidelines to protect public health, but *cannot* be enforced by law. The Agency for Toxic Substances and Disease Registry (ATSDR) and the National Institute for Occupational Safety and Health (NIOSH) are two federal organizations that develop recommendations for toxic substances.

Regulations and recommendations can be expressed as "not-to-exceed" levels, that is, levels of a toxic substance in air, water, soil, or food that do not exceed a critical value that is usually based on levels that affect animals; they are then adjusted to levels that will help protect humans. Sometimes these not-to-exceed levels differ among federal organizations because they used different exposure times (an 8-hour workday or a 24-hour day), different animal studies, or other factors.

Recommendations and regulations are also updated periodically as more information becomes available. For the most current information, check with the federal agency or organization that provides it. Some regulations and recommendations for ARSENIC include the following:

The federal government has taken several steps to protect humans from arsenic. First, EPA has set limits on the amount of arsenic that industrial sources can release into the environment. Second, EPA has restricted or canceled many of the uses of arsenic in pesticides and is considering further restrictions. Third, in January 2001, the EPA lowered the limit for arsenic in drinking water from 50 to 10 ppb. Finally, OSHA has established a permissible exposure limit (PEL), 8-hour time-weighted average, of 10 $\mu g/m^3$ for airborne arsenic in various workplaces that use inorganic arsenic.

1.10 WHERE CAN I GET MORE INFORMATION?

If you have any more questions or concerns, please contact your community or state health or environmental quality department, or contact ATSDR at the address and phone number below.

ATSDR can also tell you the location of occupational and environmental health clinics. These clinics specialize in recognizing, evaluating,

and treating illnesses that result from exposure to hazardous substances.

Toxicological profiles are also available on-line at www.atsdr.cdc.gov and on CD-ROM. You may request a copy of the ATSDR ToxProfiles™ CD-ROM by calling the toll-free information and technical assistance number at 1-800-CDCINFO (1-800-232-4636), by e-mail at cdcinfo@cdc.gov, or by writing to:

Agency for Toxic Substances and Disease Registry
Division of Toxicology and Environmental Medicine
1600 Clifton Road NE
Mailstop F-32
Atlanta, GA 30333
Fax: 1-770-488-4178

Organizations for-profit may request copies of final Toxicological Profiles from the following:

National Technical Information Service (NTIS)
5285 Port Royal Road
Springfield, VA 22161
Phone: 1-800-553-6847 or 1-703-605-6000
Web site: http://www.ntis.gov/

PUBLIC HEALTH STATEMENT
DDT, DDE, and DDD

CAS#: DDT 50-29-3
DDE 72-55-9
DDD 72-54-8

Division of Toxicology **September 2002**

This Public Health Statement is the summary chapter from the Toxicological Profile for DDT, DDE, and DDD. It is one in a series of Public Health Statements about hazardous substances and their health effects. A shorter version, the ToxFAQs™ is also available. This information is important because this substance may harm you. The effects of exposure to any hazardous substance depend on the dose, the duration, how you are exposed, personal traits and habits, and whether other chemicals are present. For more information, call the ATSDR Information Center at 1-888-422-8737.

This public health statement tells you about DDT, DDE, and DDD and the effects of exposure.

The Environmental Protection Agency (EPA) identifies the most serious hazardous waste sites in the nation. These sites make up the National Priorities List (NPL) and are the sites targeted for long-term federal cleanup activities. DDT, DDE, and DDD have been found in at least 442 of the 1,613 current or former NPL sites. However, the total number of NPL sites evaluated for these substances is not known. As more sites are evaluated, the sites at which DDT, DDE, and DDD are found may increase. This information is important because exposure to these substances may harm you and because these sites may be sources of exposure.

When a substance is released from a large area, such as an industrial plant, or from a container, such as a drum or bottle, it enters the environment. This release does not always lead to exposure. You are exposed to a substance only when you come in contact with it. You may be exposed by breathing, eating, or drinking the substance, or by skin contact.

If you are exposed to DDT, DDE, and DDD, many factors determine whether you'll be harmed. These factors include the dose (how much), the duration (how long), and how you come in contact with them. You must also consider the other chemicals you're exposed to and your age, sex, diet, family traits, lifestyle, and state of health.

While this document is specifically focused on the primary forms or isomers of DDT, DDE, and DDD (namely p,p'-DDT, p,p'-DDE, and p,p'-DDD), other isomers of these compounds will be discussed when appropriate. In some cases, the term DDT will be used to refer to the collection of all forms of DDT, DDE, and DDD. Should this not be clear from the context, the term ΣDDT (Σ is used to mean sum of) will be used.

1.1 WHAT ARE DDT, DDE, AND DDD?

DDT (1,1,1-trichloro-2,2-bis(p-chlorophenyl)ethane) is a pesticide that was once widely used to control insects on agricultural crops and insects that carry diseases like malaria and typhus, but is now used in only a few countries to control malaria. Technical-grade DDT is a mixture of three forms, p,p'-DDT (85%), o,p'-DDT (15%), and o,o'-DDT (trace amounts). All of these are white, crystalline, tasteless, and almost odorless solids. Technical grade DDT may also contain DDE (1,1-dichloro-2,2-bis(p-chlorophenyl)ethylene) and DDD (1,1-dichloro-2,2-bis(p-chlorophenyl)ethane) as contaminants. DDD was also used to kill pests,

but to a far lesser extent than DDT. One form of DDD (o,p'-DDD) has been used medically to treat cancer of the adrenal gland. Both DDE and DDD are breakdown products of DDT.

DDT does not occur naturally in the environment. After 1972, the use of DDT was no longer permitted in the United States except in cases of a public health emergency. It is, however, still used in some other areas of the world, most notably for controlling malaria. The use of DDD to kill pests has also been banned in the United States.

1.2 WHAT HAPPENS TO DDT, DDE, AND DDD WHEN THEY ENTER THE ENVIRONMENT?

Before 1973 when it was banned, DDT entered the air, water, and soil during its production and use as an insecticide. DDT is present at many waste sites, including NPL sites; releases from these sites might continue to contaminate the environment. Most DDT in the environment is a result of past use; DDD was also used as a pesticide to a limited extent in the past. DDT still enters the environment because of its current use in other areas of the world. DDE is only found in the environment as a result of contamination or breakdown of DDT. DDD also enters the environment during the breakdown of DDT.

Large amounts of DDT were released into the air and on soil or water when it was sprayed on crops and forests to control insects. DDT was also sprayed in the environment to control mosquitos. Although the use of DDT is no longer permitted in the United States, DDT may be released into the atmosphere in other countries where it is still manufactured and used, including Mexico. DDT, DDE and DDD may also enter the air when they evaporate from contaminated water and soil. DDT, DDE, and DDD in the air will then be deposited on land or surface water. This cycle of evaporation and deposition may be repeated many times. As a result, DDT, DDE, and DDD can be carried long distances in the atmosphere. These chemicals have been found in bogs, snow, and animals in the Arctic and Antarctic regions, far from where they were ever used. Some DDT may have entered the soil from waste sites. DDT, DDE, and DDD may occur in the atmosphere as a vapor or be attached to solids in air. Vapor phase DDT, DDE, and DDD may break down in the atmosphere due to reactions caused by the sun. The half-life of these chemicals in the atmosphere as vapors (the time it takes for one-half of the chemical to turn into something else) has been calculated to be approximately 1.5-3 days. However, in reality, this half-life estimate is too short to account for the ability of DDT, DDE, and DDD to be carried long distances in the atmosphere.

DDT, DDE, and DDD last in the soil for a very long time, potentially for hundreds of years. Most DDT breaks down slowly into DDE and DDD, generally by the action of microorganisms. These chemicals may also evaporate into the air and be deposited in other places. They stick strongly to soil, and therefore generally remain in the surface layers of soil. Some soil particles with attached DDT, DDE, or DDD may get into rivers and lakes in runoff. Only a very small amount, if any, will seep into the ground and get into groundwater. The length of time that DDT will last in soil depends on many factors including temperature, type of soil, and

whether the soil is wet. DDT lasts for a much shorter time in the tropics where the chemical evaporates faster and where microorganisms degrade it faster. DDT disappears faster when the soil is flooded or wet than when it is dry. DDT disappears faster when it initially enters the soil. Later on, evaporation slows down and some DDT moves into spaces in the soil that are so small that microorganisms cannot reach the DDT to break it down efficiently. In tropical areas, ΣDDT may disappear in much less than a year. In temperate areas, half of the ΣDDT initially present usually disappears in about 5 years. However, in some cases, half of the ΣDDT initially present will remain for 20, 30, or more years.

In surface water, DDT will bind to particles in the water, settle, and be deposited in the sediment. DDT is taken up by small organisms and fish in the water. It accumulates to high levels in fish and marine mammals (such as seals and whales), reaching levels many thousands of times higher than in water. In these animals, the highest levels of DDT are found in their adipose tissue. DDT in soil can also be absorbed by some plants and by the animals or people who eat those crops.

1.3 HOW MIGHT I BE EXPOSED TO DDT, DDE, AND DDD?

People in the United States are exposed to DDT, DDE, and DDD mainly by eating foods containing small amounts of these compounds. Although not common today, exposure to DDT could also occur through inhalation or absorption through the skin during the handling or application of DDT. Even though DDT has not been used in this country since 1972, soil may still contain some DDT that may be taken up by plants and eaten by animals and people. DDT from contaminated water and sediment may be taken up by fish. The amount of DDT in food has greatly decreased since DDT was banned and should continue to decline. In the years 1986 to 1991, the average adult in the United States consumed an average of 0.8 micrograms (a microgram is a millionth of a gram) of DDT a day. Adults consumed slightly different amounts based on their age and sex. The largest fraction of DDT in a person's diet comes from meat, poultry, dairy products, and fish, including the consumption of sport fish. Leafy vegetables generally contain more DDT than other vegetables, possibly because DDT in the air is deposited on the leaves. Infants may be exposed by drinking breast milk.

DDT or its breakdown products are still present in some air, water, and soil samples. However, levels in most air and water samples are presently so low that exposure is of little concern. DDT levels in air have declined to such low levels that it often cannot be detected. In cases where DDT has been detected in air, it is associated with air masses coming from regions where DDT is still used or from the evaporated DDT from contaminated water or soil. p,p'-DDT and p,p'-DDE concentrations measured in air in the Great Lakes region in 1990 reached maximum levels of 0.035 and 0.119 nanograms (a nanogram is a billionth of a gram) of chemical per cubic meter of air (ng/m^3), respectively. Levels were generally much lower, especially during the winter months. In 1995-1996, soils in the corn belt, where DDT was heavily used in the past, contained on the average about 10 nanograms of DDT in a

gram of soil. In recent years, most surface water has not contained detectable amounts of DDT.

People who work or live around NPL sites or work with contaminated soil or sediment would most likely be exposed by accidentally swallowing soil, having skin contact with the soil, inhaling DDT vapor, or breathing in DDT in dust.

1.4 HOW CAN DDT, DDE, AND DDD ENTER AND LEAVE MY BODY?

Today in the United States, DDT, DDE, or DDD enters the body mainly when a person eats contaminated food. The actual amounts of DDT, DDE, and DDD absorbed from foods depends on both the concentration of chemical in the food and the amount of food eaten. Small amounts of DDT, DDE, and DDD may also be breathed in and absorbed into the body. DDT, DDE, and DDD are often attached to particles too large to pass very far into the lungs after air containing them is breathed. These particles are more likely to be carried upward in the mucus of the air passages and swallowed than for the DDT to be absorbed in the lungs. DDT, DDE, and DDD do not enter the body through the skin very easily.

Once inside the body, DDT can break down to DDE or DDD. DDE and DDD, in turn, break down to other substances (called metabolites). DDT, DDE, and DDD are stored most readily in fatty tissue, especially DDE. Some of these stored amounts leave the body very slowly. Levels in fatty tissues may either remain relatively the same over time or even increase with continued exposure. However, as exposure decreases, the amount of DDT in the body also decreases. DDT metabolites leave the body mostly in urine, but may also leave by breast milk and pass directly to nursing infants.

1.5 HOW CAN DDT, DDE, AND DDD AFFECT MY HEALTH?

Eating food with large amounts (grams) of DDT over a short time would most likely affect the nervous system. People who swallowed large amounts of DDT became excitable and had tremors and seizures. They also experienced sweating, headache, nausea, vomiting, and dizziness. These effects on the nervous system went away once exposure stopped. The same type of effects would be expected by breathing DDT particles in the air or by contact of the skin with high amounts of DDT. Tests in laboratory animals confirm the effect of DDT on the nervous system.

No effects have been reported in adults given small daily doses of DDT by capsule for 18 months (up to 35 milligrams [mg] every day). People exposed for a long time to small amounts of DDT (less than 20 mg per day), such as people who worked in factories where DDT was made, had some minor changes in the levels of liver enzymes in the blood. A study in humans showed that increasing concentrations of p,p'-DDE in human breast milk were associated with reductions in the duration of lactation. An additional study in humans found that as the DDE levels in the blood of pregnant women increased, the chances of having a pre-term baby also increased. It should be mentioned, however, that the levels of DDE in the blood at which this was noticed were higher than those currently found in women from the general population in the United

States, but not higher than those that may be found in women in countries where DDT is still being used.

To protect the public from the harmful effects of toxic chemicals and to find ways to treat people who have been harmed, scientists use many tests.

One way to see if a chemical will hurt people is to learn how the chemical is absorbed, used, and released by the body; for some chemicals, animal testing may be necessary. Animal testing may also be used to identify health effects such as cancer or birth defects. Without laboratory animals, scientists would lose a basic method to get information needed to make wise decisions to protect public health. Scientists have the responsibility to treat research animals with care and compassion. Laws today protect the welfare of research animals, and scientists must comply with strict animal care guidelines.

Animal studies show that long-term exposure to moderate amounts of DDT (20-50 mg per kilogram [kg] of body weight every day) may affect the liver. Tests in animals also suggest that short-term exposure to DDT and metabolites in food may have a harmful effect on reproduction. In addition, we know that some breakdown products of DDT can cause harmful effects on the adrenal gland. This gland is situated near the kidney and produces hormones (substances produced by organs and released to the bloodstream to regulate the function of other organs).

Studies in animals have shown that oral exposure to DDT can cause liver cancer. Studies of DDT-exposed workers did not show increases in deaths or cancers. Based on all of the evidence available, the Department of Health and Human Services has determined that DDT is reasonably anticipated to be a human carcinogen. Similarly, the International Agency for Research on Cancer (IARC) has determined that DDT is possibly carcinogenic to humans. EPA has determined that DDT, DDE, and DDD are probable human carcinogens.

1.6 HOW CAN DDT, DDE, AND DDD AFFECT CHILDREN?

This section discusses potential health effects from exposures during the period from conception to maturity at 18 years of age in humans.

Children can be exposed to DDT, DDE, or DDD by eating food or drinking breast milk contaminated with these compounds. DDT is a pesticide, and even though it has not been used in this country since 1972, soil has small amounts and, under certain conditions, contaminated soil transfers DDT to crops. Children can be exposed also by eating food imported from countries where DDT is still being used. Because of their smaller weight, intake of an equivalent amount of DDT by children and adults would result in a higher dose (amount of DDT ingested per kilogram of body weight) in children than in adults. In the United States between 1985 and 1991, the average 8½-month-old infant consumed 4 times as much DDT for each pound of body weight than the average adult. However, the amounts of DDT consumed were much smaller than the amounts that have been tested in studies in animals.

DDT from the mother can enter her unborn baby through the placenta. DDT has been found in amniotic fluid, human placentas, fetuses, and umbilical cord blood. DDT has been measured in human milk; therefore, nursing infants are also exposed to DDT. In most cases, however, the benefits of breast-feeding outweigh any risks from exposure to DDT in mother's milk. Nevertheless, women with unusually high amounts of DDT or metabolites in their bodies (compared to background amounts measured in the general population) should be informed of the potential exposure of the fetus if they become pregnant and the potential risks of breast-feeding.

We do not know whether children differ from adults in their susceptibility to health effects from DDT. There are few studies of young children exposed to DDT. A child who drank DDT in kerosene only once vomited and had tremors and convulsions and eventually died; however, we do not know how much of this was caused by the kerosene. Adults who swallowed DDT in much greater amounts than those found in the environment had effects on their nervous systems. The same harmful effects will probably happen to young children if they eat food or drink liquids with large amounts of DDT. However, because DDT is no longer used or made in the United States, such exposure is not likely to happen. Two studies have shown a higher dose of DDT is needed to kill newborn and young rats than adult rats. In one study, when the dose was divided up and given over 4 days, the same dose of DDT killed rats of all ages.

There is no evidence that exposure to DDT at levels found in the environment causes birth defects in people. One study in U.S. children 12 to 14 years of age found that boys whose mothers had higher DDE levels in their bodies when they were pregnant were taller than those whose mothers had lower DDE levels. A study of German children found that girls with higher DDE in the blood at 8 years of age were shorter than those with lower DDE levels. The reason for the discrepancy between the two studies is unknown. Studies in animals have shown that DDT given during pregnancy can slow the growth of the fetus. Exposure to DDT or its metabolites during development may change how the reproductive and nervous systems work. This seems to be caused by the property of DDT or its metabolites to mimic the action of natural hormones. Male rats exposed to the DDT breakdown product, p,p'-DDE, as fetuses or while nursing, showed changes in the development of their reproductive system. One study found that the beginning of puberty is delayed in male rats given relatively high amounts of p,p'-DDE as juveniles. Also, one study showed that exposure of mice to DDT during the first weeks of life resulted in neurobehavioral problems when tests were done later in life. These studies raise concerns that exposure to DDT early in life might cause harmful effects that remain or begin long after exposure has stopped.

1.7 HOW CAN FAMILIES REDUCE THE RISK OF EXPOSURE TO DDT, DDE, AND DDD?

If your doctor finds that you have been exposed to significant amounts of DDT, DDE, and DDD, ask whether your children might also be exposed. Your

doctor might need to ask your state health department to investigate.

At this time, most people are exposed to DDT and its breakdown products as a result of eating foods or drinking liquids that may be contaminated with small amounts of DDT. DDT is a pesticide, but it was banned in the United States in 1972. However, because of its chemical characteristics, it has stayed in the environment and low levels of DDT may be present in foods (i.e., fruits, vegetables, meat, and fish) for many years. Studies have shown that cooking will reduce the amount of DDT in fish. Many other countries still use DDT; therefore, food brought into the United States from these countries may contain DDT. The Food and Drug Administration (FDA) analyzes a wide variety of imported food items (coffee, tropical fruits, etc.) as well as domestic products to insure that pesticide residues are below FDA tolerances. DDT has been found in both root and leafy vegetables. DDT attaches to the roots of plants, but it does not easily move to other parts of the plants. DDT in the air can be deposited on to the surfaces of plants. Washing fruits and vegetables before eating them is a healthful practice.

You and your children may be exposed to DDT by eating certain types of fish or wildlife caught from certain locations. Some states, Native American tribes, and U.S. territories have issued fish and wildlife advisories to warn people about DDT-contaminated fish and turtles. Each state, Native American tribe, or U.S. territory sets its own criteria for issuing fish and wildlife advisories. A fish advisory will specify which bodies of water have restrictions. The advisory will tell you what type and sizes of fish are of concern. The advisory may completely ban eating fish or tell you to limit your meals of a certain fish type. For example, an advisory may tell you to eat a certain type of fish no more than once a month. The advisory may tell you only to eat certain parts of the fish or turtle and how to prepare or cook the fish or turtle to decrease your exposure to DDT. The fish or wildlife advisory may be stricter to protect pregnant women, nursing mothers, and young children. To reduce your children's exposure to DDT, obey fish and wildlife advisories. Information on fish and wildlife advisories in your state is available from your state health or natural resources department. Signs may also be posted in certain fishing areas.

1.8 IS THERE A MEDICAL TEST TO DETERMINE WHETHER IHAVE BEEN EXPOSED TO DDT, DDE, AND DDD?

DDT, DDE, and DDD can be measured in fat, blood, urine, semen, and breast milk. Samples of blood and urine are easy to get, and levels in these samples may help show the amount of exposure. These tests are not readily available at your doctor's office, but your doctor can tell you where they can be done. Tests may show low, moderate, or excessive exposure to these compounds. However, such tests cannot show the exact amount of DDT, DDE, or DDD to which a person was exposed, or predict the chance of health effects in the person.

1.9 WHAT RECOMMENDATIONS HAS THE FEDERAL GOVERNMENT MADE TO PROTECT HUMAN HEALTH?

The federal government develops regulations and recommendations to protect public health. Regulations can be enforced by law. Federal agencies that develop regulations for toxic substances include the Environmental Protection Agency (EPA), the Occupational Safety and Health Administration (OSHA), and the Food and Drug Administration (FDA). Recommendations provide valuable guidelines to protect public health but cannot be enforced by law. Federal organizations that develop recommendations for toxic substances include the Agency for Toxic Substances and Disease Registry (ATSDR) and the National Institute for Occupational Safety and Health (NIOSH).

Regulations and recommendations can be expressed in not-to-exceed levels in air, water, soil, or food that are usually based on levels that affect animals; then they are adjusted to help protect people. Sometimes these not-to-exceed levels differ among federal organizations because of different exposure times (an 8-hour workday or a 24-hour day), the use of different animal studies, or other factors.

Recommendations and regulations are also periodically updated as more information becomes available. For the most current information, check with the federal agency or organization that provides it. Some regulations and recommendations for DDT, DDE, and DDD include the following:

All uses of DDT were banned by EPA in 1972, except in cases of public health emergencies. DDT was banned because the chemical was building up in the environment and possibly hurting wildlife. Also, some cancer tests in laboratory animals showed positive results. Although DDT is no longer used in the United States, federal regulations still control the amounts of DDT allowed in food and water.

OSHA states that workers may not be exposed to amounts of DDT greater than 1 milligram of DDT per cubic meter of air (1 mg/m^3) for an 8-hour workday, 40-hour work week. EPA estimates that drinking 2 liters of water per day containing 0.59 nanograms of DDT per liter of water (1 nanogram is one billionth of a gram) and eating 6.5 grams of fish and shellfish per day (from waters containing 0.59 nanograms DDT per liter) would be associated with an increased lifetime cancer risk of one in one million. Fish and shellfish tend to concentrate DDT from the surrounding water in their tissues. FDA has set action levels for DDT/DDE/DDD; these are limits at or above which FDA will take legal action to remove products from the market.

1.10 WHERE CAN I GET MORE INFORMATION?

If you have any more questions or concerns, please contact your community or state health or environmental quality department or:

Agency for Toxic Substances and Disease Registry
Division of Toxicology
1600 Clifton Road NE, Mailstop F-32
Atlanta, GA 30333

PUBLIC HEALTH STATEMENT
DDT, DDE, and DDD

CAS#: DDT 50-29-3
DDE 72-55-9
DDD 72-54-8

Division of Toxicology **September 2002**

Information line and technical assistance:

Phone: 888-422-8737
FAX: (770)-488-4178

ATSDR can also tell you the location of occupational and environmental health clinics. These clinics specialize in recognizing, evaluating, and treating illnesses resulting from exposure to hazardous substances.

To order toxicological profiles, contact:

National Technical Information Service
5285 Port Royal Road
Springfield, VA 22161
Phone: 800-553-6847 or 703-605-6000

Reference

Agency for Toxic Substances and Disease Registry (ATSDR). 2002. Toxicological Profile for DDT, DDE, DDD. Atlanta, GA: U.S. Department of Health and Human Services, Public Health Service.

Attachment DR88-1
Stormwater Calculations

CPV VACA STATION HYDROLOGY STUDY

Prepared by Phillippi Engineering, Inc.

July 2, 2009

SECTION 1: INTRODUCTION

Phillippi Engineering, Inc. has been retained to evaluate the onsite pre and post development storm runoff at the CPV Vaca Station site. The developed site drains from the West to the East into the detention pond. The City of Vacaville design criteria requires that post development storm runoff peak flow rates not exceed pre-development peak flow rates. Calculations for the pre-developed and post-developed site have been prepared and are enclosed. The Hydraulic design calculations were prepared using the SCS type 1A 24-hour 10 and 100-year storm event.

SECTION 2: PRE-DEVELOPED SITE MODEL

The pre-developed site consists of silty-clay loam soil and natural grasses. Storm runoff drains West to East across an open field with an approximate slope of 0.33% into a roadside ditch along Lewis Rd. The roadside ditch carries the runoff south through a culvert under Fry Rd. The runoff then continues South in a roadside ditch to New Alamo Creek approximately 0.5 miles South of the project site.

Several parameters were needed to model the existing site 100-year 24-hour storm. Runoff curve numbers are selected based upon the site soil group and site use. Group C soil (clay loam) and grass open space parameters were used to determine the curve number of 74. The time of concentration was calculated using a TR-55 worksheet. This takes into account the sheet flow, shallow concentrated, and open channel flow times. The site has a natural grade of 0.33% where sheet flow and shallow concentrated flow occur. The roadside ditch along Lewis Rd has a grade of approximately 0.15% where the open channel flow occurs. Using these parameters the time of concentration is 114 minutes. The pre-development site generated a 100-year peak runoff of 7.44cfs. Any increase in peak runoff resulting from the proposed project will need to be mitigated with an onsite detention pond.

SECTION 3: POST-DEVELOPMENT SITE MODEL

The developed site will consist mostly of asphalt, concrete, gravel, and perimeter landscaping. Storm runoff will be sheet flow to a series of culverts and ditches that enter into the detention pond located at the southeast corner of the site adjacent to the intersection of Fry and Lewis Road. The detention pond will have a gravity outlet to the existing culvert draining south across Fry Road into a roadside ditch. The ditch then continues South to New Alamo Creek.

Several parameters were needed to model the proposed site 100-year 24-hour storm. A runoff curve number of 91 was selected based upon soil group C (clay loam) on an industrial site. A TR-55 worksheet was used to calculate the time of concentration. At the most remote location of the site runoff will sheet flow over paved surfaces directly to inlets and vegetated swales. Sheet flow and open channel flow times have been calculated while shallow concentrated flow would not occur. The proposed site time of concentration was determined to be 34 minutes. Using these parameters the developed site storm generated a 100-year peak flow rate of 23.03cfs. This storm hydrograph was then routed to the detention pond for runoff mitigation analysis.

The detention pond was designed along the eastern side of the site with a minimum bottom elevation of 59.0 and a top elevation of 64.0. The base of the pond slopes toward the riser pipe outlet structure at approximately 0.25%. A 30’ emergency spillway weir at an elevation of 63.2 was designed along the eastern berm that will allow emergency overflows resulting from a storm event in excess of the design 100-year storm or from an outflow structure failure to release in a controlled manner into the roadside ditch adjacent to Lewis Road. The outlet structure will consist of a short (5’) 15” pipe that receives the water in the pond, which will drain through a 48” standpipe, and then through the longer (170’) 24” outlet pipe.

The analysis for the 100-year 24-hour storm resulted in a peak flow of 6.94cfs discharging from the pond with a maximum water surface elevation of 62.6’. Therefore the detention pond will mitigate the peak

storm runoff by reducing the peak flow rate to 93% of the existing 7.44cfs while providing 1.4' of freeboard in the pond.

The riser pipe outlet structure is designed to provide an emergency release. The pond has been designed such that the water surface during the 100-year storm will not overtop the riser pipe structure under normal circumstances. In the event that the shorter (5') 15"inlet pipe becomes plugged the 48" standpipe will be overtopped and provide an emergency release out of the pond. This scenario has been modeled by removing the shorter (5') 15" pipe and allowing only the 48" riser pipe to act as a weir that drains into the 24" outlet pipe. The peak 100-year runoff leaving the pond in this scenario is 7.46cfs with a maximum water surface elevation of 63.0'.

In the event that the 24" outlet pipe becomes plugged the pond's 30' Eastern emergency weir will then release excess flows prior to backing up and causing onsite flooding. These flows will be collected in the roadside ditch adjacent to Lewis Road and conveyed South to the Fry Rd culvert. If the 24" outlet pipe is plugged downstream of the riser pipe then the riser will no longer function as an emergency release. This scenario has been modeled by removing the outlet structure pipes completely and only allowing storm water flows to be released through the 30' wide broad crested weir. The peak runoff leaving the pond in this scenario is 6.20cfs with a maximum elevation of 63.4'. This will ensure that the project site is still protected in the event that there is a complete failure of the pond outlet.

SECTION 4: CONCLUSION

The CPV Vaca site will develop a relatively flat agricultural site that will require a detention pond to mitigate the concentrated peak runoff flows leaving the developed site. The detention pond and its outlet structure have been sized to store and meter the storm water runoff such that the developed site will release a smaller peak flow than the pre-developed site. As a part of the pond design the outlet structure integrates a 48" riser pipe providing an emergency release point of discharge. A 30' emergency spillway has also been incorporated into the pond design that would release storm water to the East in the event that there was a complete failure of the riser pipe outlet structure. The proposed detention pond serves as a collection point for the concentrated developed on-site storm drain system and provides on-site flood protection while reducing the downstream storm water flow below the existing condition.

PRE-DEVELOPMENT MODEL CALCULATIONS

Watershed Model Schematic

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

1

Legend

Hyd.	Origin	Description
1	SCS Runoff	SCS Storm on existing site

Hydrograph Return Period Recap

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

Hyd. No.	Hydrograph type (origin)	Inflow Hyd(s)	Peak Outflow (cfs)								Hydrograph description
			1-Yr	2-Yr	3-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr	
1	SCS Runoff	------	-------	1.030	-------	2.417	3.559	5.089	6.252	7.444	SCS Storm on existing site

Proj. file: Existing Site SCS 06-25-09.gpw

Thursday, Jul 2, 2009

Hydrograph Summary Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	SCS Runoff	3.559	1	586	130,109	------	------	------	SCS Storm on existing site

Existing Site SCS 06-25-09.gpw	Return Period: 10 Year	Thursday, Jul 2, 2009

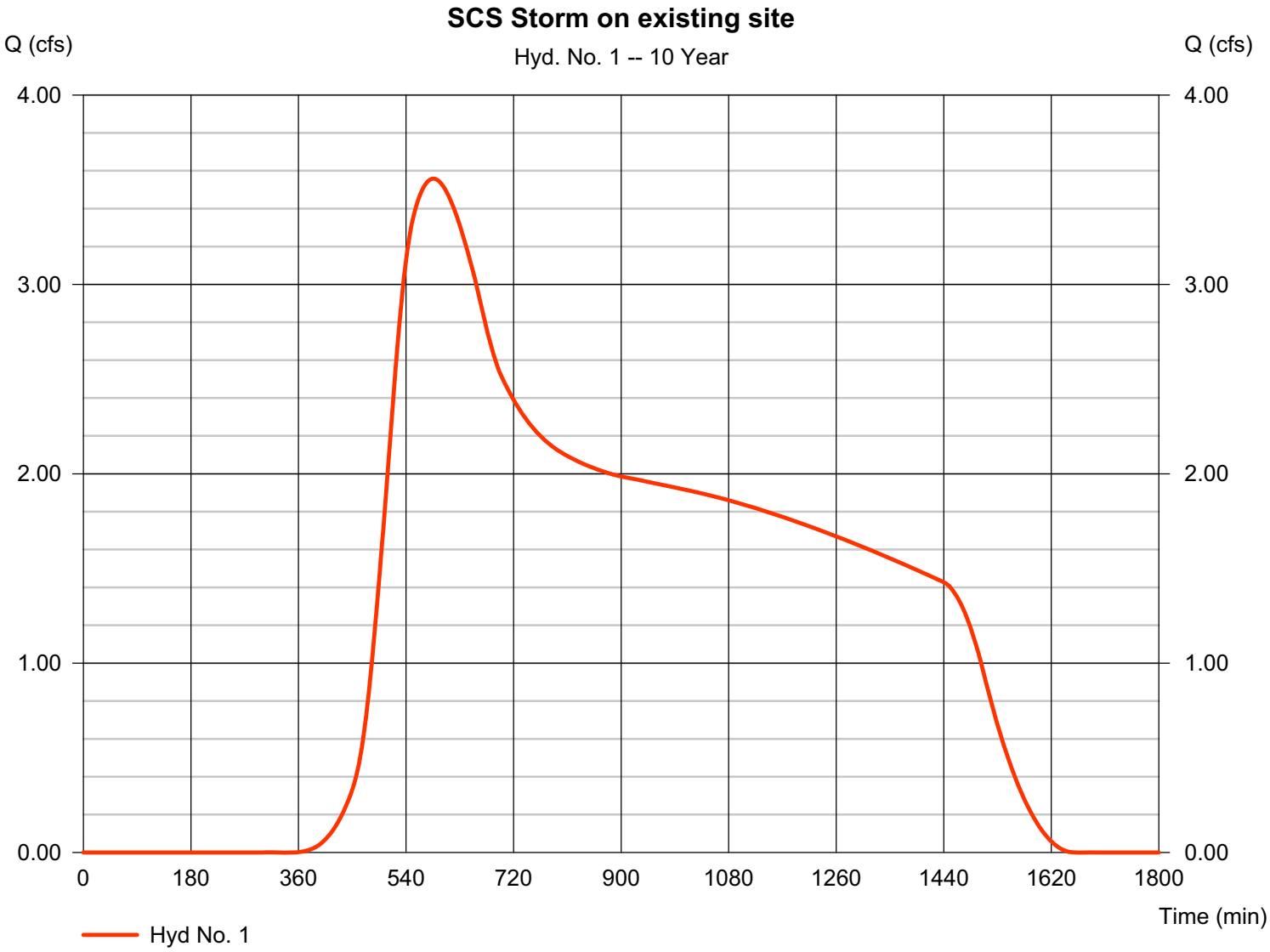
Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Hyd. No. 1

SCS Storm on existing site

Hydrograph type	=	SCS Runoff	Peak discharge	=	3.559 cfs
Storm frequency	=	10 yrs	Time to peak	=	586 min
Time interval	=	1 min	Hyd. volume	=	130,109 cuft
Drainage area	=	25.500 ac	Curve number	=	74
Basin Slope	=	0.0 %	Hydraulic length	=	0 ft
Tc method	=	TR55	Time of conc. (Tc)	=	114.10 min
Total precip.	=	3.74 in	Distribution	=	Type IA
Storm duration	=	24 hrs	Shape factor	=	400



TR55 Tc Worksheet

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

Hyd. No. 1

SCS Storm on existing site

Description		A		B		C		Totals
Sheet Flow								
Manning's n-value	=	0.240		0.011		0.011		
Flow length (ft)	=	300.0		0.0		0.0		
Two-year 24-hr precip. (in)	=	2.39		0.00		0.00		
Land slope (%)	=	0.33		0.00		0.00		
Travel Time (min)	**=**	**81.75**	**+**	**0.00**	**+**	**0.00**	**=**	**81.75**
Shallow Concentrated Flow								
Flow length (ft)	=	900.00		0.00		0.00		
Watercourse slope (%)	=	0.33		0.00		0.00		
Surface description	=	Unpaved		Paved		Paved		
Average velocity (ft/s)	=	0.93		0.00		0.00		
Travel Time (min)	**=**	**16.18**	**+**	**0.00**	**+**	**0.00**	**=**	**16.18**
Channel Flow								
X sectional flow area (sqft)	=	5.80		0.00		0.00		
Wetted perimeter (ft)	=	7.80		0.00		0.00		
Channel slope (%)	=	0.10		0.00		0.00		
Manning's n-value	=	0.025		0.015		0.015		
Velocity (ft/s)	=	1.55		0.00		0.00		
Flow length (ft)	=	1500.0		0.0		0.0		
Travel Time (min)	**=**	**16.18**	**+**	**0.00**	**+**	**0.00**	**=**	**16.18**

Total Travel Time, Tc ..... 114.10 min

Hydrograph Summary Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	SCS Runoff	7.444	1	569	240,751	------	------	------	SCS Storm on existing site

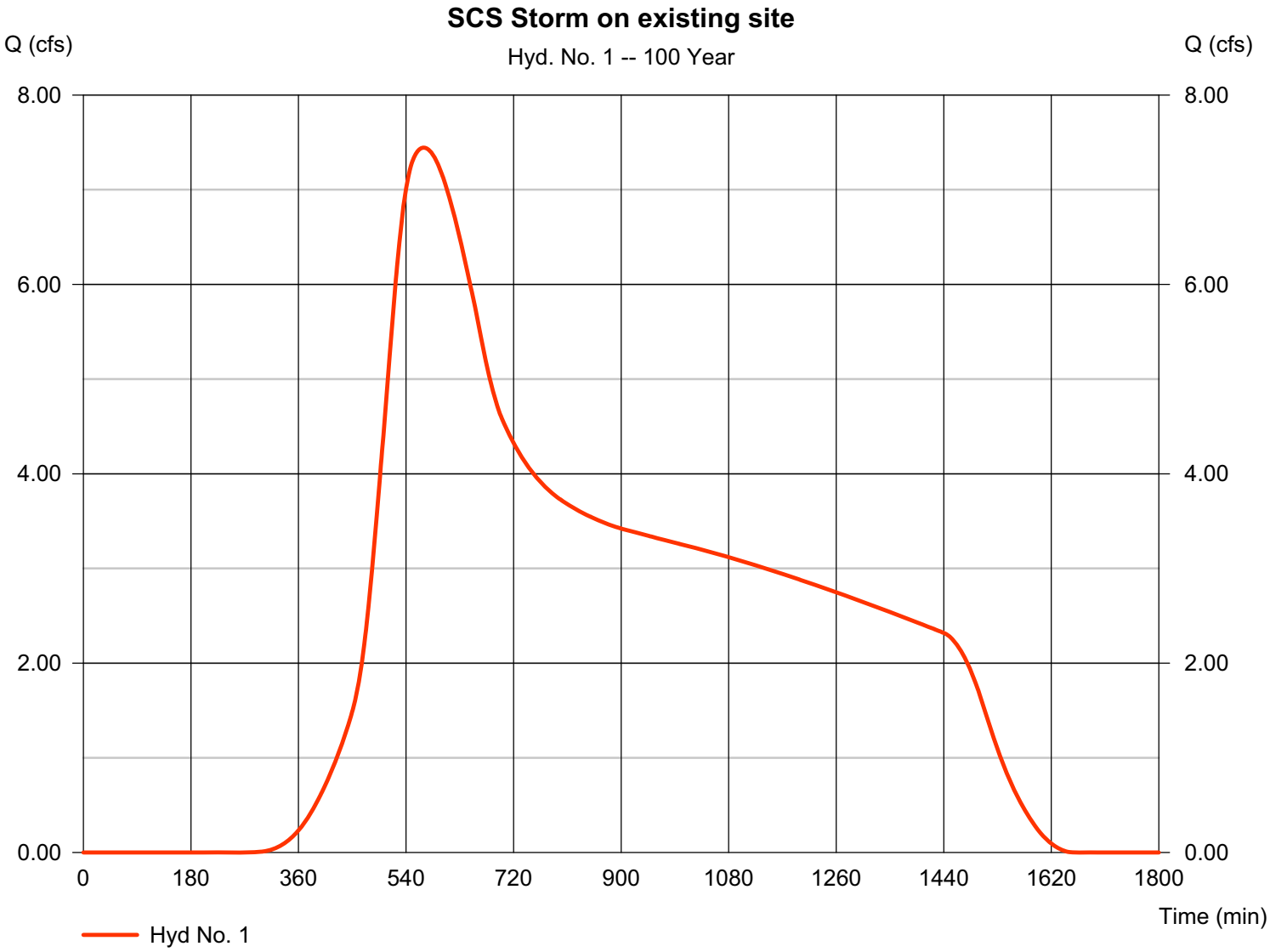
Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Hyd. No. 1

SCS Storm on existing site

Hydrograph type	=	SCS Runoff	Peak discharge	=	7.444 cfs
Storm frequency	=	100 yrs	Time to peak	=	569 min
Time interval	=	1 min	Hyd. volume	=	240,751 cuft
Drainage area	=	25.500 ac	Curve number	=	74
Basin Slope	=	0.0 %	Hydraulic length	=	0 ft
Tc method	=	TR55	Time of conc. (Tc)	=	114.10 min
Total precip.	=	5.30 in	Distribution	=	Type IA
Storm duration	=	24 hrs	Shape factor	=	400



Hydraflow Rainfall Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Return Period (Yrs)	Intensity-Duration-Frequency Equation Coefficients (FHA)			
	B	D	E	(N/A)
1	0.0000	0.0000	0.0000	--------
2	7.2795	0.3000	0.5819	--------
3	0.0000	0.0000	0.0000	--------
5	0.0000	0.0000	0.0000	--------
10	10.6394	0.1000	0.5677	--------
25	0.0000	0.0000	0.0000	--------
50	0.0000	0.0000	0.0000	--------
100	15.4902	0.1000	0.5733	--------

File name: Vacaville_ISO_22.IDF

Intensity = B / (Tc + D)^E

Return Period (Yrs)	Intensity Values (in/hr)											
	5 min	10	15	20	25	30	35	40	45	50	55	60
1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	2.76	1.87	1.49	1.26	1.11	1.00	0.91	0.85	0.79	0.74	0.70	0.67
3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
10	4.22	2.86	2.28	1.94	1.71	1.54	1.41	1.31	1.22	1.15	1.09	1.04
25	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
100	6.09	4.11	3.27	2.77	2.44	2.20	2.01	1.87	1.74	1.64	1.56	1.48

Tc = time in minutes. Values may exceed 60.

Precip. file name: Sample.pcp

Storm Distribution	Rainfall Precipitation Table (in)							
	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr
SCS 24-hour	0.00	2.39	0.00	3.20	3.74	4.39	4.85	5.30
SCS 6-Hr	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-1st	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-2nd	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-3rd	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-4th	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-Indy	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Custom	0.00	2.39	0.00	3.20	3.74	4.39	4.85	5.30

Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Hyd. No. 1

SCS Storm on existing site

Hydrograph type	= SCS Runoff	Peak discharge	= 3.559 cfs
Storm frequency	= 10 yrs	Time to peak	= 586 min
Time interval	= 1 min	Hyd. volume	= 130,109 cuft
Drainage area	= 25.500 ac	Curve number	= 74
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 114.1 min
Total precip.	= 3.74 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 400

Hydrograph Discharge Table

(Printed values >= 1.00% of Qp.)

Time -- Outflow (min cfs)		Time -- Outflow (min cfs)		Time -- Outflow (min cfs)		Time -- Outflow (min cfs)	
393	0.037	432	0.195	471	0.665	510	2.038
394	0.039	433	0.201	472	0.689	511	2.079
395	0.042	434	0.207	473	0.714	512	2.120
396	0.044	435	0.214	474	0.741	513	2.161
397	0.046	436	0.221	475	0.768	514	2.203
398	0.049	437	0.228	476	0.795	515	2.244
399	0.052	438	0.235	477	0.824	516	2.286
400	0.054	439	0.242	478	0.854	517	2.328
401	0.057	440	0.249	479	0.884	518	2.370
402	0.060	441	0.256	480	0.916	519	2.411
403	0.063	442	0.264	481	0.947	520	2.452
404	0.066	443	0.272	482	0.980	521	2.493
405	0.069	444	0.280	483	1.013	522	2.533
406	0.072	445	0.288	484	1.046	523	2.573
407	0.076	446	0.296	485	1.080	524	2.612
408	0.079	447	0.304	486	1.115	525	2.650
409	0.083	448	0.313	487	1.149	526	2.688
410	0.086	449	0.322	488	1.185	527	2.725
411	0.090	450	0.331	489	1.220	528	2.761
412	0.094	451	0.340	490	1.256	529	2.797
413	0.098	452	0.350	491	1.293	530	2.832
414	0.102	453	0.361	492	1.330	531	2.866
415	0.106	454	0.372	493	1.367	532	2.899
416	0.110	455	0.383	494	1.404	533	2.931
417	0.115	456	0.396	495	1.442	534	2.962
418	0.119	457	0.408	496	1.480	535	2.993
419	0.124	458	0.422	497	1.519	536	3.022
420	0.129	459	0.436	498	1.558	537	3.050
421	0.134	460	0.451	499	1.597	538	3.078
422	0.138	461	0.466	500	1.636	539	3.104
423	0.144	462	0.483	501	1.675	540	3.129
424	0.149	463	0.500	502	1.715	541	3.154
425	0.154	464	0.517	503	1.755	542	3.177
426	0.159	465	0.536	504	1.795	543	3.199
427	0.165	466	0.555	505	1.835	544	3.220
428	0.171	467	0.576	506	1.875	545	3.240
429	0.176	468	0.597	507	1.916	546	3.258
430	0.182	469	0.618	508	1.956	547	3.276
431	0.188	470	0.641	509	1.997	548	3.293

Continues on next page...

Hydrograph Discharge Table

Time -- Outflow (min	cfs)	Time -- Outflow (min	cfs)	Time -- Outflow (min	cfs)	Time -- Outflow (min	cfs)
549	3.308	605	3.504	661	2.953	717	2.408
550	3.324	606	3.499	662	2.940	718	2.402
551	3.338	607	3.493	663	2.926	719	2.397
552	3.352	608	3.488	664	2.913	720	2.391
553	3.366	609	3.482	665	2.900	721	2.386
554	3.378	610	3.475	666	2.886	722	2.380
555	3.391	611	3.469	667	2.873	723	2.375
556	3.402	612	3.462	668	2.859	724	2.370
557	3.414	613	3.455	669	2.845	725	2.365
558	3.424	614	3.448	670	2.832	726	2.359
559	3.434	615	3.441	671	2.818	727	2.354
560	3.444	616	3.434	672	2.805	728	2.349
561	3.453	617	3.426	673	2.791	729	2.344
562	3.462	618	3.418	674	2.778	730	2.339
563	3.470	619	3.410	675	2.765	731	2.334
564	3.478	620	3.402	676	2.752	732	2.329
565	3.485	621	3.394	677	2.739	733	2.324
566	3.492	622	3.385	678	2.727	734	2.319
567	3.499	623	3.377	679	2.714	735	2.315
568	3.505	624	3.368	680	2.702	736	2.310
569	3.511	625	3.359	681	2.690	737	2.305
570	3.516	626	3.350	682	2.679	738	2.301
571	3.521	627	3.340	683	2.667	739	2.296
572	3.526	628	3.331	684	2.656	740	2.292
573	3.531	629	3.321	685	2.645	741	2.288
574	3.535	630	3.311	686	2.634	742	2.283
575	3.539	631	3.302	687	2.623	743	2.279
576	3.542	632	3.292	688	2.613	744	2.275
577	3.545	633	3.281	689	2.603	745	2.271
578	3.548	634	3.271	690	2.594	746	2.267
579	3.551	635	3.261	691	2.584	747	2.263
580	3.553	636	3.250	692	2.575	748	2.259
581	3.555	637	3.240	693	2.566	749	2.255
582	3.556	638	3.229	694	2.558	750	2.251
583	3.557	639	3.218	695	2.549	751	2.247
584	3.558	640	3.207	696	2.541	752	2.244
585	3.559	641	3.196	697	2.534	753	2.240
586	3.559 <<	642	3.185	698	2.526	754	2.236
587	3.558	643	3.174	699	2.519	755	2.233
588	3.558	644	3.163	700	2.512	756	2.229
589	3.557	645	3.151	701	2.505	757	2.226
590	3.556	646	3.140	702	2.498	758	2.222
591	3.554	647	3.128	703	2.492	759	2.219
592	3.552	648	3.116	704	2.485	760	2.216
593	3.550	649	3.104	705	2.479	761	2.212
594	3.548	650	3.092	706	2.472	762	2.209
595	3.545	651	3.080	707	2.466	763	2.206
596	3.542	652	3.068	708	2.460	764	2.202
597	3.539	653	3.055	709	2.454	765	2.199
598	3.536	654	3.043	710	2.448	766	2.196
599	3.532	655	3.030	711	2.442	767	2.193
600	3.528	656	3.017	712	2.436	768	2.190
601	3.524	657	3.005	713	2.430	769	2.187
602	3.519	658	2.992	714	2.424	770	2.184
603	3.515	659	2.979	715	2.419	771	2.181
604	3.510	660	2.966	716	2.413	772	2.178

Continues on next page...

Hydrograph Discharge Table

Time -- Outflow (min cfs)		Time -- Outflow (min cfs)		Time -- Outflow (min cfs)		Time -- Outflow (min cfs)	
773	2.175	829	2.063	885	1.997	941	1.960
774	2.172	830	2.062	886	1.996	942	1.959
775	2.170	831	2.060	887	1.996	943	1.959
776	2.167	832	2.059	888	1.995	944	1.958
777	2.164	833	2.057	889	1.994	945	1.957
778	2.162	834	2.056	890	1.993	946	1.957
779	2.159	835	2.055	891	1.992	947	1.956
780	2.156	836	2.053	892	1.992	948	1.955
781	2.154	837	2.052	893	1.991	949	1.955
782	2.151	838	2.051	894	1.990	950	1.954
783	2.149	839	2.049	895	1.989	951	1.953
784	2.146	840	2.048	896	1.989	952	1.952
785	2.144	841	2.047	897	1.988	953	1.952
786	2.142	842	2.045	898	1.987	954	1.951
787	2.139	843	2.044	899	1.986	955	1.950
788	2.137	844	2.043	900	1.986	956	1.950
789	2.135	845	2.041	901	1.985	957	1.949
790	2.132	846	2.040	902	1.984	958	1.948
791	2.130	847	2.039	903	1.984	959	1.948
792	2.128	848	2.038	904	1.983	960	1.947
793	2.126	849	2.037	905	1.982	961	1.946
794	2.124	850	2.035	906	1.982	962	1.946
795	2.122	851	2.034	907	1.981	963	1.945
796	2.120	852	2.033	908	1.981	964	1.944
797	2.118	853	2.032	909	1.980	965	1.944
798	2.116	854	2.031	910	1.979	966	1.943
799	2.114	855	2.029	911	1.979	967	1.942
800	2.112	856	2.028	912	1.978	968	1.942
801	2.110	857	2.027	913	1.978	969	1.941
802	2.108	858	2.026	914	1.977	970	1.941
803	2.107	859	2.025	915	1.976	971	1.940
804	2.105	860	2.023	916	1.976	972	1.939
805	2.103	861	2.022	917	1.975	973	1.939
806	2.101	862	2.021	918	1.975	974	1.938
807	2.099	863	2.020	919	1.974	975	1.937
808	2.098	864	2.019	920	1.973	976	1.937
809	2.096	865	2.018	921	1.973	977	1.936
810	2.094	866	2.016	922	1.972	978	1.935
811	2.093	867	2.015	923	1.971	979	1.935
812	2.091	868	2.014	924	1.971	980	1.934
813	2.089	869	2.013	925	1.970	981	1.934
814	2.087	870	2.012	926	1.970	982	1.933
815	2.086	871	2.011	927	1.969	983	1.932
816	2.084	872	2.010	928	1.968	984	1.932
817	2.082	873	2.009	929	1.968	985	1.931
818	2.081	874	2.008	930	1.967	986	1.930
819	2.079	875	2.007	931	1.966	987	1.930
820	2.077	876	2.006	932	1.966	988	1.929
821	2.076	877	2.005	933	1.965	989	1.928
822	2.074	878	2.004	934	1.965	990	1.928
823	2.072	879	2.003	935	1.964	991	1.927
824	2.071	880	2.002	936	1.963	992	1.926
825	2.069	881	2.001	937	1.963	993	1.925
826	2.068	882	2.000	938	1.962	994	1.925
827	2.066	883	1.999	939	1.961	995	1.924
828	2.065	884	1.998	940	1.961	996	1.923

Continues on next page...

Hydrograph Discharge Table

Time (min)	Outflow (cfs)	Time (min)	Outflow (cfs)	Time (min)	Outflow (cfs)	Time (min)	Outflow (cfs)
997	1.923	1053	1.883	1109	1.834	1165	1.778
998	1.922	1054	1.882	1110	1.833	1166	1.777
999	1.921	1055	1.881	1111	1.832	1167	1.776
1000	1.921	1056	1.880	1112	1.831	1168	1.775
1001	1.920	1057	1.879	1113	1.830	1169	1.774
1002	1.919	1058	1.879	1114	1.829	1170	1.773
1003	1.918	1059	1.878	1115	1.828	1171	1.771
1004	1.918	1060	1.877	1116	1.827	1172	1.770
1005	1.917	1061	1.876	1117	1.826	1173	1.769
1006	1.916	1062	1.875	1118	1.825	1174	1.768
1007	1.916	1063	1.874	1119	1.824	1175	1.767
1008	1.915	1064	1.874	1120	1.823	1176	1.766
1009	1.914	1065	1.873	1121	1.822	1177	1.765
1010	1.914	1066	1.872	1122	1.821	1178	1.764
1011	1.913	1067	1.871	1123	1.820	1179	1.763
1012	1.912	1068	1.870	1124	1.819	1180	1.762
1013	1.912	1069	1.869	1125	1.818	1181	1.761
1014	1.911	1070	1.869	1126	1.817	1182	1.760
1015	1.910	1071	1.868	1127	1.816	1183	1.759
1016	1.910	1072	1.867	1128	1.815	1184	1.757
1017	1.909	1073	1.866	1129	1.815	1185	1.756
1018	1.908	1074	1.865	1130	1.814	1186	1.755
1019	1.908	1075	1.864	1131	1.813	1187	1.754
1020	1.907	1076	1.863	1132	1.812	1188	1.753
1021	1.906	1077	1.863	1133	1.811	1189	1.752
1022	1.905	1078	1.862	1134	1.810	1190	1.751
1023	1.905	1079	1.861	1135	1.809	1191	1.750
1024	1.904	1080	1.860	1136	1.808	1192	1.749
1025	1.903	1081	1.859	1137	1.807	1193	1.748
1026	1.903	1082	1.858	1138	1.806	1194	1.746
1027	1.902	1083	1.857	1139	1.805	1195	1.745
1028	1.901	1084	1.856	1140	1.804	1196	1.744
1029	1.901	1085	1.856	1141	1.803	1197	1.743
1030	1.900	1086	1.855	1142	1.802	1198	1.742
1031	1.899	1087	1.854	1143	1.801	1199	1.741
1032	1.899	1088	1.853	1144	1.800	1200	1.740
1033	1.898	1089	1.852	1145	1.799	1201	1.739
1034	1.897	1090	1.851	1146	1.798	1202	1.738
1035	1.896	1091	1.850	1147	1.796	1203	1.736
1036	1.896	1092	1.849	1148	1.795	1204	1.735
1037	1.895	1093	1.848	1149	1.794	1205	1.734
1038	1.894	1094	1.848	1150	1.793	1206	1.733
1039	1.893	1095	1.847	1151	1.792	1207	1.732
1040	1.893	1096	1.846	1152	1.791	1208	1.731
1041	1.892	1097	1.845	1153	1.790	1209	1.730
1042	1.891	1098	1.844	1154	1.789	1210	1.728
1043	1.890	1099	1.843	1155	1.788	1211	1.727
1044	1.890	1100	1.842	1156	1.787	1212	1.726
1045	1.889	1101	1.841	1157	1.786	1213	1.725
1046	1.888	1102	1.840	1158	1.785	1214	1.724
1047	1.887	1103	1.839	1159	1.784	1215	1.723
1048	1.887	1104	1.838	1160	1.783	1216	1.722
1049	1.886	1105	1.837	1161	1.782	1217	1.720
1050	1.885	1106	1.837	1162	1.781	1218	1.719
1051	1.884	1107	1.836	1163	1.780	1219	1.718
1052	1.883	1108	1.835	1164	1.779	1220	1.717

Continues on next page...

Hydrograph Discharge Table

Time -- Outflow (min cfs)		Time -- Outflow (min cfs)		Time -- Outflow (min cfs)		Time -- Outflow (min cfs)	
1221	1.716	1277	1.648	1333	1.576	1389	1.500
1222	1.715	1278	1.647	1334	1.575	1390	1.499
1223	1.714	1279	1.646	1335	1.574	1391	1.497
1224	1.712	1280	1.645	1336	1.572	1392	1.496
1225	1.711	1281	1.643	1337	1.571	1393	1.494
1226	1.710	1282	1.642	1338	1.570	1394	1.493
1227	1.709	1283	1.641	1339	1.568	1395	1.492
1228	1.708	1284	1.640	1340	1.567	1396	1.490
1229	1.707	1285	1.638	1341	1.566	1397	1.489
1230	1.705	1286	1.637	1342	1.564	1398	1.487
1231	1.704	1287	1.636	1343	1.563	1399	1.486
1232	1.703	1288	1.635	1344	1.562	1400	1.485
1233	1.702	1289	1.633	1345	1.560	1401	1.483
1234	1.701	1290	1.632	1346	1.559	1402	1.482
1235	1.699	1291	1.631	1347	1.558	1403	1.480
1236	1.698	1292	1.630	1348	1.556	1404	1.479
1237	1.697	1293	1.628	1349	1.555	1405	1.478
1238	1.696	1294	1.627	1350	1.554	1406	1.476
1239	1.695	1295	1.626	1351	1.552	1407	1.475
1240	1.694	1296	1.624	1352	1.551	1408	1.473
1241	1.692	1297	1.623	1353	1.550	1409	1.472
1242	1.691	1298	1.622	1354	1.548	1410	1.470
1243	1.690	1299	1.621	1355	1.547	1411	1.469
1244	1.689	1300	1.619	1356	1.545	1412	1.468
1245	1.688	1301	1.618	1357	1.544	1413	1.466
1246	1.686	1302	1.617	1358	1.543	1414	1.465
1247	1.685	1303	1.616	1359	1.541	1415	1.463
1248	1.684	1304	1.614	1360	1.540	1416	1.462
1249	1.683	1305	1.613	1361	1.539	1417	1.460
1250	1.682	1306	1.612	1362	1.537	1418	1.459
1251	1.680	1307	1.610	1363	1.536	1419	1.458
1252	1.679	1308	1.609	1364	1.535	1420	1.456
1253	1.678	1309	1.608	1365	1.533	1421	1.455
1254	1.677	1310	1.606	1366	1.532	1422	1.453
1255	1.676	1311	1.605	1367	1.530	1423	1.452
1256	1.674	1312	1.604	1368	1.529	1424	1.450
1257	1.673	1313	1.603	1369	1.528	1425	1.449
1258	1.672	1314	1.601	1370	1.526	1426	1.448
1259	1.671	1315	1.600	1371	1.525	1427	1.446
1260	1.669	1316	1.599	1372	1.524	1428	1.445
1261	1.668	1317	1.597	1373	1.522	1429	1.443
1262	1.667	1318	1.596	1374	1.521	1430	1.442
1263	1.666	1319	1.595	1375	1.519	1431	1.440
1264	1.665	1320	1.593	1376	1.518	1432	1.439
1265	1.663	1321	1.592	1377	1.517	1433	1.437
1266	1.662	1322	1.591	1378	1.515	1434	1.436
1267	1.661	1323	1.590	1379	1.514	1435	1.435
1268	1.660	1324	1.588	1380	1.513	1436	1.433
1269	1.658	1325	1.587	1381	1.511	1437	1.432
1270	1.657	1326	1.586	1382	1.510	1438	1.430
1271	1.656	1327	1.584	1383	1.508	1439	1.429
1272	1.655	1328	1.583	1384	1.507	1440	1.427
1273	1.653	1329	1.582	1385	1.506	1441	1.426
1274	1.652	1330	1.580	1386	1.504	1442	1.424
1275	1.651	1331	1.579	1387	1.503	1443	1.422
1276	1.650	1332	1.578	1388	1.501	1444	1.420

Continues on next page...

Hydrograph Discharge Table

Time (min	Outflow cfs)	Time (min	Outflow cfs)	Time (min	Outflow cfs)	Time (min	Outflow cfs)
1445	1.417	1501	1.018	1557	0.417	1613	0.082
1446	1.415	1502	1.007	1558	0.408	1614	0.078
1447	1.412	1503	0.995	1559	0.400	1615	0.075
1448	1.409	1504	0.983	1560	0.392	1616	0.071
1449	1.406	1505	0.970	1561	0.384	1617	0.068
1450	1.403	1506	0.958	1562	0.376	1618	0.065
1451	1.400	1507	0.945	1563	0.368	1619	0.062
1452	1.396	1508	0.932	1564	0.360	1620	0.058
1453	1.393	1509	0.920	1565	0.352	1621	0.055
1454	1.389	1510	0.907	1566	0.345	1622	0.053
1455	1.385	1511	0.895	1567	0.337	1623	0.050
1456	1.381	1512	0.882	1568	0.330	1624	0.047
1457	1.376	1513	0.870	1569	0.322	1625	0.044
1458	1.372	1514	0.858	1570	0.315	1626	0.042
1459	1.367	1515	0.846	1571	0.308	1627	0.039
1460	1.362	1516	0.833	1572	0.301	1628	0.037
1461	1.357	1517	0.822	1573	0.294		
1462	1.352	1518	0.810	1574	0.287	*...End*	
1463	1.346	1519	0.798	1575	0.280		
1464	1.341	1520	0.786	1576	0.273		
1465	1.335	1521	0.775	1577	0.267		
1466	1.329	1522	0.763	1578	0.260		
1467	1.323	1523	0.752	1579	0.253		
1468	1.317	1524	0.740	1580	0.247		
1469	1.311	1525	0.729	1581	0.241		
1470	1.304	1526	0.718	1582	0.234		
1471	1.297	1527	0.707	1583	0.228		
1472	1.290	1528	0.696	1584	0.222		
1473	1.283	1529	0.685	1585	0.216		
1474	1.276	1530	0.674	1586	0.210		
1475	1.269	1531	0.664	1587	0.204		
1476	1.261	1532	0.653	1588	0.199		
1477	1.253	1533	0.642	1589	0.193		
1478	1.245	1534	0.632	1590	0.187		
1479	1.237	1535	0.622	1591	0.182		
1480	1.229	1536	0.611	1592	0.176		
1481	1.221	1537	0.601	1593	0.171		
1482	1.212	1538	0.591	1594	0.166		
1483	1.203	1539	0.581	1595	0.161		
1484	1.195	1540	0.571	1596	0.156		
1485	1.185	1541	0.561	1597	0.151		
1486	1.176	1542	0.552	1598	0.146		
1487	1.167	1543	0.542	1599	0.141		
1488	1.157	1544	0.533	1600	0.136		
1489	1.148	1545	0.523	1601	0.131		
1490	1.138	1546	0.514	1602	0.127		
1491	1.128	1547	0.504	1603	0.122		
1492	1.117	1548	0.495	1604	0.118		
1493	1.107	1549	0.486	1605	0.114		
1494	1.097	1550	0.477	1606	0.109		
1495	1.086	1551	0.468	1607	0.105		
1496	1.075	1552	0.459	1608	0.101		
1497	1.064	1553	0.451	1609	0.097		
1498	1.053	1554	0.442	1610	0.093		
1499	1.042	1555	0.433	1611	0.089		
1500	1.030	1556	0.425	1612	0.086		

Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Hyd. No. 1

SCS Storm on existing site

Hydrograph type	= SCS Runoff	Peak discharge	= 7.444 cfs
Storm frequency	= 100 yrs	Time to peak	= 569 min
Time interval	= 1 min	Hyd. volume	= 240,751 cuft
Drainage area	= 25.500 ac	Curve number	= 74
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 114.1 min
Total precip.	= 5.30 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 400

Hydrograph Discharge Table

(Printed values >= 1.00% of Qp.)

Time -- Outflow (min cfs)		Time -- Outflow (min cfs)		Time -- Outflow (min cfs)		Time -- Outflow (min cfs)	
331	0.075	370	0.315	409	0.770	448	1.444
332	0.079	371	0.324	410	0.784	449	1.466
333	0.083	372	0.333	411	0.799	450	1.488
334	0.087	373	0.342	412	0.813	451	1.510
335	0.091	374	0.352	413	0.828	452	1.534
336	0.095	375	0.361	414	0.843	453	1.559
337	0.099	376	0.371	415	0.858	454	1.585
338	0.104	377	0.381	416	0.873	455	1.613
339	0.108	378	0.391	417	0.888	456	1.641
340	0.113	379	0.401	418	0.903	457	1.671
341	0.118	380	0.411	419	0.919	458	1.702
342	0.123	381	0.422	420	0.935	459	1.735
343	0.128	382	0.432	421	0.950	460	1.769
344	0.133	383	0.443	422	0.966	461	1.804
345	0.139	384	0.454	423	0.982	462	1.841
346	0.144	385	0.465	424	0.999	463	1.879
347	0.150	386	0.476	425	1.015	464	1.919
348	0.155	387	0.488	426	1.032	465	1.961
349	0.161	388	0.499	427	1.048	466	2.004
350	0.167	389	0.511	428	1.065	467	2.049
351	0.173	390	0.523	429	1.082	468	2.095
352	0.179	391	0.535	430	1.100	469	2.143
353	0.186	392	0.547	431	1.117	470	2.193
354	0.192	393	0.559	432	1.135	471	2.244
355	0.199	394	0.571	433	1.152	472	2.297
356	0.206	395	0.583	434	1.170	473	2.352
357	0.213	396	0.596	435	1.189	474	2.408
358	0.220	397	0.609	436	1.207	475	2.466
359	0.227	398	0.621	437	1.225	476	2.525
360	0.234	399	0.634	438	1.244	477	2.586
361	0.242	400	0.647	439	1.263	478	2.649
362	0.249	401	0.661	440	1.282	479	2.713
363	0.257	402	0.674	441	1.302	480	2.779
364	0.265	403	0.687	442	1.321	481	2.846
365	0.273	404	0.701	443	1.341	482	2.914
366	0.281	405	0.714	444	1.361	483	2.982
367	0.289	406	0.728	445	1.382	484	3.052
368	0.298	407	0.742	446	1.402	485	3.122
369	0.306	408	0.756	447	1.423	486	3.193

Continues on next page...

Hydrograph Discharge Table

Time -- Outflow (min	cfs)	Time -- Outflow (min	cfs)	Time -- Outflow (min	cfs)	Time -- Outflow (min	cfs)
487	3.265	543	7.116	599	7.180	655	5.770
488	3.337	544	7.147	600	7.163	656	5.739
489	3.410	545	7.175	601	7.146	657	5.708
490	3.484	546	7.202	602	7.128	658	5.677
491	3.558	547	7.225	603	7.110	659	5.647
492	3.633	548	7.247	604	7.091	660	5.615
493	3.708	549	7.267	605	7.072	661	5.584
494	3.784	550	7.286	606	7.052	662	5.553
495	3.860	551	7.304	607	7.032	663	5.522
496	3.936	552	7.320	608	7.012	664	5.491
497	4.013	553	7.336	609	6.992	665	5.459
498	4.091	554	7.350	610	6.971	666	5.428
499	4.168	555	7.363	611	6.950	667	5.396
500	4.246	556	7.374	612	6.928	668	5.365
501	4.325	557	7.385	613	6.906	669	5.333
502	4.403	558	7.395	614	6.884	670	5.302
503	4.482	559	7.404	615	6.861	671	5.270
504	4.560	560	7.411	616	6.838	672	5.240
505	4.639	561	7.418	617	6.815	673	5.209
506	4.718	562	7.424	618	6.792	674	5.179
507	4.797	563	7.430	619	6.768	675	5.150
508	4.876	564	7.434	620	6.744	676	5.120
509	4.955	565	7.437	621	6.719	677	5.092
510	5.035	566	7.440	622	6.695	678	5.064
511	5.114	567	7.442	623	6.670	679	5.036
512	5.193	568	7.444	624	6.645	680	5.009
513	5.273	569	7.444 <<	625	6.619	681	4.982
514	5.352	570	7.444	626	6.593	682	4.956
515	5.432	571	7.443	627	6.568	683	4.931
516	5.512	572	7.442	628	6.541	684	4.906
517	5.591	573	7.440	629	6.515	685	4.881
518	5.670	574	7.437	630	6.488	686	4.857
519	5.749	575	7.434	631	6.462	687	4.834
520	5.826	576	7.430	632	6.435	688	4.812
521	5.902	577	7.426	633	6.407	689	4.790
522	5.976	578	7.422	634	6.380	690	4.769
523	6.049	579	7.416	635	6.352	691	4.748
524	6.121	580	7.410	636	6.325	692	4.728
525	6.191	581	7.403	637	6.297	693	4.709
526	6.259	582	7.395	638	6.269	694	4.690
527	6.325	583	7.387	639	6.241	695	4.672
528	6.390	584	7.379	640	6.212	696	4.654
529	6.453	585	7.369	641	6.184	697	4.637
530	6.514	586	7.359	642	6.156	698	4.621
531	6.573	587	7.349	643	6.127	699	4.605
532	6.631	588	7.338	644	6.098	700	4.590
533	6.686	589	7.326	645	6.069	701	4.575
534	6.739	590	7.314	646	6.040	702	4.560
535	6.789	591	7.301	647	6.010	703	4.545
536	6.838	592	7.288	648	5.981	704	4.531
537	6.885	593	7.274	649	5.951	705	4.517
538	6.929	594	7.259	650	5.921	706	4.503
539	6.971	595	7.245	651	5.891	707	4.489
540	7.011	596	7.229	652	5.861	708	4.476
541	7.048	597	7.213	653	5.831	709	4.462
542	7.084	598	7.197	654	5.800	710	4.449

Continues on next page...

Hydrograph Discharge Table

Time -- Outflow (min cfs)		Time -- Outflow (min cfs)		Time -- Outflow (min cfs)		Time -- Outflow (min cfs)	
711	4.436	767	3.901	823	3.630	879	3.465
712	4.424	768	3.894	824	3.626	880	3.463
713	4.411	769	3.887	825	3.623	881	3.460
714	4.398	770	3.881	826	3.619	882	3.458
715	4.386	771	3.875	827	3.615	883	3.456
716	4.374	772	3.868	828	3.612	884	3.453
717	4.362	773	3.862	829	3.608	885	3.451
718	4.350	774	3.856	830	3.605	886	3.449
719	4.338	775	3.850	831	3.602	887	3.447
720	4.327	776	3.844	832	3.598	888	3.445
721	4.315	777	3.838	833	3.595	889	3.443
722	4.303	778	3.832	834	3.592	890	3.441
723	4.292	779	3.826	835	3.588	891	3.439
724	4.281	780	3.820	836	3.585	892	3.437
725	4.269	781	3.815	837	3.582	893	3.435
726	4.258	782	3.809	838	3.579	894	3.433
727	4.247	783	3.804	839	3.575	895	3.431
728	4.236	784	3.798	840	3.572	896	3.429
729	4.225	785	3.793	841	3.569	897	3.427
730	4.214	786	3.788	842	3.566	898	3.425
731	4.204	787	3.782	843	3.563	899	3.423
732	4.193	788	3.777	844	3.560	900	3.421
733	4.183	789	3.772	845	3.557	901	3.420
734	4.173	790	3.767	846	3.554	902	3.418
735	4.163	791	3.762	847	3.551	903	3.416
736	4.153	792	3.757	848	3.548	904	3.414
737	4.143	793	3.753	849	3.545	905	3.413
738	4.133	794	3.748	850	3.542	906	3.411
739	4.123	795	3.743	851	3.540	907	3.409
740	4.114	796	3.739	852	3.537	908	3.408
741	4.105	797	3.734	853	3.534	909	3.406
742	4.095	798	3.730	854	3.531	910	3.404
743	4.086	799	3.725	855	3.528	911	3.403
744	4.077	800	3.721	856	3.525	912	3.401
745	4.069	801	3.717	857	3.522	913	3.399
746	4.060	802	3.713	858	3.520	914	3.398
747	4.051	803	3.708	859	3.517	915	3.396
748	4.043	804	3.704	860	3.514	916	3.394
749	4.035	805	3.700	861	3.511	917	3.393
750	4.026	806	3.696	862	3.508	918	3.391
751	4.018	807	3.692	863	3.506	919	3.389
752	4.010	808	3.688	864	3.503	920	3.388
753	4.002	809	3.684	865	3.500	921	3.386
754	3.995	810	3.680	866	3.498	922	3.384
755	3.987	811	3.676	867	3.495	923	3.383
756	3.979	812	3.672	868	3.492	924	3.381
757	3.972	813	3.668	869	3.490	925	3.380
758	3.964	814	3.664	870	3.487	926	3.378
759	3.957	815	3.660	871	3.485	927	3.376
760	3.950	816	3.656	872	3.482	928	3.375
761	3.942	817	3.652	873	3.479	929	3.373
762	3.935	818	3.649	874	3.477	930	3.371
763	3.928	819	3.645	875	3.475	931	3.370
764	3.921	820	3.641	876	3.472	932	3.368
765	3.914	821	3.637	877	3.470	933	3.366
766	3.907	822	3.633	878	3.467	934	3.364

Continues on next page...

Hydrograph Discharge Table

Time -- Outflow (min	cfs)	Time -- Outflow (min	cfs)	Time -- Outflow (min	cfs)	Time -- Outflow (min	cfs)
935	3.363	991	3.270	1047	3.178	1103	3.076
936	3.361	992	3.268	1048	3.176	1104	3.074
937	3.359	993	3.267	1049	3.175	1105	3.072
938	3.358	994	3.265	1050	3.173	1106	3.070
939	3.356	995	3.263	1051	3.171	1107	3.068
940	3.354	996	3.262	1052	3.169	1108	3.066
941	3.353	997	3.260	1053	3.168	1109	3.064
942	3.351	998	3.258	1054	3.166	1110	3.062
943	3.349	999	3.257	1055	3.164	1111	3.060
944	3.347	1000	3.255	1056	3.162	1112	3.059
945	3.346	1001	3.253	1057	3.161	1113	3.057
946	3.344	1002	3.252	1058	3.159	1114	3.055
947	3.342	1003	3.250	1059	3.157	1115	3.053
948	3.341	1004	3.248	1060	3.155	1116	3.051
949	3.339	1005	3.247	1061	3.153	1117	3.049
950	3.337	1006	3.245	1062	3.152	1118	3.047
951	3.336	1007	3.244	1063	3.150	1119	3.045
952	3.334	1008	3.242	1064	3.148	1120	3.043
953	3.332	1009	3.240	1065	3.146	1121	3.041
954	3.330	1010	3.239	1066	3.144	1122	3.039
955	3.329	1011	3.237	1067	3.143	1123	3.037
956	3.327	1012	3.235	1068	3.141	1124	3.035
957	3.325	1013	3.234	1069	3.139	1125	3.033
958	3.324	1014	3.232	1070	3.137	1126	3.031
959	3.322	1015	3.231	1071	3.135	1127	3.029
960	3.320	1016	3.229	1072	3.134	1128	3.027
961	3.319	1017	3.227	1073	3.132	1129	3.025
962	3.317	1018	3.226	1074	3.130	1130	3.023
963	3.315	1019	3.224	1075	3.128	1131	3.021
964	3.314	1020	3.223	1076	3.126	1132	3.019
965	3.312	1021	3.221	1077	3.124	1133	3.017
966	3.310	1022	3.219	1078	3.123	1134	3.015
967	3.309	1023	3.218	1079	3.121	1135	3.013
968	3.307	1024	3.216	1080	3.119	1136	3.011
969	3.306	1025	3.215	1081	3.117	1137	3.009
970	3.304	1026	3.213	1082	3.115	1138	3.007
971	3.302	1027	3.211	1083	3.113	1139	3.005
972	3.301	1028	3.210	1084	3.112	1140	3.003
973	3.299	1029	3.208	1085	3.110	1141	3.001
974	3.298	1030	3.207	1086	3.108	1142	2.999
975	3.296	1031	3.205	1087	3.106	1143	2.997
976	3.294	1032	3.203	1088	3.104	1144	2.995
977	3.293	1033	3.202	1089	3.102	1145	2.993
978	3.291	1034	3.200	1090	3.100	1146	2.991
979	3.290	1035	3.198	1091	3.098	1147	2.989
980	3.288	1036	3.197	1092	3.097	1148	2.987
981	3.286	1037	3.195	1093	3.095	1149	2.985
982	3.285	1038	3.193	1094	3.093	1150	2.983
983	3.283	1039	3.192	1095	3.091	1151	2.981
984	3.282	1040	3.190	1096	3.089	1152	2.979
985	3.280	1041	3.188	1097	3.087	1153	2.977
986	3.278	1042	3.187	1098	3.085	1154	2.975
987	3.277	1043	3.185	1099	3.083	1155	2.973
988	3.275	1044	3.183	1100	3.081	1156	2.971
989	3.273	1045	3.182	1101	3.080	1157	2.969
990	3.272	1046	3.180	1102	3.078	1158	2.967

Continues on next page...

Hydrograph Discharge Table

Time -- Outflow (min	cfs)	Time -- Outflow (min	cfs)	Time -- Outflow (min	cfs)	Time -- Outflow (min	cfs)
1159	2.965	1215	2.847	1271	2.723	1327	2.594
1160	2.963	1216	2.845	1272	2.721	1328	2.592
1161	2.961	1217	2.843	1273	2.719	1329	2.589
1162	2.959	1218	2.841	1274	2.717	1330	2.587
1163	2.957	1219	2.839	1275	2.714	1331	2.585
1164	2.955	1220	2.837	1276	2.712	1332	2.582
1165	2.953	1221	2.834	1277	2.710	1333	2.580
1166	2.951	1222	2.832	1278	2.707	1334	2.578
1167	2.949	1223	2.830	1279	2.705	1335	2.575
1168	2.947	1224	2.828	1280	2.703	1336	2.573
1169	2.945	1225	2.826	1281	2.701	1337	2.570
1170	2.942	1226	2.823	1282	2.698	1338	2.568
1171	2.940	1227	2.821	1283	2.696	1339	2.566
1172	2.938	1228	2.819	1284	2.694	1340	2.563
1173	2.936	1229	2.817	1285	2.692	1341	2.561
1174	2.934	1230	2.815	1286	2.689	1342	2.559
1175	2.932	1231	2.813	1287	2.687	1343	2.556
1176	2.930	1232	2.810	1288	2.685	1344	2.554
1177	2.928	1233	2.808	1289	2.682	1345	2.551
1178	2.926	1234	2.806	1290	2.680	1346	2.549
1179	2.924	1235	2.804	1291	2.678	1347	2.547
1180	2.922	1236	2.802	1292	2.675	1348	2.544
1181	2.920	1237	2.799	1293	2.673	1349	2.542
1182	2.918	1238	2.797	1294	2.671	1350	2.540
1183	2.915	1239	2.795	1295	2.669	1351	2.537
1184	2.913	1240	2.793	1296	2.666	1352	2.535
1185	2.911	1241	2.791	1297	2.664	1353	2.532
1186	2.909	1242	2.788	1298	2.662	1354	2.530
1187	2.907	1243	2.786	1299	2.659	1355	2.528
1188	2.905	1244	2.784	1300	2.657	1356	2.525
1189	2.903	1245	2.782	1301	2.655	1357	2.523
1190	2.901	1246	2.779	1302	2.652	1358	2.520
1191	2.899	1247	2.777	1303	2.650	1359	2.518
1192	2.896	1248	2.775	1304	2.648	1360	2.516
1193	2.894	1249	2.773	1305	2.645	1361	2.513
1194	2.892	1250	2.771	1306	2.643	1362	2.511
1195	2.890	1251	2.768	1307	2.641	1363	2.508
1196	2.888	1252	2.766	1308	2.638	1364	2.506
1197	2.886	1253	2.764	1309	2.636	1365	2.504
1198	2.884	1254	2.762	1310	2.634	1366	2.501
1199	2.882	1255	2.759	1311	2.632	1367	2.499
1200	2.880	1256	2.757	1312	2.629	1368	2.496
1201	2.877	1257	2.755	1313	2.627	1369	2.494
1202	2.875	1258	2.753	1314	2.625	1370	2.492
1203	2.873	1259	2.750	1315	2.622	1371	2.489
1204	2.871	1260	2.748	1316	2.620	1372	2.487
1205	2.869	1261	2.746	1317	2.618	1373	2.484
1206	2.867	1262	2.744	1318	2.615	1374	2.482
1207	2.865	1263	2.741	1319	2.613	1375	2.479
1208	2.862	1264	2.739	1320	2.610	1376	2.477
1209	2.860	1265	2.737	1321	2.608	1377	2.475
1210	2.858	1266	2.735	1322	2.606	1378	2.472
1211	2.856	1267	2.732	1323	2.603	1379	2.470
1212	2.854	1268	2.730	1324	2.601	1380	2.467
1213	2.852	1269	2.728	1325	2.599	1381	2.465
1214	2.849	1270	2.726	1326	2.596	1382	2.462

Continues on next page...

Hydrograph Discharge Table

Time -- Outflow (min	cfs)	Time -- Outflow (min	cfs)	Time -- Outflow (min	cfs)	Time -- Outflow (min	cfs)
1383	2.460	1439	2.322	1495	1.760	1551	0.758
1384	2.458	1440	2.319	1496	1.743	1552	0.744
1385	2.455	1441	2.317	1497	1.725	1553	0.730
1386	2.453	1442	2.313	1498	1.707	1554	0.716
1387	2.450	1443	2.310	1499	1.688	1555	0.702
1388	2.448	1444	2.307	1500	1.670	1556	0.688
1389	2.445	1445	2.303	1501	1.651	1557	0.674
1390	2.443	1446	2.298	1502	1.632	1558	0.661
1391	2.440	1447	2.294	1503	1.612	1559	0.647
1392	2.438	1448	2.289	1504	1.592	1560	0.634
1393	2.436	1449	2.284	1505	1.572	1561	0.621
1394	2.433	1450	2.279	1506	1.552	1562	0.608
1395	2.431	1451	2.273	1507	1.532	1563	0.596
1396	2.428	1452	2.268	1508	1.511	1564	0.583
1397	2.426	1453	2.261	1509	1.490	1565	0.570
1398	2.423	1454	2.255	1510	1.470	1566	0.558
1399	2.421	1455	2.248	1511	1.450	1567	0.546
1400	2.418	1456	2.241	1512	1.430	1568	0.534
1401	2.416	1457	2.234	1513	1.410	1569	0.522
1402	2.414	1458	2.227	1514	1.390	1570	0.510
1403	2.411	1459	2.219	1515	1.370	1571	0.498
1404	2.409	1460	2.211	1516	1.350	1572	0.487
1405	2.406	1461	2.203	1517	1.331	1573	0.475
1406	2.404	1462	2.194	1518	1.312	1574	0.464
1407	2.401	1463	2.185	1519	1.293	1575	0.453
1408	2.399	1464	2.176	1520	1.274	1576	0.442
1409	2.396	1465	2.167	1521	1.255	1577	0.431
1410	2.394	1466	2.157	1522	1.236	1578	0.421
1411	2.391	1467	2.147	1523	1.218	1579	0.410
1412	2.389	1468	2.137	1524	1.199	1580	0.400
1413	2.386	1469	2.126	1525	1.181	1581	0.389
1414	2.384	1470	2.116	1526	1.163	1582	0.379
1415	2.382	1471	2.105	1527	1.145	1583	0.369
1416	2.379	1472	2.093	1528	1.127	1584	0.359
1417	2.377	1473	2.082	1529	1.110	1585	0.350
1418	2.374	1474	2.070	1530	1.092	1586	0.340
1419	2.372	1475	2.058	1531	1.075	1587	0.331
1420	2.369	1476	2.046	1532	1.058	1588	0.321
1421	2.367	1477	2.033	1533	1.041	1589	0.312
1422	2.364	1478	2.020	1534	1.024	1590	0.303
1423	2.362	1479	2.007	1535	1.007	1591	0.294
1424	2.359	1480	1.993	1536	0.990	1592	0.285
1425	2.357	1481	1.980	1537	0.974	1593	0.277
1426	2.354	1482	1.966	1538	0.957	1594	0.268
1427	2.352	1483	1.952	1539	0.941	1595	0.260
1428	2.349	1484	1.937	1540	0.925	1596	0.252
1429	2.347	1485	1.922	1541	0.909	1597	0.244
1430	2.344	1486	1.907	1542	0.894	1598	0.236
1431	2.342	1487	1.892	1543	0.878	1599	0.228
1432	2.339	1488	1.877	1544	0.862	1600	0.220
1433	2.337	1489	1.861	1545	0.847	1601	0.213
1434	2.334	1490	1.845	1546	0.832	1602	0.205
1435	2.332	1491	1.828	1547	0.817	1603	0.198
1436	2.329	1492	1.812	1548	0.802	1604	0.191
1437	2.327	1493	1.795	1549	0.787	1605	0.184
1438	2.324	1494	1.778	1550	0.773	1606	0.177

Continues on next page...

SCS Storm on existing site

Hydrograph Discharge Table

Time -- (min	Outflow cfs)
1607	0.170
1608	0.164
1609	0.157
1610	0.151
1611	0.145
1612	0.138
1613	0.132
1614	0.127
1615	0.121
1616	0.115
1617	0.110
1618	0.105
1619	0.100
1620	0.095
1621	0.090
1622	0.085
1623	0.080
1624	0.076

...End

POST-DEVELOPMENT CALCULATIONS

Watershed Model Schematic

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

Legend

Hyd.	Origin	Description
1	SCS Runoff	Developed site storm event
2	Reservoir	Detention pond outflow

Project: Proposed site SCS 06-25-09.gpw

Thursday, Jul 2, 2009

Hydrograph Return Period Recap

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

Hyd. No.	Hydrograph type (origin)	Inflow Hyd(s)	Peak Outflow (cfs)								Hydrograph description
			1-Yr	2-Yr	3-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr	
1	SCS Runoff	------	-------	7.792	-------	11.97	14.81	18.23	20.66	23.03	Developed site storm event
2	Reservoir	1	-------	1.879	-------	3.315	4.403	5.594	6.306	6.938	Detention pond outflow

Hydrograph Summary Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	SCS Runoff	14.81	1	495	257,225	------	------	------	Developed site storm event
2	Reservoir	4.403	1	627	195,513	1	61.76	90,408	Detention pond outflow

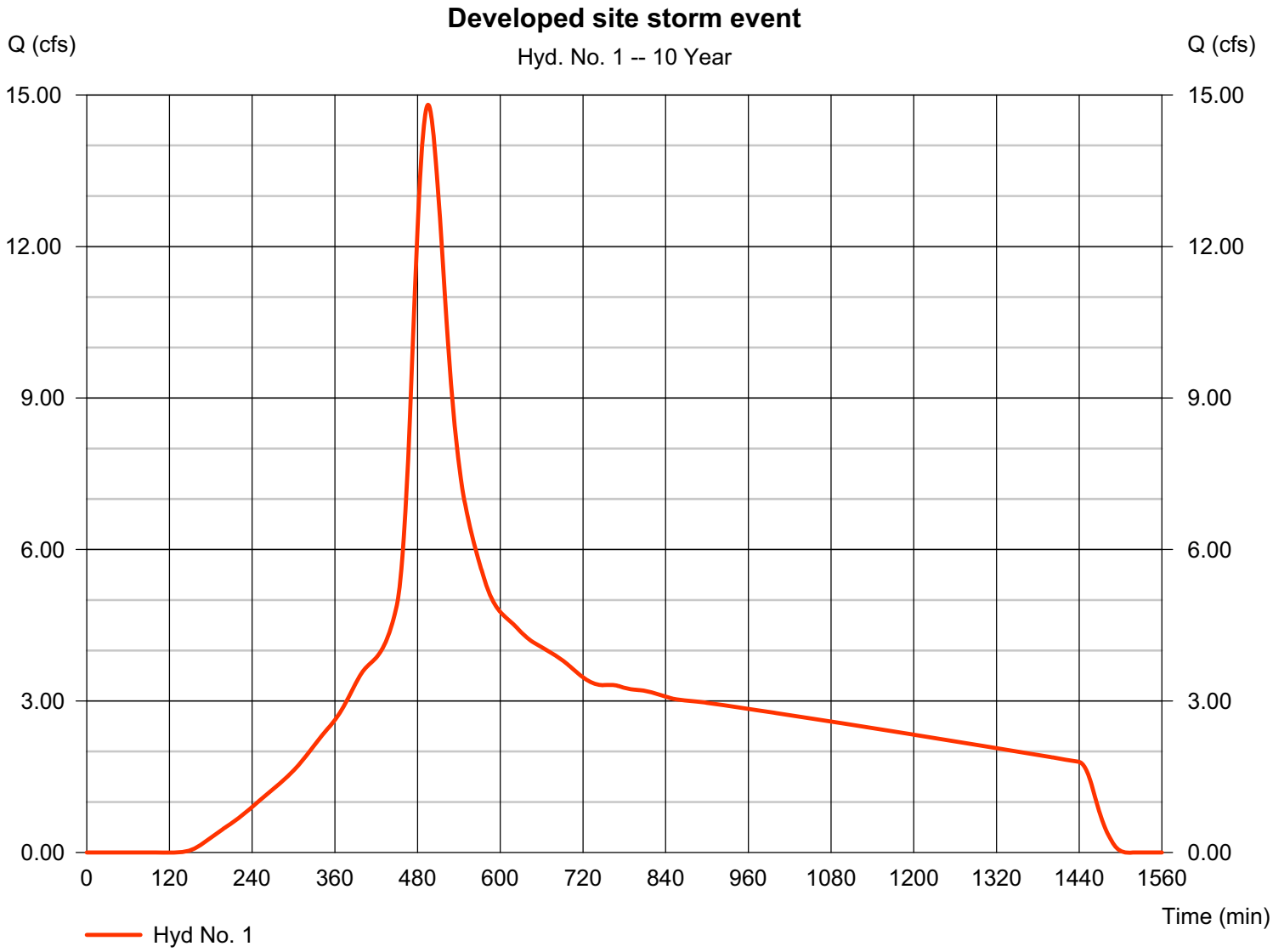
Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Hyd. No. 1

Developed site storm event

Hydrograph type	=	SCS Runoff	Peak discharge	=	14.81 cfs
Storm frequency	=	10 yrs	Time to peak	=	495 min
Time interval	=	1 min	Hyd. volume	=	257,225 cuft
Drainage area	=	25.500 ac	Curve number	=	91
Basin Slope	=	0.0 %	Hydraulic length	=	0 ft
Tc method	=	TR55	Time of conc. (Tc)	=	34.00 min
Total precip.	=	3.74 in	Distribution	=	Type IA
Storm duration	=	24 hrs	Shape factor	=	400



TR55 Tc Worksheet

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

Hyd. No. 1

Developed site storm event

Description		A		B		C		Totals
Sheet Flow								
Manning's n-value	=	0.240		0.011		0.011		
Flow length (ft)	=	180.0		0.0		0.0		
Two-year 24-hr precip. (in)	=	2.39		0.00		0.00		
Land slope (%)	=	1.50		0.00		0.00		
Travel Time (min)	**=**	**29.65**	**+**	**0.00**	**+**	**0.00**	**=**	**29.65**
Shallow Concentrated Flow								
Flow length (ft)	=	0.00		0.00		0.00		
Watercourse slope (%)	=	0.00		0.00		0.00		
Surface description	=	Paved		Paved		Paved		
Average velocity (ft/s)	=	0.00		0.00		0.00		
Travel Time (min)	**=**	**0.00**	**+**	**0.00**	**+**	**0.00**	**=**	**0.00**
Channel Flow								
X sectional flow area (sqft)	=	18.00		0.00		0.00		
Wetted perimeter (ft)	=	13.40		0.00		0.00		
Channel slope (%)	=	0.25		0.00		0.00		
Manning's n-value	=	0.025		0.015		0.015		
Velocity (ft/s)	=	3.63		0.00		0.00		
Flow length (ft)	=	950.0		0.0		0.0		
Travel Time (min)	**=**	**4.36**	**+**	**0.00**	**+**	**0.00**	**=**	**4.36**

Total Travel Time, Tc ..... 34.00 min

Hydrograph Report

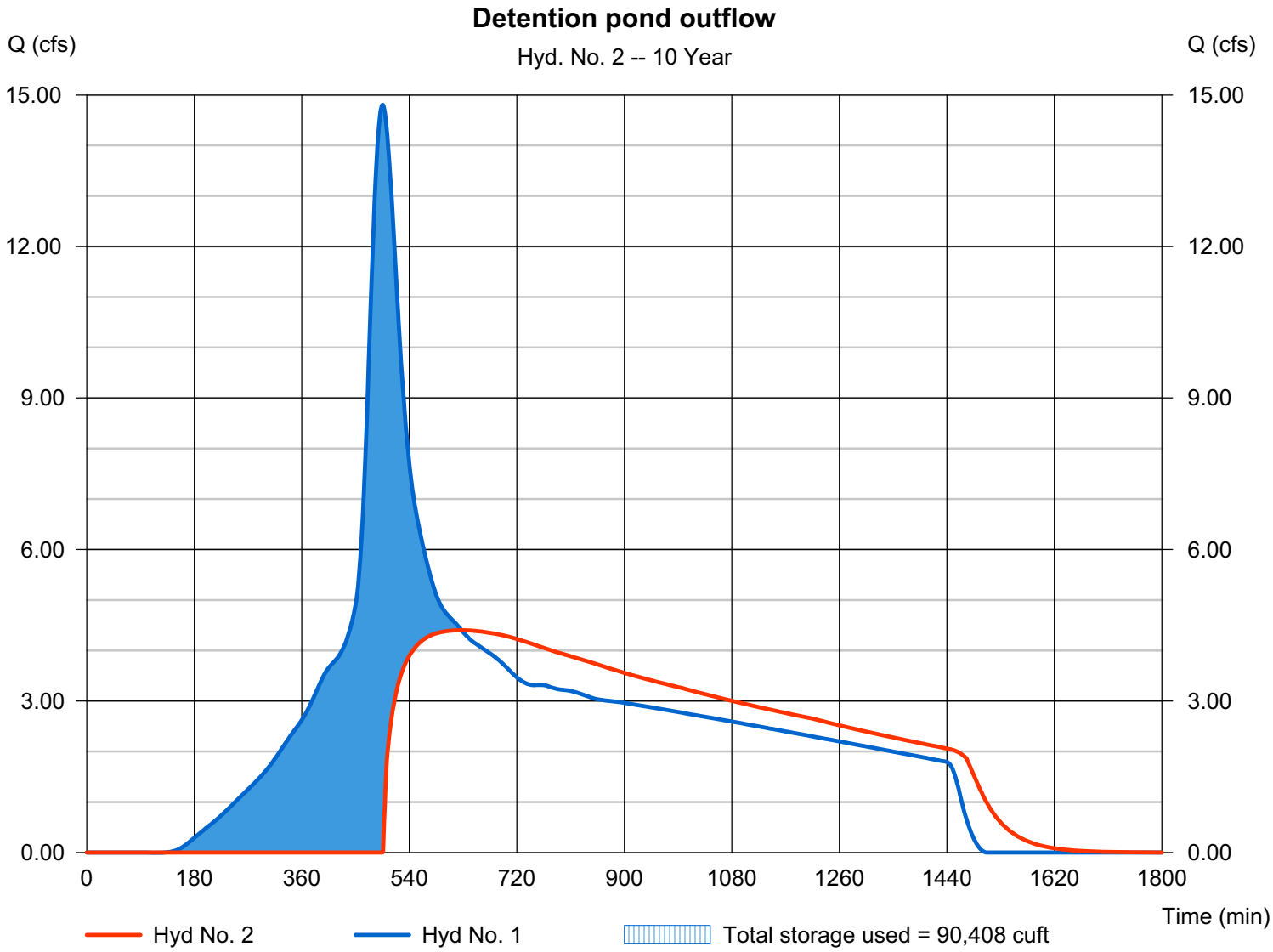
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Hyd. No. 2

Detention pond outflow

Hydrograph type	=	Reservoir	Peak discharge	=	4.403 cfs
Storm frequency	=	10 yrs	Time to peak	=	627 min
Time interval	=	1 min	Hyd. volume	=	195,513 cuft
Inflow hyd. No.	=	1 - Developed site storm event	Max. Elevation	=	61.76 ft
Reservoir name	=	Detention Pond	Max. Storage	=	90,408 cuft

Storage Indication method used.



Pond Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Pond No. 1 - Detention Pond

Pond Data

Contours - User-defined contour areas. Average end area method used for volume calculation. Begining Elevation = 59.00 ft

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	59.00	10	0	0
1.00	60.00	24,253	12,132	12,132
1.70	60.70	46,955	24,923	37,054
2.00	61.00	48,669	14,344	51,398
3.00	62.00	54,448	51,559	102,956
4.00	63.00	60,328	57,388	160,344
5.00	64.00	66,309	63,319	223,663

Culvert / Orifice Structures

	[A]	[B]	[C]	[PrfRsr]
Rise (in)	= 24.00	15.00	0.00	0.00
Span (in)	= 24.00	15.00	0.00	0.00
No. Barrels	= 1	1	0	0
Invert El. (ft)	= 59.10	59.20	0.00	0.00
Length (ft)	= 170.00	5.00	0.00	0.00
Slope (%)	= 0.23	1.00	0.00	n/a
N-Value	= .013	.013	.013	n/a
Orifice Coeff.	= 0.60	0.60	0.60	0.60
Multi-Stage	= n/a	No	No	No

Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 12.56	30.00	0.00	0.00
Crest El. (ft)	= 62.70	63.20	0.00	0.00
Weir Coeff.	= 3.33	2.60	3.33	3.33
Weir Type	= Riser	Broad	---	---
Multi-Stage	= Yes	No	No	No

Exfil.(in/hr) = 0.000 (by Wet area)

TW Elev. (ft) = 61.20

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0	59.00	0.00	0.00	---	---	0.00	0.00	---	---	---	---	0.000
0.10	1,213	59.10	0.00	0.00	---	---	0.00	0.00	---	---	---	---	0.000
0.20	2,426	59.20	0.00	0.00	---	---	0.00	0.00	---	---	---	---	0.000
0.30	3,639	59.30	0.00	0.00	---	---	0.00	0.00	---	---	---	---	0.000
0.40	4,853	59.40	0.00	0.00	---	---	0.00	0.00	---	---	---	---	0.000
0.50	6,066	59.50	0.00	0.00	---	---	0.00	0.00	---	---	---	---	0.000
0.60	7,279	59.60	0.00	0.00	---	---	0.00	0.00	---	---	---	---	0.000
0.70	8,492	59.70	0.00	0.00	---	---	0.00	0.00	---	---	---	---	0.000
0.80	9,705	59.80	0.00	0.00	---	---	0.00	0.00	---	---	---	---	0.000
0.90	10,918	59.90	0.00	0.00	---	---	0.00	0.00	---	---	---	---	0.000
1.00	12,132	60.00	0.00	0.00	---	---	0.00	0.00	---	---	---	---	0.000
1.07	14,624	60.07	0.00	0.00	---	---	0.00	0.00	---	---	---	---	0.000
1.14	17,116	60.14	0.00	0.00	---	---	0.00	0.00	---	---	---	---	0.000
1.21	19,608	60.21	0.00	0.00	---	---	0.00	0.00	---	---	---	---	0.000
1.28	22,101	60.28	0.00	0.00	---	---	0.00	0.00	---	---	---	---	0.000
1.35	24,593	60.35	0.00	0.00	---	---	0.00	0.00	---	---	---	---	0.000
1.42	27,085	60.42	0.00	0.00	---	---	0.00	0.00	---	---	---	---	0.000
1.49	29,577	60.49	0.00	0.00	---	---	0.00	0.00	---	---	---	---	0.000
1.56	32,070	60.56	0.00	0.00	---	---	0.00	0.00	---	---	---	---	0.000
1.63	34,562	60.63	0.00	0.00	---	---	0.00	0.00	---	---	---	---	0.000
1.70	37,054	60.70	0.00	0.00	---	---	0.00	0.00	---	---	---	---	0.000
1.73	38,489	60.73	0.00	0.00	---	---	0.00	0.00	---	---	---	---	0.000
1.76	39,923	60.76	0.00	0.00	---	---	0.00	0.00	---	---	---	---	0.000
1.79	41,357	60.79	0.00	0.00	---	---	0.00	0.00	---	---	---	---	0.000
1.82	42,792	60.82	0.00	0.00	---	---	0.00	0.00	---	---	---	---	0.000
1.85	44,226	60.85	0.00	0.00	---	---	0.00	0.00	---	---	---	---	0.000
1.88	45,660	60.88	0.00	0.00	---	---	0.00	0.00	---	---	---	---	0.000
1.91	47,095	60.91	0.00	0.00	---	---	0.00	0.00	---	---	---	---	0.000
1.94	48,529	60.94	0.00	0.00	---	---	0.00	0.00	---	---	---	---	0.000
1.97	49,964	60.97	0.00	0.00	---	---	0.00	0.00	---	---	---	---	0.000
2.00	51,398	61.00	0.00	0.00	---	---	0.00	0.00	---	---	---	---	0.000
2.10	56,554	61.10	0.00	0.00	---	---	0.00	0.00	---	---	---	---	0.000
2.20	61,710	61.20	0.00	0.00	---	---	0.00	0.00	---	---	---	---	0.000
2.30	66,865	61.30	0.00	1.87 ic	---	---	0.00	0.00	---	---	---	---	1.868
2.40	72,021	61.40	0.00	2.64 ic	---	---	0.00	0.00	---	---	---	---	2.642
2.50	77,177	61.50	0.00	3.24 ic	---	---	0.00	0.00	---	---	---	---	3.236
2.60	82,333	61.60	0.00	3.74 ic	---	---	0.00	0.00	---	---	---	---	3.737
2.70	87,489	61.70	0.00	4.18 ic	---	---	0.00	0.00	---	---	---	---	4.178

Continues on next page...

Detention Pond

Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
2.80	92,645	61.80	0.00	4.58 ic	---	---	0.00	0.00	---	---	---	---	4.576
2.90	97,801	61.90	0.00	4.94 ic	---	---	0.00	0.00	---	---	---	---	4.943
3.00	102,956	62.00	0.00	5.28 ic	---	---	0.00	0.00	---	---	---	---	5.284
3.10	108,695	62.10	0.00	5.60 ic	---	---	0.00	0.00	---	---	---	---	5.605
3.20	114,434	62.20	0.00	5.91 ic	---	---	0.00	0.00	---	---	---	---	5.908
3.30	120,173	62.30	0.00	6.20 ic	---	---	0.00	0.00	---	---	---	---	6.196
3.40	125,912	62.40	0.00	6.47 ic	---	---	0.00	0.00	---	---	---	---	6.472
3.50	131,650	62.50	0.00	6.74 ic	---	---	0.00	0.00	---	---	---	---	6.736
3.60	137,389	62.60	0.00	6.99 ic	---	---	0.00	0.00	---	---	---	---	6.991
3.70	143,128	62.70	0.00	7.24 ic	---	---	0.00	0.00	---	---	---	---	7.236
3.80	148,867	62.80	1.33 oc	7.47 ic	---	---	1.32	0.00	---	---	---	---	8.796
3.90	154,606	62.90	3.74 oc	7.70 ic	---	---	3.74	0.00	---	---	---	---	11.44
4.00	160,344	63.00	6.87 oc	7.93 ic	---	---	6.87	0.00	---	---	---	---	14.80
4.10	166,676	63.10	10.58 oc	8.14 ic	---	---	10.58	0.00	---	---	---	---	18.72
4.20	173,008	63.20	14.79 oc	8.36 ic	---	---	14.79	0.00	---	---	---	---	23.14
4.30	179,340	63.30	17.49 oc	8.56 ic	---	---	17.49 s	2.47	---	---	---	---	28.52
4.40	185,672	63.40	18.56 oc	8.76 ic	---	---	18.56 s	6.98	---	---	---	---	34.30
4.50	192,004	63.50	19.35 oc	8.96 ic	---	---	19.34 s	12.82	---	---	---	---	41.12
4.60	198,336	63.60	19.99 oc	9.15 ic	---	---	19.99 s	19.73	---	---	---	---	48.88
4.70	204,667	63.70	20.56 oc	9.34 ic	---	---	20.56 s	27.58	---	---	---	---	57.47
4.80	210,999	63.80	21.08 oc	9.53 ic	---	---	21.07 s	36.25	---	---	---	---	66.84
4.90	217,331	63.90	21.56 oc	9.71 ic	---	---	21.55 s	45.68	---	---	---	---	76.94
5.00	223,663	64.00	22.01 oc	9.89 ic	---	---	22.00 s	55.81	---	---	---	---	87.70

...End

Hydrograph Summary Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	SCS Runoff	23.03	1	495	397,003	------	------	------	Developed site storm event
2	Reservoir	6.938	1	609	335,290	1	62.58	136,207	Detention pond outflow

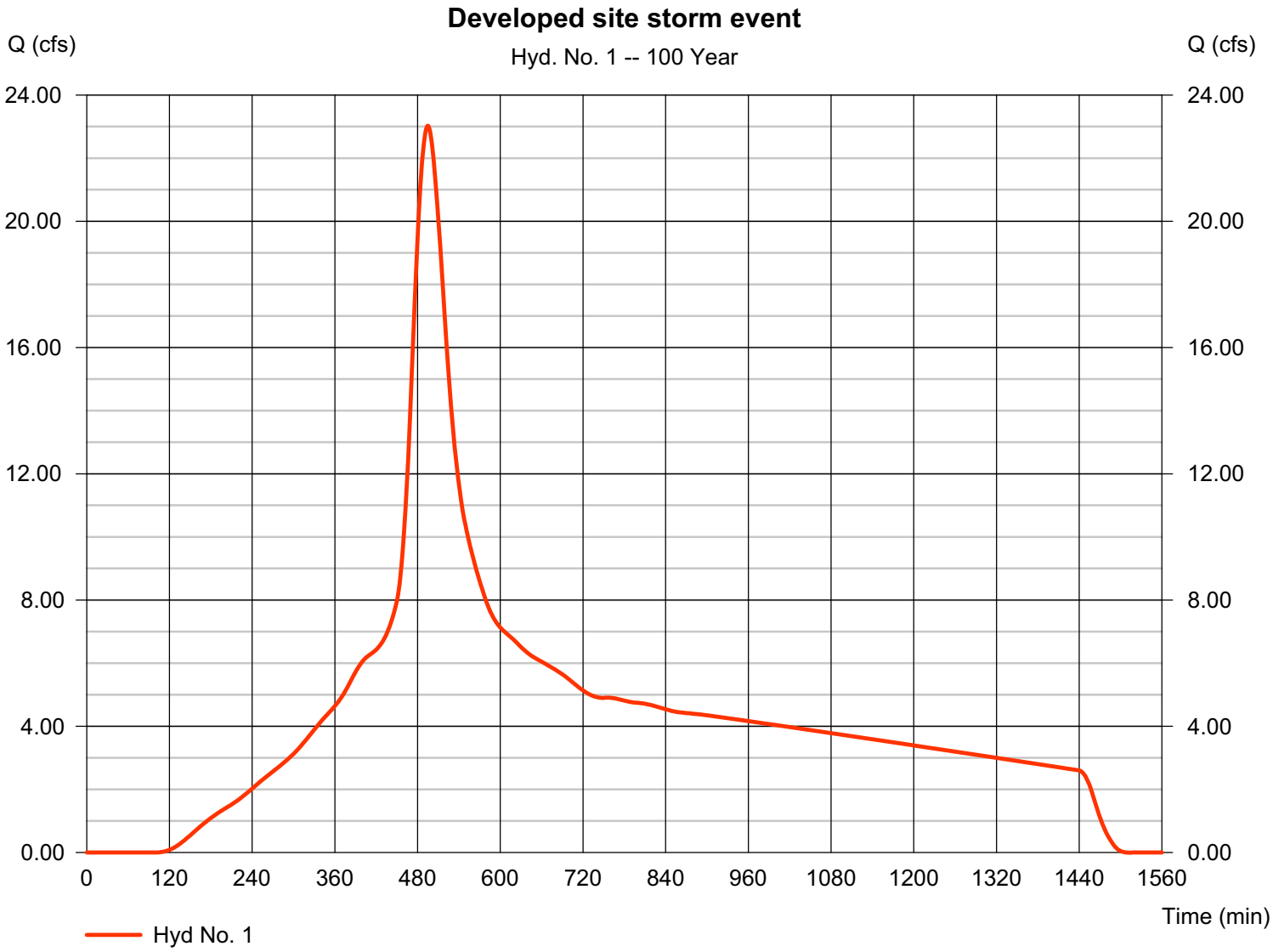
Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Hyd. No. 1

Developed site storm event

Hydrograph type	=	SCS Runoff	Peak discharge	=	23.03 cfs
Storm frequency	=	100 yrs	Time to peak	=	495 min
Time interval	=	1 min	Hyd. volume	=	397,003 cuft
Drainage area	=	25.500 ac	Curve number	=	91
Basin Slope	=	0.0 %	Hydraulic length	=	0 ft
Tc method	=	TR55	Time of conc. (Tc)	=	34.00 min
Total precip.	=	5.30 in	Distribution	=	Type IA
Storm duration	=	24 hrs	Shape factor	=	400



Hydrograph Report

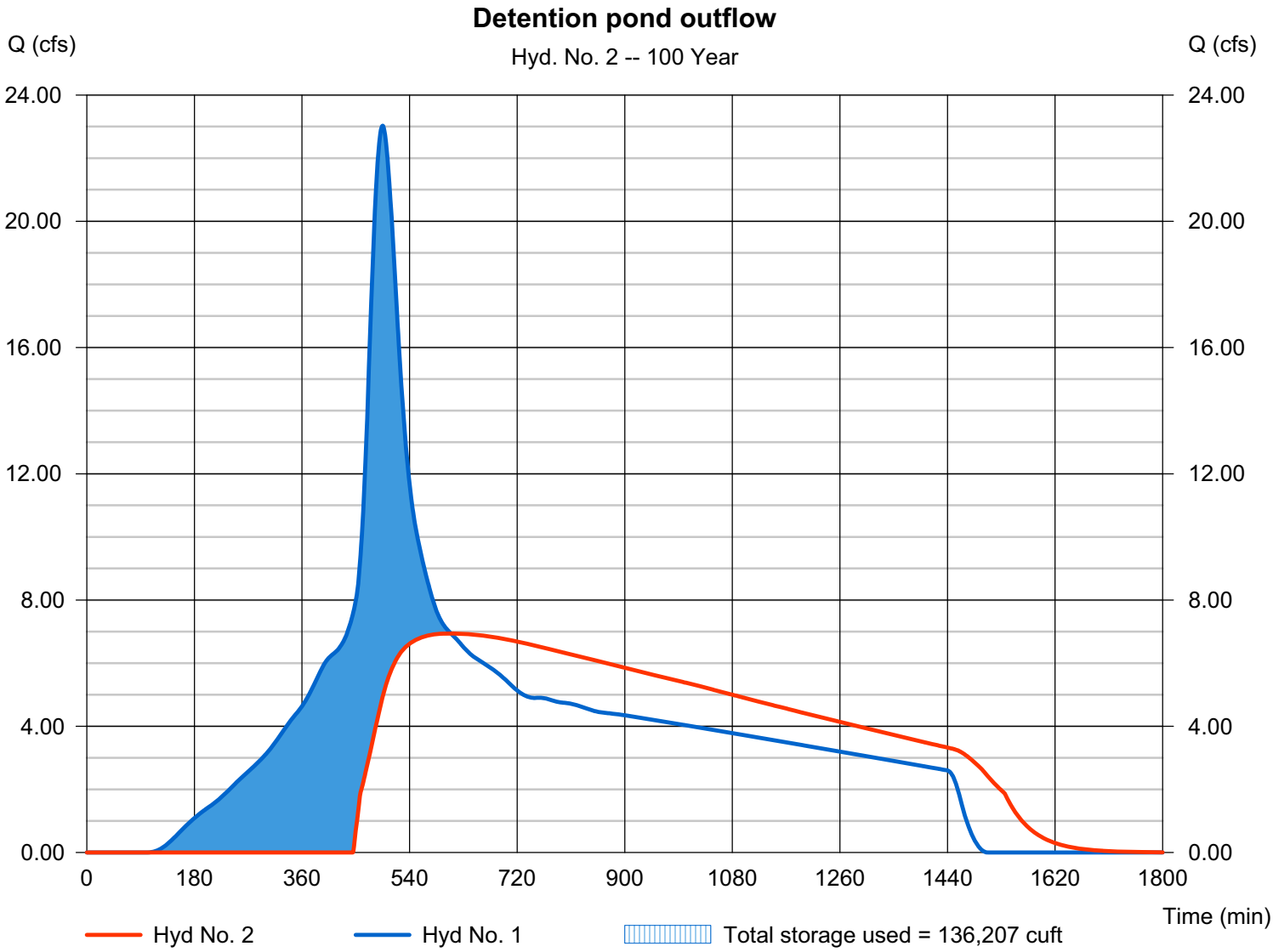
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Hyd. No. 2

Detention pond outflow

Hydrograph type	=	Reservoir	Peak discharge	=	6.938 cfs
Storm frequency	=	100 yrs	Time to peak	=	609 min
Time interval	=	1 min	Hyd. volume	=	335,290 cuft
Inflow hyd. No.	=	1 - Developed site storm event	Max. Elevation	=	62.58 ft
Reservoir name	=	Detention Pond	Max. Storage	=	136,207 cuft

Storage Indication method used.



Hydraflow Rainfall Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Return Period (Yrs)	Intensity-Duration-Frequency Equation Coefficients (FHA)			
	B	D	E	(N/A)
1	0.0000	0.0000	0.0000	--------
2	6.1078	0.1000	0.5625	--------
3	0.0000	0.0000	0.0000	--------
5	8.7423	0.3000	0.5773	--------
10	9.7582	0.1000	0.5661	--------
25	11.5209	0.1000	0.5690	--------
50	12.8436	0.1000	0.5707	--------
100	14.8890	0.3000	0.5856	--------

File name: Vacaville_ISO_22.IDF

Intensity = B / (Tc + D)^E

Return Period (Yrs)	Intensity Values (in/hr)											
	5 min	10	15	20	25	30	35	40	45	50	55	60
1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	2.44	1.66	1.33	1.13	1.00	0.90	0.83	0.77	0.72	0.68	0.64	0.61
3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5	3.34	2.27	1.81	1.54	1.35	1.22	1.12	1.03	0.97	0.91	0.86	0.82
10	3.88	2.63	2.10	1.78	1.57	1.42	1.30	1.21	1.13	1.06	1.01	0.96
25	4.56	3.09	2.46	2.09	1.84	1.66	1.52	1.41	1.32	1.24	1.18	1.12
50	5.07	3.43	2.73	2.32	2.04	1.84	1.69	1.56	1.46	1.38	1.30	1.24
100	5.61	3.80	3.01	2.55	2.24	2.02	1.85	1.71	1.60	1.50	1.42	1.35

Tc = time in minutes. Values may exceed 60.

Precip. file name: Sample.pcp

Storm Distribution	Rainfall Precipitation Table (in)							
	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr
SCS 24-hour	0.00	2.39	0.00	3.20	3.74	4.39	4.85	5.30
SCS 6-Hr	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-1st	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-2nd	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-3rd	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-4th	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-Indy	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Custom	0.00	2.39	0.00	3.20	3.74	4.39	4.85	5.30

Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Hyd. No. 1

Developed site storm event

Hydrograph type	= SCS Runoff	Peak discharge	= 14.81 cfs
Storm frequency	= 10 yrs	Time to peak	= 495 min
Time interval	= 1 min	Hyd. volume	= 257,225 cuft
Drainage area	= 25.500 ac	Curve number	= 91
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 34.0 min
Total precip.	= 3.74 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 400

Hydrograph Discharge Table

(Printed values >= 1.00% of Qp.)

Time -- Outflow (min cfs)		Time -- Outflow (min cfs)		Time -- Outflow (min cfs)		Time -- Outflow (min cfs)	
165	0.148	204	0.526	243	0.938	282	1.390
166	0.157	205	0.535	244	0.950	283	1.403
167	0.166	206	0.544	245	0.962	284	1.415
168	0.175	207	0.553	246	0.974	285	1.427
169	0.184	208	0.563	247	0.986	286	1.439
170	0.193	209	0.572	248	0.998	287	1.452
171	0.202	210	0.581	249	1.009	288	1.464
172	0.212	211	0.591	250	1.021	289	1.477
173	0.221	212	0.600	251	1.033	290	1.490
174	0.231	213	0.610	252	1.045	291	1.503
175	0.241	214	0.619	253	1.056	292	1.516
176	0.251	215	0.629	254	1.068	293	1.529
177	0.260	216	0.639	255	1.079	294	1.542
178	0.270	217	0.649	256	1.091	295	1.555
179	0.280	218	0.659	257	1.103	296	1.569
180	0.291	219	0.669	258	1.114	297	1.582
181	0.301	220	0.679	259	1.125	298	1.596
182	0.311	221	0.689	260	1.137	299	1.610
183	0.321	222	0.699	261	1.148	300	1.624
184	0.331	223	0.710	262	1.159	301	1.638
185	0.341	224	0.720	263	1.171	302	1.652
186	0.351	225	0.731	264	1.182	303	1.667
187	0.361	226	0.742	265	1.193	304	1.682
188	0.371	227	0.753	266	1.205	305	1.696
189	0.382	228	0.764	267	1.216	306	1.712
190	0.392	229	0.775	268	1.227	307	1.727
191	0.401	230	0.786	269	1.239	308	1.742
192	0.411	231	0.797	270	1.250	309	1.758
193	0.421	232	0.809	271	1.262	310	1.774
194	0.431	233	0.821	272	1.273	311	1.790
195	0.441	234	0.832	273	1.285	312	1.806
196	0.450	235	0.844	274	1.296	313	1.822
197	0.460	236	0.855	275	1.308	314	1.839
198	0.469	237	0.867	276	1.319	315	1.856
199	0.479	238	0.879	277	1.331	316	1.873
200	0.488	239	0.891	278	1.343	317	1.890
201	0.498	240	0.903	279	1.355	318	1.907
202	0.507	241	0.915	280	1.367	319	1.924
203	0.516	242	0.927	281	1.378	320	1.941

Continues on next page...

Hydrograph Discharge Table

Time (min	-- Outflow cfs)	Time (min	-- Outflow cfs)	Time (min	-- Outflow cfs)	Time (min	-- Outflow cfs)
321	1.959	377	2.995	433	4.148	489	14.38
322	1.977	378	3.021	434	4.178	490	14.50
323	1.994	379	3.048	435	4.211	491	14.61
324	2.012	380	3.074	436	4.245	492	14.69
325	2.030	381	3.101	437	4.280	493	14.75
326	2.048	382	3.129	438	4.317	494	14.79
327	2.066	383	3.156	439	4.356	495	14.81 <<
328	2.084	384	3.183	440	4.396	496	14.80
329	2.102	385	3.210	441	4.438	497	14.78
330	2.120	386	3.238	442	4.482	498	14.73
331	2.138	387	3.265	443	4.528	499	14.66
332	2.155	388	3.292	444	4.576	500	14.57
333	2.173	389	3.318	445	4.625	501	14.46
334	2.191	390	3.345	446	4.676	502	14.34
335	2.208	391	3.371	447	4.730	503	14.21
336	2.226	392	3.397	448	4.785	504	14.07
337	2.243	393	3.422	449	4.843	505	13.92
338	2.260	394	3.446	450	4.902	506	13.76
339	2.277	395	3.469	451	4.973	507	13.59
340	2.294	396	3.492	452	5.057	508	13.41
341	2.311	397	3.513	453	5.154	509	13.23
342	2.328	398	3.534	454	5.264	510	13.04
343	2.345	399	3.555	455	5.388	511	12.84
344	2.361	400	3.574	456	5.526	512	12.64
345	2.378	401	3.593	457	5.678	513	12.44
346	2.394	402	3.610	458	5.844	514	12.23
347	2.411	403	3.628	459	6.025	515	12.02
348	2.427	404	3.644	460	6.220	516	11.81
349	2.443	405	3.659	461	6.430	517	11.59
350	2.460	406	3.674	462	6.654	518	11.37
351	2.476	407	3.689	463	6.894	519	11.15
352	2.492	408	3.702	464	7.147	520	10.94
353	2.508	409	3.715	465	7.416	521	10.73
354	2.525	410	3.727	466	7.699	522	10.52
355	2.542	411	3.739	467	7.997	523	10.32
356	2.559	412	3.751	468	8.309	524	10.12
357	2.576	413	3.763	469	8.635	525	9.930
358	2.593	414	3.776	470	8.976	526	9.743
359	2.610	415	3.788	471	9.330	527	9.561
360	2.628	416	3.802	472	9.683	528	9.386
361	2.646	417	3.815	473	10.03	529	9.217
362	2.664	418	3.830	474	10.38	530	9.054
363	2.683	419	3.845	475	10.73	531	8.898
364	2.702	420	3.860	476	11.07	532	8.744
365	2.721	421	3.877	477	11.40	533	8.595
366	2.742	422	3.894	478	11.73	534	8.451
367	2.762	423	3.911	479	12.05	535	8.312
368	2.783	424	3.930	480	12.36	536	8.178
369	2.805	425	3.950	481	12.65	537	8.049
370	2.827	426	3.971	482	12.93	538	7.926
371	2.850	427	3.992	483	13.20	539	7.808
372	2.873	428	4.015	484	13.44	540	7.695
373	2.896	429	4.039	485	13.67	541	7.586
374	2.920	430	4.064	486	13.88	542	7.482
375	2.945	431	4.091	487	14.06	543	7.384
376	2.970	432	4.118	488	14.23	544	7.291

Continues on next page...

Hydrograph Discharge Table

Time (min	Outflow cfs)	Time (min	Outflow cfs)	Time (min	Outflow cfs)	Time (min	Outflow cfs)
545	7.203	601	4.749	657	4.090	713	3.544
546	7.120	602	4.735	658	4.082	714	3.532
547	7.043	603	4.721	659	4.074	715	3.521
548	6.970	604	4.708	660	4.066	716	3.510
549	6.899	605	4.695	661	4.058	717	3.500
550	6.831	606	4.682	662	4.050	718	3.489
551	6.764	607	4.670	663	4.042	719	3.479
552	6.698	608	4.657	664	4.033	720	3.469
553	6.634	609	4.644	665	4.025	721	3.459
554	6.572	610	4.632	666	4.017	722	3.449
555	6.510	611	4.619	667	4.009	723	3.440
556	6.450	612	4.607	668	4.000	724	3.431
557	6.392	613	4.594	669	3.993	725	3.422
558	6.334	614	4.582	670	3.985	726	3.414
559	6.277	615	4.570	671	3.977	727	3.405
560	6.221	616	4.558	672	3.970	728	3.398
561	6.166	617	4.545	673	3.962	729	3.390
562	6.114	618	4.533	674	3.954	730	3.383
563	6.062	619	4.521	675	3.945	731	3.376
564	6.012	620	4.509	676	3.937	732	3.369
565	5.962	621	4.497	677	3.929	733	3.363
566	5.913	622	4.482	678	3.920	734	3.357
567	5.865	623	4.467	679	3.912	735	3.352
568	5.817	624	4.452	680	3.903	736	3.347
569	5.770	625	4.437	681	3.894	737	3.342
570	5.723	626	4.423	682	3.885	738	3.337
571	5.675	627	4.408	683	3.876	739	3.333
572	5.628	628	4.394	684	3.866	740	3.330
573	5.582	629	4.380	685	3.857	741	3.326
574	5.536	630	4.366	686	3.848	742	3.324
575	5.491	631	4.352	687	3.838	743	3.321
576	5.447	632	4.339	688	3.828	744	3.319
577	5.403	633	4.326	689	3.818	745	3.317
578	5.360	634	4.313	690	3.808	746	3.316
579	5.320	635	4.300	691	3.798	747	3.315
580	5.280	636	4.288	692	3.788	748	3.315
581	5.242	637	4.276	693	3.777	749	3.315
582	5.206	638	4.265	694	3.766	750	3.315
583	5.170	639	4.253	695	3.755	751	3.315
584	5.136	640	4.241	696	3.744	752	3.316
585	5.104	641	4.230	697	3.733	753	3.317
586	5.072	642	4.219	698	3.721	754	3.317
587	5.042	643	4.208	699	3.709	755	3.318
588	5.013	644	4.198	700	3.698	756	3.318
589	4.986	645	4.188	701	3.686	757	3.319
590	4.959	646	4.179	702	3.674	758	3.319
591	4.934	647	4.170	703	3.662	759	3.319
592	4.912	648	4.161	704	3.651	760	3.319
593	4.892	649	4.153	705	3.639	761	3.319
594	4.872	650	4.144	706	3.627	762	3.318
595	4.852	651	4.137	707	3.615	763	3.318
596	4.833	652	4.129	708	3.603	764	3.317
597	4.815	653	4.121	709	3.591	765	3.315
598	4.797	654	4.113	710	3.579	766	3.314
599	4.780	655	4.105	711	3.567	767	3.312
600	4.763	656	4.097	712	3.555	768	3.309

Continues on next page...

Hydrograph Discharge Table

Time -- Outflow (min cfs)		Time -- Outflow (min cfs)		Time -- Outflow (min cfs)		Time -- Outflow (min cfs)	
769	3.306	825	3.151	881	2.994	937	2.891
770	3.303	826	3.147	882	2.993	938	2.889
771	3.299	827	3.143	883	2.991	939	2.887
772	3.295	828	3.139	884	2.990	940	2.885
773	3.291	829	3.135	885	2.988	941	2.883
774	3.286	830	3.130	886	2.987	942	2.881
775	3.282	831	3.126	887	2.986	943	2.879
776	3.278	832	3.122	888	2.984	944	2.877
777	3.274	833	3.117	889	2.983	945	2.874
778	3.270	834	3.113	890	2.981	946	2.872
779	3.266	835	3.109	891	2.980	947	2.870
780	3.262	836	3.104	892	2.978	948	2.868
781	3.258	837	3.100	893	2.976	949	2.866
782	3.254	838	3.095	894	2.975	950	2.864
783	3.251	839	3.091	895	2.973	951	2.862
784	3.247	840	3.087	896	2.971	952	2.860
785	3.244	841	3.082	897	2.970	953	2.858
786	3.242	842	3.078	898	2.968	954	2.856
787	3.239	843	3.074	899	2.966	955	2.854
788	3.236	844	3.070	900	2.964	956	2.852
789	3.234	845	3.066	901	2.962	957	2.850
790	3.232	846	3.062	902	2.961	958	2.848
791	3.230	847	3.058	903	2.959	959	2.846
792	3.228	848	3.054	904	2.957	960	2.844
793	3.227	849	3.051	905	2.955	961	2.842
794	3.225	850	3.048	906	2.953	962	2.840
795	3.224	851	3.044	907	2.951	963	2.838
796	3.223	852	3.041	908	2.949	964	2.836
797	3.222	853	3.039	909	2.947	965	2.834
798	3.221	854	3.036	910	2.945	966	2.832
799	3.220	855	3.034	911	2.943	967	2.830
800	3.219	856	3.031	912	2.941	968	2.828
801	3.218	857	3.029	913	2.939	969	2.825
802	3.217	858	3.027	914	2.937	970	2.823
803	3.216	859	3.025	915	2.935	971	2.821
804	3.214	860	3.024	916	2.933	972	2.819
805	3.212	861	3.022	917	2.931	973	2.817
806	3.210	862	3.020	918	2.929	974	2.815
807	3.208	863	3.019	919	2.927	975	2.813
808	3.206	864	3.017	920	2.925	976	2.811
809	3.203	865	3.016	921	2.923	977	2.809
810	3.201	866	3.014	922	2.921	978	2.807
811	3.198	867	3.013	923	2.919	979	2.805
812	3.195	868	3.011	924	2.917	980	2.803
813	3.192	869	3.010	925	2.915	981	2.801
814	3.189	870	3.009	926	2.913	982	2.799
815	3.186	871	3.007	927	2.911	983	2.797
816	3.183	872	3.006	928	2.909	984	2.795
817	3.180	873	3.005	929	2.907	985	2.793
818	3.176	874	3.003	930	2.905	986	2.790
819	3.173	875	3.002	931	2.903	987	2.788
820	3.170	876	3.001	932	2.901	988	2.786
821	3.166	877	2.999	933	2.899	989	2.784
822	3.163	878	2.998	934	2.897	990	2.782
823	3.159	879	2.997	935	2.895	991	2.780
824	3.155	880	2.995	936	2.893	992	2.778

Continues on next page...

Hydrograph Discharge Table

Time -- Outflow (min	cfs)	Time -- Outflow (min	cfs)	Time -- Outflow (min	cfs)	Time -- Outflow (min	cfs)
993	2.776	1049	2.659	1105	2.539	1161	2.418
994	2.774	1050	2.657	1106	2.537	1162	2.416
995	2.772	1051	2.654	1107	2.535	1163	2.414
996	2.770	1052	2.652	1108	2.533	1164	2.411
997	2.768	1053	2.650	1109	2.531	1165	2.409
998	2.766	1054	2.648	1110	2.528	1166	2.407
999	2.764	1055	2.646	1111	2.526	1167	2.405
1000	2.761	1056	2.644	1112	2.524	1168	2.403
1001	2.759	1057	2.642	1113	2.522	1169	2.400
1002	2.757	1058	2.640	1114	2.520	1170	2.398
1003	2.755	1059	2.637	1115	2.518	1171	2.396
1004	2.753	1060	2.635	1116	2.515	1172	2.394
1005	2.751	1061	2.633	1117	2.513	1173	2.392
1006	2.749	1062	2.631	1118	2.511	1174	2.389
1007	2.747	1063	2.629	1119	2.509	1175	2.387
1008	2.745	1064	2.627	1120	2.507	1176	2.385
1009	2.743	1065	2.625	1121	2.505	1177	2.383
1010	2.741	1066	2.623	1122	2.503	1178	2.381
1011	2.739	1067	2.620	1123	2.500	1179	2.379
1012	2.736	1068	2.618	1124	2.498	1180	2.376
1013	2.734	1069	2.616	1125	2.496	1181	2.374
1014	2.732	1070	2.614	1126	2.494	1182	2.372
1015	2.730	1071	2.612	1127	2.492	1183	2.370
1016	2.728	1072	2.610	1128	2.490	1184	2.368
1017	2.726	1073	2.608	1129	2.487	1185	2.365
1018	2.724	1074	2.606	1130	2.485	1186	2.363
1019	2.722	1075	2.603	1131	2.483	1187	2.361
1020	2.720	1076	2.601	1132	2.481	1188	2.359
1021	2.718	1077	2.599	1133	2.479	1189	2.357
1022	2.716	1078	2.597	1134	2.477	1190	2.354
1023	2.713	1079	2.595	1135	2.474	1191	2.352
1024	2.711	1080	2.593	1136	2.472	1192	2.350
1025	2.709	1081	2.591	1137	2.470	1193	2.348
1026	2.707	1082	2.588	1138	2.468	1194	2.346
1027	2.705	1083	2.586	1139	2.466	1195	2.343
1028	2.703	1084	2.584	1140	2.464	1196	2.341
1029	2.701	1085	2.582	1141	2.461	1197	2.339
1030	2.699	1086	2.580	1142	2.459	1198	2.337
1031	2.697	1087	2.578	1143	2.457	1199	2.335
1032	2.695	1088	2.576	1144	2.455	1200	2.332
1033	2.692	1089	2.574	1145	2.453	1201	2.330
1034	2.690	1090	2.571	1146	2.451	1202	2.328
1035	2.688	1091	2.569	1147	2.448	1203	2.326
1036	2.686	1092	2.567	1148	2.446	1204	2.324
1037	2.684	1093	2.565	1149	2.444	1205	2.321
1038	2.682	1094	2.563	1150	2.442	1206	2.319
1039	2.680	1095	2.561	1151	2.440	1207	2.317
1040	2.678	1096	2.559	1152	2.437	1208	2.315
1041	2.676	1097	2.556	1153	2.435	1209	2.313
1042	2.673	1098	2.554	1154	2.433	1210	2.310
1043	2.671	1099	2.552	1155	2.431	1211	2.308
1044	2.669	1100	2.550	1156	2.429	1212	2.306
1045	2.667	1101	2.548	1157	2.427	1213	2.304
1046	2.665	1102	2.546	1158	2.424	1214	2.302
1047	2.663	1103	2.543	1159	2.422	1215	2.299
1048	2.661	1104	2.541	1160	2.420	1216	2.297

Continues on next page...

Hydrograph Discharge Table

Time (min	Outflow cfs)	Time (min	Outflow cfs)	Time (min	Outflow cfs)	Time (min	Outflow cfs)
1217	2.295	1273	2.171	1329	2.046	1385	1.919
1218	2.293	1274	2.169	1330	2.043	1386	1.917
1219	2.291	1275	2.166	1331	2.041	1387	1.915
1220	2.288	1276	2.164	1332	2.039	1388	1.912
1221	2.286	1277	2.162	1333	2.037	1389	1.910
1222	2.284	1278	2.160	1334	2.034	1390	1.908
1223	2.282	1279	2.157	1335	2.032	1391	1.906
1224	2.280	1280	2.155	1336	2.030	1392	1.903
1225	2.277	1281	2.153	1337	2.028	1393	1.901
1226	2.275	1282	2.151	1338	2.025	1394	1.899
1227	2.273	1283	2.149	1339	2.023	1395	1.897
1228	2.271	1284	2.146	1340	2.021	1396	1.894
1229	2.269	1285	2.144	1341	2.019	1397	1.892
1230	2.266	1286	2.142	1342	2.016	1398	1.890
1231	2.264	1287	2.140	1343	2.014	1399	1.888
1232	2.262	1288	2.137	1344	2.012	1400	1.885
1233	2.260	1289	2.135	1345	2.010	1401	1.883
1234	2.257	1290	2.133	1346	2.007	1402	1.881
1235	2.255	1291	2.131	1347	2.005	1403	1.878
1236	2.253	1292	2.128	1348	2.003	1404	1.876
1237	2.251	1293	2.126	1349	2.001	1405	1.874
1238	2.249	1294	2.124	1350	1.998	1406	1.872
1239	2.246	1295	2.122	1351	1.996	1407	1.869
1240	2.244	1296	2.120	1352	1.994	1408	1.867
1241	2.242	1297	2.117	1353	1.992	1409	1.865
1242	2.240	1298	2.115	1354	1.989	1410	1.863
1243	2.238	1299	2.113	1355	1.987	1411	1.860
1244	2.235	1300	2.111	1356	1.985	1412	1.858
1245	2.233	1301	2.108	1357	1.982	1413	1.856
1246	2.231	1302	2.106	1358	1.980	1414	1.853
1247	2.229	1303	2.104	1359	1.978	1415	1.851
1248	2.226	1304	2.102	1360	1.976	1416	1.849
1249	2.224	1305	2.099	1361	1.973	1417	1.847
1250	2.222	1306	2.097	1362	1.971	1418	1.844
1251	2.220	1307	2.095	1363	1.969	1419	1.842
1252	2.218	1308	2.093	1364	1.967	1420	1.840
1253	2.215	1309	2.090	1365	1.964	1421	1.838
1254	2.213	1310	2.088	1366	1.962	1422	1.835
1255	2.211	1311	2.086	1367	1.960	1423	1.833
1256	2.209	1312	2.084	1368	1.958	1424	1.831
1257	2.206	1313	2.081	1369	1.955	1425	1.828
1258	2.204	1314	2.079	1370	1.953	1426	1.826
1259	2.202	1315	2.077	1371	1.951	1427	1.824
1260	2.200	1316	2.075	1372	1.949	1428	1.822
1261	2.198	1317	2.072	1373	1.946	1429	1.819
1262	2.195	1318	2.070	1374	1.944	1430	1.817
1263	2.193	1319	2.068	1375	1.942	1431	1.815
1264	2.191	1320	2.066	1376	1.940	1432	1.813
1265	2.189	1321	2.063	1377	1.937	1433	1.810
1266	2.186	1322	2.061	1378	1.935	1434	1.808
1267	2.184	1323	2.059	1379	1.933	1435	1.806
1268	2.182	1324	2.057	1380	1.931	1436	1.803
1269	2.180	1325	2.055	1381	1.928	1437	1.801
1270	2.178	1326	2.052	1382	1.926	1438	1.799
1271	2.175	1327	2.050	1383	1.924	1439	1.797
1272	2.173	1328	2.048	1384	1.921	1440	1.794

Continues on next page...

Developed site storm event

Hydrograph Discharge Table

Time -- (min	Outflow cfs)
1441	1.790
1442	1.783
1443	1.773
1444	1.761
1445	1.747
1446	1.730
1447	1.711
1448	1.689
1449	1.665
1450	1.639
1451	1.610
1452	1.579
1453	1.546
1454	1.510
1455	1.472
1456	1.431
1457	1.388
1458	1.343
1459	1.295
1460	1.245
1461	1.193
1462	1.142
1463	1.091
1464	1.042
1465	0.995
1466	0.948
1467	0.902
1468	0.858
1469	0.815
1470	0.773
1471	0.732
1472	0.692
1473	0.653
1474	0.616
1475	0.579
1476	0.544
1477	0.510
1478	0.476
1479	0.445
1480	0.414
1481	0.384
1482	0.355
1483	0.328
1484	0.302
1485	0.276
1486	0.252
1487	0.229
1488	0.207
1489	0.186
1490	0.167
1491	0.148

...End

Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Hyd. No. 2

Detention pond outflow

Hydrograph type	= Reservoir	Peak discharge	= 4.403 cfs
Storm frequency	= 10 yrs	Time to peak	= 627 min
Time interval	= 1 min	Hyd. volume	= 195,513 cuft
Inflow hyd. No.	= 1 - Developed site storm event	Reservoir name	= Detention Pond
Max. Elevation	= 61.76 ft	Max. Storage	= 90,408 cuft

Storage Indication method used.

Hydrograph Discharge Table

(Printed values >= 1.00% of Qp.)

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
497	14.78	61.22	-----	0.328	-----	-----	-----	-----	-----	-----	-----	0.328
498	14.73	61.23	-----	0.638	-----	-----	-----	-----	-----	-----	-----	0.638
499	14.66	61.25	-----	0.940	-----	-----	-----	-----	-----	-----	-----	0.940
500	14.57	61.27	-----	1.234	-----	-----	-----	-----	-----	-----	-----	1.234
501	14.46	61.28	-----	1.520	-----	-----	-----	-----	-----	-----	-----	1.520
502	14.34	61.30	-----	1.797	-----	-----	-----	-----	-----	-----	-----	1.797
503	14.21	61.31	-----	1.950	-----	-----	-----	-----	-----	-----	-----	1.950
504	14.07	61.32	-----	2.060	-----	-----	-----	-----	-----	-----	-----	2.060
505	13.92	61.34	-----	2.167	-----	-----	-----	-----	-----	-----	-----	2.167
506	13.76	61.35	-----	2.271	-----	-----	-----	-----	-----	-----	-----	2.271
507	13.59	61.37	-----	2.373	-----	-----	-----	-----	-----	-----	-----	2.373
508	13.41	61.38	-----	2.473	-----	-----	-----	-----	-----	-----	-----	2.473
509	13.23	61.39	-----	2.570	-----	-----	-----	-----	-----	-----	-----	2.570
510	13.04	61.40	-----	2.660	-----	-----	-----	-----	-----	-----	-----	2.660
511	12.84	61.41	-----	2.731	-----	-----	-----	-----	-----	-----	-----	2.731
512	12.64	61.43	-----	2.800	-----	-----	-----	-----	-----	-----	-----	2.800
513	12.44	61.44	-----	2.867	-----	-----	-----	-----	-----	-----	-----	2.867
514	12.23	61.45	-----	2.932	-----	-----	-----	-----	-----	-----	-----	2.932
515	12.02	61.46	-----	2.995	-----	-----	-----	-----	-----	-----	-----	2.995
516	11.81	61.47	-----	3.057	-----	-----	-----	-----	-----	-----	-----	3.057
517	11.59	61.48	-----	3.116	-----	-----	-----	-----	-----	-----	-----	3.116
518	11.37	61.49	-----	3.174	-----	-----	-----	-----	-----	-----	-----	3.174
519	11.15	61.50	-----	3.229	-----	-----	-----	-----	-----	-----	-----	3.229
520	10.94	61.51	-----	3.276	-----	-----	-----	-----	-----	-----	-----	3.276
521	10.73	61.52	-----	3.320	-----	-----	-----	-----	-----	-----	-----	3.320
522	10.52	61.53	-----	3.362	-----	-----	-----	-----	-----	-----	-----	3.362
523	10.32	61.53	-----	3.403	-----	-----	-----	-----	-----	-----	-----	3.403
524	10.12	61.54	-----	3.443	-----	-----	-----	-----	-----	-----	-----	3.443
525	9.930	61.55	-----	3.481	-----	-----	-----	-----	-----	-----	-----	3.481
526	9.743	61.56	-----	3.518	-----	-----	-----	-----	-----	-----	-----	3.518
527	9.561	61.56	-----	3.554	-----	-----	-----	-----	-----	-----	-----	3.554
528	9.386	61.57	-----	3.588	-----	-----	-----	-----	-----	-----	-----	3.588
529	9.217	61.58	-----	3.621	-----	-----	-----	-----	-----	-----	-----	3.621
530	9.054	61.58	-----	3.653	-----	-----	-----	-----	-----	-----	-----	3.653
531	8.898	61.59	-----	3.684	-----	-----	-----	-----	-----	-----	-----	3.684
532	8.744	61.60	-----	3.714	-----	-----	-----	-----	-----	-----	-----	3.714
533	8.595	61.60	-----	3.742	-----	-----	-----	-----	-----	-----	-----	3.742
534	8.451	61.61	-----	3.766	-----	-----	-----	-----	-----	-----	-----	3.766
535	8.312	61.61	-----	3.790	-----	-----	-----	-----	-----	-----	-----	3.790
536	8.178	61.62	-----	3.813	-----	-----	-----	-----	-----	-----	-----	3.813
537	8.049	61.62	-----	3.835	-----	-----	-----	-----	-----	-----	-----	3.835
538	7.926	61.63	-----	3.856	-----	-----	-----	-----	-----	-----	-----	3.856

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
539	7.808	61.63	-----	3.877	-----	-----	-----	-----	-----	-----	-----	3.877
540	7.695	61.64	-----	3.897	-----	-----	-----	-----	-----	-----	-----	3.897
541	7.586	61.64	-----	3.916	-----	-----	-----	-----	-----	-----	-----	3.916
542	7.482	61.64	-----	3.934	-----	-----	-----	-----	-----	-----	-----	3.934
543	7.384	61.65	-----	3.952	-----	-----	-----	-----	-----	-----	-----	3.952
544	7.291	61.65	-----	3.969	-----	-----	-----	-----	-----	-----	-----	3.969
545	7.203	61.66	-----	3.986	-----	-----	-----	-----	-----	-----	-----	3.986
546	7.120	61.66	-----	4.002	-----	-----	-----	-----	-----	-----	-----	4.003
547	7.043	61.66	-----	4.018	-----	-----	-----	-----	-----	-----	-----	4.018
548	6.970	61.67	-----	4.034	-----	-----	-----	-----	-----	-----	-----	4.034
549	6.899	61.67	-----	4.048	-----	-----	-----	-----	-----	-----	-----	4.048
550	6.831	61.67	-----	4.063	-----	-----	-----	-----	-----	-----	-----	4.063
551	6.764	61.68	-----	4.077	-----	-----	-----	-----	-----	-----	-----	4.077
552	6.698	61.68	-----	4.090	-----	-----	-----	-----	-----	-----	-----	4.090
553	6.634	61.68	-----	4.104	-----	-----	-----	-----	-----	-----	-----	4.104
554	6.572	61.69	-----	4.116	-----	-----	-----	-----	-----	-----	-----	4.116
555	6.510	61.69	-----	4.129	-----	-----	-----	-----	-----	-----	-----	4.129
556	6.450	61.69	-----	4.141	-----	-----	-----	-----	-----	-----	-----	4.141
557	6.392	61.69	-----	4.153	-----	-----	-----	-----	-----	-----	-----	4.153
558	6.334	61.70	-----	4.164	-----	-----	-----	-----	-----	-----	-----	4.164
559	6.277	61.70	-----	4.175	-----	-----	-----	-----	-----	-----	-----	4.175
560	6.221	61.70	-----	4.185	-----	-----	-----	-----	-----	-----	-----	4.185
561	6.166	61.70	-----	4.194	-----	-----	-----	-----	-----	-----	-----	4.194
562	6.114	61.71	-----	4.203	-----	-----	-----	-----	-----	-----	-----	4.203
563	6.062	61.71	-----	4.212	-----	-----	-----	-----	-----	-----	-----	4.212
564	6.012	61.71	-----	4.220	-----	-----	-----	-----	-----	-----	-----	4.220
565	5.962	61.71	-----	4.228	-----	-----	-----	-----	-----	-----	-----	4.228
566	5.913	61.71	-----	4.236	-----	-----	-----	-----	-----	-----	-----	4.236
567	5.865	61.72	-----	4.244	-----	-----	-----	-----	-----	-----	-----	4.244
568	5.817	61.72	-----	4.251	-----	-----	-----	-----	-----	-----	-----	4.251
569	5.770	61.72	-----	4.258	-----	-----	-----	-----	-----	-----	-----	4.258
570	5.723	61.72	-----	4.265	-----	-----	-----	-----	-----	-----	-----	4.265
571	5.675	61.72	-----	4.272	-----	-----	-----	-----	-----	-----	-----	4.272
572	5.628	61.73	-----	4.278	-----	-----	-----	-----	-----	-----	-----	4.278
573	5.582	61.73	-----	4.285	-----	-----	-----	-----	-----	-----	-----	4.284
574	5.536	61.73	-----	4.290	-----	-----	-----	-----	-----	-----	-----	4.290
575	5.491	61.73	-----	4.296	-----	-----	-----	-----	-----	-----	-----	4.296
576	5.447	61.73	-----	4.301	-----	-----	-----	-----	-----	-----	-----	4.301
577	5.403	61.73	-----	4.307	-----	-----	-----	-----	-----	-----	-----	4.307
578	5.360	61.73	-----	4.312	-----	-----	-----	-----	-----	-----	-----	4.312
579	5.320	61.73	-----	4.316	-----	-----	-----	-----	-----	-----	-----	4.316
580	5.280	61.74	-----	4.321	-----	-----	-----	-----	-----	-----	-----	4.321
581	5.242	61.74	-----	4.325	-----	-----	-----	-----	-----	-----	-----	4.325
582	5.206	61.74	-----	4.329	-----	-----	-----	-----	-----	-----	-----	4.329
583	5.170	61.74	-----	4.333	-----	-----	-----	-----	-----	-----	-----	4.333
584	5.136	61.74	-----	4.337	-----	-----	-----	-----	-----	-----	-----	4.337
585	5.104	61.74	-----	4.341	-----	-----	-----	-----	-----	-----	-----	4.341
586	5.072	61.74	-----	4.344	-----	-----	-----	-----	-----	-----	-----	4.344
587	5.042	61.74	-----	4.348	-----	-----	-----	-----	-----	-----	-----	4.348
588	5.013	61.74	-----	4.351	-----	-----	-----	-----	-----	-----	-----	4.351
589	4.986	61.74	-----	4.354	-----	-----	-----	-----	-----	-----	-----	4.354
590	4.959	61.74	-----	4.357	-----	-----	-----	-----	-----	-----	-----	4.357
591	4.934	61.75	-----	4.359	-----	-----	-----	-----	-----	-----	-----	4.359
592	4.912	61.75	-----	4.362	-----	-----	-----	-----	-----	-----	-----	4.362
593	4.892	61.75	-----	4.365	-----	-----	-----	-----	-----	-----	-----	4.365
594	4.872	61.75	-----	4.367	-----	-----	-----	-----	-----	-----	-----	4.367

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
595	4.852	61.75	-----	4.369	-----	-----	-----	-----	-----	-----	-----	4.369
596	4.833	61.75	-----	4.371	-----	-----	-----	-----	-----	-----	-----	4.371
597	4.815	61.75	-----	4.373	-----	-----	-----	-----	-----	-----	-----	4.373
598	4.797	61.75	-----	4.375	-----	-----	-----	-----	-----	-----	-----	4.375
599	4.780	61.75	-----	4.377	-----	-----	-----	-----	-----	-----	-----	4.377
600	4.763	61.75	-----	4.379	-----	-----	-----	-----	-----	-----	-----	4.379
601	4.749	61.75	-----	4.381	-----	-----	-----	-----	-----	-----	-----	4.381
602	4.735	61.75	-----	4.383	-----	-----	-----	-----	-----	-----	-----	4.383
603	4.721	61.75	-----	4.384	-----	-----	-----	-----	-----	-----	-----	4.384
604	4.708	61.75	-----	4.386	-----	-----	-----	-----	-----	-----	-----	4.386
605	4.695	61.75	-----	4.387	-----	-----	-----	-----	-----	-----	-----	4.387
606	4.682	61.75	-----	4.389	-----	-----	-----	-----	-----	-----	-----	4.389
607	4.670	61.75	-----	4.390	-----	-----	-----	-----	-----	-----	-----	4.390
608	4.657	61.75	-----	4.391	-----	-----	-----	-----	-----	-----	-----	4.391
609	4.644	61.75	-----	4.392	-----	-----	-----	-----	-----	-----	-----	4.392
610	4.632	61.75	-----	4.394	-----	-----	-----	-----	-----	-----	-----	4.394
611	4.619	61.75	-----	4.395	-----	-----	-----	-----	-----	-----	-----	4.395
612	4.607	61.75	-----	4.396	-----	-----	-----	-----	-----	-----	-----	4.396
613	4.594	61.75	-----	4.397	-----	-----	-----	-----	-----	-----	-----	4.397
614	4.582	61.76	-----	4.397	-----	-----	-----	-----	-----	-----	-----	4.397
615	4.570	61.76	-----	4.398	-----	-----	-----	-----	-----	-----	-----	4.398
616	4.558	61.76	-----	4.399	-----	-----	-----	-----	-----	-----	-----	4.399
617	4.545	61.76	-----	4.400	-----	-----	-----	-----	-----	-----	-----	4.400
618	4.533	61.76	-----	4.400	-----	-----	-----	-----	-----	-----	-----	4.400
619	4.521	61.76	-----	4.401	-----	-----	-----	-----	-----	-----	-----	4.401
620	4.509	61.76	-----	4.402	-----	-----	-----	-----	-----	-----	-----	4.402
621	4.497	61.76	-----	4.402	-----	-----	-----	-----	-----	-----	-----	4.402
622	4.482	61.76	-----	4.402	-----	-----	-----	-----	-----	-----	-----	4.402
623	4.467	61.76	-----	4.403	-----	-----	-----	-----	-----	-----	-----	4.403
624	4.452	61.76	-----	4.403	-----	-----	-----	-----	-----	-----	-----	4.403
625	4.437	61.76	-----	4.403	-----	-----	-----	-----	-----	-----	-----	4.403
626	4.423	61.76	-----	4.403	-----	-----	-----	-----	-----	-----	-----	4.403
627	4.408	61.76 <<	-----	4.403	-----	-----	-----	-----	-----	-----	-----	4.403 <<
628	4.394	61.76	-----	4.403	-----	-----	-----	-----	-----	-----	-----	4.403
629	4.380	61.76	-----	4.403	-----	-----	-----	-----	-----	-----	-----	4.403
630	4.366	61.76	-----	4.403	-----	-----	-----	-----	-----	-----	-----	4.403
631	4.352	61.76	-----	4.403	-----	-----	-----	-----	-----	-----	-----	4.403
632	4.339	61.76	-----	4.403	-----	-----	-----	-----	-----	-----	-----	4.403
633	4.326	61.76	-----	4.402	-----	-----	-----	-----	-----	-----	-----	4.402
634	4.313	61.76	-----	4.402	-----	-----	-----	-----	-----	-----	-----	4.402
635	4.300	61.76	-----	4.402	-----	-----	-----	-----	-----	-----	-----	4.402
636	4.288	61.76	-----	4.401	-----	-----	-----	-----	-----	-----	-----	4.401
637	4.276	61.76	-----	4.400	-----	-----	-----	-----	-----	-----	-----	4.400
638	4.265	61.76	-----	4.400	-----	-----	-----	-----	-----	-----	-----	4.400
639	4.253	61.76	-----	4.399	-----	-----	-----	-----	-----	-----	-----	4.399
640	4.241	61.76	-----	4.399	-----	-----	-----	-----	-----	-----	-----	4.399
641	4.230	61.76	-----	4.398	-----	-----	-----	-----	-----	-----	-----	4.398
642	4.219	61.75	-----	4.397	-----	-----	-----	-----	-----	-----	-----	4.397
643	4.208	61.75	-----	4.396	-----	-----	-----	-----	-----	-----	-----	4.396
644	4.198	61.75	-----	4.395	-----	-----	-----	-----	-----	-----	-----	4.395
645	4.188	61.75	-----	4.394	-----	-----	-----	-----	-----	-----	-----	4.394
646	4.179	61.75	-----	4.393	-----	-----	-----	-----	-----	-----	-----	4.393
647	4.170	61.75	-----	4.392	-----	-----	-----	-----	-----	-----	-----	4.392
648	4.161	61.75	-----	4.391	-----	-----	-----	-----	-----	-----	-----	4.391
649	4.153	61.75	-----	4.390	-----	-----	-----	-----	-----	-----	-----	4.390
650	4.144	61.75	-----	4.389	-----	-----	-----	-----	-----	-----	-----	4.389

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
651	4.137	61.75	-----	4.388	-----	-----	-----	-----	-----	-----	-----	4.388
652	4.129	61.75	-----	4.387	-----	-----	-----	-----	-----	-----	-----	4.387
653	4.121	61.75	-----	4.385	-----	-----	-----	-----	-----	-----	-----	4.385
654	4.113	61.75	-----	4.384	-----	-----	-----	-----	-----	-----	-----	4.384
655	4.105	61.75	-----	4.383	-----	-----	-----	-----	-----	-----	-----	4.383
656	4.097	61.75	-----	4.382	-----	-----	-----	-----	-----	-----	-----	4.382
657	4.090	61.75	-----	4.380	-----	-----	-----	-----	-----	-----	-----	4.380
658	4.082	61.75	-----	4.379	-----	-----	-----	-----	-----	-----	-----	4.379
659	4.074	61.75	-----	4.378	-----	-----	-----	-----	-----	-----	-----	4.378
660	4.066	61.75	-----	4.376	-----	-----	-----	-----	-----	-----	-----	4.376
661	4.058	61.75	-----	4.375	-----	-----	-----	-----	-----	-----	-----	4.375
662	4.050	61.75	-----	4.373	-----	-----	-----	-----	-----	-----	-----	4.373
663	4.042	61.75	-----	4.372	-----	-----	-----	-----	-----	-----	-----	4.372
664	4.033	61.75	-----	4.370	-----	-----	-----	-----	-----	-----	-----	4.370
665	4.025	61.75	-----	4.369	-----	-----	-----	-----	-----	-----	-----	4.369
666	4.017	61.75	-----	4.367	-----	-----	-----	-----	-----	-----	-----	4.367
667	4.009	61.75	-----	4.365	-----	-----	-----	-----	-----	-----	-----	4.365
668	4.000	61.75	-----	4.364	-----	-----	-----	-----	-----	-----	-----	4.364
669	3.993	61.75	-----	4.362	-----	-----	-----	-----	-----	-----	-----	4.362
670	3.985	61.75	-----	4.360	-----	-----	-----	-----	-----	-----	-----	4.360
671	3.977	61.75	-----	4.358	-----	-----	-----	-----	-----	-----	-----	4.358
672	3.970	61.74	-----	4.357	-----	-----	-----	-----	-----	-----	-----	4.357
673	3.962	61.74	-----	4.355	-----	-----	-----	-----	-----	-----	-----	4.355
674	3.954	61.74	-----	4.353	-----	-----	-----	-----	-----	-----	-----	4.353
675	3.945	61.74	-----	4.351	-----	-----	-----	-----	-----	-----	-----	4.351
676	3.937	61.74	-----	4.349	-----	-----	-----	-----	-----	-----	-----	4.349
677	3.929	61.74	-----	4.347	-----	-----	-----	-----	-----	-----	-----	4.347
678	3.920	61.74	-----	4.345	-----	-----	-----	-----	-----	-----	-----	4.345
679	3.912	61.74	-----	4.343	-----	-----	-----	-----	-----	-----	-----	4.343
680	3.903	61.74	-----	4.341	-----	-----	-----	-----	-----	-----	-----	4.341
681	3.894	61.74	-----	4.339	-----	-----	-----	-----	-----	-----	-----	4.339
682	3.885	61.74	-----	4.337	-----	-----	-----	-----	-----	-----	-----	4.337
683	3.876	61.74	-----	4.335	-----	-----	-----	-----	-----	-----	-----	4.335
684	3.866	61.74	-----	4.333	-----	-----	-----	-----	-----	-----	-----	4.333
685	3.857	61.74	-----	4.331	-----	-----	-----	-----	-----	-----	-----	4.331
686	3.848	61.74	-----	4.329	-----	-----	-----	-----	-----	-----	-----	4.329
687	3.838	61.74	-----	4.326	-----	-----	-----	-----	-----	-----	-----	4.326
688	3.828	61.74	-----	4.324	-----	-----	-----	-----	-----	-----	-----	4.324
689	3.818	61.74	-----	4.322	-----	-----	-----	-----	-----	-----	-----	4.322
690	3.808	61.74	-----	4.319	-----	-----	-----	-----	-----	-----	-----	4.319
691	3.798	61.73	-----	4.317	-----	-----	-----	-----	-----	-----	-----	4.317
692	3.788	61.73	-----	4.315	-----	-----	-----	-----	-----	-----	-----	4.315
693	3.777	61.73	-----	4.312	-----	-----	-----	-----	-----	-----	-----	4.312
694	3.766	61.73	-----	4.310	-----	-----	-----	-----	-----	-----	-----	4.310
695	3.755	61.73	-----	4.307	-----	-----	-----	-----	-----	-----	-----	4.307
696	3.744	61.73	-----	4.304	-----	-----	-----	-----	-----	-----	-----	4.304
697	3.733	61.73	-----	4.302	-----	-----	-----	-----	-----	-----	-----	4.302
698	3.721	61.73	-----	4.299	-----	-----	-----	-----	-----	-----	-----	4.299
699	3.709	61.73	-----	4.296	-----	-----	-----	-----	-----	-----	-----	4.296
700	3.698	61.73	-----	4.294	-----	-----	-----	-----	-----	-----	-----	4.294
701	3.686	61.73	-----	4.291	-----	-----	-----	-----	-----	-----	-----	4.291
702	3.674	61.73	-----	4.288	-----	-----	-----	-----	-----	-----	-----	4.288
703	3.662	61.73	-----	4.285	-----	-----	-----	-----	-----	-----	-----	4.285
704	3.651	61.73	-----	4.282	-----	-----	-----	-----	-----	-----	-----	4.282
705	3.639	61.73	-----	4.279	-----	-----	-----	-----	-----	-----	-----	4.279
706	3.627	61.72	-----	4.276	-----	-----	-----	-----	-----	-----	-----	4.276

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
707	3.615	61.72	-----	4.273	-----	-----	-----	-----	-----	-----	-----	4.273
708	3.603	61.72	-----	4.270	-----	-----	-----	-----	-----	-----	-----	4.270
709	3.591	61.72	-----	4.267	-----	-----	-----	-----	-----	-----	-----	4.267
710	3.579	61.72	-----	4.264	-----	-----	-----	-----	-----	-----	-----	4.264
711	3.567	61.72	-----	4.261	-----	-----	-----	-----	-----	-----	-----	4.261
712	3.555	61.72	-----	4.258	-----	-----	-----	-----	-----	-----	-----	4.258
713	3.544	61.72	-----	4.254	-----	-----	-----	-----	-----	-----	-----	4.254
714	3.532	61.72	-----	4.251	-----	-----	-----	-----	-----	-----	-----	4.251
715	3.521	61.72	-----	4.248	-----	-----	-----	-----	-----	-----	-----	4.248
716	3.510	61.72	-----	4.244	-----	-----	-----	-----	-----	-----	-----	4.244
717	3.500	61.72	-----	4.241	-----	-----	-----	-----	-----	-----	-----	4.241
718	3.489	61.71	-----	4.237	-----	-----	-----	-----	-----	-----	-----	4.237
719	3.479	61.71	-----	4.234	-----	-----	-----	-----	-----	-----	-----	4.234
720	3.469	61.71	-----	4.230	-----	-----	-----	-----	-----	-----	-----	4.230
721	3.459	61.71	-----	4.227	-----	-----	-----	-----	-----	-----	-----	4.227
722	3.449	61.71	-----	4.223	-----	-----	-----	-----	-----	-----	-----	4.223
723	3.440	61.71	-----	4.220	-----	-----	-----	-----	-----	-----	-----	4.220
724	3.431	61.71	-----	4.216	-----	-----	-----	-----	-----	-----	-----	4.216
725	3.422	61.71	-----	4.212	-----	-----	-----	-----	-----	-----	-----	4.212
726	3.414	61.71	-----	4.209	-----	-----	-----	-----	-----	-----	-----	4.209
727	3.405	61.71	-----	4.205	-----	-----	-----	-----	-----	-----	-----	4.205
728	3.398	61.71	-----	4.201	-----	-----	-----	-----	-----	-----	-----	4.201
729	3.390	61.70	-----	4.197	-----	-----	-----	-----	-----	-----	-----	4.197
730	3.383	61.70	-----	4.194	-----	-----	-----	-----	-----	-----	-----	4.194
731	3.376	61.70	-----	4.190	-----	-----	-----	-----	-----	-----	-----	4.190
732	3.369	61.70	-----	4.186	-----	-----	-----	-----	-----	-----	-----	4.186
733	3.363	61.70	-----	4.182	-----	-----	-----	-----	-----	-----	-----	4.182
734	3.357	61.70	-----	4.179	-----	-----	-----	-----	-----	-----	-----	4.179
735	3.352	61.70	-----	4.174	-----	-----	-----	-----	-----	-----	-----	4.174
736	3.347	61.70	-----	4.170	-----	-----	-----	-----	-----	-----	-----	4.170
737	3.342	61.70	-----	4.166	-----	-----	-----	-----	-----	-----	-----	4.166
738	3.337	61.70	-----	4.162	-----	-----	-----	-----	-----	-----	-----	4.162
739	3.333	61.70	-----	4.158	-----	-----	-----	-----	-----	-----	-----	4.158
740	3.330	61.69	-----	4.153	-----	-----	-----	-----	-----	-----	-----	4.153
741	3.326	61.69	-----	4.149	-----	-----	-----	-----	-----	-----	-----	4.149
742	3.324	61.69	-----	4.145	-----	-----	-----	-----	-----	-----	-----	4.145
743	3.321	61.69	-----	4.141	-----	-----	-----	-----	-----	-----	-----	4.141
744	3.319	61.69	-----	4.136	-----	-----	-----	-----	-----	-----	-----	4.136
745	3.317	61.69	-----	4.132	-----	-----	-----	-----	-----	-----	-----	4.132
746	3.316	61.69	-----	4.128	-----	-----	-----	-----	-----	-----	-----	4.128
747	3.315	61.69	-----	4.124	-----	-----	-----	-----	-----	-----	-----	4.124
748	3.315	61.69	-----	4.120	-----	-----	-----	-----	-----	-----	-----	4.120
749	3.315	61.69	-----	4.116	-----	-----	-----	-----	-----	-----	-----	4.116
750	3.315	61.69	-----	4.112	-----	-----	-----	-----	-----	-----	-----	4.112
751	3.315	61.68	-----	4.108	-----	-----	-----	-----	-----	-----	-----	4.108
752	3.316	61.68	-----	4.103	-----	-----	-----	-----	-----	-----	-----	4.103
753	3.317	61.68	-----	4.099	-----	-----	-----	-----	-----	-----	-----	4.099
754	3.317	61.68	-----	4.095	-----	-----	-----	-----	-----	-----	-----	4.095
755	3.318	61.68	-----	4.091	-----	-----	-----	-----	-----	-----	-----	4.091
756	3.318	61.68	-----	4.087	-----	-----	-----	-----	-----	-----	-----	4.087
757	3.319	61.68	-----	4.084	-----	-----	-----	-----	-----	-----	-----	4.084
758	3.319	61.68	-----	4.080	-----	-----	-----	-----	-----	-----	-----	4.080
759	3.319	61.68	-----	4.076	-----	-----	-----	-----	-----	-----	-----	4.076
760	3.319	61.68	-----	4.072	-----	-----	-----	-----	-----	-----	-----	4.072
761	3.319	61.68	-----	4.068	-----	-----	-----	-----	-----	-----	-----	4.068
762	3.318	61.67	-----	4.064	-----	-----	-----	-----	-----	-----	-----	4.064

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
763	3.318	61.67	-----	4.060	-----	-----	-----	-----	-----	-----	-----	4.060
764	3.317	61.67	-----	4.057	-----	-----	-----	-----	-----	-----	-----	4.057
765	3.315	61.67	-----	4.053	-----	-----	-----	-----	-----	-----	-----	4.053
766	3.314	61.67	-----	4.049	-----	-----	-----	-----	-----	-----	-----	4.049
767	3.312	61.67	-----	4.045	-----	-----	-----	-----	-----	-----	-----	4.045
768	3.309	61.67	-----	4.041	-----	-----	-----	-----	-----	-----	-----	4.041
769	3.306	61.67	-----	4.038	-----	-----	-----	-----	-----	-----	-----	4.038
770	3.303	61.67	-----	4.034	-----	-----	-----	-----	-----	-----	-----	4.034
771	3.299	61.67	-----	4.030	-----	-----	-----	-----	-----	-----	-----	4.030
772	3.295	61.67	-----	4.026	-----	-----	-----	-----	-----	-----	-----	4.026
773	3.291	61.66	-----	4.023	-----	-----	-----	-----	-----	-----	-----	4.023
774	3.286	61.66	-----	4.019	-----	-----	-----	-----	-----	-----	-----	4.019
775	3.282	61.66	-----	4.015	-----	-----	-----	-----	-----	-----	-----	4.015
776	3.278	61.66	-----	4.011	-----	-----	-----	-----	-----	-----	-----	4.011
777	3.274	61.66	-----	4.008	-----	-----	-----	-----	-----	-----	-----	4.008
778	3.270	61.66	-----	4.004	-----	-----	-----	-----	-----	-----	-----	4.004
779	3.266	61.66	-----	4.000	-----	-----	-----	-----	-----	-----	-----	4.000
780	3.262	61.66	-----	3.996	-----	-----	-----	-----	-----	-----	-----	3.996
781	3.258	61.66	-----	3.993	-----	-----	-----	-----	-----	-----	-----	3.993
782	3.254	61.66	-----	3.989	-----	-----	-----	-----	-----	-----	-----	3.989
783	3.251	61.66	-----	3.985	-----	-----	-----	-----	-----	-----	-----	3.985
784	3.247	61.66	-----	3.981	-----	-----	-----	-----	-----	-----	-----	3.981
785	3.244	61.65	-----	3.977	-----	-----	-----	-----	-----	-----	-----	3.977
786	3.242	61.65	-----	3.974	-----	-----	-----	-----	-----	-----	-----	3.974
787	3.239	61.65	-----	3.970	-----	-----	-----	-----	-----	-----	-----	3.970
788	3.236	61.65	-----	3.966	-----	-----	-----	-----	-----	-----	-----	3.966
789	3.234	61.65	-----	3.962	-----	-----	-----	-----	-----	-----	-----	3.962
790	3.232	61.65	-----	3.959	-----	-----	-----	-----	-----	-----	-----	3.959
791	3.230	61.65	-----	3.955	-----	-----	-----	-----	-----	-----	-----	3.955
792	3.228	61.65	-----	3.951	-----	-----	-----	-----	-----	-----	-----	3.951
793	3.227	61.65	-----	3.948	-----	-----	-----	-----	-----	-----	-----	3.948
794	3.225	61.65	-----	3.944	-----	-----	-----	-----	-----	-----	-----	3.944
795	3.224	61.65	-----	3.940	-----	-----	-----	-----	-----	-----	-----	3.940
796	3.223	61.65	-----	3.937	-----	-----	-----	-----	-----	-----	-----	3.937
797	3.222	61.64	-----	3.933	-----	-----	-----	-----	-----	-----	-----	3.933
798	3.221	61.64	-----	3.929	-----	-----	-----	-----	-----	-----	-----	3.929
799	3.220	61.64	-----	3.926	-----	-----	-----	-----	-----	-----	-----	3.926
800	3.219	61.64	-----	3.922	-----	-----	-----	-----	-----	-----	-----	3.922
801	3.218	61.64	-----	3.918	-----	-----	-----	-----	-----	-----	-----	3.918
802	3.217	61.64	-----	3.915	-----	-----	-----	-----	-----	-----	-----	3.915
803	3.216	61.64	-----	3.911	-----	-----	-----	-----	-----	-----	-----	3.911
804	3.214	61.64	-----	3.908	-----	-----	-----	-----	-----	-----	-----	3.908
805	3.212	61.64	-----	3.904	-----	-----	-----	-----	-----	-----	-----	3.904
806	3.210	61.64	-----	3.901	-----	-----	-----	-----	-----	-----	-----	3.901
807	3.208	61.64	-----	3.897	-----	-----	-----	-----	-----	-----	-----	3.897
808	3.206	61.64	-----	3.893	-----	-----	-----	-----	-----	-----	-----	3.893
809	3.203	61.63	-----	3.890	-----	-----	-----	-----	-----	-----	-----	3.890
810	3.201	61.63	-----	3.886	-----	-----	-----	-----	-----	-----	-----	3.886
811	3.198	61.63	-----	3.883	-----	-----	-----	-----	-----	-----	-----	3.883
812	3.195	61.63	-----	3.879	-----	-----	-----	-----	-----	-----	-----	3.879
813	3.192	61.63	-----	3.876	-----	-----	-----	-----	-----	-----	-----	3.876
814	3.189	61.63	-----	3.872	-----	-----	-----	-----	-----	-----	-----	3.872
815	3.186	61.63	-----	3.869	-----	-----	-----	-----	-----	-----	-----	3.869
816	3.183	61.63	-----	3.865	-----	-----	-----	-----	-----	-----	-----	3.865
817	3.180	61.63	-----	3.862	-----	-----	-----	-----	-----	-----	-----	3.862
818	3.176	61.63	-----	3.858	-----	-----	-----	-----	-----	-----	-----	3.858

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
819	3.173	61.63	-----	3.855	-----	-----	-----	-----	-----	-----	-----	3.855
820	3.170	61.63	-----	3.851	-----	-----	-----	-----	-----	-----	-----	3.851
821	3.166	61.63	-----	3.848	-----	-----	-----	-----	-----	-----	-----	3.848
822	3.163	61.62	-----	3.844	-----	-----	-----	-----	-----	-----	-----	3.844
823	3.159	61.62	-----	3.841	-----	-----	-----	-----	-----	-----	-----	3.841
824	3.155	61.62	-----	3.837	-----	-----	-----	-----	-----	-----	-----	3.837
825	3.151	61.62	-----	3.834	-----	-----	-----	-----	-----	-----	-----	3.834
826	3.147	61.62	-----	3.830	-----	-----	-----	-----	-----	-----	-----	3.830
827	3.143	61.62	-----	3.827	-----	-----	-----	-----	-----	-----	-----	3.827
828	3.139	61.62	-----	3.823	-----	-----	-----	-----	-----	-----	-----	3.823
829	3.135	61.62	-----	3.820	-----	-----	-----	-----	-----	-----	-----	3.820
830	3.130	61.62	-----	3.816	-----	-----	-----	-----	-----	-----	-----	3.816
831	3.126	61.62	-----	3.813	-----	-----	-----	-----	-----	-----	-----	3.813
832	3.122	61.62	-----	3.809	-----	-----	-----	-----	-----	-----	-----	3.809
833	3.117	61.62	-----	3.806	-----	-----	-----	-----	-----	-----	-----	3.806
834	3.113	61.61	-----	3.802	-----	-----	-----	-----	-----	-----	-----	3.802
835	3.109	61.61	-----	3.799	-----	-----	-----	-----	-----	-----	-----	3.799
836	3.104	61.61	-----	3.795	-----	-----	-----	-----	-----	-----	-----	3.795
837	3.100	61.61	-----	3.792	-----	-----	-----	-----	-----	-----	-----	3.792
838	3.095	61.61	-----	3.788	-----	-----	-----	-----	-----	-----	-----	3.788
839	3.091	61.61	-----	3.784	-----	-----	-----	-----	-----	-----	-----	3.784
840	3.087	61.61	-----	3.781	-----	-----	-----	-----	-----	-----	-----	3.781
841	3.082	61.61	-----	3.777	-----	-----	-----	-----	-----	-----	-----	3.777
842	3.078	61.61	-----	3.774	-----	-----	-----	-----	-----	-----	-----	3.774
843	3.074	61.61	-----	3.770	-----	-----	-----	-----	-----	-----	-----	3.770
844	3.070	61.61	-----	3.767	-----	-----	-----	-----	-----	-----	-----	3.767
845	3.066	61.61	-----	3.763	-----	-----	-----	-----	-----	-----	-----	3.763
846	3.062	61.61	-----	3.759	-----	-----	-----	-----	-----	-----	-----	3.759
847	3.058	61.60	-----	3.756	-----	-----	-----	-----	-----	-----	-----	3.756
848	3.054	61.60	-----	3.752	-----	-----	-----	-----	-----	-----	-----	3.752
849	3.051	61.60	-----	3.749	-----	-----	-----	-----	-----	-----	-----	3.749
850	3.048	61.60	-----	3.745	-----	-----	-----	-----	-----	-----	-----	3.745
851	3.044	61.60	-----	3.742	-----	-----	-----	-----	-----	-----	-----	3.742
852	3.041	61.60	-----	3.738	-----	-----	-----	-----	-----	-----	-----	3.738
853	3.039	61.60	-----	3.734	-----	-----	-----	-----	-----	-----	-----	3.734
854	3.036	61.60	-----	3.730	-----	-----	-----	-----	-----	-----	-----	3.730
855	3.034	61.60	-----	3.726	-----	-----	-----	-----	-----	-----	-----	3.726
856	3.031	61.60	-----	3.722	-----	-----	-----	-----	-----	-----	-----	3.722
857	3.029	61.60	-----	3.718	-----	-----	-----	-----	-----	-----	-----	3.718
858	3.027	61.60	-----	3.714	-----	-----	-----	-----	-----	-----	-----	3.714
859	3.025	61.59	-----	3.710	-----	-----	-----	-----	-----	-----	-----	3.710
860	3.024	61.59	-----	3.706	-----	-----	-----	-----	-----	-----	-----	3.706
861	3.022	61.59	-----	3.702	-----	-----	-----	-----	-----	-----	-----	3.702
862	3.020	61.59	-----	3.698	-----	-----	-----	-----	-----	-----	-----	3.698
863	3.019	61.59	-----	3.694	-----	-----	-----	-----	-----	-----	-----	3.694
864	3.017	61.59	-----	3.690	-----	-----	-----	-----	-----	-----	-----	3.690
865	3.016	61.59	-----	3.686	-----	-----	-----	-----	-----	-----	-----	3.686
866	3.014	61.59	-----	3.682	-----	-----	-----	-----	-----	-----	-----	3.682
867	3.013	61.59	-----	3.678	-----	-----	-----	-----	-----	-----	-----	3.678
868	3.011	61.59	-----	3.675	-----	-----	-----	-----	-----	-----	-----	3.675
869	3.010	61.59	-----	3.671	-----	-----	-----	-----	-----	-----	-----	3.671
870	3.009	61.59	-----	3.667	-----	-----	-----	-----	-----	-----	-----	3.667
871	3.007	61.59	-----	3.663	-----	-----	-----	-----	-----	-----	-----	3.663
872	3.006	61.58	-----	3.659	-----	-----	-----	-----	-----	-----	-----	3.659
873	3.005	61.58	-----	3.655	-----	-----	-----	-----	-----	-----	-----	3.655
874	3.003	61.58	-----	3.652	-----	-----	-----	-----	-----	-----	-----	3.652

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
875	3.002	61.58	-----	3.648	-----	-----	-----	-----	-----	-----	-----	3.648
876	3.001	61.58	-----	3.644	-----	-----	-----	-----	-----	-----	-----	3.644
877	2.999	61.58	-----	3.640	-----	-----	-----	-----	-----	-----	-----	3.640
878	2.998	61.58	-----	3.637	-----	-----	-----	-----	-----	-----	-----	3.637
879	2.997	61.58	-----	3.633	-----	-----	-----	-----	-----	-----	-----	3.633
880	2.995	61.58	-----	3.629	-----	-----	-----	-----	-----	-----	-----	3.629
881	2.994	61.58	-----	3.626	-----	-----	-----	-----	-----	-----	-----	3.626
882	2.993	61.58	-----	3.622	-----	-----	-----	-----	-----	-----	-----	3.622
883	2.991	61.58	-----	3.618	-----	-----	-----	-----	-----	-----	-----	3.618
884	2.990	61.58	-----	3.615	-----	-----	-----	-----	-----	-----	-----	3.615
885	2.988	61.57	-----	3.611	-----	-----	-----	-----	-----	-----	-----	3.611
886	2.987	61.57	-----	3.607	-----	-----	-----	-----	-----	-----	-----	3.607
887	2.986	61.57	-----	3.604	-----	-----	-----	-----	-----	-----	-----	3.604
888	2.984	61.57	-----	3.600	-----	-----	-----	-----	-----	-----	-----	3.600
889	2.983	61.57	-----	3.597	-----	-----	-----	-----	-----	-----	-----	3.597
890	2.981	61.57	-----	3.593	-----	-----	-----	-----	-----	-----	-----	3.593
891	2.980	61.57	-----	3.589	-----	-----	-----	-----	-----	-----	-----	3.589
892	2.978	61.57	-----	3.586	-----	-----	-----	-----	-----	-----	-----	3.586
893	2.976	61.57	-----	3.582	-----	-----	-----	-----	-----	-----	-----	3.582
894	2.975	61.57	-----	3.579	-----	-----	-----	-----	-----	-----	-----	3.579
895	2.973	61.57	-----	3.575	-----	-----	-----	-----	-----	-----	-----	3.575
896	2.971	61.57	-----	3.572	-----	-----	-----	-----	-----	-----	-----	3.572
897	2.970	61.57	-----	3.568	-----	-----	-----	-----	-----	-----	-----	3.568
898	2.968	61.57	-----	3.565	-----	-----	-----	-----	-----	-----	-----	3.565
899	2.966	61.56	-----	3.561	-----	-----	-----	-----	-----	-----	-----	3.561
900	2.964	61.56	-----	3.558	-----	-----	-----	-----	-----	-----	-----	3.558
901	2.962	61.56	-----	3.554	-----	-----	-----	-----	-----	-----	-----	3.554
902	2.961	61.56	-----	3.551	-----	-----	-----	-----	-----	-----	-----	3.551
903	2.959	61.56	-----	3.548	-----	-----	-----	-----	-----	-----	-----	3.548
904	2.957	61.56	-----	3.544	-----	-----	-----	-----	-----	-----	-----	3.544
905	2.955	61.56	-----	3.541	-----	-----	-----	-----	-----	-----	-----	3.541
906	2.953	61.56	-----	3.537	-----	-----	-----	-----	-----	-----	-----	3.537
907	2.951	61.56	-----	3.534	-----	-----	-----	-----	-----	-----	-----	3.534
908	2.949	61.56	-----	3.531	-----	-----	-----	-----	-----	-----	-----	3.531
909	2.947	61.56	-----	3.527	-----	-----	-----	-----	-----	-----	-----	3.527
910	2.945	61.56	-----	3.524	-----	-----	-----	-----	-----	-----	-----	3.524
911	2.943	61.56	-----	3.520	-----	-----	-----	-----	-----	-----	-----	3.520
912	2.941	61.56	-----	3.517	-----	-----	-----	-----	-----	-----	-----	3.517
913	2.939	61.56	-----	3.514	-----	-----	-----	-----	-----	-----	-----	3.514
914	2.937	61.55	-----	3.510	-----	-----	-----	-----	-----	-----	-----	3.510
915	2.935	61.55	-----	3.507	-----	-----	-----	-----	-----	-----	-----	3.507
916	2.933	61.55	-----	3.504	-----	-----	-----	-----	-----	-----	-----	3.504
917	2.931	61.55	-----	3.500	-----	-----	-----	-----	-----	-----	-----	3.500
918	2.929	61.55	-----	3.497	-----	-----	-----	-----	-----	-----	-----	3.497
919	2.927	61.55	-----	3.494	-----	-----	-----	-----	-----	-----	-----	3.494
920	2.925	61.55	-----	3.490	-----	-----	-----	-----	-----	-----	-----	3.490
921	2.923	61.55	-----	3.487	-----	-----	-----	-----	-----	-----	-----	3.487
922	2.921	61.55	-----	3.484	-----	-----	-----	-----	-----	-----	-----	3.484
923	2.919	61.55	-----	3.481	-----	-----	-----	-----	-----	-----	-----	3.481
924	2.917	61.55	-----	3.477	-----	-----	-----	-----	-----	-----	-----	3.477
925	2.915	61.55	-----	3.474	-----	-----	-----	-----	-----	-----	-----	3.474
926	2.913	61.55	-----	3.471	-----	-----	-----	-----	-----	-----	-----	3.471
927	2.911	61.55	-----	3.468	-----	-----	-----	-----	-----	-----	-----	3.468
928	2.909	61.55	-----	3.464	-----	-----	-----	-----	-----	-----	-----	3.464
929	2.907	61.54	-----	3.461	-----	-----	-----	-----	-----	-----	-----	3.461
930	2.905	61.54	-----	3.458	-----	-----	-----	-----	-----	-----	-----	3.458

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
931	2.903	61.54	-----	3.455	-----	-----	-----	-----	-----	-----	-----	3.455
932	2.901	61.54	-----	3.451	-----	-----	-----	-----	-----	-----	-----	3.451
933	2.899	61.54	-----	3.448	-----	-----	-----	-----	-----	-----	-----	3.448
934	2.897	61.54	-----	3.445	-----	-----	-----	-----	-----	-----	-----	3.445
935	2.895	61.54	-----	3.442	-----	-----	-----	-----	-----	-----	-----	3.442
936	2.893	61.54	-----	3.439	-----	-----	-----	-----	-----	-----	-----	3.439
937	2.891	61.54	-----	3.435	-----	-----	-----	-----	-----	-----	-----	3.435
938	2.889	61.54	-----	3.432	-----	-----	-----	-----	-----	-----	-----	3.432
939	2.887	61.54	-----	3.429	-----	-----	-----	-----	-----	-----	-----	3.429
940	2.885	61.54	-----	3.426	-----	-----	-----	-----	-----	-----	-----	3.426
941	2.883	61.54	-----	3.423	-----	-----	-----	-----	-----	-----	-----	3.423
942	2.881	61.54	-----	3.420	-----	-----	-----	-----	-----	-----	-----	3.420
943	2.879	61.54	-----	3.417	-----	-----	-----	-----	-----	-----	-----	3.417
944	2.877	61.54	-----	3.413	-----	-----	-----	-----	-----	-----	-----	3.413
945	2.874	61.53	-----	3.410	-----	-----	-----	-----	-----	-----	-----	3.410
946	2.872	61.53	-----	3.407	-----	-----	-----	-----	-----	-----	-----	3.407
947	2.870	61.53	-----	3.404	-----	-----	-----	-----	-----	-----	-----	3.404
948	2.868	61.53	-----	3.401	-----	-----	-----	-----	-----	-----	-----	3.401
949	2.866	61.53	-----	3.398	-----	-----	-----	-----	-----	-----	-----	3.398
950	2.864	61.53	-----	3.395	-----	-----	-----	-----	-----	-----	-----	3.395
951	2.862	61.53	-----	3.392	-----	-----	-----	-----	-----	-----	-----	3.392
952	2.860	61.53	-----	3.389	-----	-----	-----	-----	-----	-----	-----	3.389
953	2.858	61.53	-----	3.386	-----	-----	-----	-----	-----	-----	-----	3.386
954	2.856	61.53	-----	3.382	-----	-----	-----	-----	-----	-----	-----	3.382
955	2.854	61.53	-----	3.379	-----	-----	-----	-----	-----	-----	-----	3.379
956	2.852	61.53	-----	3.376	-----	-----	-----	-----	-----	-----	-----	3.376
957	2.850	61.53	-----	3.373	-----	-----	-----	-----	-----	-----	-----	3.373
958	2.848	61.53	-----	3.370	-----	-----	-----	-----	-----	-----	-----	3.370
959	2.846	61.53	-----	3.367	-----	-----	-----	-----	-----	-----	-----	3.367
960	2.844	61.53	-----	3.364	-----	-----	-----	-----	-----	-----	-----	3.364
961	2.842	61.53	-----	3.361	-----	-----	-----	-----	-----	-----	-----	3.361
962	2.840	61.52	-----	3.358	-----	-----	-----	-----	-----	-----	-----	3.358
963	2.838	61.52	-----	3.355	-----	-----	-----	-----	-----	-----	-----	3.355
964	2.836	61.52	-----	3.352	-----	-----	-----	-----	-----	-----	-----	3.352
965	2.834	61.52	-----	3.349	-----	-----	-----	-----	-----	-----	-----	3.349
966	2.832	61.52	-----	3.346	-----	-----	-----	-----	-----	-----	-----	3.346
967	2.830	61.52	-----	3.343	-----	-----	-----	-----	-----	-----	-----	3.343
968	2.828	61.52	-----	3.340	-----	-----	-----	-----	-----	-----	-----	3.340
969	2.825	61.52	-----	3.337	-----	-----	-----	-----	-----	-----	-----	3.337
970	2.823	61.52	-----	3.334	-----	-----	-----	-----	-----	-----	-----	3.334
971	2.821	61.52	-----	3.331	-----	-----	-----	-----	-----	-----	-----	3.331
972	2.819	61.52	-----	3.328	-----	-----	-----	-----	-----	-----	-----	3.328
973	2.817	61.52	-----	3.325	-----	-----	-----	-----	-----	-----	-----	3.325
974	2.815	61.52	-----	3.322	-----	-----	-----	-----	-----	-----	-----	3.322
975	2.813	61.52	-----	3.319	-----	-----	-----	-----	-----	-----	-----	3.319
976	2.811	61.52	-----	3.316	-----	-----	-----	-----	-----	-----	-----	3.316
977	2.809	61.52	-----	3.313	-----	-----	-----	-----	-----	-----	-----	3.313
978	2.807	61.51	-----	3.311	-----	-----	-----	-----	-----	-----	-----	3.311
979	2.805	61.51	-----	3.308	-----	-----	-----	-----	-----	-----	-----	3.308
980	2.803	61.51	-----	3.305	-----	-----	-----	-----	-----	-----	-----	3.305
981	2.801	61.51	-----	3.302	-----	-----	-----	-----	-----	-----	-----	3.302
982	2.799	61.51	-----	3.299	-----	-----	-----	-----	-----	-----	-----	3.299
983	2.797	61.51	-----	3.296	-----	-----	-----	-----	-----	-----	-----	3.296
984	2.795	61.51	-----	3.293	-----	-----	-----	-----	-----	-----	-----	3.293
985	2.793	61.51	-----	3.290	-----	-----	-----	-----	-----	-----	-----	3.290
986	2.790	61.51	-----	3.287	-----	-----	-----	-----	-----	-----	-----	3.287

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
987	2.788	61.51	-----	3.284	-----	-----	-----	-----	-----	-----	-----	3.284
988	2.786	61.51	-----	3.281	-----	-----	-----	-----	-----	-----	-----	3.281
989	2.784	61.51	-----	3.279	-----	-----	-----	-----	-----	-----	-----	3.279
990	2.782	61.51	-----	3.276	-----	-----	-----	-----	-----	-----	-----	3.276
991	2.780	61.51	-----	3.273	-----	-----	-----	-----	-----	-----	-----	3.273
992	2.778	61.51	-----	3.270	-----	-----	-----	-----	-----	-----	-----	3.270
993	2.776	61.51	-----	3.267	-----	-----	-----	-----	-----	-----	-----	3.267
994	2.774	61.51	-----	3.264	-----	-----	-----	-----	-----	-----	-----	3.264
995	2.772	61.51	-----	3.261	-----	-----	-----	-----	-----	-----	-----	3.261
996	2.770	61.50	-----	3.259	-----	-----	-----	-----	-----	-----	-----	3.258
997	2.768	61.50	-----	3.256	-----	-----	-----	-----	-----	-----	-----	3.256
998	2.766	61.50	-----	3.253	-----	-----	-----	-----	-----	-----	-----	3.253
999	2.764	61.50	-----	3.250	-----	-----	-----	-----	-----	-----	-----	3.250
1000	2.761	61.50	-----	3.247	-----	-----	-----	-----	-----	-----	-----	3.247
1001	2.759	61.50	-----	3.244	-----	-----	-----	-----	-----	-----	-----	3.244
1002	2.757	61.50	-----	3.241	-----	-----	-----	-----	-----	-----	-----	3.241
1003	2.755	61.50	-----	3.239	-----	-----	-----	-----	-----	-----	-----	3.239
1004	2.753	61.50	-----	3.236	-----	-----	-----	-----	-----	-----	-----	3.236
1005	2.751	61.50	-----	3.233	-----	-----	-----	-----	-----	-----	-----	3.233
1006	2.749	61.50	-----	3.229	-----	-----	-----	-----	-----	-----	-----	3.229
1007	2.747	61.50	-----	3.226	-----	-----	-----	-----	-----	-----	-----	3.226
1008	2.745	61.50	-----	3.223	-----	-----	-----	-----	-----	-----	-----	3.223
1009	2.743	61.50	-----	3.219	-----	-----	-----	-----	-----	-----	-----	3.219
1010	2.741	61.50	-----	3.216	-----	-----	-----	-----	-----	-----	-----	3.216
1011	2.739	61.50	-----	3.213	-----	-----	-----	-----	-----	-----	-----	3.213
1012	2.736	61.50	-----	3.209	-----	-----	-----	-----	-----	-----	-----	3.209
1013	2.734	61.49	-----	3.206	-----	-----	-----	-----	-----	-----	-----	3.206
1014	2.732	61.49	-----	3.203	-----	-----	-----	-----	-----	-----	-----	3.203
1015	2.730	61.49	-----	3.200	-----	-----	-----	-----	-----	-----	-----	3.200
1016	2.728	61.49	-----	3.196	-----	-----	-----	-----	-----	-----	-----	3.196
1017	2.726	61.49	-----	3.193	-----	-----	-----	-----	-----	-----	-----	3.193
1018	2.724	61.49	-----	3.190	-----	-----	-----	-----	-----	-----	-----	3.190
1019	2.722	61.49	-----	3.187	-----	-----	-----	-----	-----	-----	-----	3.187
1020	2.720	61.49	-----	3.184	-----	-----	-----	-----	-----	-----	-----	3.184
1021	2.718	61.49	-----	3.180	-----	-----	-----	-----	-----	-----	-----	3.180
1022	2.716	61.49	-----	3.177	-----	-----	-----	-----	-----	-----	-----	3.177
1023	2.713	61.49	-----	3.174	-----	-----	-----	-----	-----	-----	-----	3.174
1024	2.711	61.49	-----	3.171	-----	-----	-----	-----	-----	-----	-----	3.171
1025	2.709	61.49	-----	3.168	-----	-----	-----	-----	-----	-----	-----	3.168
1026	2.707	61.49	-----	3.164	-----	-----	-----	-----	-----	-----	-----	3.164
1027	2.705	61.49	-----	3.161	-----	-----	-----	-----	-----	-----	-----	3.161
1028	2.703	61.49	-----	3.158	-----	-----	-----	-----	-----	-----	-----	3.158
1029	2.701	61.49	-----	3.155	-----	-----	-----	-----	-----	-----	-----	3.155
1030	2.699	61.49	-----	3.152	-----	-----	-----	-----	-----	-----	-----	3.152
1031	2.697	61.49	-----	3.149	-----	-----	-----	-----	-----	-----	-----	3.149
1032	2.695	61.48	-----	3.146	-----	-----	-----	-----	-----	-----	-----	3.146
1033	2.692	61.48	-----	3.143	-----	-----	-----	-----	-----	-----	-----	3.142
1034	2.690	61.48	-----	3.139	-----	-----	-----	-----	-----	-----	-----	3.139
1035	2.688	61.48	-----	3.136	-----	-----	-----	-----	-----	-----	-----	3.136
1036	2.686	61.48	-----	3.133	-----	-----	-----	-----	-----	-----	-----	3.133
1037	2.684	61.48	-----	3.130	-----	-----	-----	-----	-----	-----	-----	3.130
1038	2.682	61.48	-----	3.127	-----	-----	-----	-----	-----	-----	-----	3.127
1039	2.680	61.48	-----	3.124	-----	-----	-----	-----	-----	-----	-----	3.124
1040	2.678	61.48	-----	3.121	-----	-----	-----	-----	-----	-----	-----	3.121
1041	2.676	61.48	-----	3.118	-----	-----	-----	-----	-----	-----	-----	3.118
1042	2.673	61.48	-----	3.115	-----	-----	-----	-----	-----	-----	-----	3.115

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1043	2.671	61.48	-----	3.112	-----	-----	-----	-----	-----	-----	-----	3.112
1044	2.669	61.48	-----	3.109	-----	-----	-----	-----	-----	-----	-----	3.109
1045	2.667	61.48	-----	3.106	-----	-----	-----	-----	-----	-----	-----	3.106
1046	2.665	61.48	-----	3.103	-----	-----	-----	-----	-----	-----	-----	3.103
1047	2.663	61.48	-----	3.100	-----	-----	-----	-----	-----	-----	-----	3.100
1048	2.661	61.48	-----	3.097	-----	-----	-----	-----	-----	-----	-----	3.097
1049	2.659	61.48	-----	3.094	-----	-----	-----	-----	-----	-----	-----	3.094
1050	2.657	61.48	-----	3.091	-----	-----	-----	-----	-----	-----	-----	3.091
1051	2.654	61.48	-----	3.088	-----	-----	-----	-----	-----	-----	-----	3.088
1052	2.652	61.47	-----	3.085	-----	-----	-----	-----	-----	-----	-----	3.085
1053	2.650	61.47	-----	3.082	-----	-----	-----	-----	-----	-----	-----	3.082
1054	2.648	61.47	-----	3.079	-----	-----	-----	-----	-----	-----	-----	3.079
1055	2.646	61.47	-----	3.076	-----	-----	-----	-----	-----	-----	-----	3.076
1056	2.644	61.47	-----	3.073	-----	-----	-----	-----	-----	-----	-----	3.073
1057	2.642	61.47	-----	3.070	-----	-----	-----	-----	-----	-----	-----	3.070
1058	2.640	61.47	-----	3.067	-----	-----	-----	-----	-----	-----	-----	3.067
1059	2.637	61.47	-----	3.064	-----	-----	-----	-----	-----	-----	-----	3.064
1060	2.635	61.47	-----	3.061	-----	-----	-----	-----	-----	-----	-----	3.061
1061	2.633	61.47	-----	3.058	-----	-----	-----	-----	-----	-----	-----	3.058
1062	2.631	61.47	-----	3.055	-----	-----	-----	-----	-----	-----	-----	3.055
1063	2.629	61.47	-----	3.052	-----	-----	-----	-----	-----	-----	-----	3.052
1064	2.627	61.47	-----	3.049	-----	-----	-----	-----	-----	-----	-----	3.049
1065	2.625	61.47	-----	3.046	-----	-----	-----	-----	-----	-----	-----	3.046
1066	2.623	61.47	-----	3.043	-----	-----	-----	-----	-----	-----	-----	3.043
1067	2.620	61.47	-----	3.040	-----	-----	-----	-----	-----	-----	-----	3.040
1068	2.618	61.47	-----	3.038	-----	-----	-----	-----	-----	-----	-----	3.038
1069	2.616	61.47	-----	3.035	-----	-----	-----	-----	-----	-----	-----	3.035
1070	2.614	61.47	-----	3.032	-----	-----	-----	-----	-----	-----	-----	3.032
1071	2.612	61.47	-----	3.029	-----	-----	-----	-----	-----	-----	-----	3.029
1072	2.610	61.46	-----	3.026	-----	-----	-----	-----	-----	-----	-----	3.026
1073	2.608	61.46	-----	3.023	-----	-----	-----	-----	-----	-----	-----	3.023
1074	2.606	61.46	-----	3.020	-----	-----	-----	-----	-----	-----	-----	3.020
1075	2.603	61.46	-----	3.017	-----	-----	-----	-----	-----	-----	-----	3.017
1076	2.601	61.46	-----	3.015	-----	-----	-----	-----	-----	-----	-----	3.015
1077	2.599	61.46	-----	3.012	-----	-----	-----	-----	-----	-----	-----	3.012
1078	2.597	61.46	-----	3.009	-----	-----	-----	-----	-----	-----	-----	3.009
1079	2.595	61.46	-----	3.006	-----	-----	-----	-----	-----	-----	-----	3.006
1080	2.593	61.46	-----	3.003	-----	-----	-----	-----	-----	-----	-----	3.003
1081	2.591	61.46	-----	3.000	-----	-----	-----	-----	-----	-----	-----	3.000
1082	2.588	61.46	-----	2.997	-----	-----	-----	-----	-----	-----	-----	2.997
1083	2.586	61.46	-----	2.995	-----	-----	-----	-----	-----	-----	-----	2.995
1084	2.584	61.46	-----	2.992	-----	-----	-----	-----	-----	-----	-----	2.992
1085	2.582	61.46	-----	2.989	-----	-----	-----	-----	-----	-----	-----	2.989
1086	2.580	61.46	-----	2.986	-----	-----	-----	-----	-----	-----	-----	2.986
1087	2.578	61.46	-----	2.983	-----	-----	-----	-----	-----	-----	-----	2.983
1088	2.576	61.46	-----	2.981	-----	-----	-----	-----	-----	-----	-----	2.981
1089	2.574	61.46	-----	2.978	-----	-----	-----	-----	-----	-----	-----	2.978
1090	2.571	61.46	-----	2.975	-----	-----	-----	-----	-----	-----	-----	2.975
1091	2.569	61.46	-----	2.972	-----	-----	-----	-----	-----	-----	-----	2.972
1092	2.567	61.46	-----	2.969	-----	-----	-----	-----	-----	-----	-----	2.969
1093	2.565	61.45	-----	2.967	-----	-----	-----	-----	-----	-----	-----	2.967
1094	2.563	61.45	-----	2.964	-----	-----	-----	-----	-----	-----	-----	2.964
1095	2.561	61.45	-----	2.961	-----	-----	-----	-----	-----	-----	-----	2.961
1096	2.559	61.45	-----	2.958	-----	-----	-----	-----	-----	-----	-----	2.958
1097	2.556	61.45	-----	2.956	-----	-----	-----	-----	-----	-----	-----	2.956
1098	2.554	61.45	-----	2.953	-----	-----	-----	-----	-----	-----	-----	2.953

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1099	2.552	61.45	-----	2.950	-----	-----	-----	-----	-----	-----	-----	2.950
1100	2.550	61.45	-----	2.947	-----	-----	-----	-----	-----	-----	-----	2.947
1101	2.548	61.45	-----	2.945	-----	-----	-----	-----	-----	-----	-----	2.945
1102	2.546	61.45	-----	2.942	-----	-----	-----	-----	-----	-----	-----	2.942
1103	2.543	61.45	-----	2.939	-----	-----	-----	-----	-----	-----	-----	2.939
1104	2.541	61.45	-----	2.936	-----	-----	-----	-----	-----	-----	-----	2.936
1105	2.539	61.45	-----	2.934	-----	-----	-----	-----	-----	-----	-----	2.934
1106	2.537	61.45	-----	2.931	-----	-----	-----	-----	-----	-----	-----	2.931
1107	2.535	61.45	-----	2.928	-----	-----	-----	-----	-----	-----	-----	2.928
1108	2.533	61.45	-----	2.926	-----	-----	-----	-----	-----	-----	-----	2.926
1109	2.531	61.45	-----	2.923	-----	-----	-----	-----	-----	-----	-----	2.923
1110	2.528	61.45	-----	2.920	-----	-----	-----	-----	-----	-----	-----	2.920
1111	2.526	61.45	-----	2.917	-----	-----	-----	-----	-----	-----	-----	2.917
1112	2.524	61.45	-----	2.915	-----	-----	-----	-----	-----	-----	-----	2.915
1113	2.522	61.45	-----	2.912	-----	-----	-----	-----	-----	-----	-----	2.912
1114	2.520	61.44	-----	2.909	-----	-----	-----	-----	-----	-----	-----	2.909
1115	2.518	61.44	-----	2.907	-----	-----	-----	-----	-----	-----	-----	2.907
1116	2.515	61.44	-----	2.904	-----	-----	-----	-----	-----	-----	-----	2.904
1117	2.513	61.44	-----	2.901	-----	-----	-----	-----	-----	-----	-----	2.901
1118	2.511	61.44	-----	2.899	-----	-----	-----	-----	-----	-----	-----	2.899
1119	2.509	61.44	-----	2.896	-----	-----	-----	-----	-----	-----	-----	2.896
1120	2.507	61.44	-----	2.893	-----	-----	-----	-----	-----	-----	-----	2.893
1121	2.505	61.44	-----	2.891	-----	-----	-----	-----	-----	-----	-----	2.891
1122	2.503	61.44	-----	2.888	-----	-----	-----	-----	-----	-----	-----	2.888
1123	2.500	61.44	-----	2.885	-----	-----	-----	-----	-----	-----	-----	2.885
1124	2.498	61.44	-----	2.883	-----	-----	-----	-----	-----	-----	-----	2.883
1125	2.496	61.44	-----	2.880	-----	-----	-----	-----	-----	-----	-----	2.880
1126	2.494	61.44	-----	2.877	-----	-----	-----	-----	-----	-----	-----	2.877
1127	2.492	61.44	-----	2.875	-----	-----	-----	-----	-----	-----	-----	2.875
1128	2.490	61.44	-----	2.872	-----	-----	-----	-----	-----	-----	-----	2.872
1129	2.487	61.44	-----	2.869	-----	-----	-----	-----	-----	-----	-----	2.869
1130	2.485	61.44	-----	2.867	-----	-----	-----	-----	-----	-----	-----	2.867
1131	2.483	61.44	-----	2.864	-----	-----	-----	-----	-----	-----	-----	2.864
1132	2.481	61.44	-----	2.861	-----	-----	-----	-----	-----	-----	-----	2.861
1133	2.479	61.44	-----	2.859	-----	-----	-----	-----	-----	-----	-----	2.859
1134	2.477	61.44	-----	2.856	-----	-----	-----	-----	-----	-----	-----	2.856
1135	2.474	61.44	-----	2.854	-----	-----	-----	-----	-----	-----	-----	2.854
1136	2.472	61.44	-----	2.851	-----	-----	-----	-----	-----	-----	-----	2.851
1137	2.470	61.43	-----	2.848	-----	-----	-----	-----	-----	-----	-----	2.848
1138	2.468	61.43	-----	2.846	-----	-----	-----	-----	-----	-----	-----	2.846
1139	2.466	61.43	-----	2.843	-----	-----	-----	-----	-----	-----	-----	2.843
1140	2.464	61.43	-----	2.840	-----	-----	-----	-----	-----	-----	-----	2.840
1141	2.461	61.43	-----	2.838	-----	-----	-----	-----	-----	-----	-----	2.838
1142	2.459	61.43	-----	2.835	-----	-----	-----	-----	-----	-----	-----	2.835
1143	2.457	61.43	-----	2.833	-----	-----	-----	-----	-----	-----	-----	2.833
1144	2.455	61.43	-----	2.830	-----	-----	-----	-----	-----	-----	-----	2.830
1145	2.453	61.43	-----	2.827	-----	-----	-----	-----	-----	-----	-----	2.827
1146	2.451	61.43	-----	2.825	-----	-----	-----	-----	-----	-----	-----	2.825
1147	2.448	61.43	-----	2.822	-----	-----	-----	-----	-----	-----	-----	2.822
1148	2.446	61.43	-----	2.820	-----	-----	-----	-----	-----	-----	-----	2.820
1149	2.444	61.43	-----	2.817	-----	-----	-----	-----	-----	-----	-----	2.817
1150	2.442	61.43	-----	2.815	-----	-----	-----	-----	-----	-----	-----	2.815
1151	2.440	61.43	-----	2.812	-----	-----	-----	-----	-----	-----	-----	2.812
1152	2.437	61.43	-----	2.809	-----	-----	-----	-----	-----	-----	-----	2.809
1153	2.435	61.43	-----	2.807	-----	-----	-----	-----	-----	-----	-----	2.807
1154	2.433	61.43	-----	2.804	-----	-----	-----	-----	-----	-----	-----	2.804

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1155	2.431	61.43	-----	2.802	-----	-----	-----	-----	-----	-----	-----	2.802
1156	2.429	61.43	-----	2.799	-----	-----	-----	-----	-----	-----	-----	2.799
1157	2.427	61.43	-----	2.797	-----	-----	-----	-----	-----	-----	-----	2.797
1158	2.424	61.43	-----	2.794	-----	-----	-----	-----	-----	-----	-----	2.794
1159	2.422	61.43	-----	2.791	-----	-----	-----	-----	-----	-----	-----	2.792
1160	2.420	61.42	-----	2.789	-----	-----	-----	-----	-----	-----	-----	2.789
1161	2.418	61.42	-----	2.786	-----	-----	-----	-----	-----	-----	-----	2.786
1162	2.416	61.42	-----	2.784	-----	-----	-----	-----	-----	-----	-----	2.784
1163	2.414	61.42	-----	2.781	-----	-----	-----	-----	-----	-----	-----	2.781
1164	2.411	61.42	-----	2.779	-----	-----	-----	-----	-----	-----	-----	2.779
1165	2.409	61.42	-----	2.776	-----	-----	-----	-----	-----	-----	-----	2.776
1166	2.407	61.42	-----	2.774	-----	-----	-----	-----	-----	-----	-----	2.774
1167	2.405	61.42	-----	2.771	-----	-----	-----	-----	-----	-----	-----	2.771
1168	2.403	61.42	-----	2.769	-----	-----	-----	-----	-----	-----	-----	2.769
1169	2.400	61.42	-----	2.766	-----	-----	-----	-----	-----	-----	-----	2.766
1170	2.398	61.42	-----	2.764	-----	-----	-----	-----	-----	-----	-----	2.764
1171	2.396	61.42	-----	2.761	-----	-----	-----	-----	-----	-----	-----	2.761
1172	2.394	61.42	-----	2.759	-----	-----	-----	-----	-----	-----	-----	2.759
1173	2.392	61.42	-----	2.756	-----	-----	-----	-----	-----	-----	-----	2.756
1174	2.389	61.42	-----	2.754	-----	-----	-----	-----	-----	-----	-----	2.754
1175	2.387	61.42	-----	2.751	-----	-----	-----	-----	-----	-----	-----	2.751
1176	2.385	61.42	-----	2.748	-----	-----	-----	-----	-----	-----	-----	2.748
1177	2.383	61.42	-----	2.746	-----	-----	-----	-----	-----	-----	-----	2.746
1178	2.381	61.42	-----	2.743	-----	-----	-----	-----	-----	-----	-----	2.743
1179	2.379	61.42	-----	2.741	-----	-----	-----	-----	-----	-----	-----	2.741
1180	2.376	61.42	-----	2.738	-----	-----	-----	-----	-----	-----	-----	2.738
1181	2.374	61.42	-----	2.736	-----	-----	-----	-----	-----	-----	-----	2.736
1182	2.372	61.42	-----	2.733	-----	-----	-----	-----	-----	-----	-----	2.733
1183	2.370	61.41	-----	2.731	-----	-----	-----	-----	-----	-----	-----	2.731
1184	2.368	61.41	-----	2.728	-----	-----	-----	-----	-----	-----	-----	2.728
1185	2.365	61.41	-----	2.726	-----	-----	-----	-----	-----	-----	-----	2.726
1186	2.363	61.41	-----	2.723	-----	-----	-----	-----	-----	-----	-----	2.723
1187	2.361	61.41	-----	2.721	-----	-----	-----	-----	-----	-----	-----	2.721
1188	2.359	61.41	-----	2.719	-----	-----	-----	-----	-----	-----	-----	2.719
1189	2.357	61.41	-----	2.716	-----	-----	-----	-----	-----	-----	-----	2.716
1190	2.354	61.41	-----	2.714	-----	-----	-----	-----	-----	-----	-----	2.714
1191	2.352	61.41	-----	2.711	-----	-----	-----	-----	-----	-----	-----	2.711
1192	2.350	61.41	-----	2.709	-----	-----	-----	-----	-----	-----	-----	2.709
1193	2.348	61.41	-----	2.706	-----	-----	-----	-----	-----	-----	-----	2.706
1194	2.346	61.41	-----	2.704	-----	-----	-----	-----	-----	-----	-----	2.704
1195	2.343	61.41	-----	2.701	-----	-----	-----	-----	-----	-----	-----	2.701
1196	2.341	61.41	-----	2.699	-----	-----	-----	-----	-----	-----	-----	2.699
1197	2.339	61.41	-----	2.696	-----	-----	-----	-----	-----	-----	-----	2.696
1198	2.337	61.41	-----	2.694	-----	-----	-----	-----	-----	-----	-----	2.694
1199	2.335	61.41	-----	2.691	-----	-----	-----	-----	-----	-----	-----	2.691
1200	2.332	61.41	-----	2.689	-----	-----	-----	-----	-----	-----	-----	2.689
1201	2.330	61.41	-----	2.686	-----	-----	-----	-----	-----	-----	-----	2.686
1202	2.328	61.41	-----	2.684	-----	-----	-----	-----	-----	-----	-----	2.684
1203	2.326	61.41	-----	2.681	-----	-----	-----	-----	-----	-----	-----	2.681
1204	2.324	61.41	-----	2.679	-----	-----	-----	-----	-----	-----	-----	2.679
1205	2.321	61.41	-----	2.677	-----	-----	-----	-----	-----	-----	-----	2.677
1206	2.319	61.41	-----	2.674	-----	-----	-----	-----	-----	-----	-----	2.674
1207	2.317	61.40	-----	2.672	-----	-----	-----	-----	-----	-----	-----	2.672
1208	2.315	61.40	-----	2.669	-----	-----	-----	-----	-----	-----	-----	2.669
1209	2.313	61.40	-----	2.667	-----	-----	-----	-----	-----	-----	-----	2.667
1210	2.310	61.40	-----	2.664	-----	-----	-----	-----	-----	-----	-----	2.664

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1211	2.308	61.40	-----	2.662	-----	-----	-----	-----	-----	-----	-----	2.662
1212	2.306	61.40	-----	2.659	-----	-----	-----	-----	-----	-----	-----	2.659
1213	2.304	61.40	-----	2.657	-----	-----	-----	-----	-----	-----	-----	2.657
1214	2.302	61.40	-----	2.655	-----	-----	-----	-----	-----	-----	-----	2.655
1215	2.299	61.40	-----	2.652	-----	-----	-----	-----	-----	-----	-----	2.652
1216	2.297	61.40	-----	2.650	-----	-----	-----	-----	-----	-----	-----	2.650
1217	2.295	61.40	-----	2.647	-----	-----	-----	-----	-----	-----	-----	2.647
1218	2.293	61.40	-----	2.645	-----	-----	-----	-----	-----	-----	-----	2.645
1219	2.291	61.40	-----	2.642	-----	-----	-----	-----	-----	-----	-----	2.642
1220	2.288	61.40	-----	2.639	-----	-----	-----	-----	-----	-----	-----	2.639
1221	2.286	61.40	-----	2.636	-----	-----	-----	-----	-----	-----	-----	2.636
1222	2.284	61.40	-----	2.633	-----	-----	-----	-----	-----	-----	-----	2.633
1223	2.282	61.40	-----	2.630	-----	-----	-----	-----	-----	-----	-----	2.630
1224	2.280	61.40	-----	2.627	-----	-----	-----	-----	-----	-----	-----	2.627
1225	2.277	61.40	-----	2.624	-----	-----	-----	-----	-----	-----	-----	2.624
1226	2.275	61.40	-----	2.620	-----	-----	-----	-----	-----	-----	-----	2.620
1227	2.273	61.40	-----	2.617	-----	-----	-----	-----	-----	-----	-----	2.617
1228	2.271	61.40	-----	2.614	-----	-----	-----	-----	-----	-----	-----	2.614
1229	2.269	61.40	-----	2.611	-----	-----	-----	-----	-----	-----	-----	2.611
1230	2.266	61.40	-----	2.608	-----	-----	-----	-----	-----	-----	-----	2.608
1231	2.264	61.40	-----	2.605	-----	-----	-----	-----	-----	-----	-----	2.605
1232	2.262	61.39	-----	2.602	-----	-----	-----	-----	-----	-----	-----	2.602
1233	2.260	61.39	-----	2.599	-----	-----	-----	-----	-----	-----	-----	2.599
1234	2.257	61.39	-----	2.596	-----	-----	-----	-----	-----	-----	-----	2.596
1235	2.255	61.39	-----	2.593	-----	-----	-----	-----	-----	-----	-----	2.593
1236	2.253	61.39	-----	2.590	-----	-----	-----	-----	-----	-----	-----	2.590
1237	2.251	61.39	-----	2.587	-----	-----	-----	-----	-----	-----	-----	2.587
1238	2.249	61.39	-----	2.584	-----	-----	-----	-----	-----	-----	-----	2.584
1239	2.246	61.39	-----	2.581	-----	-----	-----	-----	-----	-----	-----	2.581
1240	2.244	61.39	-----	2.578	-----	-----	-----	-----	-----	-----	-----	2.578
1241	2.242	61.39	-----	2.575	-----	-----	-----	-----	-----	-----	-----	2.575
1242	2.240	61.39	-----	2.572	-----	-----	-----	-----	-----	-----	-----	2.572
1243	2.238	61.39	-----	2.569	-----	-----	-----	-----	-----	-----	-----	2.569
1244	2.235	61.39	-----	2.566	-----	-----	-----	-----	-----	-----	-----	2.566
1245	2.233	61.39	-----	2.563	-----	-----	-----	-----	-----	-----	-----	2.563
1246	2.231	61.39	-----	2.560	-----	-----	-----	-----	-----	-----	-----	2.560
1247	2.229	61.39	-----	2.557	-----	-----	-----	-----	-----	-----	-----	2.557
1248	2.226	61.39	-----	2.554	-----	-----	-----	-----	-----	-----	-----	2.554
1249	2.224	61.39	-----	2.551	-----	-----	-----	-----	-----	-----	-----	2.551
1250	2.222	61.39	-----	2.548	-----	-----	-----	-----	-----	-----	-----	2.548
1251	2.220	61.39	-----	2.545	-----	-----	-----	-----	-----	-----	-----	2.545
1252	2.218	61.39	-----	2.542	-----	-----	-----	-----	-----	-----	-----	2.542
1253	2.215	61.39	-----	2.539	-----	-----	-----	-----	-----	-----	-----	2.539
1254	2.213	61.39	-----	2.536	-----	-----	-----	-----	-----	-----	-----	2.536
1255	2.211	61.39	-----	2.533	-----	-----	-----	-----	-----	-----	-----	2.533
1256	2.209	61.39	-----	2.531	-----	-----	-----	-----	-----	-----	-----	2.530
1257	2.206	61.39	-----	2.528	-----	-----	-----	-----	-----	-----	-----	2.528
1258	2.204	61.38	-----	2.525	-----	-----	-----	-----	-----	-----	-----	2.525
1259	2.202	61.38	-----	2.522	-----	-----	-----	-----	-----	-----	-----	2.522
1260	2.200	61.38	-----	2.519	-----	-----	-----	-----	-----	-----	-----	2.519
1261	2.198	61.38	-----	2.516	-----	-----	-----	-----	-----	-----	-----	2.516
1262	2.195	61.38	-----	2.513	-----	-----	-----	-----	-----	-----	-----	2.513
1263	2.193	61.38	-----	2.510	-----	-----	-----	-----	-----	-----	-----	2.510
1264	2.191	61.38	-----	2.508	-----	-----	-----	-----	-----	-----	-----	2.507
1265	2.189	61.38	-----	2.505	-----	-----	-----	-----	-----	-----	-----	2.505
1266	2.186	61.38	-----	2.502	-----	-----	-----	-----	-----	-----	-----	2.502

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1267	2.184	61.38	-----	2.499	-----	-----	-----	-----	-----	-----	-----	2.499
1268	2.182	61.38	-----	2.496	-----	-----	-----	-----	-----	-----	-----	2.496
1269	2.180	61.38	-----	2.493	-----	-----	-----	-----	-----	-----	-----	2.493
1270	2.178	61.38	-----	2.491	-----	-----	-----	-----	-----	-----	-----	2.490
1271	2.175	61.38	-----	2.488	-----	-----	-----	-----	-----	-----	-----	2.488
1272	2.173	61.38	-----	2.485	-----	-----	-----	-----	-----	-----	-----	2.485
1273	2.171	61.38	-----	2.482	-----	-----	-----	-----	-----	-----	-----	2.482
1274	2.169	61.38	-----	2.479	-----	-----	-----	-----	-----	-----	-----	2.479
1275	2.166	61.38	-----	2.476	-----	-----	-----	-----	-----	-----	-----	2.476
1276	2.164	61.38	-----	2.474	-----	-----	-----	-----	-----	-----	-----	2.474
1277	2.162	61.38	-----	2.471	-----	-----	-----	-----	-----	-----	-----	2.471
1278	2.160	61.38	-----	2.468	-----	-----	-----	-----	-----	-----	-----	2.468
1279	2.157	61.38	-----	2.465	-----	-----	-----	-----	-----	-----	-----	2.465
1280	2.155	61.38	-----	2.463	-----	-----	-----	-----	-----	-----	-----	2.463
1281	2.153	61.38	-----	2.460	-----	-----	-----	-----	-----	-----	-----	2.460
1282	2.151	61.38	-----	2.457	-----	-----	-----	-----	-----	-----	-----	2.457
1283	2.149	61.38	-----	2.454	-----	-----	-----	-----	-----	-----	-----	2.454
1284	2.146	61.38	-----	2.452	-----	-----	-----	-----	-----	-----	-----	2.452
1285	2.144	61.38	-----	2.449	-----	-----	-----	-----	-----	-----	-----	2.449
1286	2.142	61.37	-----	2.446	-----	-----	-----	-----	-----	-----	-----	2.446
1287	2.140	61.37	-----	2.443	-----	-----	-----	-----	-----	-----	-----	2.443
1288	2.137	61.37	-----	2.441	-----	-----	-----	-----	-----	-----	-----	2.441
1289	2.135	61.37	-----	2.438	-----	-----	-----	-----	-----	-----	-----	2.438
1290	2.133	61.37	-----	2.435	-----	-----	-----	-----	-----	-----	-----	2.435
1291	2.131	61.37	-----	2.432	-----	-----	-----	-----	-----	-----	-----	2.432
1292	2.128	61.37	-----	2.430	-----	-----	-----	-----	-----	-----	-----	2.430
1293	2.126	61.37	-----	2.427	-----	-----	-----	-----	-----	-----	-----	2.427
1294	2.124	61.37	-----	2.424	-----	-----	-----	-----	-----	-----	-----	2.424
1295	2.122	61.37	-----	2.422	-----	-----	-----	-----	-----	-----	-----	2.422
1296	2.120	61.37	-----	2.419	-----	-----	-----	-----	-----	-----	-----	2.419
1297	2.117	61.37	-----	2.416	-----	-----	-----	-----	-----	-----	-----	2.416
1298	2.115	61.37	-----	2.413	-----	-----	-----	-----	-----	-----	-----	2.413
1299	2.113	61.37	-----	2.411	-----	-----	-----	-----	-----	-----	-----	2.411
1300	2.111	61.37	-----	2.408	-----	-----	-----	-----	-----	-----	-----	2.408
1301	2.108	61.37	-----	2.405	-----	-----	-----	-----	-----	-----	-----	2.405
1302	2.106	61.37	-----	2.403	-----	-----	-----	-----	-----	-----	-----	2.403
1303	2.104	61.37	-----	2.400	-----	-----	-----	-----	-----	-----	-----	2.400
1304	2.102	61.37	-----	2.397	-----	-----	-----	-----	-----	-----	-----	2.397
1305	2.099	61.37	-----	2.395	-----	-----	-----	-----	-----	-----	-----	2.395
1306	2.097	61.37	-----	2.392	-----	-----	-----	-----	-----	-----	-----	2.392
1307	2.095	61.37	-----	2.389	-----	-----	-----	-----	-----	-----	-----	2.389
1308	2.093	61.37	-----	2.387	-----	-----	-----	-----	-----	-----	-----	2.387
1309	2.090	61.37	-----	2.384	-----	-----	-----	-----	-----	-----	-----	2.384
1310	2.088	61.37	-----	2.382	-----	-----	-----	-----	-----	-----	-----	2.382
1311	2.086	61.37	-----	2.379	-----	-----	-----	-----	-----	-----	-----	2.379
1312	2.084	61.37	-----	2.376	-----	-----	-----	-----	-----	-----	-----	2.376
1313	2.081	61.37	-----	2.374	-----	-----	-----	-----	-----	-----	-----	2.374
1314	2.079	61.36	-----	2.371	-----	-----	-----	-----	-----	-----	-----	2.371
1315	2.077	61.36	-----	2.368	-----	-----	-----	-----	-----	-----	-----	2.368
1316	2.075	61.36	-----	2.366	-----	-----	-----	-----	-----	-----	-----	2.366
1317	2.072	61.36	-----	2.363	-----	-----	-----	-----	-----	-----	-----	2.363
1318	2.070	61.36	-----	2.360	-----	-----	-----	-----	-----	-----	-----	2.360
1319	2.068	61.36	-----	2.358	-----	-----	-----	-----	-----	-----	-----	2.358
1320	2.066	61.36	-----	2.355	-----	-----	-----	-----	-----	-----	-----	2.355
1321	2.063	61.36	-----	2.353	-----	-----	-----	-----	-----	-----	-----	2.353
1322	2.061	61.36	-----	2.350	-----	-----	-----	-----	-----	-----	-----	2.350

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1323	2.059	61.36	-----	2.347	-----	-----	-----	-----	-----	-----	-----	2.347
1324	2.057	61.36	-----	2.345	-----	-----	-----	-----	-----	-----	-----	2.345
1325	2.055	61.36	-----	2.342	-----	-----	-----	-----	-----	-----	-----	2.342
1326	2.052	61.36	-----	2.340	-----	-----	-----	-----	-----	-----	-----	2.340
1327	2.050	61.36	-----	2.337	-----	-----	-----	-----	-----	-----	-----	2.337
1328	2.048	61.36	-----	2.335	-----	-----	-----	-----	-----	-----	-----	2.335
1329	2.046	61.36	-----	2.332	-----	-----	-----	-----	-----	-----	-----	2.332
1330	2.043	61.36	-----	2.329	-----	-----	-----	-----	-----	-----	-----	2.329
1331	2.041	61.36	-----	2.327	-----	-----	-----	-----	-----	-----	-----	2.327
1332	2.039	61.36	-----	2.324	-----	-----	-----	-----	-----	-----	-----	2.324
1333	2.037	61.36	-----	2.322	-----	-----	-----	-----	-----	-----	-----	2.322
1334	2.034	61.36	-----	2.319	-----	-----	-----	-----	-----	-----	-----	2.319
1335	2.032	61.36	-----	2.316	-----	-----	-----	-----	-----	-----	-----	2.317
1336	2.030	61.36	-----	2.314	-----	-----	-----	-----	-----	-----	-----	2.314
1337	2.028	61.36	-----	2.311	-----	-----	-----	-----	-----	-----	-----	2.311
1338	2.025	61.36	-----	2.309	-----	-----	-----	-----	-----	-----	-----	2.309
1339	2.023	61.36	-----	2.306	-----	-----	-----	-----	-----	-----	-----	2.306
1340	2.021	61.36	-----	2.304	-----	-----	-----	-----	-----	-----	-----	2.304
1341	2.019	61.36	-----	2.301	-----	-----	-----	-----	-----	-----	-----	2.301
1342	2.016	61.36	-----	2.299	-----	-----	-----	-----	-----	-----	-----	2.299
1343	2.014	61.36	-----	2.296	-----	-----	-----	-----	-----	-----	-----	2.296
1344	2.012	61.35	-----	2.294	-----	-----	-----	-----	-----	-----	-----	2.294
1345	2.010	61.35	-----	2.291	-----	-----	-----	-----	-----	-----	-----	2.291
1346	2.007	61.35	-----	2.288	-----	-----	-----	-----	-----	-----	-----	2.288
1347	2.005	61.35	-----	2.286	-----	-----	-----	-----	-----	-----	-----	2.286
1348	2.003	61.35	-----	2.283	-----	-----	-----	-----	-----	-----	-----	2.283
1349	2.001	61.35	-----	2.281	-----	-----	-----	-----	-----	-----	-----	2.281
1350	1.998	61.35	-----	2.278	-----	-----	-----	-----	-----	-----	-----	2.278
1351	1.996	61.35	-----	2.276	-----	-----	-----	-----	-----	-----	-----	2.276
1352	1.994	61.35	-----	2.273	-----	-----	-----	-----	-----	-----	-----	2.273
1353	1.992	61.35	-----	2.271	-----	-----	-----	-----	-----	-----	-----	2.271
1354	1.989	61.35	-----	2.268	-----	-----	-----	-----	-----	-----	-----	2.268
1355	1.987	61.35	-----	2.266	-----	-----	-----	-----	-----	-----	-----	2.266
1356	1.985	61.35	-----	2.263	-----	-----	-----	-----	-----	-----	-----	2.263
1357	1.982	61.35	-----	2.261	-----	-----	-----	-----	-----	-----	-----	2.261
1358	1.980	61.35	-----	2.258	-----	-----	-----	-----	-----	-----	-----	2.258
1359	1.978	61.35	-----	2.256	-----	-----	-----	-----	-----	-----	-----	2.256
1360	1.976	61.35	-----	2.253	-----	-----	-----	-----	-----	-----	-----	2.253
1361	1.973	61.35	-----	2.251	-----	-----	-----	-----	-----	-----	-----	2.251
1362	1.971	61.35	-----	2.248	-----	-----	-----	-----	-----	-----	-----	2.248
1363	1.969	61.35	-----	2.246	-----	-----	-----	-----	-----	-----	-----	2.246
1364	1.967	61.35	-----	2.243	-----	-----	-----	-----	-----	-----	-----	2.243
1365	1.964	61.35	-----	2.241	-----	-----	-----	-----	-----	-----	-----	2.241
1366	1.962	61.35	-----	2.238	-----	-----	-----	-----	-----	-----	-----	2.238
1367	1.960	61.35	-----	2.236	-----	-----	-----	-----	-----	-----	-----	2.236
1368	1.958	61.35	-----	2.233	-----	-----	-----	-----	-----	-----	-----	2.233
1369	1.955	61.35	-----	2.231	-----	-----	-----	-----	-----	-----	-----	2.231
1370	1.953	61.35	-----	2.228	-----	-----	-----	-----	-----	-----	-----	2.228
1371	1.951	61.35	-----	2.226	-----	-----	-----	-----	-----	-----	-----	2.226
1372	1.949	61.35	-----	2.223	-----	-----	-----	-----	-----	-----	-----	2.223
1373	1.946	61.35	-----	2.221	-----	-----	-----	-----	-----	-----	-----	2.221
1374	1.944	61.35	-----	2.218	-----	-----	-----	-----	-----	-----	-----	2.218
1375	1.942	61.34	-----	2.216	-----	-----	-----	-----	-----	-----	-----	2.216
1376	1.940	61.34	-----	2.214	-----	-----	-----	-----	-----	-----	-----	2.214
1377	1.937	61.34	-----	2.211	-----	-----	-----	-----	-----	-----	-----	2.211
1378	1.935	61.34	-----	2.209	-----	-----	-----	-----	-----	-----	-----	2.209

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1379	1.933	61.34	-----	2.206	-----	-----	-----	-----	-----	-----	-----	2.206
1380	1.931	61.34	-----	2.204	-----	-----	-----	-----	-----	-----	-----	2.204
1381	1.928	61.34	-----	2.201	-----	-----	-----	-----	-----	-----	-----	2.201
1382	1.926	61.34	-----	2.199	-----	-----	-----	-----	-----	-----	-----	2.199
1383	1.924	61.34	-----	2.196	-----	-----	-----	-----	-----	-----	-----	2.196
1384	1.921	61.34	-----	2.194	-----	-----	-----	-----	-----	-----	-----	2.194
1385	1.919	61.34	-----	2.191	-----	-----	-----	-----	-----	-----	-----	2.191
1386	1.917	61.34	-----	2.189	-----	-----	-----	-----	-----	-----	-----	2.189
1387	1.915	61.34	-----	2.187	-----	-----	-----	-----	-----	-----	-----	2.187
1388	1.912	61.34	-----	2.184	-----	-----	-----	-----	-----	-----	-----	2.184
1389	1.910	61.34	-----	2.182	-----	-----	-----	-----	-----	-----	-----	2.182
1390	1.908	61.34	-----	2.179	-----	-----	-----	-----	-----	-----	-----	2.179
1391	1.906	61.34	-----	2.177	-----	-----	-----	-----	-----	-----	-----	2.177
1392	1.903	61.34	-----	2.174	-----	-----	-----	-----	-----	-----	-----	2.174
1393	1.901	61.34	-----	2.172	-----	-----	-----	-----	-----	-----	-----	2.172
1394	1.899	61.34	-----	2.169	-----	-----	-----	-----	-----	-----	-----	2.169
1395	1.897	61.34	-----	2.167	-----	-----	-----	-----	-----	-----	-----	2.167
1396	1.894	61.34	-----	2.165	-----	-----	-----	-----	-----	-----	-----	2.165
1397	1.892	61.34	-----	2.162	-----	-----	-----	-----	-----	-----	-----	2.162
1398	1.890	61.34	-----	2.160	-----	-----	-----	-----	-----	-----	-----	2.160
1399	1.888	61.34	-----	2.157	-----	-----	-----	-----	-----	-----	-----	2.157
1400	1.885	61.34	-----	2.155	-----	-----	-----	-----	-----	-----	-----	2.155
1401	1.883	61.34	-----	2.152	-----	-----	-----	-----	-----	-----	-----	2.152
1402	1.881	61.34	-----	2.150	-----	-----	-----	-----	-----	-----	-----	2.150
1403	1.878	61.34	-----	2.148	-----	-----	-----	-----	-----	-----	-----	2.148
1404	1.876	61.34	-----	2.145	-----	-----	-----	-----	-----	-----	-----	2.145
1405	1.874	61.34	-----	2.143	-----	-----	-----	-----	-----	-----	-----	2.143
1406	1.872	61.34	-----	2.140	-----	-----	-----	-----	-----	-----	-----	2.140
1407	1.869	61.33	-----	2.138	-----	-----	-----	-----	-----	-----	-----	2.138
1408	1.867	61.33	-----	2.135	-----	-----	-----	-----	-----	-----	-----	2.135
1409	1.865	61.33	-----	2.133	-----	-----	-----	-----	-----	-----	-----	2.133
1410	1.863	61.33	-----	2.131	-----	-----	-----	-----	-----	-----	-----	2.131
1411	1.860	61.33	-----	2.128	-----	-----	-----	-----	-----	-----	-----	2.128
1412	1.858	61.33	-----	2.126	-----	-----	-----	-----	-----	-----	-----	2.126
1413	1.856	61.33	-----	2.123	-----	-----	-----	-----	-----	-----	-----	2.123
1414	1.853	61.33	-----	2.121	-----	-----	-----	-----	-----	-----	-----	2.121
1415	1.851	61.33	-----	2.119	-----	-----	-----	-----	-----	-----	-----	2.119
1416	1.849	61.33	-----	2.116	-----	-----	-----	-----	-----	-----	-----	2.116
1417	1.847	61.33	-----	2.114	-----	-----	-----	-----	-----	-----	-----	2.114
1418	1.844	61.33	-----	2.111	-----	-----	-----	-----	-----	-----	-----	2.111
1419	1.842	61.33	-----	2.109	-----	-----	-----	-----	-----	-----	-----	2.109
1420	1.840	61.33	-----	2.107	-----	-----	-----	-----	-----	-----	-----	2.107
1421	1.838	61.33	-----	2.104	-----	-----	-----	-----	-----	-----	-----	2.104
1422	1.835	61.33	-----	2.102	-----	-----	-----	-----	-----	-----	-----	2.102
1423	1.833	61.33	-----	2.099	-----	-----	-----	-----	-----	-----	-----	2.099
1424	1.831	61.33	-----	2.097	-----	-----	-----	-----	-----	-----	-----	2.097
1425	1.828	61.33	-----	2.095	-----	-----	-----	-----	-----	-----	-----	2.095
1426	1.826	61.33	-----	2.092	-----	-----	-----	-----	-----	-----	-----	2.092
1427	1.824	61.33	-----	2.090	-----	-----	-----	-----	-----	-----	-----	2.090
1428	1.822	61.33	-----	2.087	-----	-----	-----	-----	-----	-----	-----	2.087
1429	1.819	61.33	-----	2.085	-----	-----	-----	-----	-----	-----	-----	2.085
1430	1.817	61.33	-----	2.083	-----	-----	-----	-----	-----	-----	-----	2.083
1431	1.815	61.33	-----	2.080	-----	-----	-----	-----	-----	-----	-----	2.080
1432	1.813	61.33	-----	2.078	-----	-----	-----	-----	-----	-----	-----	2.078
1433	1.810	61.33	-----	2.075	-----	-----	-----	-----	-----	-----	-----	2.075
1434	1.808	61.33	-----	2.073	-----	-----	-----	-----	-----	-----	-----	2.073

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1435	1.806	61.33	-----	2.071	-----	-----	-----	-----	-----	-----	-----	2.071
1436	1.803	61.33	-----	2.068	-----	-----	-----	-----	-----	-----	-----	2.068
1437	1.801	61.33	-----	2.066	-----	-----	-----	-----	-----	-----	-----	2.066
1438	1.799	61.33	-----	2.063	-----	-----	-----	-----	-----	-----	-----	2.063
1439	1.797	61.32	-----	2.061	-----	-----	-----	-----	-----	-----	-----	2.061
1440	1.794	61.32	-----	2.059	-----	-----	-----	-----	-----	-----	-----	2.059
1441	1.790	61.32	-----	2.056	-----	-----	-----	-----	-----	-----	-----	2.056
1442	1.783	61.32	-----	2.054	-----	-----	-----	-----	-----	-----	-----	2.054
1443	1.773	61.32	-----	2.051	-----	-----	-----	-----	-----	-----	-----	2.051
1444	1.761	61.32	-----	2.049	-----	-----	-----	-----	-----	-----	-----	2.049
1445	1.747	61.32	-----	2.046	-----	-----	-----	-----	-----	-----	-----	2.046
1446	1.730	61.32	-----	2.043	-----	-----	-----	-----	-----	-----	-----	2.043
1447	1.711	61.32	-----	2.041	-----	-----	-----	-----	-----	-----	-----	2.041
1448	1.689	61.32	-----	2.038	-----	-----	-----	-----	-----	-----	-----	2.038
1449	1.665	61.32	-----	2.034	-----	-----	-----	-----	-----	-----	-----	2.034
1450	1.639	61.32	-----	2.031	-----	-----	-----	-----	-----	-----	-----	2.031
1451	1.610	61.32	-----	2.027	-----	-----	-----	-----	-----	-----	-----	2.027
1452	1.579	61.32	-----	2.023	-----	-----	-----	-----	-----	-----	-----	2.023
1453	1.546	61.32	-----	2.019	-----	-----	-----	-----	-----	-----	-----	2.019
1454	1.510	61.32	-----	2.015	-----	-----	-----	-----	-----	-----	-----	2.015
1455	1.472	61.32	-----	2.010	-----	-----	-----	-----	-----	-----	-----	2.010
1456	1.431	61.32	-----	2.005	-----	-----	-----	-----	-----	-----	-----	2.005
1457	1.388	61.32	-----	2.000	-----	-----	-----	-----	-----	-----	-----	2.000
1458	1.343	61.32	-----	1.994	-----	-----	-----	-----	-----	-----	-----	1.994
1459	1.295	61.32	-----	1.988	-----	-----	-----	-----	-----	-----	-----	1.988
1460	1.245	61.31	-----	1.982	-----	-----	-----	-----	-----	-----	-----	1.982
1461	1.193	61.31	-----	1.975	-----	-----	-----	-----	-----	-----	-----	1.975
1462	1.142	61.31	-----	1.968	-----	-----	-----	-----	-----	-----	-----	1.968
1463	1.091	61.31	-----	1.960	-----	-----	-----	-----	-----	-----	-----	1.960
1464	1.042	61.31	-----	1.952	-----	-----	-----	-----	-----	-----	-----	1.952
1465	0.995	61.31	-----	1.944	-----	-----	-----	-----	-----	-----	-----	1.944
1466	0.948	61.31	-----	1.935	-----	-----	-----	-----	-----	-----	-----	1.935
1467	0.902	61.31	-----	1.926	-----	-----	-----	-----	-----	-----	-----	1.926
1468	0.858	61.31	-----	1.916	-----	-----	-----	-----	-----	-----	-----	1.916
1469	0.815	61.30	-----	1.907	-----	-----	-----	-----	-----	-----	-----	1.907
1470	0.773	61.30	-----	1.897	-----	-----	-----	-----	-----	-----	-----	1.897
1471	0.732	61.30	-----	1.886	-----	-----	-----	-----	-----	-----	-----	1.886
1472	0.692	61.30	-----	1.876	-----	-----	-----	-----	-----	-----	-----	1.876
1473	0.653	61.30	-----	1.861	-----	-----	-----	-----	-----	-----	-----	1.861
1474	0.616	61.30	-----	1.834	-----	-----	-----	-----	-----	-----	-----	1.834
1475	0.579	61.30	-----	1.808	-----	-----	-----	-----	-----	-----	-----	1.808
1476	0.544	61.30	-----	1.781	-----	-----	-----	-----	-----	-----	-----	1.781
1477	0.510	61.29	-----	1.754	-----	-----	-----	-----	-----	-----	-----	1.754
1478	0.476	61.29	-----	1.727	-----	-----	-----	-----	-----	-----	-----	1.727
1479	0.445	61.29	-----	1.700	-----	-----	-----	-----	-----	-----	-----	1.700
1480	0.414	61.29	-----	1.672	-----	-----	-----	-----	-----	-----	-----	1.672
1481	0.384	61.29	-----	1.645	-----	-----	-----	-----	-----	-----	-----	1.645
1482	0.355	61.29	-----	1.617	-----	-----	-----	-----	-----	-----	-----	1.617
1483	0.328	61.29	-----	1.590	-----	-----	-----	-----	-----	-----	-----	1.590
1484	0.302	61.28	-----	1.563	-----	-----	-----	-----	-----	-----	-----	1.563
1485	0.276	61.28	-----	1.535	-----	-----	-----	-----	-----	-----	-----	1.535
1486	0.252	61.28	-----	1.508	-----	-----	-----	-----	-----	-----	-----	1.508
1487	0.229	61.28	-----	1.481	-----	-----	-----	-----	-----	-----	-----	1.481
1488	0.207	61.28	-----	1.454	-----	-----	-----	-----	-----	-----	-----	1.453
1489	0.186	61.28	-----	1.426	-----	-----	-----	-----	-----	-----	-----	1.426
1490	0.167	61.27	-----	1.400	-----	-----	-----	-----	-----	-----	-----	1.400

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1491	0.148	61.27	-----	1.373	-----	-----	-----	-----	-----	-----	-----	1.373
1492	0.131	61.27	-----	1.346	-----	-----	-----	-----	-----	-----	-----	1.346
1493	0.114	61.27	-----	1.320	-----	-----	-----	-----	-----	-----	-----	1.320
1494	0.099	61.27	-----	1.294	-----	-----	-----	-----	-----	-----	-----	1.294
1495	0.085	61.27	-----	1.268	-----	-----	-----	-----	-----	-----	-----	1.268
1496	0.072	61.27	-----	1.242	-----	-----	-----	-----	-----	-----	-----	1.242
1497	0.060	61.27	-----	1.217	-----	-----	-----	-----	-----	-----	-----	1.217
1498	0.049	61.26	-----	1.192	-----	-----	-----	-----	-----	-----	-----	1.192
1499	0.039	61.26	-----	1.167	-----	-----	-----	-----	-----	-----	-----	1.167
1500	0.030	61.26	-----	1.143	-----	-----	-----	-----	-----	-----	-----	1.143
1501	0.023	61.26	-----	1.119	-----	-----	-----	-----	-----	-----	-----	1.119
1502	0.016	61.26	-----	1.095	-----	-----	-----	-----	-----	-----	-----	1.095
1503	0.011	61.26	-----	1.072	-----	-----	-----	-----	-----	-----	-----	1.072
1504	0.006	61.26	-----	1.049	-----	-----	-----	-----	-----	-----	-----	1.049
1505	0.003	61.25	-----	1.027	-----	-----	-----	-----	-----	-----	-----	1.027
1506	0.001	61.25	-----	1.005	-----	-----	-----	-----	-----	-----	-----	1.005
1507	0.000	61.25	-----	0.983	-----	-----	-----	-----	-----	-----	-----	0.983
1508	0.000	61.25	-----	0.962	-----	-----	-----	-----	-----	-----	-----	0.962
1509	0.000	61.25	-----	0.941	-----	-----	-----	-----	-----	-----	-----	0.941
1510	0.000	61.25	-----	0.921	-----	-----	-----	-----	-----	-----	-----	0.921
1511	0.000	61.25	-----	0.901	-----	-----	-----	-----	-----	-----	-----	0.901
1512	0.000	61.25	-----	0.882	-----	-----	-----	-----	-----	-----	-----	0.882
1513	0.000	61.25	-----	0.863	-----	-----	-----	-----	-----	-----	-----	0.863
1514	0.000	61.25	-----	0.844	-----	-----	-----	-----	-----	-----	-----	0.844
1515	0.000	61.24	-----	0.826	-----	-----	-----	-----	-----	-----	-----	0.826
1516	0.000	61.24	-----	0.808	-----	-----	-----	-----	-----	-----	-----	0.808
1517	0.000	61.24	-----	0.791	-----	-----	-----	-----	-----	-----	-----	0.791
1518	0.000	61.24	-----	0.774	-----	-----	-----	-----	-----	-----	-----	0.774
1519	0.000	61.24	-----	0.757	-----	-----	-----	-----	-----	-----	-----	0.757
1520	0.000	61.24	-----	0.741	-----	-----	-----	-----	-----	-----	-----	0.741
1521	0.000	61.24	-----	0.725	-----	-----	-----	-----	-----	-----	-----	0.725
1522	0.000	61.24	-----	0.710	-----	-----	-----	-----	-----	-----	-----	0.710
1523	0.000	61.24	-----	0.694	-----	-----	-----	-----	-----	-----	-----	0.694
1524	0.000	61.24	-----	0.679	-----	-----	-----	-----	-----	-----	-----	0.679
1525	0.000	61.24	-----	0.665	-----	-----	-----	-----	-----	-----	-----	0.665
1526	0.000	61.23	-----	0.650	-----	-----	-----	-----	-----	-----	-----	0.650
1527	0.000	61.23	-----	0.636	-----	-----	-----	-----	-----	-----	-----	0.636
1528	0.000	61.23	-----	0.623	-----	-----	-----	-----	-----	-----	-----	0.623
1529	0.000	61.23	-----	0.609	-----	-----	-----	-----	-----	-----	-----	0.609
1530	0.000	61.23	-----	0.596	-----	-----	-----	-----	-----	-----	-----	0.596
1531	0.000	61.23	-----	0.583	-----	-----	-----	-----	-----	-----	-----	0.583
1532	0.000	61.23	-----	0.571	-----	-----	-----	-----	-----	-----	-----	0.571
1533	0.000	61.23	-----	0.559	-----	-----	-----	-----	-----	-----	-----	0.559
1534	0.000	61.23	-----	0.547	-----	-----	-----	-----	-----	-----	-----	0.547
1535	0.000	61.23	-----	0.535	-----	-----	-----	-----	-----	-----	-----	0.535
1536	0.000	61.23	-----	0.523	-----	-----	-----	-----	-----	-----	-----	0.523
1537	0.000	61.23	-----	0.512	-----	-----	-----	-----	-----	-----	-----	0.512
1538	0.000	61.23	-----	0.501	-----	-----	-----	-----	-----	-----	-----	0.501
1539	0.000	61.23	-----	0.490	-----	-----	-----	-----	-----	-----	-----	0.490
1540	0.000	61.23	-----	0.480	-----	-----	-----	-----	-----	-----	-----	0.480
1541	0.000	61.23	-----	0.469	-----	-----	-----	-----	-----	-----	-----	0.469
1542	0.000	61.22	-----	0.459	-----	-----	-----	-----	-----	-----	-----	0.459
1543	0.000	61.22	-----	0.449	-----	-----	-----	-----	-----	-----	-----	0.449
1544	0.000	61.22	-----	0.440	-----	-----	-----	-----	-----	-----	-----	0.440
1545	0.000	61.22	-----	0.430	-----	-----	-----	-----	-----	-----	-----	0.430
1546	0.000	61.22	-----	0.421	-----	-----	-----	-----	-----	-----	-----	0.421

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1547	0.000	61.22	-----	0.412	-----	-----	-----	-----	-----	-----	-----	0.412
1548	0.000	61.22	-----	0.403	-----	-----	-----	-----	-----	-----	-----	0.403
1549	0.000	61.22	-----	0.394	-----	-----	-----	-----	-----	-----	-----	0.394
1550	0.000	61.22	-----	0.386	-----	-----	-----	-----	-----	-----	-----	0.386
1551	0.000	61.22	-----	0.378	-----	-----	-----	-----	-----	-----	-----	0.378
1552	0.000	61.22	-----	0.370	-----	-----	-----	-----	-----	-----	-----	0.370
1553	0.000	61.22	-----	0.362	-----	-----	-----	-----	-----	-----	-----	0.362
1554	0.000	61.22	-----	0.354	-----	-----	-----	-----	-----	-----	-----	0.354
1555	0.000	61.22	-----	0.346	-----	-----	-----	-----	-----	-----	-----	0.346
1556	0.000	61.22	-----	0.339	-----	-----	-----	-----	-----	-----	-----	0.339
1557	0.000	61.22	-----	0.331	-----	-----	-----	-----	-----	-----	-----	0.332
1558	0.000	61.22	-----	0.324	-----	-----	-----	-----	-----	-----	-----	0.324
1559	0.000	61.22	-----	0.317	-----	-----	-----	-----	-----	-----	-----	0.317
1560	0.000	61.22	-----	0.311	-----	-----	-----	-----	-----	-----	-----	0.311
1561	0.000	61.22	-----	0.304	-----	-----	-----	-----	-----	-----	-----	0.304
1562	0.000	61.22	-----	0.297	-----	-----	-----	-----	-----	-----	-----	0.297
1563	0.000	61.22	-----	0.291	-----	-----	-----	-----	-----	-----	-----	0.291
1564	0.000	61.22	-----	0.285	-----	-----	-----	-----	-----	-----	-----	0.285
1565	0.000	61.21	-----	0.279	-----	-----	-----	-----	-----	-----	-----	0.279
1566	0.000	61.21	-----	0.273	-----	-----	-----	-----	-----	-----	-----	0.273
1567	0.000	61.21	-----	0.267	-----	-----	-----	-----	-----	-----	-----	0.267
1568	0.000	61.21	-----	0.261	-----	-----	-----	-----	-----	-----	-----	0.261
1569	0.000	61.21	-----	0.255	-----	-----	-----	-----	-----	-----	-----	0.255
1570	0.000	61.21	-----	0.250	-----	-----	-----	-----	-----	-----	-----	0.250
1571	0.000	61.21	-----	0.245	-----	-----	-----	-----	-----	-----	-----	0.245
1572	0.000	61.21	-----	0.239	-----	-----	-----	-----	-----	-----	-----	0.239
1573	0.000	61.21	-----	0.234	-----	-----	-----	-----	-----	-----	-----	0.234
1574	0.000	61.21	-----	0.229	-----	-----	-----	-----	-----	-----	-----	0.229
1575	0.000	61.21	-----	0.224	-----	-----	-----	-----	-----	-----	-----	0.224
1576	0.000	61.21	-----	0.219	-----	-----	-----	-----	-----	-----	-----	0.219
1577	0.000	61.21	-----	0.215	-----	-----	-----	-----	-----	-----	-----	0.215
1578	0.000	61.21	-----	0.210	-----	-----	-----	-----	-----	-----	-----	0.210
1579	0.000	61.21	-----	0.205	-----	-----	-----	-----	-----	-----	-----	0.205
1580	0.000	61.21	-----	0.201	-----	-----	-----	-----	-----	-----	-----	0.201
1581	0.000	61.21	-----	0.197	-----	-----	-----	-----	-----	-----	-----	0.197
1582	0.000	61.21	-----	0.193	-----	-----	-----	-----	-----	-----	-----	0.192
1583	0.000	61.21	-----	0.188	-----	-----	-----	-----	-----	-----	-----	0.188
1584	0.000	61.21	-----	0.184	-----	-----	-----	-----	-----	-----	-----	0.184
1585	0.000	61.21	-----	0.180	-----	-----	-----	-----	-----	-----	-----	0.180
1586	0.000	61.21	-----	0.176	-----	-----	-----	-----	-----	-----	-----	0.176
1587	0.000	61.21	-----	0.173	-----	-----	-----	-----	-----	-----	-----	0.173
1588	0.000	61.21	-----	0.169	-----	-----	-----	-----	-----	-----	-----	0.169
1589	0.000	61.21	-----	0.165	-----	-----	-----	-----	-----	-----	-----	0.165
1590	0.000	61.21	-----	0.162	-----	-----	-----	-----	-----	-----	-----	0.162
1591	0.000	61.21	-----	0.158	-----	-----	-----	-----	-----	-----	-----	0.158
1592	0.000	61.21	-----	0.155	-----	-----	-----	-----	-----	-----	-----	0.155
1593	0.000	61.21	-----	0.152	-----	-----	-----	-----	-----	-----	-----	0.152
1594	0.000	61.21	-----	0.148	-----	-----	-----	-----	-----	-----	-----	0.148
1595	0.000	61.21	-----	0.145	-----	-----	-----	-----	-----	-----	-----	0.145
1596	0.000	61.21	-----	0.142	-----	-----	-----	-----	-----	-----	-----	0.142
1597	0.000	61.21	-----	0.139	-----	-----	-----	-----	-----	-----	-----	0.139
1598	0.000	61.21	-----	0.136	-----	-----	-----	-----	-----	-----	-----	0.136
1599	0.000	61.21	-----	0.133	-----	-----	-----	-----	-----	-----	-----	0.133
1600	0.000	61.21	-----	0.130	-----	-----	-----	-----	-----	-----	-----	0.130
1601	0.000	61.21	-----	0.127	-----	-----	-----	-----	-----	-----	-----	0.127
1602	0.000	61.21	-----	0.125	-----	-----	-----	-----	-----	-----	-----	0.125

Continues on next page...

Detention pond outflow

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1603	0.000	61.21	-----	0.122	-----	-----	-----	-----	-----	-----	-----	0.122
1604	0.000	61.21	-----	0.119	-----	-----	-----	-----	-----	-----	-----	0.119
1605	0.000	61.21	-----	0.117	-----	-----	-----	-----	-----	-----	-----	0.117
1606	0.000	61.21	-----	0.114	-----	-----	-----	-----	-----	-----	-----	0.114
1607	0.000	61.21	-----	0.112	-----	-----	-----	-----	-----	-----	-----	0.112
1608	0.000	61.21	-----	0.109	-----	-----	-----	-----	-----	-----	-----	0.109
1609	0.000	61.21	-----	0.107	-----	-----	-----	-----	-----	-----	-----	0.107
1610	0.000	61.21	-----	0.105	-----	-----	-----	-----	-----	-----	-----	0.105
1611	0.000	61.21	-----	0.102	-----	-----	-----	-----	-----	-----	-----	0.102
1612	0.000	61.21	-----	0.100	-----	-----	-----	-----	-----	-----	-----	0.100
1613	0.000	61.21	-----	0.098	-----	-----	-----	-----	-----	-----	-----	0.098
1614	0.000	61.21	-----	0.096	-----	-----	-----	-----	-----	-----	-----	0.096
1615	0.000	61.21	-----	0.094	-----	-----	-----	-----	-----	-----	-----	0.094
1616	0.000	61.20	-----	0.092	-----	-----	-----	-----	-----	-----	-----	0.092
1617	0.000	61.20	-----	0.090	-----	-----	-----	-----	-----	-----	-----	0.090
1618	0.000	61.20	-----	0.088	-----	-----	-----	-----	-----	-----	-----	0.088
1619	0.000	61.20	-----	0.086	-----	-----	-----	-----	-----	-----	-----	0.086
1620	0.000	61.20	-----	0.084	-----	-----	-----	-----	-----	-----	-----	0.084
1621	0.000	61.20	-----	0.082	-----	-----	-----	-----	-----	-----	-----	0.082
1622	0.000	61.20	-----	0.081	-----	-----	-----	-----	-----	-----	-----	0.081
1623	0.000	61.20	-----	0.079	-----	-----	-----	-----	-----	-----	-----	0.079
1624	0.000	61.20	-----	0.077	-----	-----	-----	-----	-----	-----	-----	0.077
1625	0.000	61.20	-----	0.076	-----	-----	-----	-----	-----	-----	-----	0.076
1626	0.000	61.20	-----	0.074	-----	-----	-----	-----	-----	-----	-----	0.074
1627	0.000	61.20	-----	0.072	-----	-----	-----	-----	-----	-----	-----	0.072
1628	0.000	61.20	-----	0.071	-----	-----	-----	-----	-----	-----	-----	0.071
1629	0.000	61.20	-----	0.069	-----	-----	-----	-----	-----	-----	-----	0.069
1630	0.000	61.20	-----	0.068	-----	-----	-----	-----	-----	-----	-----	0.068
1631	0.000	61.20	-----	0.066	-----	-----	-----	-----	-----	-----	-----	0.066
1632	0.000	61.20	-----	0.065	-----	-----	-----	-----	-----	-----	-----	0.065
1633	0.000	61.20	-----	0.064	-----	-----	-----	-----	-----	-----	-----	0.064
1634	0.000	61.20	-----	0.062	-----	-----	-----	-----	-----	-----	-----	0.062
1635	0.000	61.20	-----	0.061	-----	-----	-----	-----	-----	-----	-----	0.061
1636	0.000	61.20	-----	0.060	-----	-----	-----	-----	-----	-----	-----	0.060
1637	0.000	61.20	-----	0.058	-----	-----	-----	-----	-----	-----	-----	0.058
1638	0.000	61.20	-----	0.057	-----	-----	-----	-----	-----	-----	-----	0.057
1639	0.000	61.20	-----	0.056	-----	-----	-----	-----	-----	-----	-----	0.056
1640	0.000	61.20	-----	0.055	-----	-----	-----	-----	-----	-----	-----	0.055
1641	0.000	61.20	-----	0.053	-----	-----	-----	-----	-----	-----	-----	0.053
1642	0.000	61.20	-----	0.052	-----	-----	-----	-----	-----	-----	-----	0.052
1643	0.000	61.20	-----	0.051	-----	-----	-----	-----	-----	-----	-----	0.051
1644	0.000	61.20	-----	0.050	-----	-----	-----	-----	-----	-----	-----	0.050
1645	0.000	61.20	-----	0.049	-----	-----	-----	-----	-----	-----	-----	0.049
1646	0.000	61.20	-----	0.048	-----	-----	-----	-----	-----	-----	-----	0.048
1647	0.000	61.20	-----	0.047	-----	-----	-----	-----	-----	-----	-----	0.047
1648	0.000	61.20	-----	0.046	-----	-----	-----	-----	-----	-----	-----	0.046
1649	0.000	61.20	-----	0.045	-----	-----	-----	-----	-----	-----	-----	0.045

...End

Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Hyd. No. 1

Developed site storm event

Hydrograph type	= SCS Runoff	Peak discharge	= 23.03 cfs
Storm frequency	= 100 yrs	Time to peak	= 495 min
Time interval	= 1 min	Hyd. volume	= 397,003 cuft
Drainage area	= 25.500 ac	Curve number	= 91
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 34.0 min
Total precip.	= 5.30 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 400

Hydrograph Discharge Table

(Printed values >= 1.00% of Qp.)

Time -- Outflow (min cfs)		Time -- Outflow (min cfs)		Time -- Outflow (min cfs)		Time -- Outflow (min cfs)	
133	0.243	172	0.955	211	1.536	250	2.213
134	0.258	173	0.972	212	1.549	251	2.232
135	0.274	174	0.990	213	1.564	252	2.250
136	0.290	175	1.007	214	1.578	253	2.268
137	0.306	176	1.024	215	1.592	254	2.286
138	0.323	177	1.041	216	1.607	255	2.304
139	0.340	178	1.057	217	1.622	256	2.322
140	0.358	179	1.074	218	1.637	257	2.340
141	0.375	180	1.090	219	1.653	258	2.357
142	0.393	181	1.107	220	1.668	259	2.375
143	0.411	182	1.123	221	1.684	260	2.392
144	0.429	183	1.139	222	1.700	261	2.409
145	0.448	184	1.155	223	1.717	262	2.427
146	0.467	185	1.170	224	1.733	263	2.444
147	0.485	186	1.186	225	1.750	264	2.461
148	0.504	187	1.201	226	1.767	265	2.478
149	0.523	188	1.216	227	1.784	266	2.495
150	0.543	189	1.231	228	1.802	267	2.512
151	0.562	190	1.246	229	1.820	268	2.529
152	0.581	191	1.260	230	1.838	269	2.547
153	0.600	192	1.275	231	1.856	270	2.564
154	0.620	193	1.289	232	1.874	271	2.581
155	0.639	194	1.304	233	1.893	272	2.598
156	0.659	195	1.318	234	1.912	273	2.616
157	0.678	196	1.332	235	1.930	274	2.633
158	0.697	197	1.345	236	1.949	275	2.650
159	0.716	198	1.359	237	1.968	276	2.668
160	0.736	199	1.373	238	1.987	277	2.685
161	0.755	200	1.386	239	2.006	278	2.703
162	0.774	201	1.400	240	2.025	279	2.720
163	0.792	202	1.413	241	2.044	280	2.738
164	0.811	203	1.427	242	2.063	281	2.756
165	0.830	204	1.440	243	2.082	282	2.774
166	0.848	205	1.454	244	2.101	283	2.792
167	0.866	206	1.467	245	2.120	284	2.810
168	0.884	207	1.481	246	2.139	285	2.829
169	0.902	208	1.494	247	2.158	286	2.847
170	0.920	209	1.508	248	2.176	287	2.866
171	0.938	210	1.522	249	2.195	288	2.885

Continues on next page...

Hydrograph Discharge Table

Time (min	Outflow cfs)	Time (min	Outflow cfs)	Time (min	Outflow cfs)	Time (min	Outflow cfs)
289	2.904	345	4.277	401	6.079	457	9.168
290	2.923	346	4.302	402	6.104	458	9.426
291	2.943	347	4.326	403	6.127	459	9.707
292	2.962	348	4.349	404	6.149	460	10.01
293	2.982	349	4.373	405	6.170	461	10.34
294	3.002	350	4.397	406	6.190	462	10.69
295	3.022	351	4.420	407	6.208	463	11.06
296	3.043	352	4.444	408	6.226	464	11.45
297	3.064	353	4.468	409	6.242	465	11.87
298	3.084	354	4.492	410	6.258	466	12.31
299	3.105	355	4.516	411	6.273	467	12.77
300	3.127	356	4.541	412	6.287	468	13.25
301	3.148	357	4.565	413	6.302	469	13.76
302	3.170	358	4.590	414	6.318	470	14.28
303	3.193	359	4.616	415	6.334	471	14.83
304	3.215	360	4.642	416	6.351	472	15.37
305	3.238	361	4.668	417	6.368	473	15.91
306	3.261	362	4.694	418	6.387	474	16.45
307	3.285	363	4.722	419	6.407	475	16.97
308	3.309	364	4.750	420	6.427	476	17.49
309	3.333	365	4.779	421	6.449	477	18.00
310	3.357	366	4.809	422	6.472	478	18.50
311	3.382	367	4.840	423	6.497	479	18.98
312	3.407	368	4.871	424	6.522	480	19.46
313	3.432	369	4.904	425	6.550	481	19.90
314	3.458	370	4.937	426	6.578	482	20.33
315	3.484	371	4.971	427	6.609	483	20.72
316	3.510	372	5.005	428	6.641	484	21.08
317	3.536	373	5.041	429	6.675	485	21.42
318	3.562	374	5.077	430	6.711	486	21.73
319	3.589	375	5.114	431	6.750	487	22.00
320	3.616	376	5.152	432	6.790	488	22.24
321	3.643	377	5.190	433	6.833	489	22.45
322	3.671	378	5.230	434	6.878	490	22.63
323	3.698	379	5.269	435	6.926	491	22.78
324	3.725	380	5.310	436	6.976	492	22.89
325	3.753	381	5.351	437	7.028	493	22.97
326	3.780	382	5.392	438	7.083	494	23.01
327	3.808	383	5.434	439	7.141	495	23.03 <<
328	3.835	384	5.475	440	7.201	496	23.00
329	3.863	385	5.516	441	7.265	497	22.95
330	3.890	386	5.557	442	7.331	498	22.86
331	3.917	387	5.598	443	7.400	499	22.74
332	3.945	388	5.638	444	7.472	500	22.59
333	3.971	389	5.679	445	7.547	501	22.40
334	3.998	390	5.718	446	7.625	502	22.20
335	4.025	391	5.758	447	7.705	503	21.98
336	4.051	392	5.796	448	7.790	504	21.75
337	4.077	393	5.832	449	7.877	505	21.50
338	4.103	394	5.868	450	7.967	506	21.25
339	4.128	395	5.902	451	8.076	507	20.97
340	4.154	396	5.935	452	8.206	508	20.69
341	4.179	397	5.966	453	8.355	509	20.39
342	4.204	398	5.996	454	8.526	510	20.09
343	4.229	399	6.025	455	8.718	511	19.78
344	4.253	400	6.053	456	8.932	512	19.46

Continues on next page...

Hydrograph Discharge Table

Time (min	Outflow cfs)	Time (min	Outflow cfs)	Time (min	Outflow cfs)	Time (min	Outflow cfs)
513	19.13	569	8.680	625	6.622	681	5.780
514	18.80	570	8.608	626	6.599	682	5.766
515	18.47	571	8.534	627	6.577	683	5.752
516	18.13	572	8.462	628	6.555	684	5.737
517	17.78	573	8.391	629	6.533	685	5.723
518	17.43	574	8.320	630	6.511	686	5.708
519	17.09	575	8.251	631	6.490	687	5.694
520	16.75	576	8.184	632	6.469	688	5.679
521	16.42	577	8.117	633	6.449	689	5.664
522	16.09	578	8.051	634	6.429	690	5.648
523	15.77	579	7.988	635	6.410	691	5.633
524	15.46	580	7.928	636	6.391	692	5.617
525	15.16	581	7.869	637	6.373	693	5.601
526	14.87	582	7.813	638	6.355	694	5.584
527	14.58	583	7.759	639	6.336	695	5.567
528	14.31	584	7.707	640	6.318	696	5.550
529	14.04	585	7.656	641	6.301	697	5.533
530	13.78	586	7.608	642	6.284	698	5.516
531	13.54	587	7.562	643	6.267	699	5.498
532	13.30	588	7.517	644	6.252	700	5.480
533	13.07	589	7.475	645	6.237	701	5.463
534	12.84	590	7.434	646	6.222	702	5.445
535	12.62	591	7.395	647	6.208	703	5.427
536	12.41	592	7.361	648	6.194	704	5.409
537	12.21	593	7.329	649	6.181	705	5.391
538	12.02	594	7.298	650	6.168	706	5.373
539	11.84	595	7.268	651	6.156	707	5.355
540	11.66	596	7.238	652	6.144	708	5.337
541	11.49	597	7.210	653	6.132	709	5.319
542	11.33	598	7.182	654	6.119	710	5.301
543	11.18	599	7.155	655	6.107	711	5.283
544	11.03	600	7.129	656	6.095	712	5.265
545	10.90	601	7.107	657	6.083	713	5.247
546	10.77	602	7.085	658	6.070	714	5.230
547	10.65	603	7.064	659	6.058	715	5.213
548	10.54	604	7.043	660	6.045	716	5.197
549	10.43	605	7.023	661	6.033	717	5.180
550	10.32	606	7.003	662	6.020	718	5.164
551	10.22	607	6.983	663	6.008	719	5.149
552	10.11	608	6.964	664	5.995	720	5.134
553	10.01	609	6.943	665	5.982	721	5.119
554	9.918	610	6.924	666	5.970	722	5.104
555	9.823	611	6.904	667	5.957	723	5.090
556	9.730	612	6.885	668	5.944	724	5.076
557	9.639	613	6.865	669	5.932	725	5.063
558	9.550	614	6.846	670	5.920	726	5.050
559	9.462	615	6.827	671	5.908	727	5.038
560	9.376	616	6.808	672	5.896	728	5.026
561	9.291	617	6.789	673	5.884	729	5.014
562	9.210	618	6.770	674	5.872	730	5.003
563	9.131	619	6.751	675	5.859	731	4.993
564	9.053	620	6.732	676	5.846	732	4.983
565	8.977	621	6.713	677	5.833	733	4.973
566	8.901	622	6.690	678	5.820	734	4.964
567	8.826	623	6.667	679	5.807	735	4.956
568	8.753	624	6.644	680	5.793	736	4.948

Continues on next page...

Hydrograph Discharge Table

Time (min	Outflow cfs)	Time (min	Outflow cfs)	Time (min	Outflow cfs)	Time (min	Outflow cfs)
737	4.941	793	4.756	849	4.484	905	4.333
738	4.934	794	4.753	850	4.479	906	4.330
739	4.927	795	4.751	851	4.474	907	4.327
740	4.922	796	4.749	852	4.470	908	4.324
741	4.917	797	4.747	853	4.466	909	4.321
742	4.912	798	4.745	854	4.461	910	4.318
743	4.908	799	4.743	855	4.458	911	4.315
744	4.905	800	4.742	856	4.454	912	4.312
745	4.902	801	4.740	857	4.451	913	4.309
746	4.900	802	4.739	858	4.448	914	4.306
747	4.898	803	4.737	859	4.445	915	4.302
748	4.897	804	4.734	860	4.442	916	4.299
749	4.897	805	4.731	861	4.439	917	4.296
750	4.897	806	4.728	862	4.437	918	4.293
751	4.897	807	4.725	863	4.434	919	4.290
752	4.898	808	4.721	864	4.432	920	4.287
753	4.898	809	4.717	865	4.429	921	4.284
754	4.899	810	4.713	866	4.427	922	4.281
755	4.899	811	4.708	867	4.425	923	4.278
756	4.900	812	4.704	868	4.423	924	4.275
757	4.900	813	4.699	869	4.420	925	4.271
758	4.901	814	4.695	870	4.418	926	4.268
759	4.901	815	4.690	871	4.416	927	4.265
760	4.900	816	4.685	872	4.414	928	4.262
761	4.900	817	4.680	873	4.412	929	4.259
762	4.899	818	4.675	874	4.410	930	4.256
763	4.897	819	4.670	875	4.408	931	4.253
764	4.895	820	4.665	876	4.405	932	4.250
765	4.893	821	4.660	877	4.403	933	4.247
766	4.890	822	4.654	878	4.401	934	4.243
767	4.887	823	4.648	879	4.399	935	4.240
768	4.883	824	4.643	880	4.397	936	4.237
769	4.878	825	4.637	881	4.395	937	4.234
770	4.873	826	4.630	882	4.393	938	4.231
771	4.867	827	4.624	883	4.390	939	4.228
772	4.861	828	4.618	884	4.388	940	4.225
773	4.855	829	4.612	885	4.386	941	4.222
774	4.848	830	4.605	886	4.384	942	4.219
775	4.842	831	4.599	887	4.381	943	4.215
776	4.836	832	4.592	888	4.379	944	4.212
777	4.829	833	4.585	889	4.377	945	4.209
778	4.823	834	4.579	890	4.374	946	4.206
779	4.816	835	4.572	891	4.372	947	4.203
780	4.810	836	4.565	892	4.369	948	4.200
781	4.804	837	4.559	893	4.367	949	4.197
782	4.798	838	4.552	894	4.364	950	4.194
783	4.793	839	4.545	895	4.361	951	4.191
784	4.788	840	4.539	896	4.359	952	4.187
785	4.783	841	4.532	897	4.356	953	4.184
786	4.779	842	4.526	898	4.353	954	4.181
787	4.775	843	4.519	899	4.351	955	4.178
788	4.771	844	4.513	900	4.348	956	4.175
789	4.767	845	4.507	901	4.345	957	4.172
790	4.764	846	4.501	902	4.342	958	4.169
791	4.761	847	4.495	903	4.339	959	4.165
792	4.758	848	4.490	904	4.336	960	4.162

Continues on next page...

Hydrograph Discharge Table

Time (min)	Outflow (cfs)	Time (min)	Outflow (cfs)	Time (min)	Outflow (cfs)	Time (min)	Outflow (cfs)
961	4.159	1017	3.983	1073	3.804	1129	3.624
962	4.156	1018	3.979	1074	3.801	1130	3.620
963	4.153	1019	3.976	1075	3.798	1131	3.617
964	4.150	1020	3.973	1076	3.794	1132	3.614
965	4.147	1021	3.970	1077	3.791	1133	3.611
966	4.144	1022	3.967	1078	3.788	1134	3.607
967	4.140	1023	3.964	1079	3.785	1135	3.604
968	4.137	1024	3.960	1080	3.782	1136	3.601
969	4.134	1025	3.957	1081	3.778	1137	3.598
970	4.131	1026	3.954	1082	3.775	1138	3.594
971	4.128	1027	3.951	1083	3.772	1139	3.591
972	4.125	1028	3.948	1084	3.769	1140	3.588
973	4.122	1029	3.945	1085	3.765	1141	3.585
974	4.118	1030	3.941	1086	3.762	1142	3.582
975	4.115	1031	3.938	1087	3.759	1143	3.578
976	4.112	1032	3.935	1088	3.756	1144	3.575
977	4.109	1033	3.932	1089	3.753	1145	3.572
978	4.106	1034	3.929	1090	3.749	1146	3.569
979	4.103	1035	3.925	1091	3.746	1147	3.565
980	4.100	1036	3.922	1092	3.743	1148	3.562
981	4.096	1037	3.919	1093	3.740	1149	3.559
982	4.093	1038	3.916	1094	3.737	1150	3.556
983	4.090	1039	3.913	1095	3.733	1151	3.552
984	4.087	1040	3.910	1096	3.730	1152	3.549
985	4.084	1041	3.906	1097	3.727	1153	3.546
986	4.081	1042	3.903	1098	3.724	1154	3.543
987	4.078	1043	3.900	1099	3.720	1155	3.539
988	4.074	1044	3.897	1100	3.717	1156	3.536
989	4.071	1045	3.894	1101	3.714	1157	3.533
990	4.068	1046	3.890	1102	3.711	1158	3.530
991	4.065	1047	3.887	1103	3.708	1159	3.526
992	4.062	1048	3.884	1104	3.704	1160	3.523
993	4.059	1049	3.881	1105	3.701	1161	3.520
994	4.055	1050	3.878	1106	3.698	1162	3.517
995	4.052	1051	3.874	1107	3.695	1163	3.513
996	4.049	1052	3.871	1108	3.691	1164	3.510
997	4.046	1053	3.868	1109	3.688	1165	3.507
998	4.043	1054	3.865	1110	3.685	1166	3.504
999	4.040	1055	3.862	1111	3.682	1167	3.500
1000	4.036	1056	3.858	1112	3.679	1168	3.497
1001	4.033	1057	3.855	1113	3.675	1169	3.494
1002	4.030	1058	3.852	1114	3.672	1170	3.491
1003	4.027	1059	3.849	1115	3.669	1171	3.487
1004	4.024	1060	3.846	1116	3.666	1172	3.484
1005	4.021	1061	3.842	1117	3.662	1173	3.481
1006	4.018	1062	3.839	1118	3.659	1174	3.478
1007	4.014	1063	3.836	1119	3.656	1175	3.474
1008	4.011	1064	3.833	1120	3.653	1176	3.471
1009	4.008	1065	3.830	1121	3.649	1177	3.468
1010	4.005	1066	3.826	1122	3.646	1178	3.465
1011	4.002	1067	3.823	1123	3.643	1179	3.461
1012	3.999	1068	3.820	1124	3.640	1180	3.458
1013	3.995	1069	3.817	1125	3.637	1181	3.455
1014	3.992	1070	3.814	1126	3.633	1182	3.452
1015	3.989	1071	3.810	1127	3.630	1183	3.448
1016	3.986	1072	3.807	1128	3.627	1184	3.445

Continues on next page...

Hydrograph Discharge Table

Time (min)	Outflow (cfs)	Time (min)	Outflow (cfs)	Time (min)	Outflow (cfs)	Time (min)	Outflow (cfs)
1185	3.442	1241	3.259	1297	3.075	1353	2.889
1186	3.439	1242	3.255	1298	3.071	1354	2.886
1187	3.435	1243	3.252	1299	3.068	1355	2.883
1188	3.432	1244	3.249	1300	3.065	1356	2.880
1189	3.429	1245	3.246	1301	3.061	1357	2.876
1190	3.425	1246	3.242	1302	3.058	1358	2.873
1191	3.422	1247	3.239	1303	3.055	1359	2.870
1192	3.419	1248	3.236	1304	3.051	1360	2.866
1193	3.416	1249	3.232	1305	3.048	1361	2.863
1194	3.412	1250	3.229	1306	3.045	1362	2.860
1195	3.409	1251	3.226	1307	3.042	1363	2.856
1196	3.406	1252	3.223	1308	3.038	1364	2.853
1197	3.403	1253	3.219	1309	3.035	1365	2.850
1198	3.399	1254	3.216	1310	3.032	1366	2.846
1199	3.396	1255	3.213	1311	3.028	1367	2.843
1200	3.393	1256	3.209	1312	3.025	1368	2.840
1201	3.390	1257	3.206	1313	3.022	1369	2.836
1202	3.386	1258	3.203	1314	3.018	1370	2.833
1203	3.383	1259	3.200	1315	3.015	1371	2.830
1204	3.380	1260	3.196	1316	3.012	1372	2.827
1205	3.377	1261	3.193	1317	3.009	1373	2.823
1206	3.373	1262	3.190	1318	3.005	1374	2.820
1207	3.370	1263	3.186	1319	3.002	1375	2.817
1208	3.367	1264	3.183	1320	2.999	1376	2.813
1209	3.363	1265	3.180	1321	2.995	1377	2.810
1210	3.360	1266	3.177	1322	2.992	1378	2.807
1211	3.357	1267	3.173	1323	2.989	1379	2.803
1212	3.354	1268	3.170	1324	2.985	1380	2.800
1213	3.350	1269	3.167	1325	2.982	1381	2.797
1214	3.347	1270	3.163	1326	2.979	1382	2.793
1215	3.344	1271	3.160	1327	2.975	1383	2.790
1216	3.341	1272	3.157	1328	2.972	1384	2.787
1217	3.337	1273	3.154	1329	2.969	1385	2.783
1218	3.334	1274	3.150	1330	2.966	1386	2.780
1219	3.331	1275	3.147	1331	2.962	1387	2.777
1220	3.327	1276	3.144	1332	2.959	1388	2.773
1221	3.324	1277	3.140	1333	2.956	1389	2.770
1222	3.321	1278	3.137	1334	2.952	1390	2.767
1223	3.318	1279	3.134	1335	2.949	1391	2.763
1224	3.314	1280	3.131	1336	2.946	1392	2.760
1225	3.311	1281	3.127	1337	2.942	1393	2.757
1226	3.308	1282	3.124	1338	2.939	1394	2.753
1227	3.305	1283	3.121	1339	2.936	1395	2.750
1228	3.301	1284	3.117	1340	2.933	1396	2.747
1229	3.298	1285	3.114	1341	2.929	1397	2.744
1230	3.295	1286	3.111	1342	2.926	1398	2.740
1231	3.291	1287	3.107	1343	2.923	1399	2.737
1232	3.288	1288	3.104	1344	2.919	1400	2.734
1233	3.285	1289	3.101	1345	2.916	1401	2.730
1234	3.282	1290	3.098	1346	2.913	1402	2.727
1235	3.278	1291	3.094	1347	2.909	1403	2.724
1236	3.275	1292	3.091	1348	2.906	1404	2.720
1237	3.272	1293	3.088	1349	2.903	1405	2.717
1238	3.269	1294	3.084	1350	2.899	1406	2.714
1239	3.265	1295	3.081	1351	2.896	1407	2.710
1240	3.262	1296	3.078	1352	2.893	1408	2.707

Continues on next page...

Developed site storm event

Hydrograph Discharge Table

Time (min	Outflow cfs)	Time (min	Outflow cfs)
1409	2.704	1465	1.441
1410	2.700	1466	1.374
1411	2.697	1467	1.308
1412	2.694	1468	1.243
1413	2.690	1469	1.181
1414	2.687	1470	1.120
1415	2.684	1471	1.060
1416	2.680	1472	1.002
1417	2.677	1473	0.946
1418	2.674	1474	0.892
1419	2.670	1475	0.839
1420	2.667	1476	0.788
1421	2.664	1477	0.738
1422	2.660	1478	0.690
1423	2.657	1479	0.644
1424	2.654	1480	0.599
1425	2.650	1481	0.556
1426	2.647	1482	0.515
1427	2.644	1483	0.475
1428	2.640	1484	0.437
1429	2.637	1485	0.400
1430	2.634	1486	0.365
1431	2.630	1487	0.332
1432	2.627	1488	0.300
1433	2.624	1489	0.270
1434	2.620	1490	0.242
1435	2.617		
1436	2.614	*...End*	
1437	2.610		
1438	2.607		
1439	2.604		
1440	2.600		
1441	2.594		
1442	2.583		
1443	2.570		
1444	2.552		
1445	2.531		
1446	2.507		
1447	2.479		
1448	2.448		
1449	2.413		
1450	2.375		
1451	2.334		
1452	2.289		
1453	2.240		
1454	2.188		
1455	2.133		
1456	2.074		
1457	2.012		
1458	1.946		
1459	1.877		
1460	1.804		
1461	1.728		
1462	1.654		
1463	1.581		
1464	1.511		

Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Hyd. No. 2

Detention pond outflow

Hydrograph type	= Reservoir	Peak discharge	= 6.938 cfs
Storm frequency	= 100 yrs	Time to peak	= 609 min
Time interval	= 1 min	Hyd. volume	= 335,290 cuft
Inflow hyd. No.	= 1 - Developed site storm event	Reservoir name	= Detention Pond
Max. Elevation	= 62.58 ft	Max. Storage	= 136,207 cuft

Storage Indication method used.

Hydrograph Discharge Table

(Printed values >= 1.00% of Qp.)

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
447	7.705	61.21	-----	0.208	-----	-----	-----	-----	-----	-----	-----	0.208
448	7.790	61.22	-----	0.370	-----	-----	-----	-----	-----	-----	-----	0.370
449	7.877	61.23	-----	0.530	-----	-----	-----	-----	-----	-----	-----	0.530
450	7.967	61.24	-----	0.689	-----	-----	-----	-----	-----	-----	-----	0.689
451	8.076	61.25	-----	0.847	-----	-----	-----	-----	-----	-----	-----	0.847
452	8.206	61.25	-----	1.004	-----	-----	-----	-----	-----	-----	-----	1.004
453	8.355	61.26	-----	1.160	-----	-----	-----	-----	-----	-----	-----	1.160
454	8.526	61.27	-----	1.317	-----	-----	-----	-----	-----	-----	-----	1.317
455	8.718	61.28	-----	1.474	-----	-----	-----	-----	-----	-----	-----	1.474
456	8.932	61.29	-----	1.632	-----	-----	-----	-----	-----	-----	-----	1.632
457	9.168	61.30	-----	1.792	-----	-----	-----	-----	-----	-----	-----	1.792
458	9.426	61.30	-----	1.904	-----	-----	-----	-----	-----	-----	-----	1.904
459	9.707	61.31	-----	1.972	-----	-----	-----	-----	-----	-----	-----	1.972
460	10.01	61.32	-----	2.043	-----	-----	-----	-----	-----	-----	-----	2.043
461	10.34	61.33	-----	2.116	-----	-----	-----	-----	-----	-----	-----	2.116
462	10.69	61.34	-----	2.191	-----	-----	-----	-----	-----	-----	-----	2.191
463	11.06	61.35	-----	2.269	-----	-----	-----	-----	-----	-----	-----	2.269
464	11.45	61.36	-----	2.350	-----	-----	-----	-----	-----	-----	-----	2.350
465	11.87	61.37	-----	2.433	-----	-----	-----	-----	-----	-----	-----	2.433
466	12.31	61.38	-----	2.520	-----	-----	-----	-----	-----	-----	-----	2.520
467	12.77	61.40	-----	2.609	-----	-----	-----	-----	-----	-----	-----	2.609
468	13.25	61.41	-----	2.689	-----	-----	-----	-----	-----	-----	-----	2.689
469	13.76	61.42	-----	2.763	-----	-----	-----	-----	-----	-----	-----	2.763
470	14.28	61.43	-----	2.841	-----	-----	-----	-----	-----	-----	-----	2.841
471	14.83	61.45	-----	2.921	-----	-----	-----	-----	-----	-----	-----	2.921
472	15.37	61.46	-----	3.005	-----	-----	-----	-----	-----	-----	-----	3.005
473	15.91	61.48	-----	3.092	-----	-----	-----	-----	-----	-----	-----	3.092
474	16.45	61.49	-----	3.182	-----	-----	-----	-----	-----	-----	-----	3.182
475	16.97	61.51	-----	3.269	-----	-----	-----	-----	-----	-----	-----	3.269
476	17.49	61.52	-----	3.350	-----	-----	-----	-----	-----	-----	-----	3.350
477	18.00	61.54	-----	3.434	-----	-----	-----	-----	-----	-----	-----	3.434
478	18.50	61.56	-----	3.520	-----	-----	-----	-----	-----	-----	-----	3.520
479	18.98	61.57	-----	3.609	-----	-----	-----	-----	-----	-----	-----	3.609
480	19.46	61.59	-----	3.699	-----	-----	-----	-----	-----	-----	-----	3.699
481	19.90	61.61	-----	3.785	-----	-----	-----	-----	-----	-----	-----	3.785
482	20.33	61.63	-----	3.869	-----	-----	-----	-----	-----	-----	-----	3.869
483	20.72	61.65	-----	3.954	-----	-----	-----	-----	-----	-----	-----	3.954
484	21.08	61.67	-----	4.041	-----	-----	-----	-----	-----	-----	-----	4.041
485	21.42	61.69	-----	4.129	-----	-----	-----	-----	-----	-----	-----	4.129
486	21.73	61.71	-----	4.215	-----	-----	-----	-----	-----	-----	-----	4.215
487	22.00	61.73	-----	4.296	-----	-----	-----	-----	-----	-----	-----	4.296
488	22.24	61.75	-----	4.379	-----	-----	-----	-----	-----	-----	-----	4.379

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
489	22.45	61.77	-----	4.462	-----	-----	-----	-----	-----	-----	-----	4.462
490	22.63	61.79	-----	4.546	-----	-----	-----	-----	-----	-----	-----	4.546
491	22.78	61.81	-----	4.626	-----	-----	-----	-----	-----	-----	-----	4.626
492	22.89	61.83	-----	4.703	-----	-----	-----	-----	-----	-----	-----	4.703
493	22.97	61.86	-----	4.781	-----	-----	-----	-----	-----	-----	-----	4.781
494	23.01	61.88	-----	4.858	-----	-----	-----	-----	-----	-----	-----	4.858
495	23.03 <<	61.90	-----	4.936	-----	-----	-----	-----	-----	-----	-----	4.936
496	23.00	61.92	-----	5.008	-----	-----	-----	-----	-----	-----	-----	5.008
497	22.95	61.94	-----	5.079	-----	-----	-----	-----	-----	-----	-----	5.079
498	22.86	61.96	-----	5.150	-----	-----	-----	-----	-----	-----	-----	5.150
499	22.74	61.98	-----	5.220	-----	-----	-----	-----	-----	-----	-----	5.220
500	22.59	62.00	-----	5.288	-----	-----	-----	-----	-----	-----	-----	5.288
501	22.40	62.02	-----	5.346	-----	-----	-----	-----	-----	-----	-----	5.346
502	22.20	62.04	-----	5.402	-----	-----	-----	-----	-----	-----	-----	5.402
503	21.98	62.05	-----	5.458	-----	-----	-----	-----	-----	-----	-----	5.458
504	21.75	62.07	-----	5.513	-----	-----	-----	-----	-----	-----	-----	5.513
505	21.50	62.09	-----	5.567	-----	-----	-----	-----	-----	-----	-----	5.567
506	21.25	62.10	-----	5.619	-----	-----	-----	-----	-----	-----	-----	5.619
507	20.97	62.12	-----	5.668	-----	-----	-----	-----	-----	-----	-----	5.668
508	20.69	62.14	-----	5.716	-----	-----	-----	-----	-----	-----	-----	5.716
509	20.39	62.15	-----	5.763	-----	-----	-----	-----	-----	-----	-----	5.763
510	20.09	62.17	-----	5.809	-----	-----	-----	-----	-----	-----	-----	5.809
511	19.78	62.18	-----	5.854	-----	-----	-----	-----	-----	-----	-----	5.854
512	19.46	62.20	-----	5.897	-----	-----	-----	-----	-----	-----	-----	5.897
513	19.13	62.21	-----	5.938	-----	-----	-----	-----	-----	-----	-----	5.938
514	18.80	62.22	-----	5.977	-----	-----	-----	-----	-----	-----	-----	5.977
515	18.47	62.24	-----	6.015	-----	-----	-----	-----	-----	-----	-----	6.015
516	18.13	62.25	-----	6.052	-----	-----	-----	-----	-----	-----	-----	6.052
517	17.78	62.26	-----	6.088	-----	-----	-----	-----	-----	-----	-----	6.088
518	17.43	62.27	-----	6.123	-----	-----	-----	-----	-----	-----	-----	6.123
519	17.09	62.29	-----	6.156	-----	-----	-----	-----	-----	-----	-----	6.156
520	16.75	62.30	-----	6.189	-----	-----	-----	-----	-----	-----	-----	6.189
521	16.42	62.31	-----	6.219	-----	-----	-----	-----	-----	-----	-----	6.219
522	16.09	62.32	-----	6.248	-----	-----	-----	-----	-----	-----	-----	6.248
523	15.77	62.33	-----	6.276	-----	-----	-----	-----	-----	-----	-----	6.276
524	15.46	62.34	-----	6.303	-----	-----	-----	-----	-----	-----	-----	6.303
525	15.16	62.35	-----	6.328	-----	-----	-----	-----	-----	-----	-----	6.328
526	14.87	62.36	-----	6.353	-----	-----	-----	-----	-----	-----	-----	6.353
527	14.58	62.37	-----	6.378	-----	-----	-----	-----	-----	-----	-----	6.378
528	14.31	62.37	-----	6.401	-----	-----	-----	-----	-----	-----	-----	6.401
529	14.04	62.38	-----	6.423	-----	-----	-----	-----	-----	-----	-----	6.423
530	13.78	62.39	-----	6.445	-----	-----	-----	-----	-----	-----	-----	6.445
531	13.54	62.40	-----	6.465	-----	-----	-----	-----	-----	-----	-----	6.465
532	13.30	62.40	-----	6.485	-----	-----	-----	-----	-----	-----	-----	6.485
533	13.07	62.41	-----	6.503	-----	-----	-----	-----	-----	-----	-----	6.503
534	12.84	62.42	-----	6.521	-----	-----	-----	-----	-----	-----	-----	6.521
535	12.62	62.43	-----	6.538	-----	-----	-----	-----	-----	-----	-----	6.538
536	12.41	62.43	-----	6.555	-----	-----	-----	-----	-----	-----	-----	6.555
537	12.21	62.44	-----	6.571	-----	-----	-----	-----	-----	-----	-----	6.571
538	12.02	62.44	-----	6.586	-----	-----	-----	-----	-----	-----	-----	6.586
539	11.84	62.45	-----	6.601	-----	-----	-----	-----	-----	-----	-----	6.601
540	11.66	62.45	-----	6.615	-----	-----	-----	-----	-----	-----	-----	6.615
541	11.49	62.46	-----	6.629	-----	-----	-----	-----	-----	-----	-----	6.629
542	11.33	62.46	-----	6.642	-----	-----	-----	-----	-----	-----	-----	6.642
543	11.18	62.47	-----	6.655	-----	-----	-----	-----	-----	-----	-----	6.655
544	11.03	62.47	-----	6.667	-----	-----	-----	-----	-----	-----	-----	6.667

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
545	10.90	62.48	-----	6.679	-----	-----	-----	-----	-----	-----	-----	6.679
546	10.77	62.48	-----	6.690	-----	-----	-----	-----	-----	-----	-----	6.690
547	10.65	62.49	-----	6.701	-----	-----	-----	-----	-----	-----	-----	6.701
548	10.54	62.49	-----	6.712	-----	-----	-----	-----	-----	-----	-----	6.712
549	10.43	62.49	-----	6.722	-----	-----	-----	-----	-----	-----	-----	6.722
550	10.32	62.50	-----	6.732	-----	-----	-----	-----	-----	-----	-----	6.732
551	10.22	62.50	-----	6.742	-----	-----	-----	-----	-----	-----	-----	6.742
552	10.11	62.51	-----	6.751	-----	-----	-----	-----	-----	-----	-----	6.751
553	10.01	62.51	-----	6.760	-----	-----	-----	-----	-----	-----	-----	6.760
554	9.918	62.51	-----	6.768	-----	-----	-----	-----	-----	-----	-----	6.768
555	9.823	62.52	-----	6.777	-----	-----	-----	-----	-----	-----	-----	6.777
556	9.730	62.52	-----	6.785	-----	-----	-----	-----	-----	-----	-----	6.785
557	9.639	62.52	-----	6.792	-----	-----	-----	-----	-----	-----	-----	6.792
558	9.550	62.52	-----	6.800	-----	-----	-----	-----	-----	-----	-----	6.800
559	9.462	62.53	-----	6.807	-----	-----	-----	-----	-----	-----	-----	6.807
560	9.376	62.53	-----	6.814	-----	-----	-----	-----	-----	-----	-----	6.814
561	9.291	62.53	-----	6.820	-----	-----	-----	-----	-----	-----	-----	6.820
562	9.210	62.54	-----	6.827	-----	-----	-----	-----	-----	-----	-----	6.827
563	9.131	62.54	-----	6.833	-----	-----	-----	-----	-----	-----	-----	6.833
564	9.053	62.54	-----	6.839	-----	-----	-----	-----	-----	-----	-----	6.839
565	8.977	62.54	-----	6.845	-----	-----	-----	-----	-----	-----	-----	6.845
566	8.901	62.54	-----	6.851	-----	-----	-----	-----	-----	-----	-----	6.851
567	8.826	62.55	-----	6.856	-----	-----	-----	-----	-----	-----	-----	6.856
568	8.753	62.55	-----	6.861	-----	-----	-----	-----	-----	-----	-----	6.861
569	8.680	62.55	-----	6.866	-----	-----	-----	-----	-----	-----	-----	6.866
570	8.608	62.55	-----	6.871	-----	-----	-----	-----	-----	-----	-----	6.871
571	8.534	62.55	-----	6.875	-----	-----	-----	-----	-----	-----	-----	6.875
572	8.462	62.56	-----	6.879	-----	-----	-----	-----	-----	-----	-----	6.879
573	8.391	62.56	-----	6.884	-----	-----	-----	-----	-----	-----	-----	6.884
574	8.320	62.56	-----	6.887	-----	-----	-----	-----	-----	-----	-----	6.887
575	8.251	62.56	-----	6.891	-----	-----	-----	-----	-----	-----	-----	6.891
576	8.184	62.56	-----	6.895	-----	-----	-----	-----	-----	-----	-----	6.895
577	8.117	62.56	-----	6.898	-----	-----	-----	-----	-----	-----	-----	6.898
578	8.051	62.56	-----	6.901	-----	-----	-----	-----	-----	-----	-----	6.901
579	7.988	62.57	-----	6.904	-----	-----	-----	-----	-----	-----	-----	6.904
580	7.928	62.57	-----	6.907	-----	-----	-----	-----	-----	-----	-----	6.907
581	7.869	62.57	-----	6.910	-----	-----	-----	-----	-----	-----	-----	6.910
582	7.813	62.57	-----	6.912	-----	-----	-----	-----	-----	-----	-----	6.912
583	7.759	62.57	-----	6.914	-----	-----	-----	-----	-----	-----	-----	6.914
584	7.707	62.57	-----	6.917	-----	-----	-----	-----	-----	-----	-----	6.917
585	7.656	62.57	-----	6.919	-----	-----	-----	-----	-----	-----	-----	6.919
586	7.608	62.57	-----	6.920	-----	-----	-----	-----	-----	-----	-----	6.920
587	7.562	62.57	-----	6.922	-----	-----	-----	-----	-----	-----	-----	6.922
588	7.517	62.57	-----	6.924	-----	-----	-----	-----	-----	-----	-----	6.924
589	7.475	62.57	-----	6.925	-----	-----	-----	-----	-----	-----	-----	6.925
590	7.434	62.57	-----	6.927	-----	-----	-----	-----	-----	-----	-----	6.927
591	7.395	62.58	-----	6.928	-----	-----	-----	-----	-----	-----	-----	6.928
592	7.361	62.58	-----	6.929	-----	-----	-----	-----	-----	-----	-----	6.929
593	7.329	62.58	-----	6.930	-----	-----	-----	-----	-----	-----	-----	6.930
594	7.298	62.58	-----	6.931	-----	-----	-----	-----	-----	-----	-----	6.931
595	7.268	62.58	-----	6.932	-----	-----	-----	-----	-----	-----	-----	6.932
596	7.238	62.58	-----	6.933	-----	-----	-----	-----	-----	-----	-----	6.933
597	7.210	62.58	-----	6.934	-----	-----	-----	-----	-----	-----	-----	6.934
598	7.182	62.58	-----	6.935	-----	-----	-----	-----	-----	-----	-----	6.935
599	7.155	62.58	-----	6.935	-----	-----	-----	-----	-----	-----	-----	6.935
600	7.129	62.58	-----	6.936	-----	-----	-----	-----	-----	-----	-----	6.936

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
601	7.107	62.58	-----	6.936	-----	-----	-----	-----	-----	-----	-----	6.936
602	7.085	62.58	-----	6.937	-----	-----	-----	-----	-----	-----	-----	6.937
603	7.064	62.58	-----	6.937	-----	-----	-----	-----	-----	-----	-----	6.937
604	7.043	62.58	-----	6.937	-----	-----	-----	-----	-----	-----	-----	6.937
605	7.023	62.58	-----	6.938	-----	-----	-----	-----	-----	-----	-----	6.938
606	7.003	62.58	-----	6.938	-----	-----	-----	-----	-----	-----	-----	6.938
607	6.983	62.58	-----	6.938	-----	-----	-----	-----	-----	-----	-----	6.938
608	6.964	62.58	-----	6.938	-----	-----	-----	-----	-----	-----	-----	6.938
609	6.943	62.58 <<	-----	6.938	-----	-----	-----	-----	-----	-----	-----	6.938 <<
610	6.924	62.58	-----	6.938	-----	-----	-----	-----	-----	-----	-----	6.938
611	6.904	62.58	-----	6.938	-----	-----	-----	-----	-----	-----	-----	6.938
612	6.885	62.58	-----	6.938	-----	-----	-----	-----	-----	-----	-----	6.938
613	6.865	62.58	-----	6.938	-----	-----	-----	-----	-----	-----	-----	6.938
614	6.846	62.58	-----	6.938	-----	-----	-----	-----	-----	-----	-----	6.938
615	6.827	62.58	-----	6.937	-----	-----	-----	-----	-----	-----	-----	6.937
616	6.808	62.58	-----	6.937	-----	-----	-----	-----	-----	-----	-----	6.937
617	6.789	62.58	-----	6.937	-----	-----	-----	-----	-----	-----	-----	6.937
618	6.770	62.58	-----	6.936	-----	-----	-----	-----	-----	-----	-----	6.936
619	6.751	62.58	-----	6.936	-----	-----	-----	-----	-----	-----	-----	6.936
620	6.732	62.58	-----	6.935	-----	-----	-----	-----	-----	-----	-----	6.935
621	6.713	62.58	-----	6.935	-----	-----	-----	-----	-----	-----	-----	6.935
622	6.690	62.58	-----	6.934	-----	-----	-----	-----	-----	-----	-----	6.934
623	6.667	62.58	-----	6.933	-----	-----	-----	-----	-----	-----	-----	6.933
624	6.644	62.58	-----	6.933	-----	-----	-----	-----	-----	-----	-----	6.933
625	6.622	62.58	-----	6.932	-----	-----	-----	-----	-----	-----	-----	6.932
626	6.599	62.58	-----	6.931	-----	-----	-----	-----	-----	-----	-----	6.931
627	6.577	62.58	-----	6.930	-----	-----	-----	-----	-----	-----	-----	6.930
628	6.555	62.58	-----	6.929	-----	-----	-----	-----	-----	-----	-----	6.929
629	6.533	62.58	-----	6.928	-----	-----	-----	-----	-----	-----	-----	6.928
630	6.511	62.57	-----	6.927	-----	-----	-----	-----	-----	-----	-----	6.927
631	6.490	62.57	-----	6.926	-----	-----	-----	-----	-----	-----	-----	6.926
632	6.469	62.57	-----	6.925	-----	-----	-----	-----	-----	-----	-----	6.925
633	6.449	62.57	-----	6.923	-----	-----	-----	-----	-----	-----	-----	6.923
634	6.429	62.57	-----	6.922	-----	-----	-----	-----	-----	-----	-----	6.922
635	6.410	62.57	-----	6.921	-----	-----	-----	-----	-----	-----	-----	6.921
636	6.391	62.57	-----	6.919	-----	-----	-----	-----	-----	-----	-----	6.919
637	6.373	62.57	-----	6.918	-----	-----	-----	-----	-----	-----	-----	6.918
638	6.355	62.57	-----	6.917	-----	-----	-----	-----	-----	-----	-----	6.917
639	6.336	62.57	-----	6.915	-----	-----	-----	-----	-----	-----	-----	6.915
640	6.318	62.57	-----	6.913	-----	-----	-----	-----	-----	-----	-----	6.913
641	6.301	62.57	-----	6.912	-----	-----	-----	-----	-----	-----	-----	6.912
642	6.284	62.57	-----	6.910	-----	-----	-----	-----	-----	-----	-----	6.910
643	6.267	62.57	-----	6.909	-----	-----	-----	-----	-----	-----	-----	6.909
644	6.252	62.57	-----	6.907	-----	-----	-----	-----	-----	-----	-----	6.907
645	6.237	62.57	-----	6.905	-----	-----	-----	-----	-----	-----	-----	6.905
646	6.222	62.57	-----	6.903	-----	-----	-----	-----	-----	-----	-----	6.903
647	6.208	62.56	-----	6.901	-----	-----	-----	-----	-----	-----	-----	6.901
648	6.194	62.56	-----	6.900	-----	-----	-----	-----	-----	-----	-----	6.900
649	6.181	62.56	-----	6.898	-----	-----	-----	-----	-----	-----	-----	6.898
650	6.168	62.56	-----	6.896	-----	-----	-----	-----	-----	-----	-----	6.896
651	6.156	62.56	-----	6.894	-----	-----	-----	-----	-----	-----	-----	6.894
652	6.144	62.56	-----	6.892	-----	-----	-----	-----	-----	-----	-----	6.892
653	6.132	62.56	-----	6.890	-----	-----	-----	-----	-----	-----	-----	6.890
654	6.119	62.56	-----	6.888	-----	-----	-----	-----	-----	-----	-----	6.888
655	6.107	62.56	-----	6.886	-----	-----	-----	-----	-----	-----	-----	6.886
656	6.095	62.56	-----	6.884	-----	-----	-----	-----	-----	-----	-----	6.884

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
657	6.083	62.56	-----	6.882	-----	-----	-----	-----	-----	-----	-----	6.882
658	6.070	62.56	-----	6.879	-----	-----	-----	-----	-----	-----	-----	6.879
659	6.058	62.56	-----	6.877	-----	-----	-----	-----	-----	-----	-----	6.877
660	6.045	62.55	-----	6.875	-----	-----	-----	-----	-----	-----	-----	6.875
661	6.033	62.55	-----	6.873	-----	-----	-----	-----	-----	-----	-----	6.873
662	6.020	62.55	-----	6.871	-----	-----	-----	-----	-----	-----	-----	6.871
663	6.008	62.55	-----	6.868	-----	-----	-----	-----	-----	-----	-----	6.868
664	5.995	62.55	-----	6.866	-----	-----	-----	-----	-----	-----	-----	6.866
665	5.982	62.55	-----	6.864	-----	-----	-----	-----	-----	-----	-----	6.864
666	5.970	62.55	-----	6.861	-----	-----	-----	-----	-----	-----	-----	6.861
667	5.957	62.55	-----	6.859	-----	-----	-----	-----	-----	-----	-----	6.859
668	5.944	62.55	-----	6.857	-----	-----	-----	-----	-----	-----	-----	6.857
669	5.932	62.55	-----	6.854	-----	-----	-----	-----	-----	-----	-----	6.854
670	5.920	62.55	-----	6.852	-----	-----	-----	-----	-----	-----	-----	6.852
671	5.908	62.54	-----	6.849	-----	-----	-----	-----	-----	-----	-----	6.849
672	5.896	62.54	-----	6.847	-----	-----	-----	-----	-----	-----	-----	6.847
673	5.884	62.54	-----	6.844	-----	-----	-----	-----	-----	-----	-----	6.844
674	5.872	62.54	-----	6.842	-----	-----	-----	-----	-----	-----	-----	6.842
675	5.859	62.54	-----	6.839	-----	-----	-----	-----	-----	-----	-----	6.839
676	5.846	62.54	-----	6.836	-----	-----	-----	-----	-----	-----	-----	6.836
677	5.833	62.54	-----	6.834	-----	-----	-----	-----	-----	-----	-----	6.834
678	5.820	62.54	-----	6.831	-----	-----	-----	-----	-----	-----	-----	6.831
679	5.807	62.54	-----	6.828	-----	-----	-----	-----	-----	-----	-----	6.828
680	5.793	62.54	-----	6.826	-----	-----	-----	-----	-----	-----	-----	6.826
681	5.780	62.53	-----	6.823	-----	-----	-----	-----	-----	-----	-----	6.823
682	5.766	62.53	-----	6.820	-----	-----	-----	-----	-----	-----	-----	6.820
683	5.752	62.53	-----	6.817	-----	-----	-----	-----	-----	-----	-----	6.817
684	5.737	62.53	-----	6.814	-----	-----	-----	-----	-----	-----	-----	6.814
685	5.723	62.53	-----	6.811	-----	-----	-----	-----	-----	-----	-----	6.811
686	5.708	62.53	-----	6.809	-----	-----	-----	-----	-----	-----	-----	6.809
687	5.694	62.53	-----	6.806	-----	-----	-----	-----	-----	-----	-----	6.806
688	5.679	62.53	-----	6.803	-----	-----	-----	-----	-----	-----	-----	6.803
689	5.664	62.52	-----	6.800	-----	-----	-----	-----	-----	-----	-----	6.800
690	5.648	62.52	-----	6.797	-----	-----	-----	-----	-----	-----	-----	6.797
691	5.633	62.52	-----	6.794	-----	-----	-----	-----	-----	-----	-----	6.794
692	5.617	62.52	-----	6.790	-----	-----	-----	-----	-----	-----	-----	6.790
693	5.601	62.52	-----	6.787	-----	-----	-----	-----	-----	-----	-----	6.787
694	5.584	62.52	-----	6.784	-----	-----	-----	-----	-----	-----	-----	6.784
695	5.567	62.52	-----	6.781	-----	-----	-----	-----	-----	-----	-----	6.781
696	5.550	62.52	-----	6.778	-----	-----	-----	-----	-----	-----	-----	6.778
697	5.533	62.51	-----	6.774	-----	-----	-----	-----	-----	-----	-----	6.774
698	5.516	62.51	-----	6.771	-----	-----	-----	-----	-----	-----	-----	6.771
699	5.498	62.51	-----	6.768	-----	-----	-----	-----	-----	-----	-----	6.768
700	5.480	62.51	-----	6.764	-----	-----	-----	-----	-----	-----	-----	6.764
701	5.463	62.51	-----	6.761	-----	-----	-----	-----	-----	-----	-----	6.761
702	5.445	62.51	-----	6.757	-----	-----	-----	-----	-----	-----	-----	6.757
703	5.427	62.51	-----	6.754	-----	-----	-----	-----	-----	-----	-----	6.754
704	5.409	62.51	-----	6.750	-----	-----	-----	-----	-----	-----	-----	6.750
705	5.391	62.50	-----	6.747	-----	-----	-----	-----	-----	-----	-----	6.747
706	5.373	62.50	-----	6.743	-----	-----	-----	-----	-----	-----	-----	6.743
707	5.355	62.50	-----	6.739	-----	-----	-----	-----	-----	-----	-----	6.739
708	5.337	62.50	-----	6.736	-----	-----	-----	-----	-----	-----	-----	6.736
709	5.319	62.50	-----	6.732	-----	-----	-----	-----	-----	-----	-----	6.732
710	5.301	62.50	-----	6.728	-----	-----	-----	-----	-----	-----	-----	6.728
711	5.283	62.50	-----	6.724	-----	-----	-----	-----	-----	-----	-----	6.724
712	5.265	62.49	-----	6.720	-----	-----	-----	-----	-----	-----	-----	6.720

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
713	5.247	62.49	-----	6.716	-----	-----	-----	-----	-----	-----	-----	6.716
714	5.230	62.49	-----	6.712	-----	-----	-----	-----	-----	-----	-----	6.712
715	5.213	62.49	-----	6.708	-----	-----	-----	-----	-----	-----	-----	6.708
716	5.197	62.49	-----	6.704	-----	-----	-----	-----	-----	-----	-----	6.704
717	5.180	62.49	-----	6.699	-----	-----	-----	-----	-----	-----	-----	6.699
718	5.164	62.48	-----	6.695	-----	-----	-----	-----	-----	-----	-----	6.695
719	5.149	62.48	-----	6.691	-----	-----	-----	-----	-----	-----	-----	6.691
720	5.134	62.48	-----	6.687	-----	-----	-----	-----	-----	-----	-----	6.687
721	5.119	62.48	-----	6.682	-----	-----	-----	-----	-----	-----	-----	6.682
722	5.104	62.48	-----	6.678	-----	-----	-----	-----	-----	-----	-----	6.678
723	5.090	62.48	-----	6.674	-----	-----	-----	-----	-----	-----	-----	6.674
724	5.076	62.47	-----	6.669	-----	-----	-----	-----	-----	-----	-----	6.669
725	5.063	62.47	-----	6.665	-----	-----	-----	-----	-----	-----	-----	6.665
726	5.050	62.47	-----	6.660	-----	-----	-----	-----	-----	-----	-----	6.660
727	5.038	62.47	-----	6.656	-----	-----	-----	-----	-----	-----	-----	6.656
728	5.026	62.47	-----	6.652	-----	-----	-----	-----	-----	-----	-----	6.652
729	5.014	62.47	-----	6.647	-----	-----	-----	-----	-----	-----	-----	6.647
730	5.003	62.46	-----	6.642	-----	-----	-----	-----	-----	-----	-----	6.642
731	4.993	62.46	-----	6.638	-----	-----	-----	-----	-----	-----	-----	6.638
732	4.983	62.46	-----	6.633	-----	-----	-----	-----	-----	-----	-----	6.633
733	4.973	62.46	-----	6.629	-----	-----	-----	-----	-----	-----	-----	6.629
734	4.964	62.46	-----	6.624	-----	-----	-----	-----	-----	-----	-----	6.624
735	4.956	62.46	-----	6.620	-----	-----	-----	-----	-----	-----	-----	6.620
736	4.948	62.45	-----	6.615	-----	-----	-----	-----	-----	-----	-----	6.615
737	4.941	62.45	-----	6.610	-----	-----	-----	-----	-----	-----	-----	6.610
738	4.934	62.45	-----	6.606	-----	-----	-----	-----	-----	-----	-----	6.606
739	4.927	62.45	-----	6.601	-----	-----	-----	-----	-----	-----	-----	6.601
740	4.922	62.45	-----	6.597	-----	-----	-----	-----	-----	-----	-----	6.597
741	4.917	62.45	-----	6.592	-----	-----	-----	-----	-----	-----	-----	6.592
742	4.912	62.44	-----	6.587	-----	-----	-----	-----	-----	-----	-----	6.587
743	4.908	62.44	-----	6.583	-----	-----	-----	-----	-----	-----	-----	6.583
744	4.905	62.44	-----	6.578	-----	-----	-----	-----	-----	-----	-----	6.578
745	4.902	62.44	-----	6.573	-----	-----	-----	-----	-----	-----	-----	6.573
746	4.900	62.44	-----	6.569	-----	-----	-----	-----	-----	-----	-----	6.569
747	4.898	62.43	-----	6.564	-----	-----	-----	-----	-----	-----	-----	6.564
748	4.897	62.43	-----	6.560	-----	-----	-----	-----	-----	-----	-----	6.560
749	4.897	62.43	-----	6.555	-----	-----	-----	-----	-----	-----	-----	6.555
750	4.897	62.43	-----	6.550	-----	-----	-----	-----	-----	-----	-----	6.550
751	4.897	62.43	-----	6.546	-----	-----	-----	-----	-----	-----	-----	6.546
752	4.898	62.43	-----	6.541	-----	-----	-----	-----	-----	-----	-----	6.541
753	4.898	62.42	-----	6.537	-----	-----	-----	-----	-----	-----	-----	6.537
754	4.899	62.42	-----	6.532	-----	-----	-----	-----	-----	-----	-----	6.532
755	4.899	62.42	-----	6.528	-----	-----	-----	-----	-----	-----	-----	6.528
756	4.900	62.42	-----	6.523	-----	-----	-----	-----	-----	-----	-----	6.523
757	4.900	62.42	-----	6.519	-----	-----	-----	-----	-----	-----	-----	6.519
758	4.901	62.42	-----	6.514	-----	-----	-----	-----	-----	-----	-----	6.514
759	4.901	62.41	-----	6.510	-----	-----	-----	-----	-----	-----	-----	6.510
760	4.900	62.41	-----	6.505	-----	-----	-----	-----	-----	-----	-----	6.505
761	4.900	62.41	-----	6.501	-----	-----	-----	-----	-----	-----	-----	6.501
762	4.899	62.41	-----	6.497	-----	-----	-----	-----	-----	-----	-----	6.497
763	4.897	62.41	-----	6.492	-----	-----	-----	-----	-----	-----	-----	6.492
764	4.895	62.41	-----	6.488	-----	-----	-----	-----	-----	-----	-----	6.488
765	4.893	62.40	-----	6.483	-----	-----	-----	-----	-----	-----	-----	6.483
766	4.890	62.40	-----	6.479	-----	-----	-----	-----	-----	-----	-----	6.479
767	4.887	62.40	-----	6.475	-----	-----	-----	-----	-----	-----	-----	6.475
768	4.883	62.40	-----	6.470	-----	-----	-----	-----	-----	-----	-----	6.470

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
769	4.878	62.40	-----	6.466	-----	-----	-----	-----	-----	-----	-----	6.466
770	4.873	62.40	-----	6.461	-----	-----	-----	-----	-----	-----	-----	6.461
771	4.867	62.39	-----	6.456	-----	-----	-----	-----	-----	-----	-----	6.456
772	4.861	62.39	-----	6.452	-----	-----	-----	-----	-----	-----	-----	6.452
773	4.855	62.39	-----	6.447	-----	-----	-----	-----	-----	-----	-----	6.447
774	4.848	62.39	-----	6.443	-----	-----	-----	-----	-----	-----	-----	6.443
775	4.842	62.39	-----	6.438	-----	-----	-----	-----	-----	-----	-----	6.438
776	4.836	62.39	-----	6.433	-----	-----	-----	-----	-----	-----	-----	6.433
777	4.829	62.38	-----	6.429	-----	-----	-----	-----	-----	-----	-----	6.429
778	4.823	62.38	-----	6.424	-----	-----	-----	-----	-----	-----	-----	6.424
779	4.816	62.38	-----	6.420	-----	-----	-----	-----	-----	-----	-----	6.420
780	4.810	62.38	-----	6.415	-----	-----	-----	-----	-----	-----	-----	6.415
781	4.804	62.38	-----	6.410	-----	-----	-----	-----	-----	-----	-----	6.410
782	4.798	62.38	-----	6.406	-----	-----	-----	-----	-----	-----	-----	6.406
783	4.793	62.37	-----	6.401	-----	-----	-----	-----	-----	-----	-----	6.401
784	4.788	62.37	-----	6.397	-----	-----	-----	-----	-----	-----	-----	6.397
785	4.783	62.37	-----	6.392	-----	-----	-----	-----	-----	-----	-----	6.392
786	4.779	62.37	-----	6.387	-----	-----	-----	-----	-----	-----	-----	6.387
787	4.775	62.37	-----	6.383	-----	-----	-----	-----	-----	-----	-----	6.383
788	4.771	62.37	-----	6.378	-----	-----	-----	-----	-----	-----	-----	6.378
789	4.767	62.36	-----	6.373	-----	-----	-----	-----	-----	-----	-----	6.373
790	4.764	62.36	-----	6.369	-----	-----	-----	-----	-----	-----	-----	6.369
791	4.761	62.36	-----	6.364	-----	-----	-----	-----	-----	-----	-----	6.364
792	4.758	62.36	-----	6.360	-----	-----	-----	-----	-----	-----	-----	6.360
793	4.756	62.36	-----	6.355	-----	-----	-----	-----	-----	-----	-----	6.355
794	4.753	62.36	-----	6.350	-----	-----	-----	-----	-----	-----	-----	6.350
795	4.751	62.35	-----	6.346	-----	-----	-----	-----	-----	-----	-----	6.346
796	4.749	62.35	-----	6.341	-----	-----	-----	-----	-----	-----	-----	6.341
797	4.747	62.35	-----	6.337	-----	-----	-----	-----	-----	-----	-----	6.337
798	4.745	62.35	-----	6.332	-----	-----	-----	-----	-----	-----	-----	6.332
799	4.743	62.35	-----	6.327	-----	-----	-----	-----	-----	-----	-----	6.327
800	4.742	62.35	-----	6.323	-----	-----	-----	-----	-----	-----	-----	6.323
801	4.740	62.34	-----	6.318	-----	-----	-----	-----	-----	-----	-----	6.318
802	4.739	62.34	-----	6.314	-----	-----	-----	-----	-----	-----	-----	6.314
803	4.737	62.34	-----	6.309	-----	-----	-----	-----	-----	-----	-----	6.309
804	4.734	62.34	-----	6.305	-----	-----	-----	-----	-----	-----	-----	6.305
805	4.731	62.34	-----	6.300	-----	-----	-----	-----	-----	-----	-----	6.300
806	4.728	62.34	-----	6.296	-----	-----	-----	-----	-----	-----	-----	6.296
807	4.725	62.33	-----	6.291	-----	-----	-----	-----	-----	-----	-----	6.291
808	4.721	62.33	-----	6.287	-----	-----	-----	-----	-----	-----	-----	6.287
809	4.717	62.33	-----	6.282	-----	-----	-----	-----	-----	-----	-----	6.282
810	4.713	62.33	-----	6.278	-----	-----	-----	-----	-----	-----	-----	6.278
811	4.708	62.33	-----	6.273	-----	-----	-----	-----	-----	-----	-----	6.273
812	4.704	62.33	-----	6.269	-----	-----	-----	-----	-----	-----	-----	6.269
813	4.699	62.32	-----	6.264	-----	-----	-----	-----	-----	-----	-----	6.264
814	4.695	62.32	-----	6.260	-----	-----	-----	-----	-----	-----	-----	6.260
815	4.690	62.32	-----	6.255	-----	-----	-----	-----	-----	-----	-----	6.255
816	4.685	62.32	-----	6.251	-----	-----	-----	-----	-----	-----	-----	6.251
817	4.680	62.32	-----	6.246	-----	-----	-----	-----	-----	-----	-----	6.246
818	4.675	62.32	-----	6.242	-----	-----	-----	-----	-----	-----	-----	6.242
819	4.670	62.31	-----	6.237	-----	-----	-----	-----	-----	-----	-----	6.237
820	4.665	62.31	-----	6.233	-----	-----	-----	-----	-----	-----	-----	6.232
821	4.660	62.31	-----	6.228	-----	-----	-----	-----	-----	-----	-----	6.228
822	4.654	62.31	-----	6.223	-----	-----	-----	-----	-----	-----	-----	6.223
823	4.648	62.31	-----	6.219	-----	-----	-----	-----	-----	-----	-----	6.219
824	4.643	62.31	-----	6.214	-----	-----	-----	-----	-----	-----	-----	6.214

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
825	4.637	62.30	-----	6.210	-----	-----	-----	-----	-----	-----	-----	6.210
826	4.630	62.30	-----	6.205	-----	-----	-----	-----	-----	-----	-----	6.205
827	4.624	62.30	-----	6.201	-----	-----	-----	-----	-----	-----	-----	6.201
828	4.618	62.30	-----	6.196	-----	-----	-----	-----	-----	-----	-----	6.196
829	4.612	62.30	-----	6.191	-----	-----	-----	-----	-----	-----	-----	6.191
830	4.605	62.30	-----	6.187	-----	-----	-----	-----	-----	-----	-----	6.187
831	4.599	62.29	-----	6.182	-----	-----	-----	-----	-----	-----	-----	6.182
832	4.592	62.29	-----	6.177	-----	-----	-----	-----	-----	-----	-----	6.177
833	4.585	62.29	-----	6.172	-----	-----	-----	-----	-----	-----	-----	6.172
834	4.579	62.29	-----	6.168	-----	-----	-----	-----	-----	-----	-----	6.168
835	4.572	62.29	-----	6.163	-----	-----	-----	-----	-----	-----	-----	6.163
836	4.565	62.29	-----	6.158	-----	-----	-----	-----	-----	-----	-----	6.158
837	4.559	62.28	-----	6.153	-----	-----	-----	-----	-----	-----	-----	6.153
838	4.552	62.28	-----	6.148	-----	-----	-----	-----	-----	-----	-----	6.148
839	4.545	62.28	-----	6.144	-----	-----	-----	-----	-----	-----	-----	6.144
840	4.539	62.28	-----	6.139	-----	-----	-----	-----	-----	-----	-----	6.139
841	4.532	62.28	-----	6.134	-----	-----	-----	-----	-----	-----	-----	6.134
842	4.526	62.28	-----	6.129	-----	-----	-----	-----	-----	-----	-----	6.129
843	4.519	62.27	-----	6.124	-----	-----	-----	-----	-----	-----	-----	6.124
844	4.513	62.27	-----	6.119	-----	-----	-----	-----	-----	-----	-----	6.119
845	4.507	62.27	-----	6.115	-----	-----	-----	-----	-----	-----	-----	6.115
846	4.501	62.27	-----	6.110	-----	-----	-----	-----	-----	-----	-----	6.110
847	4.495	62.27	-----	6.105	-----	-----	-----	-----	-----	-----	-----	6.105
848	4.490	62.27	-----	6.100	-----	-----	-----	-----	-----	-----	-----	6.100
849	4.484	62.26	-----	6.095	-----	-----	-----	-----	-----	-----	-----	6.095
850	4.479	62.26	-----	6.090	-----	-----	-----	-----	-----	-----	-----	6.090
851	4.474	62.26	-----	6.085	-----	-----	-----	-----	-----	-----	-----	6.085
852	4.470	62.26	-----	6.081	-----	-----	-----	-----	-----	-----	-----	6.081
853	4.466	62.26	-----	6.076	-----	-----	-----	-----	-----	-----	-----	6.076
854	4.461	62.26	-----	6.071	-----	-----	-----	-----	-----	-----	-----	6.071
855	4.458	62.25	-----	6.066	-----	-----	-----	-----	-----	-----	-----	6.066
856	4.454	62.25	-----	6.061	-----	-----	-----	-----	-----	-----	-----	6.061
857	4.451	62.25	-----	6.056	-----	-----	-----	-----	-----	-----	-----	6.056
858	4.448	62.25	-----	6.052	-----	-----	-----	-----	-----	-----	-----	6.052
859	4.445	62.25	-----	6.047	-----	-----	-----	-----	-----	-----	-----	6.047
860	4.442	62.25	-----	6.042	-----	-----	-----	-----	-----	-----	-----	6.042
861	4.439	62.24	-----	6.037	-----	-----	-----	-----	-----	-----	-----	6.037
862	4.437	62.24	-----	6.032	-----	-----	-----	-----	-----	-----	-----	6.032
863	4.434	62.24	-----	6.027	-----	-----	-----	-----	-----	-----	-----	6.027
864	4.432	62.24	-----	6.023	-----	-----	-----	-----	-----	-----	-----	6.023
865	4.429	62.24	-----	6.018	-----	-----	-----	-----	-----	-----	-----	6.018
866	4.427	62.24	-----	6.013	-----	-----	-----	-----	-----	-----	-----	6.013
867	4.425	62.23	-----	6.008	-----	-----	-----	-----	-----	-----	-----	6.008
868	4.423	62.23	-----	6.003	-----	-----	-----	-----	-----	-----	-----	6.003
869	4.420	62.23	-----	5.999	-----	-----	-----	-----	-----	-----	-----	5.999
870	4.418	62.23	-----	5.994	-----	-----	-----	-----	-----	-----	-----	5.994
871	4.416	62.23	-----	5.989	-----	-----	-----	-----	-----	-----	-----	5.989
872	4.414	62.23	-----	5.984	-----	-----	-----	-----	-----	-----	-----	5.984
873	4.412	62.22	-----	5.980	-----	-----	-----	-----	-----	-----	-----	5.980
874	4.410	62.22	-----	5.975	-----	-----	-----	-----	-----	-----	-----	5.975
875	4.408	62.22	-----	5.970	-----	-----	-----	-----	-----	-----	-----	5.970
876	4.405	62.22	-----	5.966	-----	-----	-----	-----	-----	-----	-----	5.966
877	4.403	62.22	-----	5.961	-----	-----	-----	-----	-----	-----	-----	5.961
878	4.401	62.22	-----	5.956	-----	-----	-----	-----	-----	-----	-----	5.956
879	4.399	62.22	-----	5.952	-----	-----	-----	-----	-----	-----	-----	5.952
880	4.397	62.21	-----	5.947	-----	-----	-----	-----	-----	-----	-----	5.947

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
881	4.395	62.21	-----	5.942	-----	-----	-----	-----	-----	-----	-----	5.942
882	4.393	62.21	-----	5.938	-----	-----	-----	-----	-----	-----	-----	5.938
883	4.390	62.21	-----	5.933	-----	-----	-----	-----	-----	-----	-----	5.933
884	4.388	62.21	-----	5.928	-----	-----	-----	-----	-----	-----	-----	5.928
885	4.386	62.21	-----	5.924	-----	-----	-----	-----	-----	-----	-----	5.924
886	4.384	62.20	-----	5.919	-----	-----	-----	-----	-----	-----	-----	5.919
887	4.381	62.20	-----	5.914	-----	-----	-----	-----	-----	-----	-----	5.914
888	4.379	62.20	-----	5.910	-----	-----	-----	-----	-----	-----	-----	5.910
889	4.377	62.20	-----	5.905	-----	-----	-----	-----	-----	-----	-----	5.905
890	4.374	62.20	-----	5.900	-----	-----	-----	-----	-----	-----	-----	5.900
891	4.372	62.20	-----	5.895	-----	-----	-----	-----	-----	-----	-----	5.895
892	4.369	62.19	-----	5.890	-----	-----	-----	-----	-----	-----	-----	5.890
893	4.367	62.19	-----	5.886	-----	-----	-----	-----	-----	-----	-----	5.886
894	4.364	62.19	-----	5.881	-----	-----	-----	-----	-----	-----	-----	5.881
895	4.361	62.19	-----	5.876	-----	-----	-----	-----	-----	-----	-----	5.876
896	4.359	62.19	-----	5.871	-----	-----	-----	-----	-----	-----	-----	5.871
897	4.356	62.19	-----	5.866	-----	-----	-----	-----	-----	-----	-----	5.866
898	4.353	62.18	-----	5.862	-----	-----	-----	-----	-----	-----	-----	5.862
899	4.351	62.18	-----	5.857	-----	-----	-----	-----	-----	-----	-----	5.857
900	4.348	62.18	-----	5.852	-----	-----	-----	-----	-----	-----	-----	5.852
901	4.345	62.18	-----	5.847	-----	-----	-----	-----	-----	-----	-----	5.847
902	4.342	62.18	-----	5.843	-----	-----	-----	-----	-----	-----	-----	5.843
903	4.339	62.18	-----	5.838	-----	-----	-----	-----	-----	-----	-----	5.838
904	4.336	62.18	-----	5.833	-----	-----	-----	-----	-----	-----	-----	5.833
905	4.333	62.17	-----	5.828	-----	-----	-----	-----	-----	-----	-----	5.828
906	4.330	62.17	-----	5.824	-----	-----	-----	-----	-----	-----	-----	5.824
907	4.327	62.17	-----	5.819	-----	-----	-----	-----	-----	-----	-----	5.819
908	4.324	62.17	-----	5.814	-----	-----	-----	-----	-----	-----	-----	5.814
909	4.321	62.17	-----	5.809	-----	-----	-----	-----	-----	-----	-----	5.809
910	4.318	62.17	-----	5.805	-----	-----	-----	-----	-----	-----	-----	5.805
911	4.315	62.16	-----	5.800	-----	-----	-----	-----	-----	-----	-----	5.800
912	4.312	62.16	-----	5.795	-----	-----	-----	-----	-----	-----	-----	5.795
913	4.309	62.16	-----	5.791	-----	-----	-----	-----	-----	-----	-----	5.791
914	4.306	62.16	-----	5.786	-----	-----	-----	-----	-----	-----	-----	5.786
915	4.302	62.16	-----	5.781	-----	-----	-----	-----	-----	-----	-----	5.781
916	4.299	62.16	-----	5.777	-----	-----	-----	-----	-----	-----	-----	5.777
917	4.296	62.16	-----	5.772	-----	-----	-----	-----	-----	-----	-----	5.772
918	4.293	62.15	-----	5.767	-----	-----	-----	-----	-----	-----	-----	5.767
919	4.290	62.15	-----	5.762	-----	-----	-----	-----	-----	-----	-----	5.762
920	4.287	62.15	-----	5.758	-----	-----	-----	-----	-----	-----	-----	5.758
921	4.284	62.15	-----	5.753	-----	-----	-----	-----	-----	-----	-----	5.753
922	4.281	62.15	-----	5.748	-----	-----	-----	-----	-----	-----	-----	5.749
923	4.278	62.15	-----	5.744	-----	-----	-----	-----	-----	-----	-----	5.744
924	4.275	62.14	-----	5.739	-----	-----	-----	-----	-----	-----	-----	5.739
925	4.271	62.14	-----	5.735	-----	-----	-----	-----	-----	-----	-----	5.735
926	4.268	62.14	-----	5.730	-----	-----	-----	-----	-----	-----	-----	5.730
927	4.265	62.14	-----	5.725	-----	-----	-----	-----	-----	-----	-----	5.725
928	4.262	62.14	-----	5.721	-----	-----	-----	-----	-----	-----	-----	5.721
929	4.259	62.14	-----	5.716	-----	-----	-----	-----	-----	-----	-----	5.716
930	4.256	62.14	-----	5.711	-----	-----	-----	-----	-----	-----	-----	5.711
931	4.253	62.13	-----	5.707	-----	-----	-----	-----	-----	-----	-----	5.707
932	4.250	62.13	-----	5.702	-----	-----	-----	-----	-----	-----	-----	5.702
933	4.247	62.13	-----	5.698	-----	-----	-----	-----	-----	-----	-----	5.698
934	4.243	62.13	-----	5.693	-----	-----	-----	-----	-----	-----	-----	5.693
935	4.240	62.13	-----	5.688	-----	-----	-----	-----	-----	-----	-----	5.688
936	4.237	62.13	-----	5.684	-----	-----	-----	-----	-----	-----	-----	5.684

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
937	4.234	62.12	-----	5.679	-----	-----	-----	-----	-----	-----	-----	5.679
938	4.231	62.12	-----	5.675	-----	-----	-----	-----	-----	-----	-----	5.675
939	4.228	62.12	-----	5.670	-----	-----	-----	-----	-----	-----	-----	5.670
940	4.225	62.12	-----	5.666	-----	-----	-----	-----	-----	-----	-----	5.666
941	4.222	62.12	-----	5.661	-----	-----	-----	-----	-----	-----	-----	5.661
942	4.219	62.12	-----	5.656	-----	-----	-----	-----	-----	-----	-----	5.656
943	4.215	62.12	-----	5.652	-----	-----	-----	-----	-----	-----	-----	5.652
944	4.212	62.11	-----	5.647	-----	-----	-----	-----	-----	-----	-----	5.647
945	4.209	62.11	-----	5.643	-----	-----	-----	-----	-----	-----	-----	5.643
946	4.206	62.11	-----	5.638	-----	-----	-----	-----	-----	-----	-----	5.638
947	4.203	62.11	-----	5.634	-----	-----	-----	-----	-----	-----	-----	5.634
948	4.200	62.11	-----	5.629	-----	-----	-----	-----	-----	-----	-----	5.629
949	4.197	62.11	-----	5.625	-----	-----	-----	-----	-----	-----	-----	5.625
950	4.194	62.11	-----	5.620	-----	-----	-----	-----	-----	-----	-----	5.620
951	4.191	62.10	-----	5.616	-----	-----	-----	-----	-----	-----	-----	5.616
952	4.187	62.10	-----	5.611	-----	-----	-----	-----	-----	-----	-----	5.611
953	4.184	62.10	-----	5.607	-----	-----	-----	-----	-----	-----	-----	5.607
954	4.181	62.10	-----	5.602	-----	-----	-----	-----	-----	-----	-----	5.602
955	4.178	62.10	-----	5.597	-----	-----	-----	-----	-----	-----	-----	5.597
956	4.175	62.10	-----	5.592	-----	-----	-----	-----	-----	-----	-----	5.592
957	4.172	62.09	-----	5.588	-----	-----	-----	-----	-----	-----	-----	5.588
958	4.169	62.09	-----	5.583	-----	-----	-----	-----	-----	-----	-----	5.583
959	4.165	62.09	-----	5.578	-----	-----	-----	-----	-----	-----	-----	5.578
960	4.162	62.09	-----	5.573	-----	-----	-----	-----	-----	-----	-----	5.573
961	4.159	62.09	-----	5.569	-----	-----	-----	-----	-----	-----	-----	5.569
962	4.156	62.09	-----	5.564	-----	-----	-----	-----	-----	-----	-----	5.564
963	4.153	62.09	-----	5.559	-----	-----	-----	-----	-----	-----	-----	5.559
964	4.150	62.08	-----	5.555	-----	-----	-----	-----	-----	-----	-----	5.555
965	4.147	62.08	-----	5.550	-----	-----	-----	-----	-----	-----	-----	5.550
966	4.144	62.08	-----	5.545	-----	-----	-----	-----	-----	-----	-----	5.545
967	4.140	62.08	-----	5.540	-----	-----	-----	-----	-----	-----	-----	5.540
968	4.137	62.08	-----	5.536	-----	-----	-----	-----	-----	-----	-----	5.536
969	4.134	62.08	-----	5.531	-----	-----	-----	-----	-----	-----	-----	5.531
970	4.131	62.08	-----	5.526	-----	-----	-----	-----	-----	-----	-----	5.526
971	4.128	62.07	-----	5.522	-----	-----	-----	-----	-----	-----	-----	5.522
972	4.125	62.07	-----	5.517	-----	-----	-----	-----	-----	-----	-----	5.517
973	4.122	62.07	-----	5.512	-----	-----	-----	-----	-----	-----	-----	5.512
974	4.118	62.07	-----	5.508	-----	-----	-----	-----	-----	-----	-----	5.508
975	4.115	62.07	-----	5.503	-----	-----	-----	-----	-----	-----	-----	5.503
976	4.112	62.07	-----	5.498	-----	-----	-----	-----	-----	-----	-----	5.498
977	4.109	62.07	-----	5.494	-----	-----	-----	-----	-----	-----	-----	5.494
978	4.106	62.06	-----	5.489	-----	-----	-----	-----	-----	-----	-----	5.489
979	4.103	62.06	-----	5.484	-----	-----	-----	-----	-----	-----	-----	5.484
980	4.100	62.06	-----	5.480	-----	-----	-----	-----	-----	-----	-----	5.480
981	4.096	62.06	-----	5.475	-----	-----	-----	-----	-----	-----	-----	5.475
982	4.093	62.06	-----	5.471	-----	-----	-----	-----	-----	-----	-----	5.471
983	4.090	62.06	-----	5.466	-----	-----	-----	-----	-----	-----	-----	5.466
984	4.087	62.06	-----	5.461	-----	-----	-----	-----	-----	-----	-----	5.461
985	4.084	62.05	-----	5.457	-----	-----	-----	-----	-----	-----	-----	5.457
986	4.081	62.05	-----	5.452	-----	-----	-----	-----	-----	-----	-----	5.452
987	4.078	62.05	-----	5.448	-----	-----	-----	-----	-----	-----	-----	5.448
988	4.074	62.05	-----	5.443	-----	-----	-----	-----	-----	-----	-----	5.443
989	4.071	62.05	-----	5.438	-----	-----	-----	-----	-----	-----	-----	5.438
990	4.068	62.05	-----	5.434	-----	-----	-----	-----	-----	-----	-----	5.434
991	4.065	62.05	-----	5.429	-----	-----	-----	-----	-----	-----	-----	5.429
992	4.062	62.04	-----	5.425	-----	-----	-----	-----	-----	-----	-----	5.425

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
993	4.059	62.04	-----	5.420	-----	-----	-----	-----	-----	-----	-----	5.420
994	4.055	62.04	-----	5.416	-----	-----	-----	-----	-----	-----	-----	5.416
995	4.052	62.04	-----	5.411	-----	-----	-----	-----	-----	-----	-----	5.411
996	4.049	62.04	-----	5.406	-----	-----	-----	-----	-----	-----	-----	5.406
997	4.046	62.04	-----	5.402	-----	-----	-----	-----	-----	-----	-----	5.402
998	4.043	62.04	-----	5.397	-----	-----	-----	-----	-----	-----	-----	5.397
999	4.040	62.03	-----	5.393	-----	-----	-----	-----	-----	-----	-----	5.393
1000	4.036	62.03	-----	5.388	-----	-----	-----	-----	-----	-----	-----	5.388
1001	4.033	62.03	-----	5.384	-----	-----	-----	-----	-----	-----	-----	5.384
1002	4.030	62.03	-----	5.379	-----	-----	-----	-----	-----	-----	-----	5.379
1003	4.027	62.03	-----	5.375	-----	-----	-----	-----	-----	-----	-----	5.375
1004	4.024	62.03	-----	5.370	-----	-----	-----	-----	-----	-----	-----	5.370
1005	4.021	62.03	-----	5.366	-----	-----	-----	-----	-----	-----	-----	5.366
1006	4.018	62.02	-----	5.361	-----	-----	-----	-----	-----	-----	-----	5.361
1007	4.014	62.02	-----	5.357	-----	-----	-----	-----	-----	-----	-----	5.357
1008	4.011	62.02	-----	5.352	-----	-----	-----	-----	-----	-----	-----	5.352
1009	4.008	62.02	-----	5.348	-----	-----	-----	-----	-----	-----	-----	5.348
1010	4.005	62.02	-----	5.343	-----	-----	-----	-----	-----	-----	-----	5.343
1011	4.002	62.02	-----	5.339	-----	-----	-----	-----	-----	-----	-----	5.339
1012	3.999	62.02	-----	5.334	-----	-----	-----	-----	-----	-----	-----	5.334
1013	3.995	62.01	-----	5.330	-----	-----	-----	-----	-----	-----	-----	5.330
1014	3.992	62.01	-----	5.325	-----	-----	-----	-----	-----	-----	-----	5.325
1015	3.989	62.01	-----	5.321	-----	-----	-----	-----	-----	-----	-----	5.321
1016	3.986	62.01	-----	5.316	-----	-----	-----	-----	-----	-----	-----	5.316
1017	3.983	62.01	-----	5.312	-----	-----	-----	-----	-----	-----	-----	5.312
1018	3.979	62.01	-----	5.307	-----	-----	-----	-----	-----	-----	-----	5.307
1019	3.976	62.01	-----	5.303	-----	-----	-----	-----	-----	-----	-----	5.303
1020	3.973	62.00	-----	5.299	-----	-----	-----	-----	-----	-----	-----	5.299
1021	3.970	62.00	-----	5.294	-----	-----	-----	-----	-----	-----	-----	5.294
1022	3.967	62.00	-----	5.290	-----	-----	-----	-----	-----	-----	-----	5.290
1023	3.964	62.00	-----	5.285	-----	-----	-----	-----	-----	-----	-----	5.285
1024	3.960	62.00	-----	5.280	-----	-----	-----	-----	-----	-----	-----	5.280
1025	3.957	62.00	-----	5.275	-----	-----	-----	-----	-----	-----	-----	5.275
1026	3.954	62.00	-----	5.270	-----	-----	-----	-----	-----	-----	-----	5.270
1027	3.951	61.99	-----	5.265	-----	-----	-----	-----	-----	-----	-----	5.265
1028	3.948	61.99	-----	5.259	-----	-----	-----	-----	-----	-----	-----	5.259
1029	3.945	61.99	-----	5.254	-----	-----	-----	-----	-----	-----	-----	5.254
1030	3.941	61.99	-----	5.249	-----	-----	-----	-----	-----	-----	-----	5.249
1031	3.938	61.99	-----	5.244	-----	-----	-----	-----	-----	-----	-----	5.244
1032	3.935	61.99	-----	5.239	-----	-----	-----	-----	-----	-----	-----	5.239
1033	3.932	61.99	-----	5.233	-----	-----	-----	-----	-----	-----	-----	5.233
1034	3.929	61.98	-----	5.228	-----	-----	-----	-----	-----	-----	-----	5.228
1035	3.925	61.98	-----	5.223	-----	-----	-----	-----	-----	-----	-----	5.223
1036	3.922	61.98	-----	5.218	-----	-----	-----	-----	-----	-----	-----	5.218
1037	3.919	61.98	-----	5.213	-----	-----	-----	-----	-----	-----	-----	5.213
1038	3.916	61.98	-----	5.208	-----	-----	-----	-----	-----	-----	-----	5.208
1039	3.913	61.98	-----	5.202	-----	-----	-----	-----	-----	-----	-----	5.202
1040	3.910	61.97	-----	5.197	-----	-----	-----	-----	-----	-----	-----	5.197
1041	3.906	61.97	-----	5.192	-----	-----	-----	-----	-----	-----	-----	5.192
1042	3.903	61.97	-----	5.187	-----	-----	-----	-----	-----	-----	-----	5.187
1043	3.900	61.97	-----	5.182	-----	-----	-----	-----	-----	-----	-----	5.182
1044	3.897	61.97	-----	5.177	-----	-----	-----	-----	-----	-----	-----	5.177
1045	3.894	61.97	-----	5.172	-----	-----	-----	-----	-----	-----	-----	5.172
1046	3.890	61.97	-----	5.167	-----	-----	-----	-----	-----	-----	-----	5.167
1047	3.887	61.96	-----	5.162	-----	-----	-----	-----	-----	-----	-----	5.162
1048	3.884	61.96	-----	5.157	-----	-----	-----	-----	-----	-----	-----	5.157

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1049	3.881	61.96	-----	5.152	-----	-----	-----	-----	-----	-----	-----	5.152
1050	3.878	61.96	-----	5.147	-----	-----	-----	-----	-----	-----	-----	5.147
1051	3.874	61.96	-----	5.142	-----	-----	-----	-----	-----	-----	-----	5.142
1052	3.871	61.96	-----	5.137	-----	-----	-----	-----	-----	-----	-----	5.137
1053	3.868	61.96	-----	5.132	-----	-----	-----	-----	-----	-----	-----	5.131
1054	3.865	61.95	-----	5.126	-----	-----	-----	-----	-----	-----	-----	5.126
1055	3.862	61.95	-----	5.121	-----	-----	-----	-----	-----	-----	-----	5.121
1056	3.858	61.95	-----	5.116	-----	-----	-----	-----	-----	-----	-----	5.116
1057	3.855	61.95	-----	5.111	-----	-----	-----	-----	-----	-----	-----	5.111
1058	3.852	61.95	-----	5.106	-----	-----	-----	-----	-----	-----	-----	5.106
1059	3.849	61.95	-----	5.102	-----	-----	-----	-----	-----	-----	-----	5.102
1060	3.846	61.94	-----	5.097	-----	-----	-----	-----	-----	-----	-----	5.097
1061	3.842	61.94	-----	5.092	-----	-----	-----	-----	-----	-----	-----	5.092
1062	3.839	61.94	-----	5.087	-----	-----	-----	-----	-----	-----	-----	5.087
1063	3.836	61.94	-----	5.082	-----	-----	-----	-----	-----	-----	-----	5.082
1064	3.833	61.94	-----	5.077	-----	-----	-----	-----	-----	-----	-----	5.077
1065	3.830	61.94	-----	5.072	-----	-----	-----	-----	-----	-----	-----	5.072
1066	3.826	61.94	-----	5.067	-----	-----	-----	-----	-----	-----	-----	5.067
1067	3.823	61.93	-----	5.062	-----	-----	-----	-----	-----	-----	-----	5.062
1068	3.820	61.93	-----	5.057	-----	-----	-----	-----	-----	-----	-----	5.057
1069	3.817	61.93	-----	5.052	-----	-----	-----	-----	-----	-----	-----	5.052
1070	3.814	61.93	-----	5.047	-----	-----	-----	-----	-----	-----	-----	5.047
1071	3.810	61.93	-----	5.042	-----	-----	-----	-----	-----	-----	-----	5.042
1072	3.807	61.93	-----	5.037	-----	-----	-----	-----	-----	-----	-----	5.037
1073	3.804	61.93	-----	5.033	-----	-----	-----	-----	-----	-----	-----	5.033
1074	3.801	61.92	-----	5.028	-----	-----	-----	-----	-----	-----	-----	5.028
1075	3.798	61.92	-----	5.023	-----	-----	-----	-----	-----	-----	-----	5.023
1076	3.794	61.92	-----	5.018	-----	-----	-----	-----	-----	-----	-----	5.018
1077	3.791	61.92	-----	5.013	-----	-----	-----	-----	-----	-----	-----	5.013
1078	3.788	61.92	-----	5.008	-----	-----	-----	-----	-----	-----	-----	5.008
1079	3.785	61.92	-----	5.003	-----	-----	-----	-----	-----	-----	-----	5.003
1080	3.782	61.92	-----	4.999	-----	-----	-----	-----	-----	-----	-----	4.999
1081	3.778	61.91	-----	4.994	-----	-----	-----	-----	-----	-----	-----	4.994
1082	3.775	61.91	-----	4.989	-----	-----	-----	-----	-----	-----	-----	4.989
1083	3.772	61.91	-----	4.984	-----	-----	-----	-----	-----	-----	-----	4.984
1084	3.769	61.91	-----	4.979	-----	-----	-----	-----	-----	-----	-----	4.979
1085	3.765	61.91	-----	4.974	-----	-----	-----	-----	-----	-----	-----	4.974
1086	3.762	61.91	-----	4.970	-----	-----	-----	-----	-----	-----	-----	4.970
1087	3.759	61.91	-----	4.965	-----	-----	-----	-----	-----	-----	-----	4.965
1088	3.756	61.90	-----	4.960	-----	-----	-----	-----	-----	-----	-----	4.960
1089	3.753	61.90	-----	4.955	-----	-----	-----	-----	-----	-----	-----	4.955
1090	3.749	61.90	-----	4.951	-----	-----	-----	-----	-----	-----	-----	4.951
1091	3.746	61.90	-----	4.946	-----	-----	-----	-----	-----	-----	-----	4.946
1092	3.743	61.90	-----	4.941	-----	-----	-----	-----	-----	-----	-----	4.941
1093	3.740	61.90	-----	4.936	-----	-----	-----	-----	-----	-----	-----	4.936
1094	3.737	61.90	-----	4.931	-----	-----	-----	-----	-----	-----	-----	4.931
1095	3.733	61.90	-----	4.926	-----	-----	-----	-----	-----	-----	-----	4.926
1096	3.730	61.89	-----	4.920	-----	-----	-----	-----	-----	-----	-----	4.920
1097	3.727	61.89	-----	4.915	-----	-----	-----	-----	-----	-----	-----	4.915
1098	3.724	61.89	-----	4.910	-----	-----	-----	-----	-----	-----	-----	4.910
1099	3.720	61.89	-----	4.905	-----	-----	-----	-----	-----	-----	-----	4.905
1100	3.717	61.89	-----	4.900	-----	-----	-----	-----	-----	-----	-----	4.900
1101	3.714	61.89	-----	4.895	-----	-----	-----	-----	-----	-----	-----	4.895
1102	3.711	61.89	-----	4.890	-----	-----	-----	-----	-----	-----	-----	4.890
1103	3.708	61.88	-----	4.885	-----	-----	-----	-----	-----	-----	-----	4.885
1104	3.704	61.88	-----	4.880	-----	-----	-----	-----	-----	-----	-----	4.880

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1105	3.701	61.88	-----	4.875	-----	-----	-----	-----	-----	-----	-----	4.875
1106	3.698	61.88	-----	4.870	-----	-----	-----	-----	-----	-----	-----	4.870
1107	3.695	61.88	-----	4.865	-----	-----	-----	-----	-----	-----	-----	4.865
1108	3.691	61.88	-----	4.860	-----	-----	-----	-----	-----	-----	-----	4.860
1109	3.688	61.88	-----	4.855	-----	-----	-----	-----	-----	-----	-----	4.855
1110	3.685	61.87	-----	4.850	-----	-----	-----	-----	-----	-----	-----	4.850
1111	3.682	61.87	-----	4.845	-----	-----	-----	-----	-----	-----	-----	4.845
1112	3.679	61.87	-----	4.840	-----	-----	-----	-----	-----	-----	-----	4.840
1113	3.675	61.87	-----	4.835	-----	-----	-----	-----	-----	-----	-----	4.835
1114	3.672	61.87	-----	4.830	-----	-----	-----	-----	-----	-----	-----	4.830
1115	3.669	61.87	-----	4.825	-----	-----	-----	-----	-----	-----	-----	4.825
1116	3.666	61.87	-----	4.820	-----	-----	-----	-----	-----	-----	-----	4.820
1117	3.662	61.87	-----	4.815	-----	-----	-----	-----	-----	-----	-----	4.815
1118	3.659	61.86	-----	4.811	-----	-----	-----	-----	-----	-----	-----	4.811
1119	3.656	61.86	-----	4.806	-----	-----	-----	-----	-----	-----	-----	4.806
1120	3.653	61.86	-----	4.801	-----	-----	-----	-----	-----	-----	-----	4.801
1121	3.649	61.86	-----	4.796	-----	-----	-----	-----	-----	-----	-----	4.796
1122	3.646	61.86	-----	4.791	-----	-----	-----	-----	-----	-----	-----	4.791
1123	3.643	61.86	-----	4.786	-----	-----	-----	-----	-----	-----	-----	4.786
1124	3.640	61.86	-----	4.781	-----	-----	-----	-----	-----	-----	-----	4.781
1125	3.637	61.85	-----	4.776	-----	-----	-----	-----	-----	-----	-----	4.776
1126	3.633	61.85	-----	4.771	-----	-----	-----	-----	-----	-----	-----	4.771
1127	3.630	61.85	-----	4.767	-----	-----	-----	-----	-----	-----	-----	4.767
1128	3.627	61.85	-----	4.762	-----	-----	-----	-----	-----	-----	-----	4.762
1129	3.624	61.85	-----	4.757	-----	-----	-----	-----	-----	-----	-----	4.757
1130	3.620	61.85	-----	4.752	-----	-----	-----	-----	-----	-----	-----	4.752
1131	3.617	61.85	-----	4.747	-----	-----	-----	-----	-----	-----	-----	4.747
1132	3.614	61.85	-----	4.742	-----	-----	-----	-----	-----	-----	-----	4.742
1133	3.611	61.84	-----	4.738	-----	-----	-----	-----	-----	-----	-----	4.738
1134	3.607	61.84	-----	4.733	-----	-----	-----	-----	-----	-----	-----	4.733
1135	3.604	61.84	-----	4.728	-----	-----	-----	-----	-----	-----	-----	4.728
1136	3.601	61.84	-----	4.723	-----	-----	-----	-----	-----	-----	-----	4.723
1137	3.598	61.84	-----	4.718	-----	-----	-----	-----	-----	-----	-----	4.718
1138	3.594	61.84	-----	4.714	-----	-----	-----	-----	-----	-----	-----	4.714
1139	3.591	61.84	-----	4.709	-----	-----	-----	-----	-----	-----	-----	4.709
1140	3.588	61.83	-----	4.704	-----	-----	-----	-----	-----	-----	-----	4.704
1141	3.585	61.83	-----	4.699	-----	-----	-----	-----	-----	-----	-----	4.699
1142	3.582	61.83	-----	4.695	-----	-----	-----	-----	-----	-----	-----	4.695
1143	3.578	61.83	-----	4.690	-----	-----	-----	-----	-----	-----	-----	4.690
1144	3.575	61.83	-----	4.685	-----	-----	-----	-----	-----	-----	-----	4.685
1145	3.572	61.83	-----	4.680	-----	-----	-----	-----	-----	-----	-----	4.680
1146	3.569	61.83	-----	4.676	-----	-----	-----	-----	-----	-----	-----	4.676
1147	3.565	61.83	-----	4.671	-----	-----	-----	-----	-----	-----	-----	4.671
1148	3.562	61.82	-----	4.666	-----	-----	-----	-----	-----	-----	-----	4.666
1149	3.559	61.82	-----	4.662	-----	-----	-----	-----	-----	-----	-----	4.662
1150	3.556	61.82	-----	4.657	-----	-----	-----	-----	-----	-----	-----	4.657
1151	3.552	61.82	-----	4.652	-----	-----	-----	-----	-----	-----	-----	4.652
1152	3.549	61.82	-----	4.647	-----	-----	-----	-----	-----	-----	-----	4.647
1153	3.546	61.82	-----	4.643	-----	-----	-----	-----	-----	-----	-----	4.643
1154	3.543	61.82	-----	4.638	-----	-----	-----	-----	-----	-----	-----	4.638
1155	3.539	61.82	-----	4.633	-----	-----	-----	-----	-----	-----	-----	4.633
1156	3.536	61.81	-----	4.629	-----	-----	-----	-----	-----	-----	-----	4.629
1157	3.533	61.81	-----	4.624	-----	-----	-----	-----	-----	-----	-----	4.624
1158	3.530	61.81	-----	4.619	-----	-----	-----	-----	-----	-----	-----	4.619
1159	3.526	61.81	-----	4.615	-----	-----	-----	-----	-----	-----	-----	4.615
1160	3.523	61.81	-----	4.610	-----	-----	-----	-----	-----	-----	-----	4.610

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1161	3.520	61.81	-----	4.606	-----	-----	-----	-----	-----	-----	-----	4.606
1162	3.517	61.81	-----	4.601	-----	-----	-----	-----	-----	-----	-----	4.601
1163	3.513	61.81	-----	4.596	-----	-----	-----	-----	-----	-----	-----	4.596
1164	3.510	61.80	-----	4.592	-----	-----	-----	-----	-----	-----	-----	4.592
1165	3.507	61.80	-----	4.587	-----	-----	-----	-----	-----	-----	-----	4.587
1166	3.504	61.80	-----	4.582	-----	-----	-----	-----	-----	-----	-----	4.582
1167	3.500	61.80	-----	4.578	-----	-----	-----	-----	-----	-----	-----	4.578
1168	3.497	61.80	-----	4.573	-----	-----	-----	-----	-----	-----	-----	4.573
1169	3.494	61.80	-----	4.568	-----	-----	-----	-----	-----	-----	-----	4.568
1170	3.491	61.80	-----	4.563	-----	-----	-----	-----	-----	-----	-----	4.563
1171	3.487	61.80	-----	4.558	-----	-----	-----	-----	-----	-----	-----	4.558
1172	3.484	61.79	-----	4.553	-----	-----	-----	-----	-----	-----	-----	4.553
1173	3.481	61.79	-----	4.548	-----	-----	-----	-----	-----	-----	-----	4.548
1174	3.478	61.79	-----	4.543	-----	-----	-----	-----	-----	-----	-----	4.543
1175	3.474	61.79	-----	4.538	-----	-----	-----	-----	-----	-----	-----	4.538
1176	3.471	61.79	-----	4.533	-----	-----	-----	-----	-----	-----	-----	4.533
1177	3.468	61.79	-----	4.528	-----	-----	-----	-----	-----	-----	-----	4.528
1178	3.465	61.79	-----	4.523	-----	-----	-----	-----	-----	-----	-----	4.523
1179	3.461	61.79	-----	4.519	-----	-----	-----	-----	-----	-----	-----	4.519
1180	3.458	61.78	-----	4.514	-----	-----	-----	-----	-----	-----	-----	4.514
1181	3.455	61.78	-----	4.509	-----	-----	-----	-----	-----	-----	-----	4.509
1182	3.452	61.78	-----	4.504	-----	-----	-----	-----	-----	-----	-----	4.504
1183	3.448	61.78	-----	4.499	-----	-----	-----	-----	-----	-----	-----	4.499
1184	3.445	61.78	-----	4.494	-----	-----	-----	-----	-----	-----	-----	4.494
1185	3.442	61.78	-----	4.489	-----	-----	-----	-----	-----	-----	-----	4.489
1186	3.439	61.78	-----	4.484	-----	-----	-----	-----	-----	-----	-----	4.484
1187	3.435	61.78	-----	4.480	-----	-----	-----	-----	-----	-----	-----	4.480
1188	3.432	61.77	-----	4.475	-----	-----	-----	-----	-----	-----	-----	4.475
1189	3.429	61.77	-----	4.470	-----	-----	-----	-----	-----	-----	-----	4.470
1190	3.425	61.77	-----	4.465	-----	-----	-----	-----	-----	-----	-----	4.465
1191	3.422	61.77	-----	4.460	-----	-----	-----	-----	-----	-----	-----	4.460
1192	3.419	61.77	-----	4.455	-----	-----	-----	-----	-----	-----	-----	4.455
1193	3.416	61.77	-----	4.451	-----	-----	-----	-----	-----	-----	-----	4.451
1194	3.412	61.77	-----	4.446	-----	-----	-----	-----	-----	-----	-----	4.446
1195	3.409	61.77	-----	4.441	-----	-----	-----	-----	-----	-----	-----	4.441
1196	3.406	61.76	-----	4.436	-----	-----	-----	-----	-----	-----	-----	4.436
1197	3.403	61.76	-----	4.431	-----	-----	-----	-----	-----	-----	-----	4.431
1198	3.399	61.76	-----	4.427	-----	-----	-----	-----	-----	-----	-----	4.427
1199	3.396	61.76	-----	4.422	-----	-----	-----	-----	-----	-----	-----	4.422
1200	3.393	61.76	-----	4.417	-----	-----	-----	-----	-----	-----	-----	4.417
1201	3.390	61.76	-----	4.412	-----	-----	-----	-----	-----	-----	-----	4.412
1202	3.386	61.76	-----	4.408	-----	-----	-----	-----	-----	-----	-----	4.408
1203	3.383	61.76	-----	4.403	-----	-----	-----	-----	-----	-----	-----	4.403
1204	3.380	61.76	-----	4.398	-----	-----	-----	-----	-----	-----	-----	4.398
1205	3.377	61.75	-----	4.393	-----	-----	-----	-----	-----	-----	-----	4.393
1206	3.373	61.75	-----	4.389	-----	-----	-----	-----	-----	-----	-----	4.389
1207	3.370	61.75	-----	4.384	-----	-----	-----	-----	-----	-----	-----	4.384
1208	3.367	61.75	-----	4.379	-----	-----	-----	-----	-----	-----	-----	4.379
1209	3.363	61.75	-----	4.375	-----	-----	-----	-----	-----	-----	-----	4.375
1210	3.360	61.75	-----	4.370	-----	-----	-----	-----	-----	-----	-----	4.370
1211	3.357	61.75	-----	4.365	-----	-----	-----	-----	-----	-----	-----	4.365
1212	3.354	61.75	-----	4.361	-----	-----	-----	-----	-----	-----	-----	4.361
1213	3.350	61.74	-----	4.356	-----	-----	-----	-----	-----	-----	-----	4.356
1214	3.347	61.74	-----	4.351	-----	-----	-----	-----	-----	-----	-----	4.351
1215	3.344	61.74	-----	4.347	-----	-----	-----	-----	-----	-----	-----	4.347
1216	3.341	61.74	-----	4.342	-----	-----	-----	-----	-----	-----	-----	4.342

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1217	3.337	61.74	-----	4.337	-----	-----	-----	-----	-----	-----	-----	4.337
1218	3.334	61.74	-----	4.333	-----	-----	-----	-----	-----	-----	-----	4.333
1219	3.331	61.74	-----	4.328	-----	-----	-----	-----	-----	-----	-----	4.328
1220	3.327	61.74	-----	4.323	-----	-----	-----	-----	-----	-----	-----	4.323
1221	3.324	61.74	-----	4.319	-----	-----	-----	-----	-----	-----	-----	4.319
1222	3.321	61.73	-----	4.314	-----	-----	-----	-----	-----	-----	-----	4.314
1223	3.318	61.73	-----	4.310	-----	-----	-----	-----	-----	-----	-----	4.310
1224	3.314	61.73	-----	4.305	-----	-----	-----	-----	-----	-----	-----	4.305
1225	3.311	61.73	-----	4.300	-----	-----	-----	-----	-----	-----	-----	4.300
1226	3.308	61.73	-----	4.296	-----	-----	-----	-----	-----	-----	-----	4.296
1227	3.305	61.73	-----	4.291	-----	-----	-----	-----	-----	-----	-----	4.291
1228	3.301	61.73	-----	4.287	-----	-----	-----	-----	-----	-----	-----	4.287
1229	3.298	61.73	-----	4.282	-----	-----	-----	-----	-----	-----	-----	4.282
1230	3.295	61.73	-----	4.278	-----	-----	-----	-----	-----	-----	-----	4.278
1231	3.291	61.72	-----	4.273	-----	-----	-----	-----	-----	-----	-----	4.273
1232	3.288	61.72	-----	4.268	-----	-----	-----	-----	-----	-----	-----	4.268
1233	3.285	61.72	-----	4.264	-----	-----	-----	-----	-----	-----	-----	4.264
1234	3.282	61.72	-----	4.259	-----	-----	-----	-----	-----	-----	-----	4.259
1235	3.278	61.72	-----	4.255	-----	-----	-----	-----	-----	-----	-----	4.255
1236	3.275	61.72	-----	4.250	-----	-----	-----	-----	-----	-----	-----	4.250
1237	3.272	61.72	-----	4.246	-----	-----	-----	-----	-----	-----	-----	4.246
1238	3.269	61.72	-----	4.241	-----	-----	-----	-----	-----	-----	-----	4.241
1239	3.265	61.71	-----	4.237	-----	-----	-----	-----	-----	-----	-----	4.237
1240	3.262	61.71	-----	4.232	-----	-----	-----	-----	-----	-----	-----	4.232
1241	3.259	61.71	-----	4.228	-----	-----	-----	-----	-----	-----	-----	4.228
1242	3.255	61.71	-----	4.223	-----	-----	-----	-----	-----	-----	-----	4.223
1243	3.252	61.71	-----	4.219	-----	-----	-----	-----	-----	-----	-----	4.219
1244	3.249	61.71	-----	4.214	-----	-----	-----	-----	-----	-----	-----	4.214
1245	3.246	61.71	-----	4.210	-----	-----	-----	-----	-----	-----	-----	4.210
1246	3.242	61.71	-----	4.205	-----	-----	-----	-----	-----	-----	-----	4.205
1247	3.239	61.71	-----	4.201	-----	-----	-----	-----	-----	-----	-----	4.201
1248	3.236	61.70	-----	4.196	-----	-----	-----	-----	-----	-----	-----	4.196
1249	3.232	61.70	-----	4.192	-----	-----	-----	-----	-----	-----	-----	4.192
1250	3.229	61.70	-----	4.187	-----	-----	-----	-----	-----	-----	-----	4.187
1251	3.226	61.70	-----	4.183	-----	-----	-----	-----	-----	-----	-----	4.183
1252	3.223	61.70	-----	4.179	-----	-----	-----	-----	-----	-----	-----	4.179
1253	3.219	61.70	-----	4.174	-----	-----	-----	-----	-----	-----	-----	4.174
1254	3.216	61.70	-----	4.169	-----	-----	-----	-----	-----	-----	-----	4.169
1255	3.213	61.70	-----	4.164	-----	-----	-----	-----	-----	-----	-----	4.164
1256	3.209	61.70	-----	4.159	-----	-----	-----	-----	-----	-----	-----	4.159
1257	3.206	61.69	-----	4.154	-----	-----	-----	-----	-----	-----	-----	4.154
1258	3.203	61.69	-----	4.149	-----	-----	-----	-----	-----	-----	-----	4.149
1259	3.200	61.69	-----	4.145	-----	-----	-----	-----	-----	-----	-----	4.145
1260	3.196	61.69	-----	4.140	-----	-----	-----	-----	-----	-----	-----	4.140
1261	3.193	61.69	-----	4.135	-----	-----	-----	-----	-----	-----	-----	4.135
1262	3.190	61.69	-----	4.130	-----	-----	-----	-----	-----	-----	-----	4.130
1263	3.186	61.69	-----	4.125	-----	-----	-----	-----	-----	-----	-----	4.125
1264	3.183	61.69	-----	4.120	-----	-----	-----	-----	-----	-----	-----	4.120
1265	3.180	61.69	-----	4.116	-----	-----	-----	-----	-----	-----	-----	4.116
1266	3.177	61.68	-----	4.111	-----	-----	-----	-----	-----	-----	-----	4.111
1267	3.173	61.68	-----	4.106	-----	-----	-----	-----	-----	-----	-----	4.106
1268	3.170	61.68	-----	4.101	-----	-----	-----	-----	-----	-----	-----	4.101
1269	3.167	61.68	-----	4.096	-----	-----	-----	-----	-----	-----	-----	4.096
1270	3.163	61.68	-----	4.092	-----	-----	-----	-----	-----	-----	-----	4.092
1271	3.160	61.68	-----	4.087	-----	-----	-----	-----	-----	-----	-----	4.087
1272	3.157	61.68	-----	4.082	-----	-----	-----	-----	-----	-----	-----	4.082

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1273	3.154	61.68	-----	4.077	-----	-----	-----	-----	-----	-----	-----	4.077
1274	3.150	61.68	-----	4.073	-----	-----	-----	-----	-----	-----	-----	4.073
1275	3.147	61.68	-----	4.068	-----	-----	-----	-----	-----	-----	-----	4.068
1276	3.144	61.67	-----	4.063	-----	-----	-----	-----	-----	-----	-----	4.063
1277	3.140	61.67	-----	4.058	-----	-----	-----	-----	-----	-----	-----	4.058
1278	3.137	61.67	-----	4.054	-----	-----	-----	-----	-----	-----	-----	4.054
1279	3.134	61.67	-----	4.049	-----	-----	-----	-----	-----	-----	-----	4.049
1280	3.131	61.67	-----	4.044	-----	-----	-----	-----	-----	-----	-----	4.044
1281	3.127	61.67	-----	4.040	-----	-----	-----	-----	-----	-----	-----	4.040
1282	3.124	61.67	-----	4.035	-----	-----	-----	-----	-----	-----	-----	4.035
1283	3.121	61.67	-----	4.030	-----	-----	-----	-----	-----	-----	-----	4.030
1284	3.117	61.67	-----	4.026	-----	-----	-----	-----	-----	-----	-----	4.026
1285	3.114	61.66	-----	4.021	-----	-----	-----	-----	-----	-----	-----	4.021
1286	3.111	61.66	-----	4.016	-----	-----	-----	-----	-----	-----	-----	4.016
1287	3.107	61.66	-----	4.012	-----	-----	-----	-----	-----	-----	-----	4.012
1288	3.104	61.66	-----	4.007	-----	-----	-----	-----	-----	-----	-----	4.007
1289	3.101	61.66	-----	4.002	-----	-----	-----	-----	-----	-----	-----	4.002
1290	3.098	61.66	-----	3.998	-----	-----	-----	-----	-----	-----	-----	3.998
1291	3.094	61.66	-----	3.993	-----	-----	-----	-----	-----	-----	-----	3.993
1292	3.091	61.66	-----	3.989	-----	-----	-----	-----	-----	-----	-----	3.989
1293	3.088	61.66	-----	3.984	-----	-----	-----	-----	-----	-----	-----	3.984
1294	3.084	61.66	-----	3.979	-----	-----	-----	-----	-----	-----	-----	3.979
1295	3.081	61.65	-----	3.975	-----	-----	-----	-----	-----	-----	-----	3.975
1296	3.078	61.65	-----	3.970	-----	-----	-----	-----	-----	-----	-----	3.970
1297	3.075	61.65	-----	3.966	-----	-----	-----	-----	-----	-----	-----	3.966
1298	3.071	61.65	-----	3.961	-----	-----	-----	-----	-----	-----	-----	3.961
1299	3.068	61.65	-----	3.957	-----	-----	-----	-----	-----	-----	-----	3.957
1300	3.065	61.65	-----	3.952	-----	-----	-----	-----	-----	-----	-----	3.952
1301	3.061	61.65	-----	3.947	-----	-----	-----	-----	-----	-----	-----	3.947
1302	3.058	61.65	-----	3.943	-----	-----	-----	-----	-----	-----	-----	3.943
1303	3.055	61.65	-----	3.938	-----	-----	-----	-----	-----	-----	-----	3.938
1304	3.051	61.64	-----	3.934	-----	-----	-----	-----	-----	-----	-----	3.934
1305	3.048	61.64	-----	3.929	-----	-----	-----	-----	-----	-----	-----	3.929
1306	3.045	61.64	-----	3.925	-----	-----	-----	-----	-----	-----	-----	3.925
1307	3.042	61.64	-----	3.920	-----	-----	-----	-----	-----	-----	-----	3.920
1308	3.038	61.64	-----	3.916	-----	-----	-----	-----	-----	-----	-----	3.916
1309	3.035	61.64	-----	3.911	-----	-----	-----	-----	-----	-----	-----	3.911
1310	3.032	61.64	-----	3.907	-----	-----	-----	-----	-----	-----	-----	3.907
1311	3.028	61.64	-----	3.902	-----	-----	-----	-----	-----	-----	-----	3.902
1312	3.025	61.64	-----	3.898	-----	-----	-----	-----	-----	-----	-----	3.898
1313	3.022	61.64	-----	3.893	-----	-----	-----	-----	-----	-----	-----	3.893
1314	3.018	61.63	-----	3.889	-----	-----	-----	-----	-----	-----	-----	3.889
1315	3.015	61.63	-----	3.884	-----	-----	-----	-----	-----	-----	-----	3.884
1316	3.012	61.63	-----	3.880	-----	-----	-----	-----	-----	-----	-----	3.880
1317	3.009	61.63	-----	3.875	-----	-----	-----	-----	-----	-----	-----	3.875
1318	3.005	61.63	-----	3.871	-----	-----	-----	-----	-----	-----	-----	3.871
1319	3.002	61.63	-----	3.867	-----	-----	-----	-----	-----	-----	-----	3.867
1320	2.999	61.63	-----	3.862	-----	-----	-----	-----	-----	-----	-----	3.862
1321	2.995	61.63	-----	3.858	-----	-----	-----	-----	-----	-----	-----	3.858
1322	2.992	61.63	-----	3.853	-----	-----	-----	-----	-----	-----	-----	3.853
1323	2.989	61.63	-----	3.849	-----	-----	-----	-----	-----	-----	-----	3.849
1324	2.985	61.62	-----	3.844	-----	-----	-----	-----	-----	-----	-----	3.844
1325	2.982	61.62	-----	3.840	-----	-----	-----	-----	-----	-----	-----	3.840
1326	2.979	61.62	-----	3.836	-----	-----	-----	-----	-----	-----	-----	3.836
1327	2.975	61.62	-----	3.831	-----	-----	-----	-----	-----	-----	-----	3.831
1328	2.972	61.62	-----	3.827	-----	-----	-----	-----	-----	-----	-----	3.827

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1329	2.969	61.62	-----	3.822	-----	-----	-----	-----	-----	-----	-----	3.822
1330	2.966	61.62	-----	3.818	-----	-----	-----	-----	-----	-----	-----	3.818
1331	2.962	61.62	-----	3.814	-----	-----	-----	-----	-----	-----	-----	3.814
1332	2.959	61.62	-----	3.809	-----	-----	-----	-----	-----	-----	-----	3.809
1333	2.956	61.62	-----	3.805	-----	-----	-----	-----	-----	-----	-----	3.805
1334	2.952	61.61	-----	3.801	-----	-----	-----	-----	-----	-----	-----	3.801
1335	2.949	61.61	-----	3.796	-----	-----	-----	-----	-----	-----	-----	3.796
1336	2.946	61.61	-----	3.792	-----	-----	-----	-----	-----	-----	-----	3.792
1337	2.942	61.61	-----	3.788	-----	-----	-----	-----	-----	-----	-----	3.788
1338	2.939	61.61	-----	3.783	-----	-----	-----	-----	-----	-----	-----	3.783
1339	2.936	61.61	-----	3.779	-----	-----	-----	-----	-----	-----	-----	3.779
1340	2.933	61.61	-----	3.775	-----	-----	-----	-----	-----	-----	-----	3.775
1341	2.929	61.61	-----	3.770	-----	-----	-----	-----	-----	-----	-----	3.770
1342	2.926	61.61	-----	3.766	-----	-----	-----	-----	-----	-----	-----	3.766
1343	2.923	61.61	-----	3.762	-----	-----	-----	-----	-----	-----	-----	3.762
1344	2.919	61.60	-----	3.757	-----	-----	-----	-----	-----	-----	-----	3.757
1345	2.916	61.60	-----	3.753	-----	-----	-----	-----	-----	-----	-----	3.753
1346	2.913	61.60	-----	3.749	-----	-----	-----	-----	-----	-----	-----	3.749
1347	2.909	61.60	-----	3.744	-----	-----	-----	-----	-----	-----	-----	3.744
1348	2.906	61.60	-----	3.740	-----	-----	-----	-----	-----	-----	-----	3.740
1349	2.903	61.60	-----	3.736	-----	-----	-----	-----	-----	-----	-----	3.736
1350	2.899	61.60	-----	3.731	-----	-----	-----	-----	-----	-----	-----	3.731
1351	2.896	61.60	-----	3.726	-----	-----	-----	-----	-----	-----	-----	3.726
1352	2.893	61.60	-----	3.721	-----	-----	-----	-----	-----	-----	-----	3.721
1353	2.889	61.60	-----	3.716	-----	-----	-----	-----	-----	-----	-----	3.716
1354	2.886	61.60	-----	3.712	-----	-----	-----	-----	-----	-----	-----	3.712
1355	2.883	61.59	-----	3.707	-----	-----	-----	-----	-----	-----	-----	3.707
1356	2.880	61.59	-----	3.702	-----	-----	-----	-----	-----	-----	-----	3.702
1357	2.876	61.59	-----	3.697	-----	-----	-----	-----	-----	-----	-----	3.697
1358	2.873	61.59	-----	3.692	-----	-----	-----	-----	-----	-----	-----	3.692
1359	2.870	61.59	-----	3.688	-----	-----	-----	-----	-----	-----	-----	3.688
1360	2.866	61.59	-----	3.683	-----	-----	-----	-----	-----	-----	-----	3.683
1361	2.863	61.59	-----	3.678	-----	-----	-----	-----	-----	-----	-----	3.678
1362	2.860	61.59	-----	3.673	-----	-----	-----	-----	-----	-----	-----	3.673
1363	2.856	61.59	-----	3.669	-----	-----	-----	-----	-----	-----	-----	3.669
1364	2.853	61.59	-----	3.664	-----	-----	-----	-----	-----	-----	-----	3.664
1365	2.850	61.58	-----	3.659	-----	-----	-----	-----	-----	-----	-----	3.659
1366	2.846	61.58	-----	3.655	-----	-----	-----	-----	-----	-----	-----	3.655
1367	2.843	61.58	-----	3.650	-----	-----	-----	-----	-----	-----	-----	3.650
1368	2.840	61.58	-----	3.645	-----	-----	-----	-----	-----	-----	-----	3.645
1369	2.836	61.58	-----	3.640	-----	-----	-----	-----	-----	-----	-----	3.640
1370	2.833	61.58	-----	3.636	-----	-----	-----	-----	-----	-----	-----	3.636
1371	2.830	61.58	-----	3.631	-----	-----	-----	-----	-----	-----	-----	3.631
1372	2.827	61.58	-----	3.626	-----	-----	-----	-----	-----	-----	-----	3.626
1373	2.823	61.58	-----	3.622	-----	-----	-----	-----	-----	-----	-----	3.622
1374	2.820	61.58	-----	3.617	-----	-----	-----	-----	-----	-----	-----	3.617
1375	2.817	61.58	-----	3.613	-----	-----	-----	-----	-----	-----	-----	3.613
1376	2.813	61.57	-----	3.608	-----	-----	-----	-----	-----	-----	-----	3.608
1377	2.810	61.57	-----	3.603	-----	-----	-----	-----	-----	-----	-----	3.603
1378	2.807	61.57	-----	3.599	-----	-----	-----	-----	-----	-----	-----	3.599
1379	2.803	61.57	-----	3.594	-----	-----	-----	-----	-----	-----	-----	3.594
1380	2.800	61.57	-----	3.589	-----	-----	-----	-----	-----	-----	-----	3.589
1381	2.797	61.57	-----	3.585	-----	-----	-----	-----	-----	-----	-----	3.585
1382	2.793	61.57	-----	3.580	-----	-----	-----	-----	-----	-----	-----	3.580
1383	2.790	61.57	-----	3.576	-----	-----	-----	-----	-----	-----	-----	3.576
1384	2.787	61.57	-----	3.571	-----	-----	-----	-----	-----	-----	-----	3.571

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1385	2.783	61.57	-----	3.567	-----	-----	-----	-----	-----	-----	-----	3.567
1386	2.780	61.57	-----	3.562	-----	-----	-----	-----	-----	-----	-----	3.562
1387	2.777	61.56	-----	3.557	-----	-----	-----	-----	-----	-----	-----	3.557
1388	2.773	61.56	-----	3.553	-----	-----	-----	-----	-----	-----	-----	3.553
1389	2.770	61.56	-----	3.548	-----	-----	-----	-----	-----	-----	-----	3.548
1390	2.767	61.56	-----	3.544	-----	-----	-----	-----	-----	-----	-----	3.544
1391	2.763	61.56	-----	3.539	-----	-----	-----	-----	-----	-----	-----	3.539
1392	2.760	61.56	-----	3.535	-----	-----	-----	-----	-----	-----	-----	3.535
1393	2.757	61.56	-----	3.530	-----	-----	-----	-----	-----	-----	-----	3.530
1394	2.753	61.56	-----	3.526	-----	-----	-----	-----	-----	-----	-----	3.526
1395	2.750	61.56	-----	3.521	-----	-----	-----	-----	-----	-----	-----	3.521
1396	2.747	61.56	-----	3.517	-----	-----	-----	-----	-----	-----	-----	3.517
1397	2.744	61.56	-----	3.512	-----	-----	-----	-----	-----	-----	-----	3.512
1398	2.740	61.55	-----	3.508	-----	-----	-----	-----	-----	-----	-----	3.508
1399	2.737	61.55	-----	3.503	-----	-----	-----	-----	-----	-----	-----	3.503
1400	2.734	61.55	-----	3.499	-----	-----	-----	-----	-----	-----	-----	3.499
1401	2.730	61.55	-----	3.494	-----	-----	-----	-----	-----	-----	-----	3.494
1402	2.727	61.55	-----	3.490	-----	-----	-----	-----	-----	-----	-----	3.490
1403	2.724	61.55	-----	3.486	-----	-----	-----	-----	-----	-----	-----	3.486
1404	2.720	61.55	-----	3.481	-----	-----	-----	-----	-----	-----	-----	3.481
1405	2.717	61.55	-----	3.477	-----	-----	-----	-----	-----	-----	-----	3.477
1406	2.714	61.55	-----	3.472	-----	-----	-----	-----	-----	-----	-----	3.472
1407	2.710	61.55	-----	3.468	-----	-----	-----	-----	-----	-----	-----	3.468
1408	2.707	61.55	-----	3.463	-----	-----	-----	-----	-----	-----	-----	3.463
1409	2.704	61.54	-----	3.459	-----	-----	-----	-----	-----	-----	-----	3.459
1410	2.700	61.54	-----	3.455	-----	-----	-----	-----	-----	-----	-----	3.455
1411	2.697	61.54	-----	3.450	-----	-----	-----	-----	-----	-----	-----	3.450
1412	2.694	61.54	-----	3.446	-----	-----	-----	-----	-----	-----	-----	3.446
1413	2.690	61.54	-----	3.441	-----	-----	-----	-----	-----	-----	-----	3.441
1414	2.687	61.54	-----	3.437	-----	-----	-----	-----	-----	-----	-----	3.437
1415	2.684	61.54	-----	3.433	-----	-----	-----	-----	-----	-----	-----	3.433
1416	2.680	61.54	-----	3.428	-----	-----	-----	-----	-----	-----	-----	3.428
1417	2.677	61.54	-----	3.424	-----	-----	-----	-----	-----	-----	-----	3.424
1418	2.674	61.54	-----	3.420	-----	-----	-----	-----	-----	-----	-----	3.420
1419	2.670	61.54	-----	3.415	-----	-----	-----	-----	-----	-----	-----	3.415
1420	2.667	61.53	-----	3.411	-----	-----	-----	-----	-----	-----	-----	3.411
1421	2.664	61.53	-----	3.407	-----	-----	-----	-----	-----	-----	-----	3.407
1422	2.660	61.53	-----	3.402	-----	-----	-----	-----	-----	-----	-----	3.402
1423	2.657	61.53	-----	3.398	-----	-----	-----	-----	-----	-----	-----	3.398
1424	2.654	61.53	-----	3.394	-----	-----	-----	-----	-----	-----	-----	3.394
1425	2.650	61.53	-----	3.389	-----	-----	-----	-----	-----	-----	-----	3.389
1426	2.647	61.53	-----	3.385	-----	-----	-----	-----	-----	-----	-----	3.385
1427	2.644	61.53	-----	3.381	-----	-----	-----	-----	-----	-----	-----	3.381
1428	2.640	61.53	-----	3.376	-----	-----	-----	-----	-----	-----	-----	3.376
1429	2.637	61.53	-----	3.372	-----	-----	-----	-----	-----	-----	-----	3.372
1430	2.634	61.53	-----	3.368	-----	-----	-----	-----	-----	-----	-----	3.368
1431	2.630	61.53	-----	3.364	-----	-----	-----	-----	-----	-----	-----	3.364
1432	2.627	61.52	-----	3.359	-----	-----	-----	-----	-----	-----	-----	3.359
1433	2.624	61.52	-----	3.355	-----	-----	-----	-----	-----	-----	-----	3.355
1434	2.620	61.52	-----	3.351	-----	-----	-----	-----	-----	-----	-----	3.351
1435	2.617	61.52	-----	3.347	-----	-----	-----	-----	-----	-----	-----	3.347
1436	2.614	61.52	-----	3.342	-----	-----	-----	-----	-----	-----	-----	3.342
1437	2.610	61.52	-----	3.338	-----	-----	-----	-----	-----	-----	-----	3.338
1438	2.607	61.52	-----	3.334	-----	-----	-----	-----	-----	-----	-----	3.334
1439	2.604	61.52	-----	3.330	-----	-----	-----	-----	-----	-----	-----	3.330
1440	2.600	61.52	-----	3.325	-----	-----	-----	-----	-----	-----	-----	3.325

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1441	2.594	61.52	-----	3.321	-----	-----	-----	-----	-----	-----	-----	3.321
1442	2.583	61.52	-----	3.317	-----	-----	-----	-----	-----	-----	-----	3.317
1443	2.570	61.52	-----	3.313	-----	-----	-----	-----	-----	-----	-----	3.313
1444	2.552	61.51	-----	3.308	-----	-----	-----	-----	-----	-----	-----	3.308
1445	2.531	61.51	-----	3.304	-----	-----	-----	-----	-----	-----	-----	3.304
1446	2.507	61.51	-----	3.299	-----	-----	-----	-----	-----	-----	-----	3.299
1447	2.479	61.51	-----	3.295	-----	-----	-----	-----	-----	-----	-----	3.295
1448	2.448	61.51	-----	3.290	-----	-----	-----	-----	-----	-----	-----	3.290
1449	2.413	61.51	-----	3.285	-----	-----	-----	-----	-----	-----	-----	3.285
1450	2.375	61.51	-----	3.280	-----	-----	-----	-----	-----	-----	-----	3.280
1451	2.334	61.51	-----	3.274	-----	-----	-----	-----	-----	-----	-----	3.274
1452	2.289	61.51	-----	3.269	-----	-----	-----	-----	-----	-----	-----	3.269
1453	2.240	61.51	-----	3.263	-----	-----	-----	-----	-----	-----	-----	3.263
1454	2.188	61.50	-----	3.257	-----	-----	-----	-----	-----	-----	-----	3.257
1455	2.133	61.50	-----	3.250	-----	-----	-----	-----	-----	-----	-----	3.250
1456	2.074	61.50	-----	3.244	-----	-----	-----	-----	-----	-----	-----	3.244
1457	2.012	61.50	-----	3.237	-----	-----	-----	-----	-----	-----	-----	3.237
1458	1.946	61.50	-----	3.228	-----	-----	-----	-----	-----	-----	-----	3.228
1459	1.877	61.50	-----	3.219	-----	-----	-----	-----	-----	-----	-----	3.219
1460	1.804	61.50	-----	3.210	-----	-----	-----	-----	-----	-----	-----	3.210
1461	1.728	61.49	-----	3.200	-----	-----	-----	-----	-----	-----	-----	3.200
1462	1.654	61.49	-----	3.189	-----	-----	-----	-----	-----	-----	-----	3.189
1463	1.581	61.49	-----	3.178	-----	-----	-----	-----	-----	-----	-----	3.178
1464	1.511	61.49	-----	3.167	-----	-----	-----	-----	-----	-----	-----	3.167
1465	1.441	61.49	-----	3.156	-----	-----	-----	-----	-----	-----	-----	3.156
1466	1.374	61.48	-----	3.144	-----	-----	-----	-----	-----	-----	-----	3.144
1467	1.308	61.48	-----	3.131	-----	-----	-----	-----	-----	-----	-----	3.131
1468	1.243	61.48	-----	3.118	-----	-----	-----	-----	-----	-----	-----	3.118
1469	1.181	61.48	-----	3.105	-----	-----	-----	-----	-----	-----	-----	3.105
1470	1.120	61.48	-----	3.092	-----	-----	-----	-----	-----	-----	-----	3.092
1471	1.060	61.47	-----	3.078	-----	-----	-----	-----	-----	-----	-----	3.078
1472	1.002	61.47	-----	3.064	-----	-----	-----	-----	-----	-----	-----	3.064
1473	0.946	61.47	-----	3.049	-----	-----	-----	-----	-----	-----	-----	3.049
1474	0.892	61.47	-----	3.035	-----	-----	-----	-----	-----	-----	-----	3.035
1475	0.839	61.46	-----	3.020	-----	-----	-----	-----	-----	-----	-----	3.020
1476	0.788	61.46	-----	3.005	-----	-----	-----	-----	-----	-----	-----	3.005
1477	0.738	61.46	-----	2.989	-----	-----	-----	-----	-----	-----	-----	2.989
1478	0.690	61.46	-----	2.974	-----	-----	-----	-----	-----	-----	-----	2.974
1479	0.644	61.45	-----	2.958	-----	-----	-----	-----	-----	-----	-----	2.958
1480	0.599	61.45	-----	2.942	-----	-----	-----	-----	-----	-----	-----	2.942
1481	0.556	61.45	-----	2.925	-----	-----	-----	-----	-----	-----	-----	2.925
1482	0.515	61.44	-----	2.909	-----	-----	-----	-----	-----	-----	-----	2.909
1483	0.475	61.44	-----	2.892	-----	-----	-----	-----	-----	-----	-----	2.892
1484	0.437	61.44	-----	2.875	-----	-----	-----	-----	-----	-----	-----	2.875
1485	0.400	61.44	-----	2.859	-----	-----	-----	-----	-----	-----	-----	2.859
1486	0.365	61.43	-----	2.841	-----	-----	-----	-----	-----	-----	-----	2.841
1487	0.332	61.43	-----	2.824	-----	-----	-----	-----	-----	-----	-----	2.824
1488	0.300	61.43	-----	2.807	-----	-----	-----	-----	-----	-----	-----	2.807
1489	0.270	61.42	-----	2.790	-----	-----	-----	-----	-----	-----	-----	2.790
1490	0.242	61.42	-----	2.772	-----	-----	-----	-----	-----	-----	-----	2.772
1491	0.215	61.42	-----	2.755	-----	-----	-----	-----	-----	-----	-----	2.755
1492	0.189	61.42	-----	2.737	-----	-----	-----	-----	-----	-----	-----	2.737
1493	0.166	61.41	-----	2.719	-----	-----	-----	-----	-----	-----	-----	2.719
1494	0.143	61.41	-----	2.702	-----	-----	-----	-----	-----	-----	-----	2.702
1495	0.123	61.41	-----	2.684	-----	-----	-----	-----	-----	-----	-----	2.684
1496	0.104	61.40	-----	2.666	-----	-----	-----	-----	-----	-----	-----	2.666

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1497	0.087	61.40	-----	2.649	-----	-----	-----	-----	-----	-----	-----	2.649
1498	0.071	61.40	-----	2.628	-----	-----	-----	-----	-----	-----	-----	2.628
1499	0.057	61.40	-----	2.605	-----	-----	-----	-----	-----	-----	-----	2.605
1500	0.044	61.39	-----	2.582	-----	-----	-----	-----	-----	-----	-----	2.582
1501	0.033	61.39	-----	2.559	-----	-----	-----	-----	-----	-----	-----	2.559
1502	0.024	61.39	-----	2.536	-----	-----	-----	-----	-----	-----	-----	2.536
1503	0.016	61.38	-----	2.514	-----	-----	-----	-----	-----	-----	-----	2.514
1504	0.009	61.38	-----	2.491	-----	-----	-----	-----	-----	-----	-----	2.491
1505	0.005	61.38	-----	2.469	-----	-----	-----	-----	-----	-----	-----	2.469
1506	0.002	61.37	-----	2.447	-----	-----	-----	-----	-----	-----	-----	2.447
1507	0.000	61.37	-----	2.425	-----	-----	-----	-----	-----	-----	-----	2.425
1508	0.000	61.37	-----	2.403	-----	-----	-----	-----	-----	-----	-----	2.403
1509	0.000	61.37	-----	2.382	-----	-----	-----	-----	-----	-----	-----	2.382
1510	0.000	61.36	-----	2.360	-----	-----	-----	-----	-----	-----	-----	2.360
1511	0.000	61.36	-----	2.339	-----	-----	-----	-----	-----	-----	-----	2.339
1512	0.000	61.36	-----	2.318	-----	-----	-----	-----	-----	-----	-----	2.318
1513	0.000	61.36	-----	2.297	-----	-----	-----	-----	-----	-----	-----	2.297
1514	0.000	61.35	-----	2.277	-----	-----	-----	-----	-----	-----	-----	2.277
1515	0.000	61.35	-----	2.256	-----	-----	-----	-----	-----	-----	-----	2.256
1516	0.000	61.35	-----	2.236	-----	-----	-----	-----	-----	-----	-----	2.236
1517	0.000	61.34	-----	2.216	-----	-----	-----	-----	-----	-----	-----	2.216
1518	0.000	61.34	-----	2.196	-----	-----	-----	-----	-----	-----	-----	2.196
1519	0.000	61.34	-----	2.177	-----	-----	-----	-----	-----	-----	-----	2.177
1520	0.000	61.34	-----	2.157	-----	-----	-----	-----	-----	-----	-----	2.157
1521	0.000	61.33	-----	2.138	-----	-----	-----	-----	-----	-----	-----	2.138
1522	0.000	61.33	-----	2.119	-----	-----	-----	-----	-----	-----	-----	2.119
1523	0.000	61.33	-----	2.100	-----	-----	-----	-----	-----	-----	-----	2.100
1524	0.000	61.33	-----	2.081	-----	-----	-----	-----	-----	-----	-----	2.081
1525	0.000	61.33	-----	2.062	-----	-----	-----	-----	-----	-----	-----	2.062
1526	0.000	61.32	-----	2.044	-----	-----	-----	-----	-----	-----	-----	2.044
1527	0.000	61.32	-----	2.025	-----	-----	-----	-----	-----	-----	-----	2.025
1528	0.000	61.32	-----	2.007	-----	-----	-----	-----	-----	-----	-----	2.007
1529	0.000	61.32	-----	1.989	-----	-----	-----	-----	-----	-----	-----	1.989
1530	0.000	61.31	-----	1.971	-----	-----	-----	-----	-----	-----	-----	1.971
1531	0.000	61.31	-----	1.954	-----	-----	-----	-----	-----	-----	-----	1.954
1532	0.000	61.31	-----	1.936	-----	-----	-----	-----	-----	-----	-----	1.936
1533	0.000	61.31	-----	1.919	-----	-----	-----	-----	-----	-----	-----	1.919
1534	0.000	61.30	-----	1.902	-----	-----	-----	-----	-----	-----	-----	1.902
1535	0.000	61.30	-----	1.885	-----	-----	-----	-----	-----	-----	-----	1.885
1536	0.000	61.30	-----	1.867	-----	-----	-----	-----	-----	-----	-----	1.867
1537	0.000	61.30	-----	1.827	-----	-----	-----	-----	-----	-----	-----	1.827
1538	0.000	61.30	-----	1.787	-----	-----	-----	-----	-----	-----	-----	1.787
1539	0.000	61.29	-----	1.749	-----	-----	-----	-----	-----	-----	-----	1.749
1540	0.000	61.29	-----	1.711	-----	-----	-----	-----	-----	-----	-----	1.711
1541	0.000	61.29	-----	1.674	-----	-----	-----	-----	-----	-----	-----	1.674
1542	0.000	61.29	-----	1.638	-----	-----	-----	-----	-----	-----	-----	1.638
1543	0.000	61.29	-----	1.603	-----	-----	-----	-----	-----	-----	-----	1.603
1544	0.000	61.28	-----	1.569	-----	-----	-----	-----	-----	-----	-----	1.569
1545	0.000	61.28	-----	1.535	-----	-----	-----	-----	-----	-----	-----	1.535
1546	0.000	61.28	-----	1.502	-----	-----	-----	-----	-----	-----	-----	1.502
1547	0.000	61.28	-----	1.470	-----	-----	-----	-----	-----	-----	-----	1.470
1548	0.000	61.28	-----	1.438	-----	-----	-----	-----	-----	-----	-----	1.438
1549	0.000	61.28	-----	1.407	-----	-----	-----	-----	-----	-----	-----	1.407
1550	0.000	61.27	-----	1.377	-----	-----	-----	-----	-----	-----	-----	1.377
1551	0.000	61.27	-----	1.347	-----	-----	-----	-----	-----	-----	-----	1.347
1552	0.000	61.27	-----	1.318	-----	-----	-----	-----	-----	-----	-----	1.318

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1553	0.000	61.27	-----	1.290	-----	-----	-----	-----	-----	-----	-----	1.290
1554	0.000	61.27	-----	1.262	-----	-----	-----	-----	-----	-----	-----	1.262
1555	0.000	61.27	-----	1.235	-----	-----	-----	-----	-----	-----	-----	1.235
1556	0.000	61.26	-----	1.208	-----	-----	-----	-----	-----	-----	-----	1.208
1557	0.000	61.26	-----	1.182	-----	-----	-----	-----	-----	-----	-----	1.182
1558	0.000	61.26	-----	1.157	-----	-----	-----	-----	-----	-----	-----	1.157
1559	0.000	61.26	-----	1.132	-----	-----	-----	-----	-----	-----	-----	1.132
1560	0.000	61.26	-----	1.108	-----	-----	-----	-----	-----	-----	-----	1.108
1561	0.000	61.26	-----	1.084	-----	-----	-----	-----	-----	-----	-----	1.084
1562	0.000	61.26	-----	1.061	-----	-----	-----	-----	-----	-----	-----	1.061
1563	0.000	61.26	-----	1.038	-----	-----	-----	-----	-----	-----	-----	1.038
1564	0.000	61.25	-----	1.016	-----	-----	-----	-----	-----	-----	-----	1.016
1565	0.000	61.25	-----	0.994	-----	-----	-----	-----	-----	-----	-----	0.994
1566	0.000	61.25	-----	0.972	-----	-----	-----	-----	-----	-----	-----	0.972
1567	0.000	61.25	-----	0.951	-----	-----	-----	-----	-----	-----	-----	0.951
1568	0.000	61.25	-----	0.931	-----	-----	-----	-----	-----	-----	-----	0.931
1569	0.000	61.25	-----	0.911	-----	-----	-----	-----	-----	-----	-----	0.911
1570	0.000	61.25	-----	0.891	-----	-----	-----	-----	-----	-----	-----	0.891
1571	0.000	61.25	-----	0.872	-----	-----	-----	-----	-----	-----	-----	0.872
1572	0.000	61.25	-----	0.853	-----	-----	-----	-----	-----	-----	-----	0.853
1573	0.000	61.24	-----	0.835	-----	-----	-----	-----	-----	-----	-----	0.835
1574	0.000	61.24	-----	0.817	-----	-----	-----	-----	-----	-----	-----	0.817
1575	0.000	61.24	-----	0.800	-----	-----	-----	-----	-----	-----	-----	0.799
1576	0.000	61.24	-----	0.782	-----	-----	-----	-----	-----	-----	-----	0.782
1577	0.000	61.24	-----	0.765	-----	-----	-----	-----	-----	-----	-----	0.765
1578	0.000	61.24	-----	0.749	-----	-----	-----	-----	-----	-----	-----	0.749
1579	0.000	61.24	-----	0.733	-----	-----	-----	-----	-----	-----	-----	0.733
1580	0.000	61.24	-----	0.717	-----	-----	-----	-----	-----	-----	-----	0.717
1581	0.000	61.24	-----	0.702	-----	-----	-----	-----	-----	-----	-----	0.702
1582	0.000	61.24	-----	0.687	-----	-----	-----	-----	-----	-----	-----	0.687
1583	0.000	61.24	-----	0.672	-----	-----	-----	-----	-----	-----	-----	0.672
1584	0.000	61.24	-----	0.657	-----	-----	-----	-----	-----	-----	-----	0.657
1585	0.000	61.23	-----	0.643	-----	-----	-----	-----	-----	-----	-----	0.643
1586	0.000	61.23	-----	0.629	-----	-----	-----	-----	-----	-----	-----	0.629
1587	0.000	61.23	-----	0.616	-----	-----	-----	-----	-----	-----	-----	0.616
1588	0.000	61.23	-----	0.603	-----	-----	-----	-----	-----	-----	-----	0.603
1589	0.000	61.23	-----	0.590	-----	-----	-----	-----	-----	-----	-----	0.590
1590	0.000	61.23	-----	0.577	-----	-----	-----	-----	-----	-----	-----	0.577
1591	0.000	61.23	-----	0.565	-----	-----	-----	-----	-----	-----	-----	0.565
1592	0.000	61.23	-----	0.552	-----	-----	-----	-----	-----	-----	-----	0.552
1593	0.000	61.23	-----	0.541	-----	-----	-----	-----	-----	-----	-----	0.541
1594	0.000	61.23	-----	0.529	-----	-----	-----	-----	-----	-----	-----	0.529
1595	0.000	61.23	-----	0.518	-----	-----	-----	-----	-----	-----	-----	0.518
1596	0.000	61.23	-----	0.506	-----	-----	-----	-----	-----	-----	-----	0.506
1597	0.000	61.23	-----	0.496	-----	-----	-----	-----	-----	-----	-----	0.496
1598	0.000	61.23	-----	0.485	-----	-----	-----	-----	-----	-----	-----	0.485
1599	0.000	61.23	-----	0.474	-----	-----	-----	-----	-----	-----	-----	0.474
1600	0.000	61.22	-----	0.464	-----	-----	-----	-----	-----	-----	-----	0.464
1601	0.000	61.22	-----	0.454	-----	-----	-----	-----	-----	-----	-----	0.454
1602	0.000	61.22	-----	0.445	-----	-----	-----	-----	-----	-----	-----	0.444
1603	0.000	61.22	-----	0.435	-----	-----	-----	-----	-----	-----	-----	0.435
1604	0.000	61.22	-----	0.426	-----	-----	-----	-----	-----	-----	-----	0.426
1605	0.000	61.22	-----	0.416	-----	-----	-----	-----	-----	-----	-----	0.416
1606	0.000	61.22	-----	0.407	-----	-----	-----	-----	-----	-----	-----	0.407
1607	0.000	61.22	-----	0.399	-----	-----	-----	-----	-----	-----	-----	0.399
1608	0.000	61.22	-----	0.390	-----	-----	-----	-----	-----	-----	-----	0.390

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1609	0.000	61.22	-----	0.382	-----	-----	-----	-----	-----	-----	-----	0.382
1610	0.000	61.22	-----	0.374	-----	-----	-----	-----	-----	-----	-----	0.374
1611	0.000	61.22	-----	0.365	-----	-----	-----	-----	-----	-----	-----	0.365
1612	0.000	61.22	-----	0.358	-----	-----	-----	-----	-----	-----	-----	0.358
1613	0.000	61.22	-----	0.350	-----	-----	-----	-----	-----	-----	-----	0.350
1614	0.000	61.22	-----	0.342	-----	-----	-----	-----	-----	-----	-----	0.342
1615	0.000	61.22	-----	0.335	-----	-----	-----	-----	-----	-----	-----	0.335
1616	0.000	61.22	-----	0.328	-----	-----	-----	-----	-----	-----	-----	0.328
1617	0.000	61.22	-----	0.321	-----	-----	-----	-----	-----	-----	-----	0.321
1618	0.000	61.22	-----	0.314	-----	-----	-----	-----	-----	-----	-----	0.314
1619	0.000	61.22	-----	0.307	-----	-----	-----	-----	-----	-----	-----	0.307
1620	0.000	61.22	-----	0.301	-----	-----	-----	-----	-----	-----	-----	0.301
1621	0.000	61.22	-----	0.294	-----	-----	-----	-----	-----	-----	-----	0.294
1622	0.000	61.22	-----	0.288	-----	-----	-----	-----	-----	-----	-----	0.288
1623	0.000	61.22	-----	0.282	-----	-----	-----	-----	-----	-----	-----	0.282
1624	0.000	61.21	-----	0.275	-----	-----	-----	-----	-----	-----	-----	0.275
1625	0.000	61.21	-----	0.270	-----	-----	-----	-----	-----	-----	-----	0.270
1626	0.000	61.21	-----	0.264	-----	-----	-----	-----	-----	-----	-----	0.264
1627	0.000	61.21	-----	0.258	-----	-----	-----	-----	-----	-----	-----	0.258
1628	0.000	61.21	-----	0.253	-----	-----	-----	-----	-----	-----	-----	0.253
1629	0.000	61.21	-----	0.247	-----	-----	-----	-----	-----	-----	-----	0.247
1630	0.000	61.21	-----	0.242	-----	-----	-----	-----	-----	-----	-----	0.242
1631	0.000	61.21	-----	0.237	-----	-----	-----	-----	-----	-----	-----	0.237
1632	0.000	61.21	-----	0.231	-----	-----	-----	-----	-----	-----	-----	0.232
1633	0.000	61.21	-----	0.227	-----	-----	-----	-----	-----	-----	-----	0.227
1634	0.000	61.21	-----	0.222	-----	-----	-----	-----	-----	-----	-----	0.222
1635	0.000	61.21	-----	0.217	-----	-----	-----	-----	-----	-----	-----	0.217
1636	0.000	61.21	-----	0.212	-----	-----	-----	-----	-----	-----	-----	0.212
1637	0.000	61.21	-----	0.208	-----	-----	-----	-----	-----	-----	-----	0.208
1638	0.000	61.21	-----	0.203	-----	-----	-----	-----	-----	-----	-----	0.203
1639	0.000	61.21	-----	0.199	-----	-----	-----	-----	-----	-----	-----	0.199
1640	0.000	61.21	-----	0.195	-----	-----	-----	-----	-----	-----	-----	0.195
1641	0.000	61.21	-----	0.190	-----	-----	-----	-----	-----	-----	-----	0.190
1642	0.000	61.21	-----	0.186	-----	-----	-----	-----	-----	-----	-----	0.186
1643	0.000	61.21	-----	0.182	-----	-----	-----	-----	-----	-----	-----	0.182
1644	0.000	61.21	-----	0.178	-----	-----	-----	-----	-----	-----	-----	0.178
1645	0.000	61.21	-----	0.175	-----	-----	-----	-----	-----	-----	-----	0.175
1646	0.000	61.21	-----	0.171	-----	-----	-----	-----	-----	-----	-----	0.171
1647	0.000	61.21	-----	0.167	-----	-----	-----	-----	-----	-----	-----	0.167
1648	0.000	61.21	-----	0.163	-----	-----	-----	-----	-----	-----	-----	0.163
1649	0.000	61.21	-----	0.160	-----	-----	-----	-----	-----	-----	-----	0.160
1650	0.000	61.21	-----	0.157	-----	-----	-----	-----	-----	-----	-----	0.157
1651	0.000	61.21	-----	0.153	-----	-----	-----	-----	-----	-----	-----	0.153
1652	0.000	61.21	-----	0.150	-----	-----	-----	-----	-----	-----	-----	0.150
1653	0.000	61.21	-----	0.147	-----	-----	-----	-----	-----	-----	-----	0.147
1654	0.000	61.21	-----	0.143	-----	-----	-----	-----	-----	-----	-----	0.143
1655	0.000	61.21	-----	0.140	-----	-----	-----	-----	-----	-----	-----	0.140
1656	0.000	61.21	-----	0.137	-----	-----	-----	-----	-----	-----	-----	0.137
1657	0.000	61.21	-----	0.134	-----	-----	-----	-----	-----	-----	-----	0.134
1658	0.000	61.21	-----	0.132	-----	-----	-----	-----	-----	-----	-----	0.132
1659	0.000	61.21	-----	0.129	-----	-----	-----	-----	-----	-----	-----	0.129
1660	0.000	61.21	-----	0.126	-----	-----	-----	-----	-----	-----	-----	0.126
1661	0.000	61.21	-----	0.123	-----	-----	-----	-----	-----	-----	-----	0.123
1662	0.000	61.21	-----	0.121	-----	-----	-----	-----	-----	-----	-----	0.121
1663	0.000	61.21	-----	0.118	-----	-----	-----	-----	-----	-----	-----	0.118
1664	0.000	61.21	-----	0.115	-----	-----	-----	-----	-----	-----	-----	0.115

Continues on next page...

Detention pond outflow

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1665	0.000	61.21	-----	0.113	-----	-----	-----	-----	-----	-----	-----	0.113
1666	0.000	61.21	-----	0.111	-----	-----	-----	-----	-----	-----	-----	0.111
1667	0.000	61.21	-----	0.108	-----	-----	-----	-----	-----	-----	-----	0.108
1668	0.000	61.21	-----	0.106	-----	-----	-----	-----	-----	-----	-----	0.106
1669	0.000	61.21	-----	0.104	-----	-----	-----	-----	-----	-----	-----	0.104
1670	0.000	61.21	-----	0.101	-----	-----	-----	-----	-----	-----	-----	0.101
1671	0.000	61.21	-----	0.099	-----	-----	-----	-----	-----	-----	-----	0.099
1672	0.000	61.21	-----	0.097	-----	-----	-----	-----	-----	-----	-----	0.097
1673	0.000	61.21	-----	0.095	-----	-----	-----	-----	-----	-----	-----	0.095
1674	0.000	61.20	-----	0.093	-----	-----	-----	-----	-----	-----	-----	0.093
1675	0.000	61.20	-----	0.091	-----	-----	-----	-----	-----	-----	-----	0.091
1676	0.000	61.20	-----	0.089	-----	-----	-----	-----	-----	-----	-----	0.089
1677	0.000	61.20	-----	0.087	-----	-----	-----	-----	-----	-----	-----	0.087
1678	0.000	61.20	-----	0.085	-----	-----	-----	-----	-----	-----	-----	0.085
1679	0.000	61.20	-----	0.083	-----	-----	-----	-----	-----	-----	-----	0.083
1680	0.000	61.20	-----	0.082	-----	-----	-----	-----	-----	-----	-----	0.082
1681	0.000	61.20	-----	0.080	-----	-----	-----	-----	-----	-----	-----	0.080
1682	0.000	61.20	-----	0.078	-----	-----	-----	-----	-----	-----	-----	0.078
1683	0.000	61.20	-----	0.076	-----	-----	-----	-----	-----	-----	-----	0.076
1684	0.000	61.20	-----	0.075	-----	-----	-----	-----	-----	-----	-----	0.075
1685	0.000	61.20	-----	0.073	-----	-----	-----	-----	-----	-----	-----	0.073
1686	0.000	61.20	-----	0.072	-----	-----	-----	-----	-----	-----	-----	0.072
1687	0.000	61.20	-----	0.070	-----	-----	-----	-----	-----	-----	-----	0.070

...End

EMERGENCY RELEASE THROUGH 48” RISER PIPE MODEL CALCULATIONS

Watershed Model Schematic

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

Legend

Hyd.	Origin	Description
1	SCS Runoff	Developed site storm event
2	Reservoir	Detention pond outflow

Project: Proposed site SCS 06-25-09 Riser pipe emergency.gpw

Thursday, Jul 2, 2009

Hydrograph Return Period Recap

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

Hyd. No.	Hydrograph type (origin)	Inflow Hyd(s)	Peak Outflow (cfs)								Hydrograph description
			1-Yr	2-Yr	3-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr	
1	SCS Runoff	------	-------	7.792	-------	11.97	14.81	18.23	20.66	23.03	Developed site storm event
2	Reservoir	1	-------	0.000	-------	2.186	2.990	4.375	5.685	7.458	Detention pond outflow

Hydrograph Summary Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	SCS Runoff	14.81	1	495	257,225	------	------	------	Developed site storm event
2	Reservoir	2.990	1	884	114,093	1	62.87	152,824	Detention pond outflow

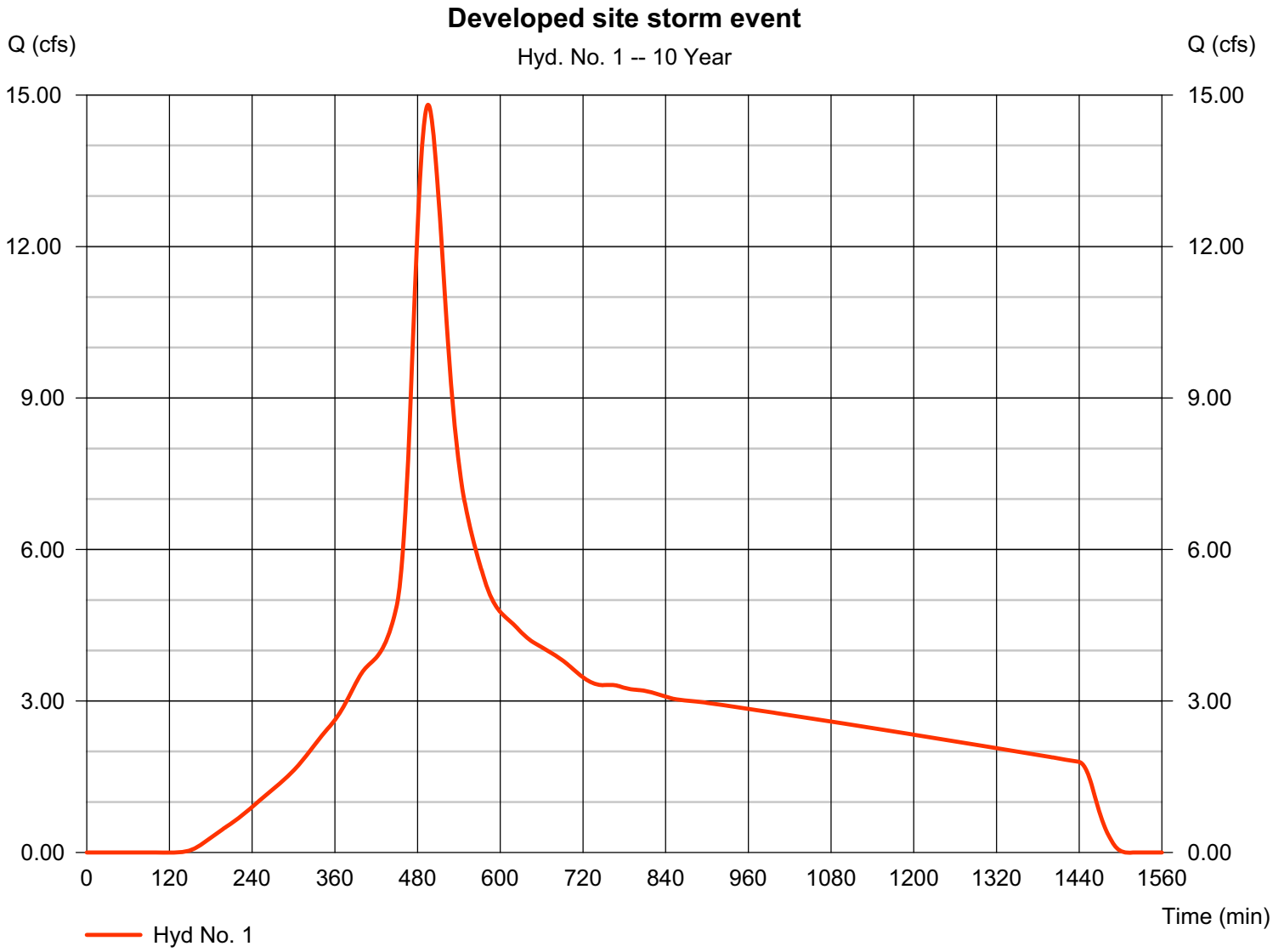
Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Hyd. No. 1

Developed site storm event

Hydrograph type	=	SCS Runoff	Peak discharge	=	14.81 cfs
Storm frequency	=	10 yrs	Time to peak	=	495 min
Time interval	=	1 min	Hyd. volume	=	257,225 cuft
Drainage area	=	25.500 ac	Curve number	=	91
Basin Slope	=	0.0 %	Hydraulic length	=	0 ft
Tc method	=	TR55	Time of conc. (Tc)	=	34.00 min
Total precip.	=	3.74 in	Distribution	=	Type IA
Storm duration	=	24 hrs	Shape factor	=	400



TR55 Tc Worksheet

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

Hyd. No. 1

Developed site storm event

Description		A		B		C		Totals
Sheet Flow								
Manning's n-value	=	0.240		0.011		0.011		
Flow length (ft)	=	180.0		0.0		0.0		
Two-year 24-hr precip. (in)	=	2.39		0.00		0.00		
Land slope (%)	=	1.50		0.00		0.00		
Travel Time (min)	**=**	**29.65**	**+**	**0.00**	**+**	**0.00**	**=**	**29.65**
Shallow Concentrated Flow								
Flow length (ft)	=	0.00		0.00		0.00		
Watercourse slope (%)	=	0.00		0.00		0.00		
Surface description	=	Paved		Paved		Paved		
Average velocity (ft/s)	=	0.00		0.00		0.00		
Travel Time (min)	**=**	**0.00**	**+**	**0.00**	**+**	**0.00**	**=**	**0.00**
Channel Flow								
X sectional flow area (sqft)	=	18.00		0.00		0.00		
Wetted perimeter (ft)	=	13.40		0.00		0.00		
Channel slope (%)	=	0.25		0.00		0.00		
Manning's n-value	=	0.025		0.015		0.015		
Velocity (ft/s)	=	3.63		0.00		0.00		
Flow length (ft)	=	950.0		0.0		0.0		
Travel Time (min)	**=**	**4.36**	**+**	**0.00**	**+**	**0.00**	**=**	**4.36**

Total Travel Time, Tc ..... 34.00 min

Hydrograph Report

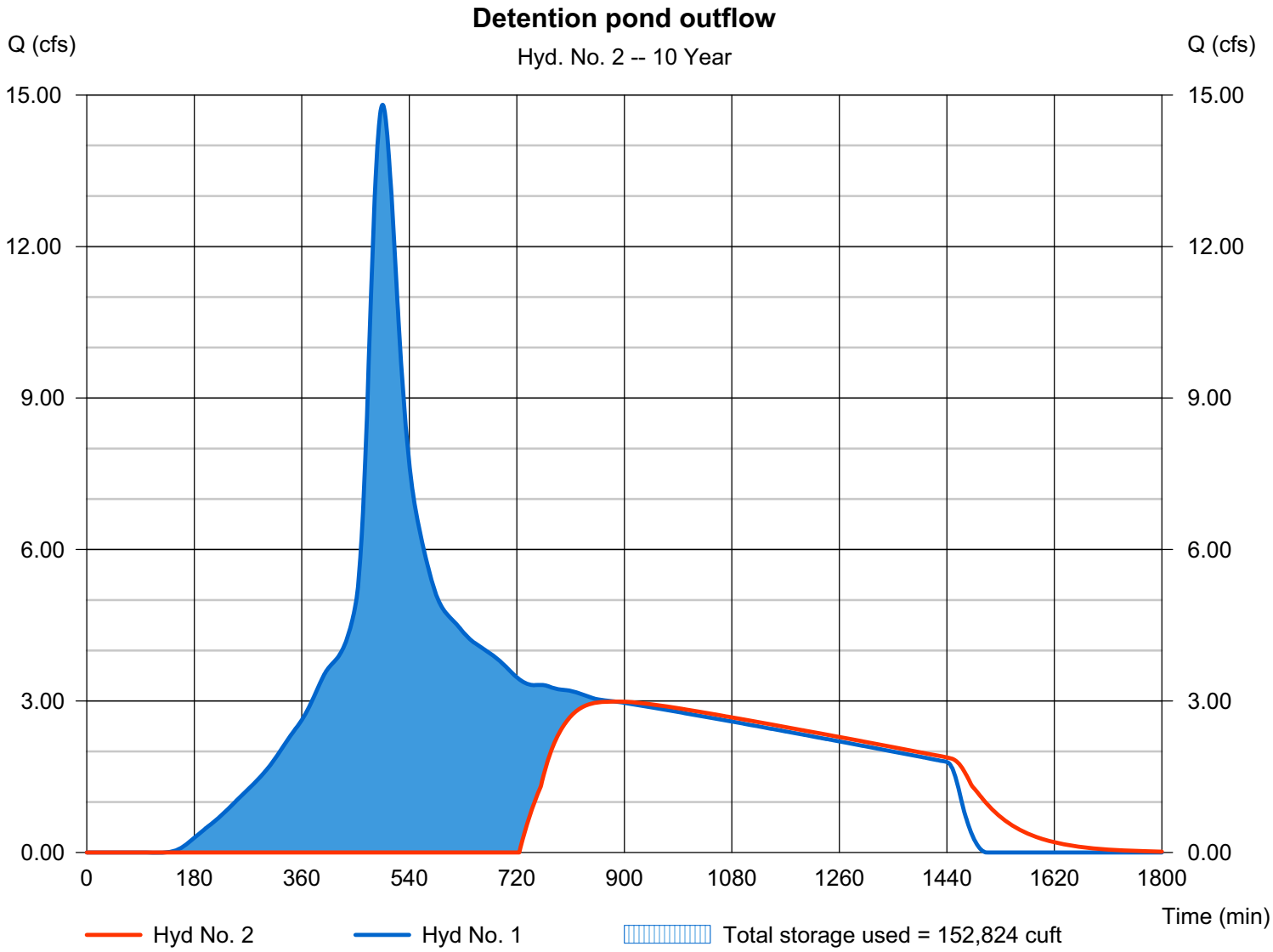
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Hyd. No. 2

Detention pond outflow

Hydrograph type	=	Reservoir	Peak discharge	=	2.990 cfs
Storm frequency	=	10 yrs	Time to peak	=	884 min
Time interval	=	1 min	Hyd. volume	=	114,093 cuft
Inflow hyd. No.	=	1 - Developed site storm event	Max. Elevation	=	62.87 ft
Reservoir name	=	Detention Pond	Max. Storage	=	152,824 cuft

Storage Indication method used.



Pond Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Pond No. 1 - Detention Pond

Pond Data

Contours - User-defined contour areas. Average end area method used for volume calculation. Begining Elevation = 59.00 ft

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	59.00	10	0	0
1.00	60.00	24,253	12,132	12,132
1.70	60.70	46,955	24,923	37,054
2.00	61.00	48,669	14,344	51,398
3.00	62.00	54,448	51,559	102,956
4.00	63.00	60,328	57,388	160,344
5.00	64.00	66,309	63,319	223,663

Culvert / Orifice Structures

	[A]	[B]	[C]	[PrfRsr]
Rise (in)	= 24.00	0.00	0.00	0.00
Span (in)	= 24.00	0.00	0.00	0.00
No. Barrels	= 1	1	0	0
Invert El. (ft)	= 59.10	0.00	0.00	0.00
Length (ft)	= 170.00	0.00	0.00	0.00
Slope (%)	= 0.23	0.00	0.00	n/a
N-Value	= .013	.013	.013	n/a
Orifice Coeff.	= 0.60	0.60	0.60	0.60
Multi-Stage	= n/a	No	No	No

Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 12.56	30.00	0.00	0.00
Crest El. (ft)	= 62.70	63.20	0.00	0.00
Weir Coeff.	= 3.33	2.60	3.33	3.33
Weir Type	= Riser	Broad	---	---
Multi-Stage	= Yes	No	No	No

Exfil.(in/hr) = 0.000 (by Wet area)
TW Elev. (ft) = 61.20

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0	59.00	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
0.10	1,213	59.10	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
0.20	2,426	59.20	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
0.30	3,639	59.30	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
0.40	4,853	59.40	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
0.50	6,066	59.50	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
0.60	7,279	59.60	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
0.70	8,492	59.70	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
0.80	9,705	59.80	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
0.90	10,918	59.90	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
1.00	12,132	60.00	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
1.07	14,624	60.07	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
1.14	17,116	60.14	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
1.21	19,608	60.21	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
1.28	22,101	60.28	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
1.35	24,593	60.35	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
1.42	27,085	60.42	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
1.49	29,577	60.49	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
1.56	32,070	60.56	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
1.63	34,562	60.63	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
1.70	37,054	60.70	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
1.73	38,489	60.73	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
1.76	39,923	60.76	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
1.79	41,357	60.79	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
1.82	42,792	60.82	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
1.85	44,226	60.85	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
1.88	45,660	60.88	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
1.91	47,095	60.91	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
1.94	48,529	60.94	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
1.97	49,964	60.97	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
2.00	51,398	61.00	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
2.10	56,554	61.10	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
2.20	61,710	61.20	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
2.30	66,865	61.30	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
2.40	72,021	61.40	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
2.50	77,177	61.50	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
2.60	82,333	61.60	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
2.70	87,489	61.70	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000

Continues on next page...

Detention Pond

Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
2.80	92,645	61.80	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
2.90	97,801	61.90	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
3.00	102,956	62.00	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
3.10	108,695	62.10	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
3.20	114,434	62.20	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
3.30	120,173	62.30	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
3.40	125,912	62.40	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
3.50	131,650	62.50	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
3.60	137,389	62.60	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
3.70	143,128	62.70	0.00	---	---	---	0.00	0.00	---	---	---	---	0.000
3.80	148,867	62.80	1.33 oc	---	---	---	1.32	0.00	---	---	---	---	1.322
3.90	154,606	62.90	3.74 oc	---	---	---	3.74	0.00	---	---	---	---	3.741
4.00	160,344	63.00	6.87 oc	---	---	---	6.87	0.00	---	---	---	---	6.872
4.10	166,676	63.10	10.58 oc	---	---	---	10.58	0.00	---	---	---	---	10.58
4.20	173,008	63.20	14.79 oc	---	---	---	14.79	0.00	---	---	---	---	14.79
4.30	179,340	63.30	17.49 oc	---	---	---	17.49 s	2.47	---	---	---	---	19.96
4.40	185,672	63.40	18.56 oc	---	---	---	18.56 s	6.98	---	---	---	---	25.54
4.50	192,004	63.50	19.35 oc	---	---	---	19.34 s	12.82	---	---	---	---	32.16
4.60	198,336	63.60	19.99 oc	---	---	---	19.99 s	19.73	---	---	---	---	39.72
4.70	204,667	63.70	20.56 oc	---	---	---	20.56 s	27.58	---	---	---	---	48.13
4.80	210,999	63.80	21.08 oc	---	---	---	21.07 s	36.25	---	---	---	---	57.32
4.90	217,331	63.90	21.56 oc	---	---	---	21.55 s	45.68	---	---	---	---	67.24
5.00	223,663	64.00	22.01 oc	---	---	---	22.00 s	55.81	---	---	---	---	77.81

...End

Hydrograph Summary Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	SCS Runoff	23.03	1	495	397,003	------	------	------	Developed site storm event
2	Reservoir	7.458	1	589	253,870	1	63.02	161,345	Detention pond outflow

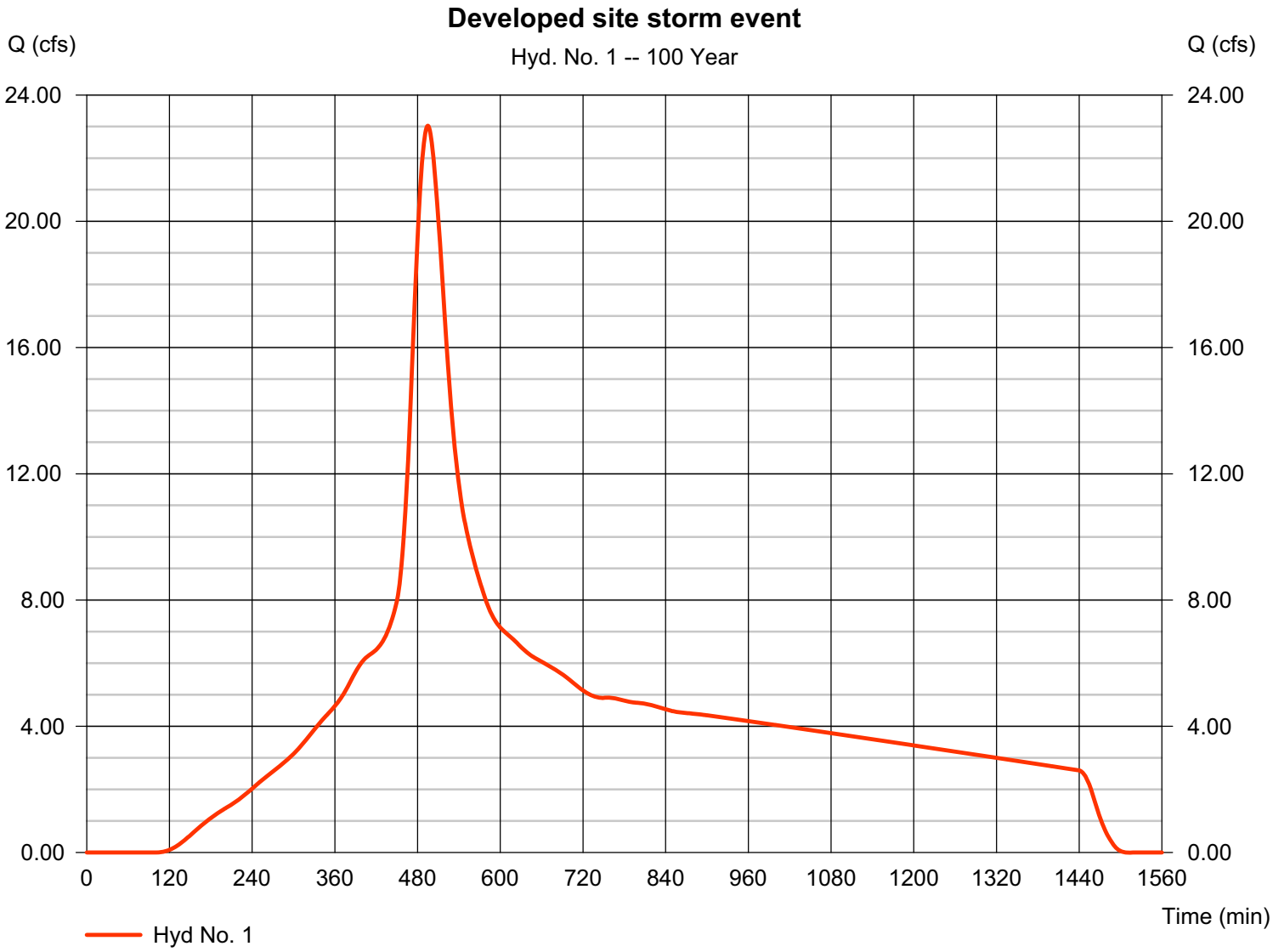
Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Hyd. No. 1

Developed site storm event

Hydrograph type	=	SCS Runoff	Peak discharge	=	23.03 cfs
Storm frequency	=	100 yrs	Time to peak	=	495 min
Time interval	=	1 min	Hyd. volume	=	397,003 cuft
Drainage area	=	25.500 ac	Curve number	=	91
Basin Slope	=	0.0 %	Hydraulic length	=	0 ft
Tc method	=	TR55	Time of conc. (Tc)	=	34.00 min
Total precip.	=	5.30 in	Distribution	=	Type IA
Storm duration	=	24 hrs	Shape factor	=	400



Hydrograph Report

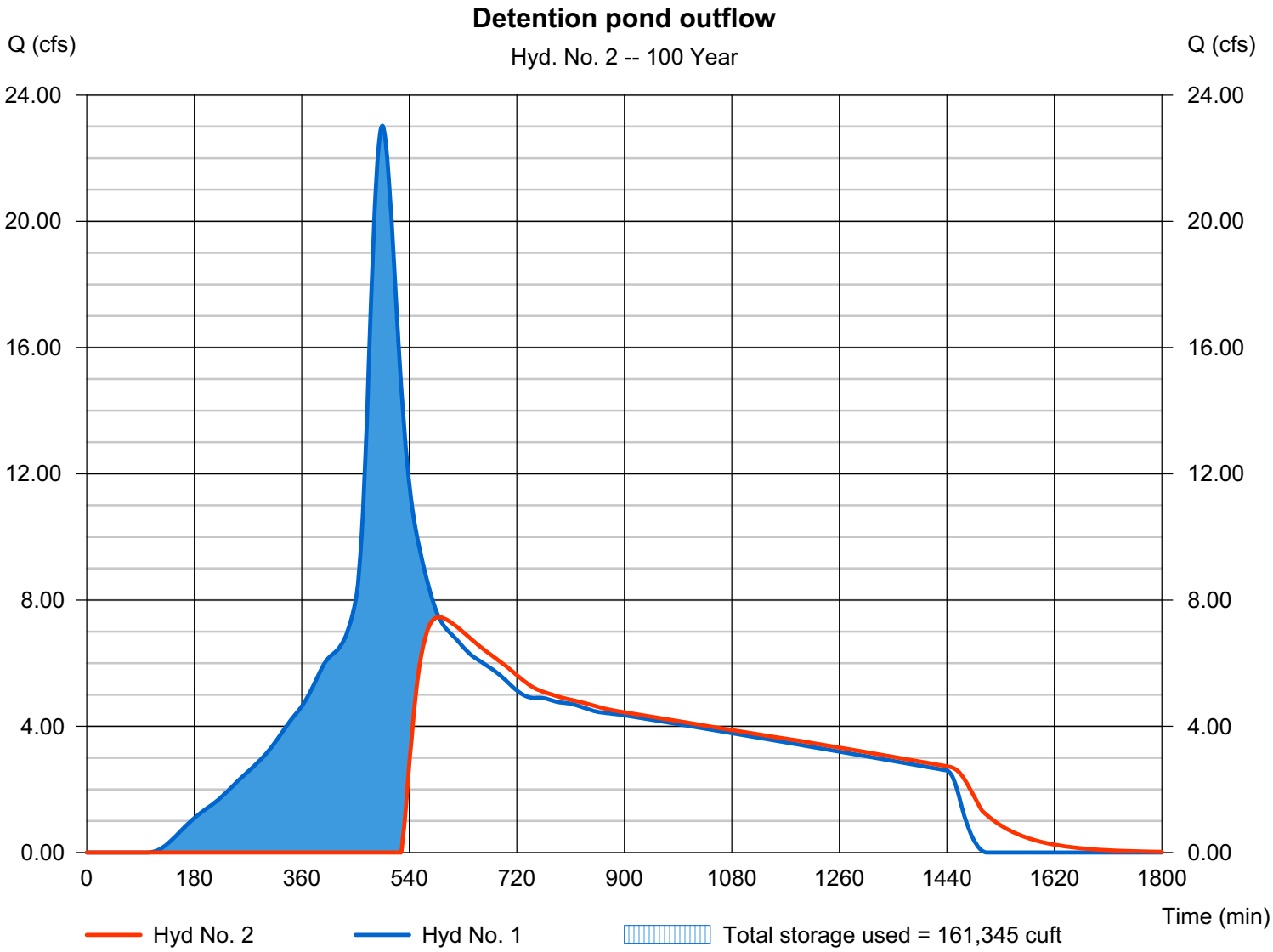
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Hyd. No. 2

Detention pond outflow

Hydrograph type	=	Reservoir	Peak discharge	=	7.458 cfs
Storm frequency	=	100 yrs	Time to peak	=	589 min
Time interval	=	1 min	Hyd. volume	=	253,870 cuft
Inflow hyd. No.	=	1 - Developed site storm event	Max. Elevation	=	63.02 ft
Reservoir name	=	Detention Pond	Max. Storage	=	161,345 cuft

Storage Indication method used.



Hydraflow Rainfall Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Return Period (Yrs)	Intensity-Duration-Frequency Equation Coefficients (FHA)			
	B	D	E	(N/A)
1	0.0000	0.0000	0.0000	--------
2	6.1078	0.1000	0.5625	--------
3	0.0000	0.0000	0.0000	--------
5	8.7423	0.3000	0.5773	--------
10	9.7582	0.1000	0.5661	--------
25	11.5209	0.1000	0.5690	--------
50	12.8436	0.1000	0.5707	--------
100	14.8890	0.3000	0.5856	--------

File name: Vacaville_ISO_22.IDF

Intensity = B / (Tc + D)^E

Return Period (Yrs)	Intensity Values (in/hr)											
	5 min	10	15	20	25	30	35	40	45	50	55	60
1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	2.44	1.66	1.33	1.13	1.00	0.90	0.83	0.77	0.72	0.68	0.64	0.61
3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5	3.34	2.27	1.81	1.54	1.35	1.22	1.12	1.03	0.97	0.91	0.86	0.82
10	3.88	2.63	2.10	1.78	1.57	1.42	1.30	1.21	1.13	1.06	1.01	0.96
25	4.56	3.09	2.46	2.09	1.84	1.66	1.52	1.41	1.32	1.24	1.18	1.12
50	5.07	3.43	2.73	2.32	2.04	1.84	1.69	1.56	1.46	1.38	1.30	1.24
100	5.61	3.80	3.01	2.55	2.24	2.02	1.85	1.71	1.60	1.50	1.42	1.35

Tc = time in minutes. Values may exceed 60.

Precip. file name: Sample.pcp

Storm Distribution	Rainfall Precipitation Table (in)							
	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr
SCS 24-hour	0.00	2.39	0.00	3.20	3.74	4.39	4.85	5.30
SCS 6-Hr	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-1st	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-2nd	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-3rd	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-4th	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-Indy	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Custom	0.00	2.39	0.00	3.20	3.74	4.39	4.85	5.30

Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Hyd. No. 1

Developed site storm event

Hydrograph type	= SCS Runoff	Peak discharge	= 14.81 cfs
Storm frequency	= 10 yrs	Time to peak	= 495 min
Time interval	= 1 min	Hyd. volume	= 257,225 cuft
Drainage area	= 25.500 ac	Curve number	= 91
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 34.0 min
Total precip.	= 3.74 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 400

Hydrograph Discharge Table

(Printed values >= 1.00% of Qp.)

Time -- Outflow (min cfs)		Time -- Outflow (min cfs)		Time -- Outflow (min cfs)		Time -- Outflow (min cfs)	
165	0.148	204	0.526	243	0.938	282	1.390
166	0.157	205	0.535	244	0.950	283	1.403
167	0.166	206	0.544	245	0.962	284	1.415
168	0.175	207	0.553	246	0.974	285	1.427
169	0.184	208	0.563	247	0.986	286	1.439
170	0.193	209	0.572	248	0.998	287	1.452
171	0.202	210	0.581	249	1.009	288	1.464
172	0.212	211	0.591	250	1.021	289	1.477
173	0.221	212	0.600	251	1.033	290	1.490
174	0.231	213	0.610	252	1.045	291	1.503
175	0.241	214	0.619	253	1.056	292	1.516
176	0.251	215	0.629	254	1.068	293	1.529
177	0.260	216	0.639	255	1.079	294	1.542
178	0.270	217	0.649	256	1.091	295	1.555
179	0.280	218	0.659	257	1.103	296	1.569
180	0.291	219	0.669	258	1.114	297	1.582
181	0.301	220	0.679	259	1.125	298	1.596
182	0.311	221	0.689	260	1.137	299	1.610
183	0.321	222	0.699	261	1.148	300	1.624
184	0.331	223	0.710	262	1.159	301	1.638
185	0.341	224	0.720	263	1.171	302	1.652
186	0.351	225	0.731	264	1.182	303	1.667
187	0.361	226	0.742	265	1.193	304	1.682
188	0.371	227	0.753	266	1.205	305	1.696
189	0.382	228	0.764	267	1.216	306	1.712
190	0.392	229	0.775	268	1.227	307	1.727
191	0.401	230	0.786	269	1.239	308	1.742
192	0.411	231	0.797	270	1.250	309	1.758
193	0.421	232	0.809	271	1.262	310	1.774
194	0.431	233	0.821	272	1.273	311	1.790
195	0.441	234	0.832	273	1.285	312	1.806
196	0.450	235	0.844	274	1.296	313	1.822
197	0.460	236	0.855	275	1.308	314	1.839
198	0.469	237	0.867	276	1.319	315	1.856
199	0.479	238	0.879	277	1.331	316	1.873
200	0.488	239	0.891	278	1.343	317	1.890
201	0.498	240	0.903	279	1.355	318	1.907
202	0.507	241	0.915	280	1.367	319	1.924
203	0.516	242	0.927	281	1.378	320	1.941

Continues on next page...

Hydrograph Discharge Table

Time (min	-- Outflow cfs)	Time (min	-- Outflow cfs)	Time (min	-- Outflow cfs)	Time (min	-- Outflow cfs)
321	1.959	377	2.995	433	4.148	489	14.38
322	1.977	378	3.021	434	4.178	490	14.50
323	1.994	379	3.048	435	4.211	491	14.61
324	2.012	380	3.074	436	4.245	492	14.69
325	2.030	381	3.101	437	4.280	493	14.75
326	2.048	382	3.129	438	4.317	494	14.79
327	2.066	383	3.156	439	4.356	495	14.81 <<
328	2.084	384	3.183	440	4.396	496	14.80
329	2.102	385	3.210	441	4.438	497	14.78
330	2.120	386	3.238	442	4.482	498	14.73
331	2.138	387	3.265	443	4.528	499	14.66
332	2.155	388	3.292	444	4.576	500	14.57
333	2.173	389	3.318	445	4.625	501	14.46
334	2.191	390	3.345	446	4.676	502	14.34
335	2.208	391	3.371	447	4.730	503	14.21
336	2.226	392	3.397	448	4.785	504	14.07
337	2.243	393	3.422	449	4.843	505	13.92
338	2.260	394	3.446	450	4.902	506	13.76
339	2.277	395	3.469	451	4.973	507	13.59
340	2.294	396	3.492	452	5.057	508	13.41
341	2.311	397	3.513	453	5.154	509	13.23
342	2.328	398	3.534	454	5.264	510	13.04
343	2.345	399	3.555	455	5.388	511	12.84
344	2.361	400	3.574	456	5.526	512	12.64
345	2.378	401	3.593	457	5.678	513	12.44
346	2.394	402	3.610	458	5.844	514	12.23
347	2.411	403	3.628	459	6.025	515	12.02
348	2.427	404	3.644	460	6.220	516	11.81
349	2.443	405	3.659	461	6.430	517	11.59
350	2.460	406	3.674	462	6.654	518	11.37
351	2.476	407	3.689	463	6.894	519	11.15
352	2.492	408	3.702	464	7.147	520	10.94
353	2.508	409	3.715	465	7.416	521	10.73
354	2.525	410	3.727	466	7.699	522	10.52
355	2.542	411	3.739	467	7.997	523	10.32
356	2.559	412	3.751	468	8.309	524	10.12
357	2.576	413	3.763	469	8.635	525	9.930
358	2.593	414	3.776	470	8.976	526	9.743
359	2.610	415	3.788	471	9.330	527	9.561
360	2.628	416	3.802	472	9.683	528	9.386
361	2.646	417	3.815	473	10.03	529	9.217
362	2.664	418	3.830	474	10.38	530	9.054
363	2.683	419	3.845	475	10.73	531	8.898
364	2.702	420	3.860	476	11.07	532	8.744
365	2.721	421	3.877	477	11.40	533	8.595
366	2.742	422	3.894	478	11.73	534	8.451
367	2.762	423	3.911	479	12.05	535	8.312
368	2.783	424	3.930	480	12.36	536	8.178
369	2.805	425	3.950	481	12.65	537	8.049
370	2.827	426	3.971	482	12.93	538	7.926
371	2.850	427	3.992	483	13.20	539	7.808
372	2.873	428	4.015	484	13.44	540	7.695
373	2.896	429	4.039	485	13.67	541	7.586
374	2.920	430	4.064	486	13.88	542	7.482
375	2.945	431	4.091	487	14.06	543	7.384
376	2.970	432	4.118	488	14.23	544	7.291

Continues on next page...

Hydrograph Discharge Table

Time (min	Outflow cfs)	Time (min	Outflow cfs)	Time (min	Outflow cfs)	Time (min	Outflow cfs)
545	7.203	601	4.749	657	4.090	713	3.544
546	7.120	602	4.735	658	4.082	714	3.532
547	7.043	603	4.721	659	4.074	715	3.521
548	6.970	604	4.708	660	4.066	716	3.510
549	6.899	605	4.695	661	4.058	717	3.500
550	6.831	606	4.682	662	4.050	718	3.489
551	6.764	607	4.670	663	4.042	719	3.479
552	6.698	608	4.657	664	4.033	720	3.469
553	6.634	609	4.644	665	4.025	721	3.459
554	6.572	610	4.632	666	4.017	722	3.449
555	6.510	611	4.619	667	4.009	723	3.440
556	6.450	612	4.607	668	4.000	724	3.431
557	6.392	613	4.594	669	3.993	725	3.422
558	6.334	614	4.582	670	3.985	726	3.414
559	6.277	615	4.570	671	3.977	727	3.405
560	6.221	616	4.558	672	3.970	728	3.398
561	6.166	617	4.545	673	3.962	729	3.390
562	6.114	618	4.533	674	3.954	730	3.383
563	6.062	619	4.521	675	3.945	731	3.376
564	6.012	620	4.509	676	3.937	732	3.369
565	5.962	621	4.497	677	3.929	733	3.363
566	5.913	622	4.482	678	3.920	734	3.357
567	5.865	623	4.467	679	3.912	735	3.352
568	5.817	624	4.452	680	3.903	736	3.347
569	5.770	625	4.437	681	3.894	737	3.342
570	5.723	626	4.423	682	3.885	738	3.337
571	5.675	627	4.408	683	3.876	739	3.333
572	5.628	628	4.394	684	3.866	740	3.330
573	5.582	629	4.380	685	3.857	741	3.326
574	5.536	630	4.366	686	3.848	742	3.324
575	5.491	631	4.352	687	3.838	743	3.321
576	5.447	632	4.339	688	3.828	744	3.319
577	5.403	633	4.326	689	3.818	745	3.317
578	5.360	634	4.313	690	3.808	746	3.316
579	5.320	635	4.300	691	3.798	747	3.315
580	5.280	636	4.288	692	3.788	748	3.315
581	5.242	637	4.276	693	3.777	749	3.315
582	5.206	638	4.265	694	3.766	750	3.315
583	5.170	639	4.253	695	3.755	751	3.315
584	5.136	640	4.241	696	3.744	752	3.316
585	5.104	641	4.230	697	3.733	753	3.317
586	5.072	642	4.219	698	3.721	754	3.317
587	5.042	643	4.208	699	3.709	755	3.318
588	5.013	644	4.198	700	3.698	756	3.318
589	4.986	645	4.188	701	3.686	757	3.319
590	4.959	646	4.179	702	3.674	758	3.319
591	4.934	647	4.170	703	3.662	759	3.319
592	4.912	648	4.161	704	3.651	760	3.319
593	4.892	649	4.153	705	3.639	761	3.319
594	4.872	650	4.144	706	3.627	762	3.318
595	4.852	651	4.137	707	3.615	763	3.318
596	4.833	652	4.129	708	3.603	764	3.317
597	4.815	653	4.121	709	3.591	765	3.315
598	4.797	654	4.113	710	3.579	766	3.314
599	4.780	655	4.105	711	3.567	767	3.312
600	4.763	656	4.097	712	3.555	768	3.309

Continues on next page...

Hydrograph Discharge Table

Time -- Outflow (min cfs)		Time -- Outflow (min cfs)		Time -- Outflow (min cfs)		Time -- Outflow (min cfs)	
769	3.306	825	3.151	881	2.994	937	2.891
770	3.303	826	3.147	882	2.993	938	2.889
771	3.299	827	3.143	883	2.991	939	2.887
772	3.295	828	3.139	884	2.990	940	2.885
773	3.291	829	3.135	885	2.988	941	2.883
774	3.286	830	3.130	886	2.987	942	2.881
775	3.282	831	3.126	887	2.986	943	2.879
776	3.278	832	3.122	888	2.984	944	2.877
777	3.274	833	3.117	889	2.983	945	2.874
778	3.270	834	3.113	890	2.981	946	2.872
779	3.266	835	3.109	891	2.980	947	2.870
780	3.262	836	3.104	892	2.978	948	2.868
781	3.258	837	3.100	893	2.976	949	2.866
782	3.254	838	3.095	894	2.975	950	2.864
783	3.251	839	3.091	895	2.973	951	2.862
784	3.247	840	3.087	896	2.971	952	2.860
785	3.244	841	3.082	897	2.970	953	2.858
786	3.242	842	3.078	898	2.968	954	2.856
787	3.239	843	3.074	899	2.966	955	2.854
788	3.236	844	3.070	900	2.964	956	2.852
789	3.234	845	3.066	901	2.962	957	2.850
790	3.232	846	3.062	902	2.961	958	2.848
791	3.230	847	3.058	903	2.959	959	2.846
792	3.228	848	3.054	904	2.957	960	2.844
793	3.227	849	3.051	905	2.955	961	2.842
794	3.225	850	3.048	906	2.953	962	2.840
795	3.224	851	3.044	907	2.951	963	2.838
796	3.223	852	3.041	908	2.949	964	2.836
797	3.222	853	3.039	909	2.947	965	2.834
798	3.221	854	3.036	910	2.945	966	2.832
799	3.220	855	3.034	911	2.943	967	2.830
800	3.219	856	3.031	912	2.941	968	2.828
801	3.218	857	3.029	913	2.939	969	2.825
802	3.217	858	3.027	914	2.937	970	2.823
803	3.216	859	3.025	915	2.935	971	2.821
804	3.214	860	3.024	916	2.933	972	2.819
805	3.212	861	3.022	917	2.931	973	2.817
806	3.210	862	3.020	918	2.929	974	2.815
807	3.208	863	3.019	919	2.927	975	2.813
808	3.206	864	3.017	920	2.925	976	2.811
809	3.203	865	3.016	921	2.923	977	2.809
810	3.201	866	3.014	922	2.921	978	2.807
811	3.198	867	3.013	923	2.919	979	2.805
812	3.195	868	3.011	924	2.917	980	2.803
813	3.192	869	3.010	925	2.915	981	2.801
814	3.189	870	3.009	926	2.913	982	2.799
815	3.186	871	3.007	927	2.911	983	2.797
816	3.183	872	3.006	928	2.909	984	2.795
817	3.180	873	3.005	929	2.907	985	2.793
818	3.176	874	3.003	930	2.905	986	2.790
819	3.173	875	3.002	931	2.903	987	2.788
820	3.170	876	3.001	932	2.901	988	2.786
821	3.166	877	2.999	933	2.899	989	2.784
822	3.163	878	2.998	934	2.897	990	2.782
823	3.159	879	2.997	935	2.895	991	2.780
824	3.155	880	2.995	936	2.893	992	2.778

Continues on next page...

Hydrograph Discharge Table

Time -- Outflow (min	cfs)	Time -- Outflow (min	cfs)	Time -- Outflow (min	cfs)	Time -- Outflow (min	cfs)
993	2.776	1049	2.659	1105	2.539	1161	2.418
994	2.774	1050	2.657	1106	2.537	1162	2.416
995	2.772	1051	2.654	1107	2.535	1163	2.414
996	2.770	1052	2.652	1108	2.533	1164	2.411
997	2.768	1053	2.650	1109	2.531	1165	2.409
998	2.766	1054	2.648	1110	2.528	1166	2.407
999	2.764	1055	2.646	1111	2.526	1167	2.405
1000	2.761	1056	2.644	1112	2.524	1168	2.403
1001	2.759	1057	2.642	1113	2.522	1169	2.400
1002	2.757	1058	2.640	1114	2.520	1170	2.398
1003	2.755	1059	2.637	1115	2.518	1171	2.396
1004	2.753	1060	2.635	1116	2.515	1172	2.394
1005	2.751	1061	2.633	1117	2.513	1173	2.392
1006	2.749	1062	2.631	1118	2.511	1174	2.389
1007	2.747	1063	2.629	1119	2.509	1175	2.387
1008	2.745	1064	2.627	1120	2.507	1176	2.385
1009	2.743	1065	2.625	1121	2.505	1177	2.383
1010	2.741	1066	2.623	1122	2.503	1178	2.381
1011	2.739	1067	2.620	1123	2.500	1179	2.379
1012	2.736	1068	2.618	1124	2.498	1180	2.376
1013	2.734	1069	2.616	1125	2.496	1181	2.374
1014	2.732	1070	2.614	1126	2.494	1182	2.372
1015	2.730	1071	2.612	1127	2.492	1183	2.370
1016	2.728	1072	2.610	1128	2.490	1184	2.368
1017	2.726	1073	2.608	1129	2.487	1185	2.365
1018	2.724	1074	2.606	1130	2.485	1186	2.363
1019	2.722	1075	2.603	1131	2.483	1187	2.361
1020	2.720	1076	2.601	1132	2.481	1188	2.359
1021	2.718	1077	2.599	1133	2.479	1189	2.357
1022	2.716	1078	2.597	1134	2.477	1190	2.354
1023	2.713	1079	2.595	1135	2.474	1191	2.352
1024	2.711	1080	2.593	1136	2.472	1192	2.350
1025	2.709	1081	2.591	1137	2.470	1193	2.348
1026	2.707	1082	2.588	1138	2.468	1194	2.346
1027	2.705	1083	2.586	1139	2.466	1195	2.343
1028	2.703	1084	2.584	1140	2.464	1196	2.341
1029	2.701	1085	2.582	1141	2.461	1197	2.339
1030	2.699	1086	2.580	1142	2.459	1198	2.337
1031	2.697	1087	2.578	1143	2.457	1199	2.335
1032	2.695	1088	2.576	1144	2.455	1200	2.332
1033	2.692	1089	2.574	1145	2.453	1201	2.330
1034	2.690	1090	2.571	1146	2.451	1202	2.328
1035	2.688	1091	2.569	1147	2.448	1203	2.326
1036	2.686	1092	2.567	1148	2.446	1204	2.324
1037	2.684	1093	2.565	1149	2.444	1205	2.321
1038	2.682	1094	2.563	1150	2.442	1206	2.319
1039	2.680	1095	2.561	1151	2.440	1207	2.317
1040	2.678	1096	2.559	1152	2.437	1208	2.315
1041	2.676	1097	2.556	1153	2.435	1209	2.313
1042	2.673	1098	2.554	1154	2.433	1210	2.310
1043	2.671	1099	2.552	1155	2.431	1211	2.308
1044	2.669	1100	2.550	1156	2.429	1212	2.306
1045	2.667	1101	2.548	1157	2.427	1213	2.304
1046	2.665	1102	2.546	1158	2.424	1214	2.302
1047	2.663	1103	2.543	1159	2.422	1215	2.299
1048	2.661	1104	2.541	1160	2.420	1216	2.297

Continues on next page...

Hydrograph Discharge Table

Time (min	Outflow cfs)	Time (min	Outflow cfs)	Time (min	Outflow cfs)	Time (min	Outflow cfs)
1217	2.295	1273	2.171	1329	2.046	1385	1.919
1218	2.293	1274	2.169	1330	2.043	1386	1.917
1219	2.291	1275	2.166	1331	2.041	1387	1.915
1220	2.288	1276	2.164	1332	2.039	1388	1.912
1221	2.286	1277	2.162	1333	2.037	1389	1.910
1222	2.284	1278	2.160	1334	2.034	1390	1.908
1223	2.282	1279	2.157	1335	2.032	1391	1.906
1224	2.280	1280	2.155	1336	2.030	1392	1.903
1225	2.277	1281	2.153	1337	2.028	1393	1.901
1226	2.275	1282	2.151	1338	2.025	1394	1.899
1227	2.273	1283	2.149	1339	2.023	1395	1.897
1228	2.271	1284	2.146	1340	2.021	1396	1.894
1229	2.269	1285	2.144	1341	2.019	1397	1.892
1230	2.266	1286	2.142	1342	2.016	1398	1.890
1231	2.264	1287	2.140	1343	2.014	1399	1.888
1232	2.262	1288	2.137	1344	2.012	1400	1.885
1233	2.260	1289	2.135	1345	2.010	1401	1.883
1234	2.257	1290	2.133	1346	2.007	1402	1.881
1235	2.255	1291	2.131	1347	2.005	1403	1.878
1236	2.253	1292	2.128	1348	2.003	1404	1.876
1237	2.251	1293	2.126	1349	2.001	1405	1.874
1238	2.249	1294	2.124	1350	1.998	1406	1.872
1239	2.246	1295	2.122	1351	1.996	1407	1.869
1240	2.244	1296	2.120	1352	1.994	1408	1.867
1241	2.242	1297	2.117	1353	1.992	1409	1.865
1242	2.240	1298	2.115	1354	1.989	1410	1.863
1243	2.238	1299	2.113	1355	1.987	1411	1.860
1244	2.235	1300	2.111	1356	1.985	1412	1.858
1245	2.233	1301	2.108	1357	1.982	1413	1.856
1246	2.231	1302	2.106	1358	1.980	1414	1.853
1247	2.229	1303	2.104	1359	1.978	1415	1.851
1248	2.226	1304	2.102	1360	1.976	1416	1.849
1249	2.224	1305	2.099	1361	1.973	1417	1.847
1250	2.222	1306	2.097	1362	1.971	1418	1.844
1251	2.220	1307	2.095	1363	1.969	1419	1.842
1252	2.218	1308	2.093	1364	1.967	1420	1.840
1253	2.215	1309	2.090	1365	1.964	1421	1.838
1254	2.213	1310	2.088	1366	1.962	1422	1.835
1255	2.211	1311	2.086	1367	1.960	1423	1.833
1256	2.209	1312	2.084	1368	1.958	1424	1.831
1257	2.206	1313	2.081	1369	1.955	1425	1.828
1258	2.204	1314	2.079	1370	1.953	1426	1.826
1259	2.202	1315	2.077	1371	1.951	1427	1.824
1260	2.200	1316	2.075	1372	1.949	1428	1.822
1261	2.198	1317	2.072	1373	1.946	1429	1.819
1262	2.195	1318	2.070	1374	1.944	1430	1.817
1263	2.193	1319	2.068	1375	1.942	1431	1.815
1264	2.191	1320	2.066	1376	1.940	1432	1.813
1265	2.189	1321	2.063	1377	1.937	1433	1.810
1266	2.186	1322	2.061	1378	1.935	1434	1.808
1267	2.184	1323	2.059	1379	1.933	1435	1.806
1268	2.182	1324	2.057	1380	1.931	1436	1.803
1269	2.180	1325	2.055	1381	1.928	1437	1.801
1270	2.178	1326	2.052	1382	1.926	1438	1.799
1271	2.175	1327	2.050	1383	1.924	1439	1.797
1272	2.173	1328	2.048	1384	1.921	1440	1.794

Continues on next page...

Developed site storm event

Hydrograph Discharge Table

Time -- (min	Outflow cfs)
1441	1.790
1442	1.783
1443	1.773
1444	1.761
1445	1.747
1446	1.730
1447	1.711
1448	1.689
1449	1.665
1450	1.639
1451	1.610
1452	1.579
1453	1.546
1454	1.510
1455	1.472
1456	1.431
1457	1.388
1458	1.343
1459	1.295
1460	1.245
1461	1.193
1462	1.142
1463	1.091
1464	1.042
1465	0.995
1466	0.948
1467	0.902
1468	0.858
1469	0.815
1470	0.773
1471	0.732
1472	0.692
1473	0.653
1474	0.616
1475	0.579
1476	0.544
1477	0.510
1478	0.476
1479	0.445
1480	0.414
1481	0.384
1482	0.355
1483	0.328
1484	0.302
1485	0.276
1486	0.252
1487	0.229
1488	0.207
1489	0.186
1490	0.167
1491	0.148

...End

Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Hyd. No. 2

Detention pond outflow

Hydrograph type	= Reservoir	Peak discharge	= 2.737 cfs
Storm frequency	= 10 yrs	Time to peak	= 1012 min
Time interval	= 1 min	Hyd. volume	= 84,215 cuft
Inflow hyd. No.	= 1 - Developed site storm event	Reservoir name	= Detention Pond
Max. Elevation	= 63.31 ft	Max. Storage	= 179,719 cuft

Storage Indication method used.

Hydrograph Discharge Table

(Printed values >= 1.00% of Qp.)

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
881	2.994	63.20	-----	-----	-----	-----	0.084	-----	-----	-----	-----	0.084
882	2.993	63.21	-----	-----	-----	-----	0.151	-----	-----	-----	-----	0.151
883	2.991	63.21	-----	-----	-----	-----	0.216	-----	-----	-----	-----	0.216
884	2.990	63.21	-----	-----	-----	-----	0.280	-----	-----	-----	-----	0.281
885	2.988	63.21	-----	-----	-----	-----	0.343	-----	-----	-----	-----	0.343
886	2.987	63.22	-----	-----	-----	-----	0.404	-----	-----	-----	-----	0.404
887	2.986	63.22	-----	-----	-----	-----	0.464	-----	-----	-----	-----	0.464
888	2.984	63.22	-----	-----	-----	-----	0.522	-----	-----	-----	-----	0.522
889	2.983	63.22	-----	-----	-----	-----	0.579	-----	-----	-----	-----	0.579
890	2.981	63.23	-----	-----	-----	-----	0.634	-----	-----	-----	-----	0.634
891	2.980	63.23	-----	-----	-----	-----	0.689	-----	-----	-----	-----	0.689
892	2.978	63.23	-----	-----	-----	-----	0.742	-----	-----	-----	-----	0.742
893	2.976	63.23	-----	-----	-----	-----	0.793	-----	-----	-----	-----	0.793
894	2.975	63.23	-----	-----	-----	-----	0.844	-----	-----	-----	-----	0.844
895	2.973	63.24	-----	-----	-----	-----	0.893	-----	-----	-----	-----	0.893
896	2.971	63.24	-----	-----	-----	-----	0.941	-----	-----	-----	-----	0.941
897	2.970	63.24	-----	-----	-----	-----	0.988	-----	-----	-----	-----	0.988
898	2.968	63.24	-----	-----	-----	-----	1.034	-----	-----	-----	-----	1.034
899	2.966	63.24	-----	-----	-----	-----	1.078	-----	-----	-----	-----	1.078
900	2.964	63.25	-----	-----	-----	-----	1.122	-----	-----	-----	-----	1.122
901	2.962	63.25	-----	-----	-----	-----	1.164	-----	-----	-----	-----	1.164
902	2.961	63.25	-----	-----	-----	-----	1.206	-----	-----	-----	-----	1.206
903	2.959	63.25	-----	-----	-----	-----	1.246	-----	-----	-----	-----	1.246
904	2.957	63.25	-----	-----	-----	-----	1.286	-----	-----	-----	-----	1.286
905	2.955	63.25	-----	-----	-----	-----	1.325	-----	-----	-----	-----	1.325
906	2.953	63.26	-----	-----	-----	-----	1.362	-----	-----	-----	-----	1.362
907	2.951	63.26	-----	-----	-----	-----	1.399	-----	-----	-----	-----	1.399
908	2.949	63.26	-----	-----	-----	-----	1.435	-----	-----	-----	-----	1.435
909	2.947	63.26	-----	-----	-----	-----	1.470	-----	-----	-----	-----	1.470
910	2.945	63.26	-----	-----	-----	-----	1.504	-----	-----	-----	-----	1.504
911	2.943	63.26	-----	-----	-----	-----	1.537	-----	-----	-----	-----	1.537
912	2.941	63.26	-----	-----	-----	-----	1.570	-----	-----	-----	-----	1.570
913	2.939	63.26	-----	-----	-----	-----	1.601	-----	-----	-----	-----	1.601
914	2.937	63.27	-----	-----	-----	-----	1.632	-----	-----	-----	-----	1.632
915	2.935	63.27	-----	-----	-----	-----	1.662	-----	-----	-----	-----	1.662
916	2.933	63.27	-----	-----	-----	-----	1.692	-----	-----	-----	-----	1.692
917	2.931	63.27	-----	-----	-----	-----	1.720	-----	-----	-----	-----	1.720
918	2.929	63.27	-----	-----	-----	-----	1.748	-----	-----	-----	-----	1.748
919	2.927	63.27	-----	-----	-----	-----	1.775	-----	-----	-----	-----	1.775
920	2.925	63.27	-----	-----	-----	-----	1.802	-----	-----	-----	-----	1.802
921	2.923	63.27	-----	-----	-----	-----	1.828	-----	-----	-----	-----	1.828
922	2.921	63.28	-----	-----	-----	-----	1.853	-----	-----	-----	-----	1.853

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
923	2.919	63.28	-----	-----	-----	-----	1.878	-----	-----	-----	-----	1.878
924	2.917	63.28	-----	-----	-----	-----	1.902	-----	-----	-----	-----	1.902
925	2.915	63.28	-----	-----	-----	-----	1.925	-----	-----	-----	-----	1.925
926	2.913	63.28	-----	-----	-----	-----	1.948	-----	-----	-----	-----	1.948
927	2.911	63.28	-----	-----	-----	-----	1.970	-----	-----	-----	-----	1.970
928	2.909	63.28	-----	-----	-----	-----	1.992	-----	-----	-----	-----	1.992
929	2.907	63.28	-----	-----	-----	-----	2.013	-----	-----	-----	-----	2.013
930	2.905	63.28	-----	-----	-----	-----	2.034	-----	-----	-----	-----	2.034
931	2.903	63.28	-----	-----	-----	-----	2.054	-----	-----	-----	-----	2.054
932	2.901	63.28	-----	-----	-----	-----	2.074	-----	-----	-----	-----	2.074
933	2.899	63.28	-----	-----	-----	-----	2.093	-----	-----	-----	-----	2.093
934	2.897	63.29	-----	-----	-----	-----	2.111	-----	-----	-----	-----	2.111
935	2.895	63.29	-----	-----	-----	-----	2.129	-----	-----	-----	-----	2.129
936	2.893	63.29	-----	-----	-----	-----	2.147	-----	-----	-----	-----	2.147
937	2.891	63.29	-----	-----	-----	-----	2.164	-----	-----	-----	-----	2.164
938	2.889	63.29	-----	-----	-----	-----	2.181	-----	-----	-----	-----	2.181
939	2.887	63.29	-----	-----	-----	-----	2.197	-----	-----	-----	-----	2.197
940	2.885	63.29	-----	-----	-----	-----	2.213	-----	-----	-----	-----	2.213
941	2.883	63.29	-----	-----	-----	-----	2.229	-----	-----	-----	-----	2.229
942	2.881	63.29	-----	-----	-----	-----	2.244	-----	-----	-----	-----	2.244
943	2.879	63.29	-----	-----	-----	-----	2.258	-----	-----	-----	-----	2.258
944	2.877	63.29	-----	-----	-----	-----	2.273	-----	-----	-----	-----	2.273
945	2.874	63.29	-----	-----	-----	-----	2.287	-----	-----	-----	-----	2.287
946	2.872	63.29	-----	-----	-----	-----	2.300	-----	-----	-----	-----	2.300
947	2.870	63.29	-----	-----	-----	-----	2.313	-----	-----	-----	-----	2.313
948	2.868	63.29	-----	-----	-----	-----	2.326	-----	-----	-----	-----	2.326
949	2.866	63.29	-----	-----	-----	-----	2.339	-----	-----	-----	-----	2.339
950	2.864	63.30	-----	-----	-----	-----	2.351	-----	-----	-----	-----	2.351
951	2.862	63.30	-----	-----	-----	-----	2.363	-----	-----	-----	-----	2.363
952	2.860	63.30	-----	-----	-----	-----	2.374	-----	-----	-----	-----	2.374
953	2.858	63.30	-----	-----	-----	-----	2.386	-----	-----	-----	-----	2.386
954	2.856	63.30	-----	-----	-----	-----	2.396	-----	-----	-----	-----	2.396
955	2.854	63.30	-----	-----	-----	-----	2.407	-----	-----	-----	-----	2.407
956	2.852	63.30	-----	-----	-----	-----	2.417	-----	-----	-----	-----	2.417
957	2.850	63.30	-----	-----	-----	-----	2.427	-----	-----	-----	-----	2.427
958	2.848	63.30	-----	-----	-----	-----	2.437	-----	-----	-----	-----	2.437
959	2.846	63.30	-----	-----	-----	-----	2.447	-----	-----	-----	-----	2.447
960	2.844	63.30	-----	-----	-----	-----	2.456	-----	-----	-----	-----	2.456
961	2.842	63.30	-----	-----	-----	-----	2.465	-----	-----	-----	-----	2.465
962	2.840	63.30	-----	-----	-----	-----	2.479	-----	-----	-----	-----	2.479
963	2.838	63.30	-----	-----	-----	-----	2.494	-----	-----	-----	-----	2.494
964	2.836	63.30	-----	-----	-----	-----	2.508	-----	-----	-----	-----	2.508
965	2.834	63.30	-----	-----	-----	-----	2.522	-----	-----	-----	-----	2.522
966	2.832	63.30	-----	-----	-----	-----	2.535	-----	-----	-----	-----	2.535
967	2.830	63.30	-----	-----	-----	-----	2.547	-----	-----	-----	-----	2.547
968	2.828	63.30	-----	-----	-----	-----	2.559	-----	-----	-----	-----	2.559
969	2.825	63.30	-----	-----	-----	-----	2.570	-----	-----	-----	-----	2.570
970	2.823	63.30	-----	-----	-----	-----	2.581	-----	-----	-----	-----	2.581
971	2.821	63.30	-----	-----	-----	-----	2.591	-----	-----	-----	-----	2.591
972	2.819	63.30	-----	-----	-----	-----	2.601	-----	-----	-----	-----	2.601
973	2.817	63.30	-----	-----	-----	-----	2.610	-----	-----	-----	-----	2.610
974	2.815	63.30	-----	-----	-----	-----	2.618	-----	-----	-----	-----	2.618
975	2.813	63.30	-----	-----	-----	-----	2.627	-----	-----	-----	-----	2.627
976	2.811	63.30	-----	-----	-----	-----	2.634	-----	-----	-----	-----	2.634
977	2.809	63.30	-----	-----	-----	-----	2.642	-----	-----	-----	-----	2.642
978	2.807	63.30	-----	-----	-----	-----	2.649	-----	-----	-----	-----	2.649

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
979	2.805	63.30	-----	-----	-----	-----	2.655	-----	-----	-----	-----	2.655
980	2.803	63.30	-----	-----	-----	-----	2.661	-----	-----	-----	-----	2.661
981	2.801	63.30	-----	-----	-----	-----	2.667	-----	-----	-----	-----	2.667
982	2.799	63.30	-----	-----	-----	-----	2.673	-----	-----	-----	-----	2.673
983	2.797	63.30	-----	-----	-----	-----	2.678	-----	-----	-----	-----	2.678
984	2.795	63.30	-----	-----	-----	-----	2.683	-----	-----	-----	-----	2.683
985	2.793	63.30	-----	-----	-----	-----	2.688	-----	-----	-----	-----	2.688
986	2.790	63.31	-----	-----	-----	-----	2.692	-----	-----	-----	-----	2.692
987	2.788	63.31	-----	-----	-----	-----	2.696	-----	-----	-----	-----	2.696
988	2.786	63.31	-----	-----	-----	-----	2.700	-----	-----	-----	-----	2.700
989	2.784	63.31	-----	-----	-----	-----	2.703	-----	-----	-----	-----	2.703
990	2.782	63.31	-----	-----	-----	-----	2.707	-----	-----	-----	-----	2.707
991	2.780	63.31	-----	-----	-----	-----	2.710	-----	-----	-----	-----	2.710
992	2.778	63.31	-----	-----	-----	-----	2.713	-----	-----	-----	-----	2.713
993	2.776	63.31	-----	-----	-----	-----	2.715	-----	-----	-----	-----	2.715
994	2.774	63.31	-----	-----	-----	-----	2.718	-----	-----	-----	-----	2.718
995	2.772	63.31	-----	-----	-----	-----	2.720	-----	-----	-----	-----	2.720
996	2.770	63.31	-----	-----	-----	-----	2.722	-----	-----	-----	-----	2.722
997	2.768	63.31	-----	-----	-----	-----	2.724	-----	-----	-----	-----	2.724
998	2.766	63.31	-----	-----	-----	-----	2.726	-----	-----	-----	-----	2.726
999	2.764	63.31	-----	-----	-----	-----	2.728	-----	-----	-----	-----	2.728
1000	2.761	63.31	-----	-----	-----	-----	2.729	-----	-----	-----	-----	2.729
1001	2.759	63.31	-----	-----	-----	-----	2.730	-----	-----	-----	-----	2.730
1002	2.757	63.31	-----	-----	-----	-----	2.732	-----	-----	-----	-----	2.732
1003	2.755	63.31	-----	-----	-----	-----	2.733	-----	-----	-----	-----	2.733
1004	2.753	63.31	-----	-----	-----	-----	2.734	-----	-----	-----	-----	2.734
1005	2.751	63.31	-----	-----	-----	-----	2.734	-----	-----	-----	-----	2.734
1006	2.749	63.31	-----	-----	-----	-----	2.735	-----	-----	-----	-----	2.735
1007	2.747	63.31	-----	-----	-----	-----	2.736	-----	-----	-----	-----	2.736
1008	2.745	63.31	-----	-----	-----	-----	2.736	-----	-----	-----	-----	2.736
1009	2.743	63.31	-----	-----	-----	-----	2.736	-----	-----	-----	-----	2.736
1010	2.741	63.31	-----	-----	-----	-----	2.736	-----	-----	-----	-----	2.737
1011	2.739	63.31	-----	-----	-----	-----	2.737	-----	-----	-----	-----	2.737
1012	2.736	63.31 <<	-----	-----	-----	-----	2.737	-----	-----	-----	-----	2.737 <<
1013	2.734	63.31	-----	-----	-----	-----	2.737	-----	-----	-----	-----	2.737
1014	2.732	63.31	-----	-----	-----	-----	2.736	-----	-----	-----	-----	2.736
1015	2.730	63.31	-----	-----	-----	-----	2.736	-----	-----	-----	-----	2.736
1016	2.728	63.31	-----	-----	-----	-----	2.736	-----	-----	-----	-----	2.736
1017	2.726	63.31	-----	-----	-----	-----	2.736	-----	-----	-----	-----	2.736
1018	2.724	63.31	-----	-----	-----	-----	2.735	-----	-----	-----	-----	2.735
1019	2.722	63.31	-----	-----	-----	-----	2.735	-----	-----	-----	-----	2.735
1020	2.720	63.31	-----	-----	-----	-----	2.734	-----	-----	-----	-----	2.734
1021	2.718	63.31	-----	-----	-----	-----	2.733	-----	-----	-----	-----	2.733
1022	2.716	63.31	-----	-----	-----	-----	2.733	-----	-----	-----	-----	2.733
1023	2.713	63.31	-----	-----	-----	-----	2.732	-----	-----	-----	-----	2.732
1024	2.711	63.31	-----	-----	-----	-----	2.731	-----	-----	-----	-----	2.731
1025	2.709	63.31	-----	-----	-----	-----	2.730	-----	-----	-----	-----	2.730
1026	2.707	63.31	-----	-----	-----	-----	2.729	-----	-----	-----	-----	2.729
1027	2.705	63.31	-----	-----	-----	-----	2.728	-----	-----	-----	-----	2.728
1028	2.703	63.31	-----	-----	-----	-----	2.727	-----	-----	-----	-----	2.727
1029	2.701	63.31	-----	-----	-----	-----	2.726	-----	-----	-----	-----	2.726
1030	2.699	63.31	-----	-----	-----	-----	2.725	-----	-----	-----	-----	2.725
1031	2.697	63.31	-----	-----	-----	-----	2.724	-----	-----	-----	-----	2.724
1032	2.695	63.31	-----	-----	-----	-----	2.723	-----	-----	-----	-----	2.723
1033	2.692	63.31	-----	-----	-----	-----	2.722	-----	-----	-----	-----	2.722
1034	2.690	63.31	-----	-----	-----	-----	2.720	-----	-----	-----	-----	2.720

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1035	2.688	63.31	-----	-----	-----	-----	2.719	-----	-----	-----	-----	2.719
1036	2.686	63.31	-----	-----	-----	-----	2.718	-----	-----	-----	-----	2.718
1037	2.684	63.31	-----	-----	-----	-----	2.716	-----	-----	-----	-----	2.716
1038	2.682	63.31	-----	-----	-----	-----	2.715	-----	-----	-----	-----	2.715
1039	2.680	63.31	-----	-----	-----	-----	2.714	-----	-----	-----	-----	2.714
1040	2.678	63.31	-----	-----	-----	-----	2.712	-----	-----	-----	-----	2.712
1041	2.676	63.31	-----	-----	-----	-----	2.711	-----	-----	-----	-----	2.711
1042	2.673	63.31	-----	-----	-----	-----	2.709	-----	-----	-----	-----	2.709
1043	2.671	63.31	-----	-----	-----	-----	2.708	-----	-----	-----	-----	2.708
1044	2.669	63.31	-----	-----	-----	-----	2.706	-----	-----	-----	-----	2.706
1045	2.667	63.31	-----	-----	-----	-----	2.704	-----	-----	-----	-----	2.704
1046	2.665	63.31	-----	-----	-----	-----	2.703	-----	-----	-----	-----	2.703
1047	2.663	63.31	-----	-----	-----	-----	2.701	-----	-----	-----	-----	2.701
1048	2.661	63.31	-----	-----	-----	-----	2.699	-----	-----	-----	-----	2.700
1049	2.659	63.31	-----	-----	-----	-----	2.698	-----	-----	-----	-----	2.698
1050	2.657	63.31	-----	-----	-----	-----	2.696	-----	-----	-----	-----	2.696
1051	2.654	63.31	-----	-----	-----	-----	2.694	-----	-----	-----	-----	2.694
1052	2.652	63.31	-----	-----	-----	-----	2.693	-----	-----	-----	-----	2.693
1053	2.650	63.30	-----	-----	-----	-----	2.691	-----	-----	-----	-----	2.691
1054	2.648	63.30	-----	-----	-----	-----	2.689	-----	-----	-----	-----	2.689
1055	2.646	63.30	-----	-----	-----	-----	2.688	-----	-----	-----	-----	2.688
1056	2.644	63.30	-----	-----	-----	-----	2.686	-----	-----	-----	-----	2.686
1057	2.642	63.30	-----	-----	-----	-----	2.684	-----	-----	-----	-----	2.684
1058	2.640	63.30	-----	-----	-----	-----	2.682	-----	-----	-----	-----	2.682
1059	2.637	63.30	-----	-----	-----	-----	2.680	-----	-----	-----	-----	2.680
1060	2.635	63.30	-----	-----	-----	-----	2.678	-----	-----	-----	-----	2.678
1061	2.633	63.30	-----	-----	-----	-----	2.677	-----	-----	-----	-----	2.677
1062	2.631	63.30	-----	-----	-----	-----	2.675	-----	-----	-----	-----	2.675
1063	2.629	63.30	-----	-----	-----	-----	2.673	-----	-----	-----	-----	2.673
1064	2.627	63.30	-----	-----	-----	-----	2.671	-----	-----	-----	-----	2.671
1065	2.625	63.30	-----	-----	-----	-----	2.669	-----	-----	-----	-----	2.669
1066	2.623	63.30	-----	-----	-----	-----	2.667	-----	-----	-----	-----	2.667
1067	2.620	63.30	-----	-----	-----	-----	2.665	-----	-----	-----	-----	2.665
1068	2.618	63.30	-----	-----	-----	-----	2.663	-----	-----	-----	-----	2.663
1069	2.616	63.30	-----	-----	-----	-----	2.661	-----	-----	-----	-----	2.661
1070	2.614	63.30	-----	-----	-----	-----	2.660	-----	-----	-----	-----	2.660
1071	2.612	63.30	-----	-----	-----	-----	2.658	-----	-----	-----	-----	2.658
1072	2.610	63.30	-----	-----	-----	-----	2.656	-----	-----	-----	-----	2.656
1073	2.608	63.30	-----	-----	-----	-----	2.654	-----	-----	-----	-----	2.654
1074	2.606	63.30	-----	-----	-----	-----	2.652	-----	-----	-----	-----	2.652
1075	2.603	63.30	-----	-----	-----	-----	2.650	-----	-----	-----	-----	2.650
1076	2.601	63.30	-----	-----	-----	-----	2.648	-----	-----	-----	-----	2.648
1077	2.599	63.30	-----	-----	-----	-----	2.646	-----	-----	-----	-----	2.646
1078	2.597	63.30	-----	-----	-----	-----	2.644	-----	-----	-----	-----	2.644
1079	2.595	63.30	-----	-----	-----	-----	2.642	-----	-----	-----	-----	2.642
1080	2.593	63.30	-----	-----	-----	-----	2.640	-----	-----	-----	-----	2.640
1081	2.591	63.30	-----	-----	-----	-----	2.638	-----	-----	-----	-----	2.638
1082	2.588	63.30	-----	-----	-----	-----	2.636	-----	-----	-----	-----	2.636
1083	2.586	63.30	-----	-----	-----	-----	2.634	-----	-----	-----	-----	2.634
1084	2.584	63.30	-----	-----	-----	-----	2.632	-----	-----	-----	-----	2.632
1085	2.582	63.30	-----	-----	-----	-----	2.630	-----	-----	-----	-----	2.630
1086	2.580	63.30	-----	-----	-----	-----	2.628	-----	-----	-----	-----	2.628
1087	2.578	63.30	-----	-----	-----	-----	2.626	-----	-----	-----	-----	2.626
1088	2.576	63.30	-----	-----	-----	-----	2.624	-----	-----	-----	-----	2.624
1089	2.574	63.30	-----	-----	-----	-----	2.622	-----	-----	-----	-----	2.622
1090	2.571	63.30	-----	-----	-----	-----	2.619	-----	-----	-----	-----	2.619

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1091	2.569	63.30	-----	-----	-----	-----	2.617	-----	-----	-----	-----	2.617
1092	2.567	63.30	-----	-----	-----	-----	2.615	-----	-----	-----	-----	2.615
1093	2.565	63.30	-----	-----	-----	-----	2.613	-----	-----	-----	-----	2.613
1094	2.563	63.30	-----	-----	-----	-----	2.611	-----	-----	-----	-----	2.611
1095	2.561	63.30	-----	-----	-----	-----	2.609	-----	-----	-----	-----	2.609
1096	2.559	63.30	-----	-----	-----	-----	2.607	-----	-----	-----	-----	2.607
1097	2.556	63.30	-----	-----	-----	-----	2.605	-----	-----	-----	-----	2.605
1098	2.554	63.30	-----	-----	-----	-----	2.603	-----	-----	-----	-----	2.603
1099	2.552	63.30	-----	-----	-----	-----	2.601	-----	-----	-----	-----	2.601
1100	2.550	63.30	-----	-----	-----	-----	2.599	-----	-----	-----	-----	2.599
1101	2.548	63.30	-----	-----	-----	-----	2.597	-----	-----	-----	-----	2.597
1102	2.546	63.30	-----	-----	-----	-----	2.595	-----	-----	-----	-----	2.595
1103	2.543	63.30	-----	-----	-----	-----	2.592	-----	-----	-----	-----	2.592
1104	2.541	63.30	-----	-----	-----	-----	2.590	-----	-----	-----	-----	2.590
1105	2.539	63.30	-----	-----	-----	-----	2.588	-----	-----	-----	-----	2.588
1106	2.537	63.30	-----	-----	-----	-----	2.586	-----	-----	-----	-----	2.586
1107	2.535	63.30	-----	-----	-----	-----	2.584	-----	-----	-----	-----	2.584
1108	2.533	63.30	-----	-----	-----	-----	2.582	-----	-----	-----	-----	2.582
1109	2.531	63.30	-----	-----	-----	-----	2.580	-----	-----	-----	-----	2.580
1110	2.528	63.30	-----	-----	-----	-----	2.578	-----	-----	-----	-----	2.578
1111	2.526	63.30	-----	-----	-----	-----	2.576	-----	-----	-----	-----	2.576
1112	2.524	63.30	-----	-----	-----	-----	2.574	-----	-----	-----	-----	2.574
1113	2.522	63.30	-----	-----	-----	-----	2.571	-----	-----	-----	-----	2.571
1114	2.520	63.30	-----	-----	-----	-----	2.569	-----	-----	-----	-----	2.569
1115	2.518	63.30	-----	-----	-----	-----	2.567	-----	-----	-----	-----	2.567
1116	2.515	63.30	-----	-----	-----	-----	2.565	-----	-----	-----	-----	2.565
1117	2.513	63.30	-----	-----	-----	-----	2.563	-----	-----	-----	-----	2.563
1118	2.511	63.30	-----	-----	-----	-----	2.561	-----	-----	-----	-----	2.561
1119	2.509	63.30	-----	-----	-----	-----	2.559	-----	-----	-----	-----	2.559
1120	2.507	63.30	-----	-----	-----	-----	2.557	-----	-----	-----	-----	2.557
1121	2.505	63.30	-----	-----	-----	-----	2.554	-----	-----	-----	-----	2.554
1122	2.503	63.30	-----	-----	-----	-----	2.552	-----	-----	-----	-----	2.552
1123	2.500	63.30	-----	-----	-----	-----	2.550	-----	-----	-----	-----	2.550
1124	2.498	63.30	-----	-----	-----	-----	2.548	-----	-----	-----	-----	2.548
1125	2.496	63.30	-----	-----	-----	-----	2.546	-----	-----	-----	-----	2.546
1126	2.494	63.30	-----	-----	-----	-----	2.544	-----	-----	-----	-----	2.544
1127	2.492	63.30	-----	-----	-----	-----	2.542	-----	-----	-----	-----	2.542
1128	2.490	63.30	-----	-----	-----	-----	2.540	-----	-----	-----	-----	2.540
1129	2.487	63.30	-----	-----	-----	-----	2.537	-----	-----	-----	-----	2.537
1130	2.485	63.30	-----	-----	-----	-----	2.535	-----	-----	-----	-----	2.535
1131	2.483	63.30	-----	-----	-----	-----	2.533	-----	-----	-----	-----	2.533
1132	2.481	63.30	-----	-----	-----	-----	2.531	-----	-----	-----	-----	2.531
1133	2.479	63.30	-----	-----	-----	-----	2.529	-----	-----	-----	-----	2.529
1134	2.477	63.30	-----	-----	-----	-----	2.527	-----	-----	-----	-----	2.527
1135	2.474	63.30	-----	-----	-----	-----	2.525	-----	-----	-----	-----	2.525
1136	2.472	63.30	-----	-----	-----	-----	2.522	-----	-----	-----	-----	2.522
1137	2.470	63.30	-----	-----	-----	-----	2.520	-----	-----	-----	-----	2.520
1138	2.468	63.30	-----	-----	-----	-----	2.518	-----	-----	-----	-----	2.518
1139	2.466	63.30	-----	-----	-----	-----	2.516	-----	-----	-----	-----	2.516
1140	2.464	63.30	-----	-----	-----	-----	2.514	-----	-----	-----	-----	2.514
1141	2.461	63.30	-----	-----	-----	-----	2.512	-----	-----	-----	-----	2.512
1142	2.459	63.30	-----	-----	-----	-----	2.510	-----	-----	-----	-----	2.510
1143	2.457	63.30	-----	-----	-----	-----	2.507	-----	-----	-----	-----	2.507
1144	2.455	63.30	-----	-----	-----	-----	2.505	-----	-----	-----	-----	2.505
1145	2.453	63.30	-----	-----	-----	-----	2.503	-----	-----	-----	-----	2.503
1146	2.451	63.30	-----	-----	-----	-----	2.501	-----	-----	-----	-----	2.501

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1147	2.448	63.30	-----	-----	-----	-----	2.499	-----	-----	-----	-----	2.499
1148	2.446	63.30	-----	-----	-----	-----	2.497	-----	-----	-----	-----	2.497
1149	2.444	63.30	-----	-----	-----	-----	2.494	-----	-----	-----	-----	2.494
1150	2.442	63.30	-----	-----	-----	-----	2.492	-----	-----	-----	-----	2.492
1151	2.440	63.30	-----	-----	-----	-----	2.490	-----	-----	-----	-----	2.490
1152	2.437	63.30	-----	-----	-----	-----	2.488	-----	-----	-----	-----	2.488
1153	2.435	63.30	-----	-----	-----	-----	2.486	-----	-----	-----	-----	2.486
1154	2.433	63.30	-----	-----	-----	-----	2.484	-----	-----	-----	-----	2.484
1155	2.431	63.30	-----	-----	-----	-----	2.481	-----	-----	-----	-----	2.482
1156	2.429	63.30	-----	-----	-----	-----	2.479	-----	-----	-----	-----	2.479
1157	2.427	63.30	-----	-----	-----	-----	2.477	-----	-----	-----	-----	2.477
1158	2.424	63.30	-----	-----	-----	-----	2.475	-----	-----	-----	-----	2.475
1159	2.422	63.30	-----	-----	-----	-----	2.473	-----	-----	-----	-----	2.473
1160	2.420	63.30	-----	-----	-----	-----	2.471	-----	-----	-----	-----	2.471
1161	2.418	63.30	-----	-----	-----	-----	2.469	-----	-----	-----	-----	2.469
1162	2.416	63.30	-----	-----	-----	-----	2.466	-----	-----	-----	-----	2.466
1163	2.414	63.30	-----	-----	-----	-----	2.465	-----	-----	-----	-----	2.465
1164	2.411	63.30	-----	-----	-----	-----	2.464	-----	-----	-----	-----	2.464
1165	2.409	63.30	-----	-----	-----	-----	2.463	-----	-----	-----	-----	2.463
1166	2.407	63.30	-----	-----	-----	-----	2.462	-----	-----	-----	-----	2.462
1167	2.405	63.30	-----	-----	-----	-----	2.460	-----	-----	-----	-----	2.460
1168	2.403	63.30	-----	-----	-----	-----	2.459	-----	-----	-----	-----	2.459
1169	2.400	63.30	-----	-----	-----	-----	2.458	-----	-----	-----	-----	2.458
1170	2.398	63.30	-----	-----	-----	-----	2.456	-----	-----	-----	-----	2.456
1171	2.396	63.30	-----	-----	-----	-----	2.455	-----	-----	-----	-----	2.455
1172	2.394	63.30	-----	-----	-----	-----	2.454	-----	-----	-----	-----	2.454
1173	2.392	63.30	-----	-----	-----	-----	2.452	-----	-----	-----	-----	2.452
1174	2.389	63.30	-----	-----	-----	-----	2.451	-----	-----	-----	-----	2.451
1175	2.387	63.30	-----	-----	-----	-----	2.449	-----	-----	-----	-----	2.449
1176	2.385	63.30	-----	-----	-----	-----	2.448	-----	-----	-----	-----	2.448
1177	2.383	63.30	-----	-----	-----	-----	2.446	-----	-----	-----	-----	2.446
1178	2.381	63.30	-----	-----	-----	-----	2.445	-----	-----	-----	-----	2.445
1179	2.379	63.30	-----	-----	-----	-----	2.443	-----	-----	-----	-----	2.443
1180	2.376	63.30	-----	-----	-----	-----	2.442	-----	-----	-----	-----	2.442
1181	2.374	63.30	-----	-----	-----	-----	2.440	-----	-----	-----	-----	2.440
1182	2.372	63.30	-----	-----	-----	-----	2.439	-----	-----	-----	-----	2.439
1183	2.370	63.30	-----	-----	-----	-----	2.437	-----	-----	-----	-----	2.437
1184	2.368	63.30	-----	-----	-----	-----	2.436	-----	-----	-----	-----	2.436
1185	2.365	63.30	-----	-----	-----	-----	2.434	-----	-----	-----	-----	2.434
1186	2.363	63.30	-----	-----	-----	-----	2.432	-----	-----	-----	-----	2.432
1187	2.361	63.30	-----	-----	-----	-----	2.431	-----	-----	-----	-----	2.431
1188	2.359	63.30	-----	-----	-----	-----	2.429	-----	-----	-----	-----	2.429
1189	2.357	63.30	-----	-----	-----	-----	2.427	-----	-----	-----	-----	2.427
1190	2.354	63.30	-----	-----	-----	-----	2.426	-----	-----	-----	-----	2.426
1191	2.352	63.30	-----	-----	-----	-----	2.424	-----	-----	-----	-----	2.424
1192	2.350	63.30	-----	-----	-----	-----	2.422	-----	-----	-----	-----	2.422
1193	2.348	63.30	-----	-----	-----	-----	2.421	-----	-----	-----	-----	2.421
1194	2.346	63.30	-----	-----	-----	-----	2.419	-----	-----	-----	-----	2.419
1195	2.343	63.30	-----	-----	-----	-----	2.417	-----	-----	-----	-----	2.417
1196	2.341	63.30	-----	-----	-----	-----	2.416	-----	-----	-----	-----	2.416
1197	2.339	63.30	-----	-----	-----	-----	2.414	-----	-----	-----	-----	2.414
1198	2.337	63.30	-----	-----	-----	-----	2.412	-----	-----	-----	-----	2.412
1199	2.335	63.30	-----	-----	-----	-----	2.410	-----	-----	-----	-----	2.410
1200	2.332	63.30	-----	-----	-----	-----	2.409	-----	-----	-----	-----	2.409
1201	2.330	63.30	-----	-----	-----	-----	2.407	-----	-----	-----	-----	2.407
1202	2.328	63.30	-----	-----	-----	-----	2.405	-----	-----	-----	-----	2.405

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1203	2.326	63.30	-----	-----	-----	-----	2.403	-----	-----	-----	-----	2.403
1204	2.324	63.30	-----	-----	-----	-----	2.401	-----	-----	-----	-----	2.401
1205	2.321	63.30	-----	-----	-----	-----	2.400	-----	-----	-----	-----	2.400
1206	2.319	63.30	-----	-----	-----	-----	2.398	-----	-----	-----	-----	2.398
1207	2.317	63.30	-----	-----	-----	-----	2.396	-----	-----	-----	-----	2.396
1208	2.315	63.30	-----	-----	-----	-----	2.394	-----	-----	-----	-----	2.394
1209	2.313	63.30	-----	-----	-----	-----	2.392	-----	-----	-----	-----	2.392
1210	2.310	63.30	-----	-----	-----	-----	2.390	-----	-----	-----	-----	2.390
1211	2.308	63.30	-----	-----	-----	-----	2.388	-----	-----	-----	-----	2.388
1212	2.306	63.30	-----	-----	-----	-----	2.387	-----	-----	-----	-----	2.387
1213	2.304	63.30	-----	-----	-----	-----	2.385	-----	-----	-----	-----	2.385
1214	2.302	63.30	-----	-----	-----	-----	2.383	-----	-----	-----	-----	2.383
1215	2.299	63.30	-----	-----	-----	-----	2.381	-----	-----	-----	-----	2.381
1216	2.297	63.30	-----	-----	-----	-----	2.379	-----	-----	-----	-----	2.379
1217	2.295	63.30	-----	-----	-----	-----	2.377	-----	-----	-----	-----	2.377
1218	2.293	63.30	-----	-----	-----	-----	2.375	-----	-----	-----	-----	2.375
1219	2.291	63.30	-----	-----	-----	-----	2.373	-----	-----	-----	-----	2.373
1220	2.288	63.30	-----	-----	-----	-----	2.371	-----	-----	-----	-----	2.371
1221	2.286	63.30	-----	-----	-----	-----	2.369	-----	-----	-----	-----	2.369
1222	2.284	63.30	-----	-----	-----	-----	2.367	-----	-----	-----	-----	2.367
1223	2.282	63.30	-----	-----	-----	-----	2.365	-----	-----	-----	-----	2.365
1224	2.280	63.30	-----	-----	-----	-----	2.363	-----	-----	-----	-----	2.363
1225	2.277	63.30	-----	-----	-----	-----	2.362	-----	-----	-----	-----	2.361
1226	2.275	63.30	-----	-----	-----	-----	2.360	-----	-----	-----	-----	2.360
1227	2.273	63.30	-----	-----	-----	-----	2.358	-----	-----	-----	-----	2.358
1228	2.271	63.30	-----	-----	-----	-----	2.356	-----	-----	-----	-----	2.356
1229	2.269	63.30	-----	-----	-----	-----	2.354	-----	-----	-----	-----	2.354
1230	2.266	63.30	-----	-----	-----	-----	2.352	-----	-----	-----	-----	2.352
1231	2.264	63.30	-----	-----	-----	-----	2.350	-----	-----	-----	-----	2.350
1232	2.262	63.30	-----	-----	-----	-----	2.348	-----	-----	-----	-----	2.348
1233	2.260	63.30	-----	-----	-----	-----	2.346	-----	-----	-----	-----	2.346
1234	2.257	63.30	-----	-----	-----	-----	2.344	-----	-----	-----	-----	2.344
1235	2.255	63.29	-----	-----	-----	-----	2.342	-----	-----	-----	-----	2.342
1236	2.253	63.29	-----	-----	-----	-----	2.339	-----	-----	-----	-----	2.340
1237	2.251	63.29	-----	-----	-----	-----	2.338	-----	-----	-----	-----	2.338
1238	2.249	63.29	-----	-----	-----	-----	2.335	-----	-----	-----	-----	2.335
1239	2.246	63.29	-----	-----	-----	-----	2.333	-----	-----	-----	-----	2.333
1240	2.244	63.29	-----	-----	-----	-----	2.331	-----	-----	-----	-----	2.331
1241	2.242	63.29	-----	-----	-----	-----	2.329	-----	-----	-----	-----	2.329
1242	2.240	63.29	-----	-----	-----	-----	2.327	-----	-----	-----	-----	2.327
1243	2.238	63.29	-----	-----	-----	-----	2.325	-----	-----	-----	-----	2.325
1244	2.235	63.29	-----	-----	-----	-----	2.323	-----	-----	-----	-----	2.323
1245	2.233	63.29	-----	-----	-----	-----	2.321	-----	-----	-----	-----	2.321
1246	2.231	63.29	-----	-----	-----	-----	2.319	-----	-----	-----	-----	2.319
1247	2.229	63.29	-----	-----	-----	-----	2.317	-----	-----	-----	-----	2.317
1248	2.226	63.29	-----	-----	-----	-----	2.315	-----	-----	-----	-----	2.315
1249	2.224	63.29	-----	-----	-----	-----	2.313	-----	-----	-----	-----	2.313
1250	2.222	63.29	-----	-----	-----	-----	2.311	-----	-----	-----	-----	2.311
1251	2.220	63.29	-----	-----	-----	-----	2.309	-----	-----	-----	-----	2.309
1252	2.218	63.29	-----	-----	-----	-----	2.307	-----	-----	-----	-----	2.307
1253	2.215	63.29	-----	-----	-----	-----	2.305	-----	-----	-----	-----	2.305
1254	2.213	63.29	-----	-----	-----	-----	2.303	-----	-----	-----	-----	2.303
1255	2.211	63.29	-----	-----	-----	-----	2.300	-----	-----	-----	-----	2.300
1256	2.209	63.29	-----	-----	-----	-----	2.298	-----	-----	-----	-----	2.298
1257	2.206	63.29	-----	-----	-----	-----	2.296	-----	-----	-----	-----	2.296
1258	2.204	63.29	-----	-----	-----	-----	2.294	-----	-----	-----	-----	2.294

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1259	2.202	63.29	-----	-----	-----	-----	2.292	-----	-----	-----	-----	2.292
1260	2.200	63.29	-----	-----	-----	-----	2.290	-----	-----	-----	-----	2.290
1261	2.198	63.29	-----	-----	-----	-----	2.288	-----	-----	-----	-----	2.288
1262	2.195	63.29	-----	-----	-----	-----	2.286	-----	-----	-----	-----	2.286
1263	2.193	63.29	-----	-----	-----	-----	2.284	-----	-----	-----	-----	2.284
1264	2.191	63.29	-----	-----	-----	-----	2.281	-----	-----	-----	-----	2.281
1265	2.189	63.29	-----	-----	-----	-----	2.279	-----	-----	-----	-----	2.279
1266	2.186	63.29	-----	-----	-----	-----	2.277	-----	-----	-----	-----	2.277
1267	2.184	63.29	-----	-----	-----	-----	2.275	-----	-----	-----	-----	2.275
1268	2.182	63.29	-----	-----	-----	-----	2.273	-----	-----	-----	-----	2.273
1269	2.180	63.29	-----	-----	-----	-----	2.271	-----	-----	-----	-----	2.271
1270	2.178	63.29	-----	-----	-----	-----	2.269	-----	-----	-----	-----	2.269
1271	2.175	63.29	-----	-----	-----	-----	2.267	-----	-----	-----	-----	2.267
1272	2.173	63.29	-----	-----	-----	-----	2.264	-----	-----	-----	-----	2.264
1273	2.171	63.29	-----	-----	-----	-----	2.262	-----	-----	-----	-----	2.262
1274	2.169	63.29	-----	-----	-----	-----	2.260	-----	-----	-----	-----	2.260
1275	2.166	63.29	-----	-----	-----	-----	2.258	-----	-----	-----	-----	2.258
1276	2.164	63.29	-----	-----	-----	-----	2.256	-----	-----	-----	-----	2.256
1277	2.162	63.29	-----	-----	-----	-----	2.254	-----	-----	-----	-----	2.254
1278	2.160	63.29	-----	-----	-----	-----	2.252	-----	-----	-----	-----	2.252
1279	2.157	63.29	-----	-----	-----	-----	2.249	-----	-----	-----	-----	2.249
1280	2.155	63.29	-----	-----	-----	-----	2.247	-----	-----	-----	-----	2.247
1281	2.153	63.29	-----	-----	-----	-----	2.245	-----	-----	-----	-----	2.245
1282	2.151	63.29	-----	-----	-----	-----	2.243	-----	-----	-----	-----	2.243
1283	2.149	63.29	-----	-----	-----	-----	2.241	-----	-----	-----	-----	2.241
1284	2.146	63.29	-----	-----	-----	-----	2.239	-----	-----	-----	-----	2.239
1285	2.144	63.29	-----	-----	-----	-----	2.237	-----	-----	-----	-----	2.237
1286	2.142	63.29	-----	-----	-----	-----	2.234	-----	-----	-----	-----	2.234
1287	2.140	63.29	-----	-----	-----	-----	2.232	-----	-----	-----	-----	2.232
1288	2.137	63.29	-----	-----	-----	-----	2.230	-----	-----	-----	-----	2.230
1289	2.135	63.29	-----	-----	-----	-----	2.228	-----	-----	-----	-----	2.228
1290	2.133	63.29	-----	-----	-----	-----	2.226	-----	-----	-----	-----	2.226
1291	2.131	63.29	-----	-----	-----	-----	2.224	-----	-----	-----	-----	2.224
1292	2.128	63.29	-----	-----	-----	-----	2.221	-----	-----	-----	-----	2.221
1293	2.126	63.29	-----	-----	-----	-----	2.219	-----	-----	-----	-----	2.219
1294	2.124	63.29	-----	-----	-----	-----	2.217	-----	-----	-----	-----	2.217
1295	2.122	63.29	-----	-----	-----	-----	2.215	-----	-----	-----	-----	2.215
1296	2.120	63.29	-----	-----	-----	-----	2.213	-----	-----	-----	-----	2.213
1297	2.117	63.29	-----	-----	-----	-----	2.210	-----	-----	-----	-----	2.210
1298	2.115	63.29	-----	-----	-----	-----	2.208	-----	-----	-----	-----	2.208
1299	2.113	63.29	-----	-----	-----	-----	2.206	-----	-----	-----	-----	2.206
1300	2.111	63.29	-----	-----	-----	-----	2.204	-----	-----	-----	-----	2.204
1301	2.108	63.29	-----	-----	-----	-----	2.202	-----	-----	-----	-----	2.202
1302	2.106	63.29	-----	-----	-----	-----	2.200	-----	-----	-----	-----	2.200
1303	2.104	63.29	-----	-----	-----	-----	2.197	-----	-----	-----	-----	2.197
1304	2.102	63.29	-----	-----	-----	-----	2.195	-----	-----	-----	-----	2.195
1305	2.099	63.29	-----	-----	-----	-----	2.193	-----	-----	-----	-----	2.193
1306	2.097	63.29	-----	-----	-----	-----	2.191	-----	-----	-----	-----	2.191
1307	2.095	63.29	-----	-----	-----	-----	2.189	-----	-----	-----	-----	2.189
1308	2.093	63.29	-----	-----	-----	-----	2.186	-----	-----	-----	-----	2.186
1309	2.090	63.29	-----	-----	-----	-----	2.184	-----	-----	-----	-----	2.184
1310	2.088	63.29	-----	-----	-----	-----	2.182	-----	-----	-----	-----	2.182
1311	2.086	63.29	-----	-----	-----	-----	2.180	-----	-----	-----	-----	2.180
1312	2.084	63.29	-----	-----	-----	-----	2.178	-----	-----	-----	-----	2.178
1313	2.081	63.29	-----	-----	-----	-----	2.175	-----	-----	-----	-----	2.175
1314	2.079	63.29	-----	-----	-----	-----	2.173	-----	-----	-----	-----	2.173

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1315	2.077	63.29	-----	-----	-----	-----	2.171	-----	-----	-----	-----	2.171
1316	2.075	63.29	-----	-----	-----	-----	2.169	-----	-----	-----	-----	2.169
1317	2.072	63.29	-----	-----	-----	-----	2.167	-----	-----	-----	-----	2.167
1318	2.070	63.29	-----	-----	-----	-----	2.164	-----	-----	-----	-----	2.164
1319	2.068	63.29	-----	-----	-----	-----	2.162	-----	-----	-----	-----	2.162
1320	2.066	63.29	-----	-----	-----	-----	2.160	-----	-----	-----	-----	2.160
1321	2.063	63.29	-----	-----	-----	-----	2.158	-----	-----	-----	-----	2.158
1322	2.061	63.29	-----	-----	-----	-----	2.156	-----	-----	-----	-----	2.156
1323	2.059	63.29	-----	-----	-----	-----	2.153	-----	-----	-----	-----	2.153
1324	2.057	63.29	-----	-----	-----	-----	2.151	-----	-----	-----	-----	2.151
1325	2.055	63.29	-----	-----	-----	-----	2.149	-----	-----	-----	-----	2.149
1326	2.052	63.29	-----	-----	-----	-----	2.147	-----	-----	-----	-----	2.147
1327	2.050	63.29	-----	-----	-----	-----	2.145	-----	-----	-----	-----	2.145
1328	2.048	63.29	-----	-----	-----	-----	2.142	-----	-----	-----	-----	2.142
1329	2.046	63.29	-----	-----	-----	-----	2.140	-----	-----	-----	-----	2.140
1330	2.043	63.29	-----	-----	-----	-----	2.138	-----	-----	-----	-----	2.138
1331	2.041	63.29	-----	-----	-----	-----	2.136	-----	-----	-----	-----	2.136
1332	2.039	63.29	-----	-----	-----	-----	2.134	-----	-----	-----	-----	2.134
1333	2.037	63.29	-----	-----	-----	-----	2.131	-----	-----	-----	-----	2.131
1334	2.034	63.29	-----	-----	-----	-----	2.129	-----	-----	-----	-----	2.129
1335	2.032	63.29	-----	-----	-----	-----	2.127	-----	-----	-----	-----	2.127
1336	2.030	63.29	-----	-----	-----	-----	2.125	-----	-----	-----	-----	2.125
1337	2.028	63.29	-----	-----	-----	-----	2.122	-----	-----	-----	-----	2.122
1338	2.025	63.29	-----	-----	-----	-----	2.120	-----	-----	-----	-----	2.120
1339	2.023	63.29	-----	-----	-----	-----	2.118	-----	-----	-----	-----	2.118
1340	2.021	63.29	-----	-----	-----	-----	2.116	-----	-----	-----	-----	2.116
1341	2.019	63.29	-----	-----	-----	-----	2.114	-----	-----	-----	-----	2.114
1342	2.016	63.29	-----	-----	-----	-----	2.111	-----	-----	-----	-----	2.111
1343	2.014	63.29	-----	-----	-----	-----	2.109	-----	-----	-----	-----	2.109
1344	2.012	63.29	-----	-----	-----	-----	2.107	-----	-----	-----	-----	2.107
1345	2.010	63.29	-----	-----	-----	-----	2.105	-----	-----	-----	-----	2.105
1346	2.007	63.29	-----	-----	-----	-----	2.102	-----	-----	-----	-----	2.102
1347	2.005	63.29	-----	-----	-----	-----	2.100	-----	-----	-----	-----	2.100
1348	2.003	63.29	-----	-----	-----	-----	2.098	-----	-----	-----	-----	2.098
1349	2.001	63.28	-----	-----	-----	-----	2.096	-----	-----	-----	-----	2.096
1350	1.998	63.28	-----	-----	-----	-----	2.094	-----	-----	-----	-----	2.094
1351	1.996	63.28	-----	-----	-----	-----	2.091	-----	-----	-----	-----	2.091
1352	1.994	63.28	-----	-----	-----	-----	2.089	-----	-----	-----	-----	2.089
1353	1.992	63.28	-----	-----	-----	-----	2.087	-----	-----	-----	-----	2.087
1354	1.989	63.28	-----	-----	-----	-----	2.085	-----	-----	-----	-----	2.085
1355	1.987	63.28	-----	-----	-----	-----	2.082	-----	-----	-----	-----	2.082
1356	1.985	63.28	-----	-----	-----	-----	2.080	-----	-----	-----	-----	2.080
1357	1.982	63.28	-----	-----	-----	-----	2.078	-----	-----	-----	-----	2.078
1358	1.980	63.28	-----	-----	-----	-----	2.076	-----	-----	-----	-----	2.076
1359	1.978	63.28	-----	-----	-----	-----	2.073	-----	-----	-----	-----	2.073
1360	1.976	63.28	-----	-----	-----	-----	2.071	-----	-----	-----	-----	2.071
1361	1.973	63.28	-----	-----	-----	-----	2.069	-----	-----	-----	-----	2.069
1362	1.971	63.28	-----	-----	-----	-----	2.067	-----	-----	-----	-----	2.067
1363	1.969	63.28	-----	-----	-----	-----	2.065	-----	-----	-----	-----	2.065
1364	1.967	63.28	-----	-----	-----	-----	2.062	-----	-----	-----	-----	2.062
1365	1.964	63.28	-----	-----	-----	-----	2.060	-----	-----	-----	-----	2.060
1366	1.962	63.28	-----	-----	-----	-----	2.058	-----	-----	-----	-----	2.058
1367	1.960	63.28	-----	-----	-----	-----	2.056	-----	-----	-----	-----	2.056
1368	1.958	63.28	-----	-----	-----	-----	2.053	-----	-----	-----	-----	2.053
1369	1.955	63.28	-----	-----	-----	-----	2.051	-----	-----	-----	-----	2.051
1370	1.953	63.28	-----	-----	-----	-----	2.049	-----	-----	-----	-----	2.049

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1371	1.951	63.28	-----	-----	-----	-----	2.047	-----	-----	-----	-----	2.047
1372	1.949	63.28	-----	-----	-----	-----	2.044	-----	-----	-----	-----	2.044
1373	1.946	63.28	-----	-----	-----	-----	2.042	-----	-----	-----	-----	2.042
1374	1.944	63.28	-----	-----	-----	-----	2.040	-----	-----	-----	-----	2.040
1375	1.942	63.28	-----	-----	-----	-----	2.038	-----	-----	-----	-----	2.038
1376	1.940	63.28	-----	-----	-----	-----	2.035	-----	-----	-----	-----	2.035
1377	1.937	63.28	-----	-----	-----	-----	2.033	-----	-----	-----	-----	2.033
1378	1.935	63.28	-----	-----	-----	-----	2.031	-----	-----	-----	-----	2.031
1379	1.933	63.28	-----	-----	-----	-----	2.029	-----	-----	-----	-----	2.029
1380	1.931	63.28	-----	-----	-----	-----	2.026	-----	-----	-----	-----	2.026
1381	1.928	63.28	-----	-----	-----	-----	2.024	-----	-----	-----	-----	2.024
1382	1.926	63.28	-----	-----	-----	-----	2.022	-----	-----	-----	-----	2.022
1383	1.924	63.28	-----	-----	-----	-----	2.020	-----	-----	-----	-----	2.020
1384	1.921	63.28	-----	-----	-----	-----	2.018	-----	-----	-----	-----	2.018
1385	1.919	63.28	-----	-----	-----	-----	2.015	-----	-----	-----	-----	2.015
1386	1.917	63.28	-----	-----	-----	-----	2.013	-----	-----	-----	-----	2.013
1387	1.915	63.28	-----	-----	-----	-----	2.011	-----	-----	-----	-----	2.011
1388	1.912	63.28	-----	-----	-----	-----	2.009	-----	-----	-----	-----	2.009
1389	1.910	63.28	-----	-----	-----	-----	2.006	-----	-----	-----	-----	2.006
1390	1.908	63.28	-----	-----	-----	-----	2.004	-----	-----	-----	-----	2.004
1391	1.906	63.28	-----	-----	-----	-----	2.002	-----	-----	-----	-----	2.002
1392	1.903	63.28	-----	-----	-----	-----	2.000	-----	-----	-----	-----	2.000
1393	1.901	63.28	-----	-----	-----	-----	1.997	-----	-----	-----	-----	1.997
1394	1.899	63.28	-----	-----	-----	-----	1.995	-----	-----	-----	-----	1.995
1395	1.897	63.28	-----	-----	-----	-----	1.993	-----	-----	-----	-----	1.993
1396	1.894	63.28	-----	-----	-----	-----	1.991	-----	-----	-----	-----	1.991
1397	1.892	63.28	-----	-----	-----	-----	1.988	-----	-----	-----	-----	1.988
1398	1.890	63.28	-----	-----	-----	-----	1.986	-----	-----	-----	-----	1.986
1399	1.888	63.28	-----	-----	-----	-----	1.984	-----	-----	-----	-----	1.984
1400	1.885	63.28	-----	-----	-----	-----	1.982	-----	-----	-----	-----	1.982
1401	1.883	63.28	-----	-----	-----	-----	1.979	-----	-----	-----	-----	1.979
1402	1.881	63.28	-----	-----	-----	-----	1.977	-----	-----	-----	-----	1.977
1403	1.878	63.28	-----	-----	-----	-----	1.975	-----	-----	-----	-----	1.975
1404	1.876	63.28	-----	-----	-----	-----	1.973	-----	-----	-----	-----	1.973
1405	1.874	63.28	-----	-----	-----	-----	1.970	-----	-----	-----	-----	1.970
1406	1.872	63.28	-----	-----	-----	-----	1.968	-----	-----	-----	-----	1.968
1407	1.869	63.28	-----	-----	-----	-----	1.966	-----	-----	-----	-----	1.966
1408	1.867	63.28	-----	-----	-----	-----	1.964	-----	-----	-----	-----	1.964
1409	1.865	63.28	-----	-----	-----	-----	1.961	-----	-----	-----	-----	1.961
1410	1.863	63.28	-----	-----	-----	-----	1.959	-----	-----	-----	-----	1.959
1411	1.860	63.28	-----	-----	-----	-----	1.957	-----	-----	-----	-----	1.957
1412	1.858	63.28	-----	-----	-----	-----	1.954	-----	-----	-----	-----	1.955
1413	1.856	63.28	-----	-----	-----	-----	1.952	-----	-----	-----	-----	1.952
1414	1.853	63.28	-----	-----	-----	-----	1.950	-----	-----	-----	-----	1.950
1415	1.851	63.28	-----	-----	-----	-----	1.948	-----	-----	-----	-----	1.948
1416	1.849	63.28	-----	-----	-----	-----	1.945	-----	-----	-----	-----	1.945
1417	1.847	63.28	-----	-----	-----	-----	1.943	-----	-----	-----	-----	1.943
1418	1.844	63.28	-----	-----	-----	-----	1.941	-----	-----	-----	-----	1.941
1419	1.842	63.28	-----	-----	-----	-----	1.939	-----	-----	-----	-----	1.939
1420	1.840	63.28	-----	-----	-----	-----	1.937	-----	-----	-----	-----	1.936
1421	1.838	63.28	-----	-----	-----	-----	1.934	-----	-----	-----	-----	1.934
1422	1.835	63.28	-----	-----	-----	-----	1.932	-----	-----	-----	-----	1.932
1423	1.833	63.28	-----	-----	-----	-----	1.930	-----	-----	-----	-----	1.930
1424	1.831	63.28	-----	-----	-----	-----	1.927	-----	-----	-----	-----	1.927
1425	1.828	63.28	-----	-----	-----	-----	1.925	-----	-----	-----	-----	1.925
1426	1.826	63.28	-----	-----	-----	-----	1.923	-----	-----	-----	-----	1.923

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1427	1.824	63.28	-----	-----	-----	-----	1.921	-----	-----	-----	-----	1.921
1428	1.822	63.28	-----	-----	-----	-----	1.918	-----	-----	-----	-----	1.918
1429	1.819	63.28	-----	-----	-----	-----	1.916	-----	-----	-----	-----	1.916
1430	1.817	63.28	-----	-----	-----	-----	1.914	-----	-----	-----	-----	1.914
1431	1.815	63.28	-----	-----	-----	-----	1.912	-----	-----	-----	-----	1.912
1432	1.813	63.28	-----	-----	-----	-----	1.909	-----	-----	-----	-----	1.909
1433	1.810	63.28	-----	-----	-----	-----	1.907	-----	-----	-----	-----	1.907
1434	1.808	63.28	-----	-----	-----	-----	1.905	-----	-----	-----	-----	1.905
1435	1.806	63.28	-----	-----	-----	-----	1.903	-----	-----	-----	-----	1.903
1436	1.803	63.28	-----	-----	-----	-----	1.900	-----	-----	-----	-----	1.900
1437	1.801	63.28	-----	-----	-----	-----	1.898	-----	-----	-----	-----	1.898
1438	1.799	63.28	-----	-----	-----	-----	1.896	-----	-----	-----	-----	1.896
1439	1.797	63.28	-----	-----	-----	-----	1.894	-----	-----	-----	-----	1.894
1440	1.794	63.28	-----	-----	-----	-----	1.891	-----	-----	-----	-----	1.891
1441	1.790	63.28	-----	-----	-----	-----	1.889	-----	-----	-----	-----	1.889
1442	1.783	63.28	-----	-----	-----	-----	1.887	-----	-----	-----	-----	1.887
1443	1.773	63.28	-----	-----	-----	-----	1.884	-----	-----	-----	-----	1.884
1444	1.761	63.28	-----	-----	-----	-----	1.881	-----	-----	-----	-----	1.881
1445	1.747	63.28	-----	-----	-----	-----	1.878	-----	-----	-----	-----	1.878
1446	1.730	63.28	-----	-----	-----	-----	1.875	-----	-----	-----	-----	1.875
1447	1.711	63.28	-----	-----	-----	-----	1.872	-----	-----	-----	-----	1.872
1448	1.689	63.28	-----	-----	-----	-----	1.868	-----	-----	-----	-----	1.868
1449	1.665	63.28	-----	-----	-----	-----	1.863	-----	-----	-----	-----	1.863
1450	1.639	63.28	-----	-----	-----	-----	1.858	-----	-----	-----	-----	1.858
1451	1.610	63.28	-----	-----	-----	-----	1.853	-----	-----	-----	-----	1.853
1452	1.579	63.27	-----	-----	-----	-----	1.847	-----	-----	-----	-----	1.847
1453	1.546	63.27	-----	-----	-----	-----	1.840	-----	-----	-----	-----	1.840
1454	1.510	63.27	-----	-----	-----	-----	1.833	-----	-----	-----	-----	1.833
1455	1.472	63.27	-----	-----	-----	-----	1.825	-----	-----	-----	-----	1.825
1456	1.431	63.27	-----	-----	-----	-----	1.817	-----	-----	-----	-----	1.817
1457	1.388	63.27	-----	-----	-----	-----	1.807	-----	-----	-----	-----	1.807
1458	1.343	63.27	-----	-----	-----	-----	1.797	-----	-----	-----	-----	1.797
1459	1.295	63.27	-----	-----	-----	-----	1.786	-----	-----	-----	-----	1.786
1460	1.245	63.27	-----	-----	-----	-----	1.774	-----	-----	-----	-----	1.774
1461	1.193	63.27	-----	-----	-----	-----	1.761	-----	-----	-----	-----	1.761
1462	1.142	63.27	-----	-----	-----	-----	1.748	-----	-----	-----	-----	1.748
1463	1.091	63.27	-----	-----	-----	-----	1.733	-----	-----	-----	-----	1.733
1464	1.042	63.27	-----	-----	-----	-----	1.718	-----	-----	-----	-----	1.718
1465	0.995	63.27	-----	-----	-----	-----	1.701	-----	-----	-----	-----	1.701
1466	0.948	63.27	-----	-----	-----	-----	1.685	-----	-----	-----	-----	1.685
1467	0.902	63.27	-----	-----	-----	-----	1.667	-----	-----	-----	-----	1.667
1468	0.858	63.27	-----	-----	-----	-----	1.649	-----	-----	-----	-----	1.649
1469	0.815	63.27	-----	-----	-----	-----	1.630	-----	-----	-----	-----	1.630
1470	0.773	63.27	-----	-----	-----	-----	1.611	-----	-----	-----	-----	1.611
1471	0.732	63.26	-----	-----	-----	-----	1.591	-----	-----	-----	-----	1.591
1472	0.692	63.26	-----	-----	-----	-----	1.571	-----	-----	-----	-----	1.571
1473	0.653	63.26	-----	-----	-----	-----	1.550	-----	-----	-----	-----	1.550
1474	0.616	63.26	-----	-----	-----	-----	1.529	-----	-----	-----	-----	1.529
1475	0.579	63.26	-----	-----	-----	-----	1.507	-----	-----	-----	-----	1.507
1476	0.544	63.26	-----	-----	-----	-----	1.485	-----	-----	-----	-----	1.485
1477	0.510	63.26	-----	-----	-----	-----	1.463	-----	-----	-----	-----	1.463
1478	0.476	63.26	-----	-----	-----	-----	1.441	-----	-----	-----	-----	1.441
1479	0.445	63.26	-----	-----	-----	-----	1.418	-----	-----	-----	-----	1.418
1480	0.414	63.26	-----	-----	-----	-----	1.395	-----	-----	-----	-----	1.395
1481	0.384	63.26	-----	-----	-----	-----	1.372	-----	-----	-----	-----	1.372
1482	0.355	63.25	-----	-----	-----	-----	1.349	-----	-----	-----	-----	1.349

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1483	0.328	63.25	-----	-----	-----	-----	1.326	-----	-----	-----	-----	1.326
1484	0.302	63.25	-----	-----	-----	-----	1.302	-----	-----	-----	-----	1.302
1485	0.276	63.25	-----	-----	-----	-----	1.279	-----	-----	-----	-----	1.279
1486	0.252	63.25	-----	-----	-----	-----	1.256	-----	-----	-----	-----	1.256
1487	0.229	63.25	-----	-----	-----	-----	1.232	-----	-----	-----	-----	1.232
1488	0.207	63.25	-----	-----	-----	-----	1.209	-----	-----	-----	-----	1.209
1489	0.186	63.25	-----	-----	-----	-----	1.185	-----	-----	-----	-----	1.185
1490	0.167	63.25	-----	-----	-----	-----	1.162	-----	-----	-----	-----	1.162
1491	0.148	63.25	-----	-----	-----	-----	1.139	-----	-----	-----	-----	1.139
1492	0.131	63.25	-----	-----	-----	-----	1.116	-----	-----	-----	-----	1.116
1493	0.114	63.24	-----	-----	-----	-----	1.093	-----	-----	-----	-----	1.093
1494	0.099	63.24	-----	-----	-----	-----	1.070	-----	-----	-----	-----	1.070
1495	0.085	63.24	-----	-----	-----	-----	1.047	-----	-----	-----	-----	1.047
1496	0.072	63.24	-----	-----	-----	-----	1.025	-----	-----	-----	-----	1.025
1497	0.060	63.24	-----	-----	-----	-----	1.003	-----	-----	-----	-----	1.003
1498	0.049	63.24	-----	-----	-----	-----	0.981	-----	-----	-----	-----	0.981
1499	0.039	63.24	-----	-----	-----	-----	0.959	-----	-----	-----	-----	0.959
1500	0.030	63.24	-----	-----	-----	-----	0.938	-----	-----	-----	-----	0.938
1501	0.023	63.24	-----	-----	-----	-----	0.917	-----	-----	-----	-----	0.917
1502	0.016	63.24	-----	-----	-----	-----	0.896	-----	-----	-----	-----	0.896
1503	0.011	63.24	-----	-----	-----	-----	0.876	-----	-----	-----	-----	0.876
1504	0.006	63.23	-----	-----	-----	-----	0.856	-----	-----	-----	-----	0.856
1505	0.003	63.23	-----	-----	-----	-----	0.836	-----	-----	-----	-----	0.836
1506	0.001	63.23	-----	-----	-----	-----	0.817	-----	-----	-----	-----	0.817
1507	0.000	63.23	-----	-----	-----	-----	0.798	-----	-----	-----	-----	0.798
1508	0.000	63.23	-----	-----	-----	-----	0.779	-----	-----	-----	-----	0.780
1509	0.000	63.23	-----	-----	-----	-----	0.761	-----	-----	-----	-----	0.761
1510	0.000	63.23	-----	-----	-----	-----	0.744	-----	-----	-----	-----	0.744
1511	0.000	63.23	-----	-----	-----	-----	0.727	-----	-----	-----	-----	0.727
1512	0.000	63.23	-----	-----	-----	-----	0.710	-----	-----	-----	-----	0.710
1513	0.000	63.23	-----	-----	-----	-----	0.694	-----	-----	-----	-----	0.694
1514	0.000	63.23	-----	-----	-----	-----	0.677	-----	-----	-----	-----	0.677
1515	0.000	63.23	-----	-----	-----	-----	0.662	-----	-----	-----	-----	0.662
1516	0.000	63.23	-----	-----	-----	-----	0.647	-----	-----	-----	-----	0.647
1517	0.000	63.23	-----	-----	-----	-----	0.632	-----	-----	-----	-----	0.632
1518	0.000	63.23	-----	-----	-----	-----	0.617	-----	-----	-----	-----	0.617
1519	0.000	63.22	-----	-----	-----	-----	0.603	-----	-----	-----	-----	0.603
1520	0.000	63.22	-----	-----	-----	-----	0.589	-----	-----	-----	-----	0.589
1521	0.000	63.22	-----	-----	-----	-----	0.575	-----	-----	-----	-----	0.575
1522	0.000	63.22	-----	-----	-----	-----	0.562	-----	-----	-----	-----	0.562
1523	0.000	63.22	-----	-----	-----	-----	0.549	-----	-----	-----	-----	0.549
1524	0.000	63.22	-----	-----	-----	-----	0.536	-----	-----	-----	-----	0.536
1525	0.000	63.22	-----	-----	-----	-----	0.524	-----	-----	-----	-----	0.524
1526	0.000	63.22	-----	-----	-----	-----	0.512	-----	-----	-----	-----	0.512
1527	0.000	63.22	-----	-----	-----	-----	0.500	-----	-----	-----	-----	0.500
1528	0.000	63.22	-----	-----	-----	-----	0.488	-----	-----	-----	-----	0.488
1529	0.000	63.22	-----	-----	-----	-----	0.477	-----	-----	-----	-----	0.477
1530	0.000	63.22	-----	-----	-----	-----	0.466	-----	-----	-----	-----	0.466
1531	0.000	63.22	-----	-----	-----	-----	0.455	-----	-----	-----	-----	0.455
1532	0.000	63.22	-----	-----	-----	-----	0.445	-----	-----	-----	-----	0.445
1533	0.000	63.22	-----	-----	-----	-----	0.435	-----	-----	-----	-----	0.435
1534	0.000	63.22	-----	-----	-----	-----	0.425	-----	-----	-----	-----	0.425
1535	0.000	63.22	-----	-----	-----	-----	0.415	-----	-----	-----	-----	0.415
1536	0.000	63.22	-----	-----	-----	-----	0.405	-----	-----	-----	-----	0.405
1537	0.000	63.22	-----	-----	-----	-----	0.396	-----	-----	-----	-----	0.396
1538	0.000	63.22	-----	-----	-----	-----	0.387	-----	-----	-----	-----	0.387

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1539	0.000	63.22	-----	-----	-----	-----	0.378	-----	-----	-----	-----	0.378
1540	0.000	63.21	-----	-----	-----	-----	0.369	-----	-----	-----	-----	0.369
1541	0.000	63.21	-----	-----	-----	-----	0.360	-----	-----	-----	-----	0.360
1542	0.000	63.21	-----	-----	-----	-----	0.352	-----	-----	-----	-----	0.352
1543	0.000	63.21	-----	-----	-----	-----	0.344	-----	-----	-----	-----	0.344
1544	0.000	63.21	-----	-----	-----	-----	0.336	-----	-----	-----	-----	0.336
1545	0.000	63.21	-----	-----	-----	-----	0.328	-----	-----	-----	-----	0.328
1546	0.000	63.21	-----	-----	-----	-----	0.321	-----	-----	-----	-----	0.321
1547	0.000	63.21	-----	-----	-----	-----	0.313	-----	-----	-----	-----	0.313
1548	0.000	63.21	-----	-----	-----	-----	0.306	-----	-----	-----	-----	0.306
1549	0.000	63.21	-----	-----	-----	-----	0.299	-----	-----	-----	-----	0.299
1550	0.000	63.21	-----	-----	-----	-----	0.292	-----	-----	-----	-----	0.292
1551	0.000	63.21	-----	-----	-----	-----	0.285	-----	-----	-----	-----	0.285
1552	0.000	63.21	-----	-----	-----	-----	0.279	-----	-----	-----	-----	0.279
1553	0.000	63.21	-----	-----	-----	-----	0.272	-----	-----	-----	-----	0.272
1554	0.000	63.21	-----	-----	-----	-----	0.266	-----	-----	-----	-----	0.266
1555	0.000	63.21	-----	-----	-----	-----	0.260	-----	-----	-----	-----	0.260
1556	0.000	63.21	-----	-----	-----	-----	0.254	-----	-----	-----	-----	0.254
1557	0.000	63.21	-----	-----	-----	-----	0.248	-----	-----	-----	-----	0.248
1558	0.000	63.21	-----	-----	-----	-----	0.242	-----	-----	-----	-----	0.242
1559	0.000	63.21	-----	-----	-----	-----	0.237	-----	-----	-----	-----	0.237
1560	0.000	63.21	-----	-----	-----	-----	0.231	-----	-----	-----	-----	0.231
1561	0.000	63.21	-----	-----	-----	-----	0.226	-----	-----	-----	-----	0.226
1562	0.000	63.21	-----	-----	-----	-----	0.221	-----	-----	-----	-----	0.221
1563	0.000	63.21	-----	-----	-----	-----	0.216	-----	-----	-----	-----	0.216
1564	0.000	63.21	-----	-----	-----	-----	0.211	-----	-----	-----	-----	0.211
1565	0.000	63.21	-----	-----	-----	-----	0.206	-----	-----	-----	-----	0.206
1566	0.000	63.21	-----	-----	-----	-----	0.201	-----	-----	-----	-----	0.201
1567	0.000	63.21	-----	-----	-----	-----	0.196	-----	-----	-----	-----	0.196
1568	0.000	63.21	-----	-----	-----	-----	0.192	-----	-----	-----	-----	0.192
1569	0.000	63.21	-----	-----	-----	-----	0.187	-----	-----	-----	-----	0.187
1570	0.000	63.21	-----	-----	-----	-----	0.183	-----	-----	-----	-----	0.183
1571	0.000	63.21	-----	-----	-----	-----	0.179	-----	-----	-----	-----	0.179
1572	0.000	63.21	-----	-----	-----	-----	0.175	-----	-----	-----	-----	0.175
1573	0.000	63.21	-----	-----	-----	-----	0.171	-----	-----	-----	-----	0.171
1574	0.000	63.21	-----	-----	-----	-----	0.167	-----	-----	-----	-----	0.167
1575	0.000	63.21	-----	-----	-----	-----	0.163	-----	-----	-----	-----	0.163
1576	0.000	63.21	-----	-----	-----	-----	0.159	-----	-----	-----	-----	0.159
1577	0.000	63.21	-----	-----	-----	-----	0.155	-----	-----	-----	-----	0.155
1578	0.000	63.21	-----	-----	-----	-----	0.152	-----	-----	-----	-----	0.152
1579	0.000	63.21	-----	-----	-----	-----	0.148	-----	-----	-----	-----	0.148
1580	0.000	63.21	-----	-----	-----	-----	0.145	-----	-----	-----	-----	0.145
1581	0.000	63.21	-----	-----	-----	-----	0.142	-----	-----	-----	-----	0.142
1582	0.000	63.21	-----	-----	-----	-----	0.138	-----	-----	-----	-----	0.138
1583	0.000	63.21	-----	-----	-----	-----	0.135	-----	-----	-----	-----	0.135
1584	0.000	63.21	-----	-----	-----	-----	0.132	-----	-----	-----	-----	0.132
1585	0.000	63.21	-----	-----	-----	-----	0.129	-----	-----	-----	-----	0.129
1586	0.000	63.21	-----	-----	-----	-----	0.126	-----	-----	-----	-----	0.126
1587	0.000	63.20	-----	-----	-----	-----	0.123	-----	-----	-----	-----	0.123
1588	0.000	63.20	-----	-----	-----	-----	0.120	-----	-----	-----	-----	0.120
1589	0.000	63.20	-----	-----	-----	-----	0.117	-----	-----	-----	-----	0.117
1590	0.000	63.20	-----	-----	-----	-----	0.115	-----	-----	-----	-----	0.115
1591	0.000	63.20	-----	-----	-----	-----	0.112	-----	-----	-----	-----	0.112
1592	0.000	63.20	-----	-----	-----	-----	0.109	-----	-----	-----	-----	0.109
1593	0.000	63.20	-----	-----	-----	-----	0.107	-----	-----	-----	-----	0.107
1594	0.000	63.20	-----	-----	-----	-----	0.104	-----	-----	-----	-----	0.104

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1595	0.000	63.20	-----	-----	-----	-----	0.102	-----	-----	-----	-----	0.102
1596	0.000	63.20	-----	-----	-----	-----	0.100	-----	-----	-----	-----	0.100
1597	0.000	63.20	-----	-----	-----	-----	0.097	-----	-----	-----	-----	0.097
1598	0.000	63.20	-----	-----	-----	-----	0.095	-----	-----	-----	-----	0.095
1599	0.000	63.20	-----	-----	-----	-----	0.093	-----	-----	-----	-----	0.093
1600	0.000	63.20	-----	-----	-----	-----	0.091	-----	-----	-----	-----	0.091
1601	0.000	63.20	-----	-----	-----	-----	0.089	-----	-----	-----	-----	0.089
1602	0.000	63.20	-----	-----	-----	-----	0.087	-----	-----	-----	-----	0.087
1603	0.000	63.20	-----	-----	-----	-----	0.085	-----	-----	-----	-----	0.085
1604	0.000	63.20	-----	-----	-----	-----	0.083	-----	-----	-----	-----	0.083
1605	0.000	63.20	-----	-----	-----	-----	0.081	-----	-----	-----	-----	0.081
1606	0.000	63.20	-----	-----	-----	-----	0.079	-----	-----	-----	-----	0.079
1607	0.000	63.20	-----	-----	-----	-----	0.077	-----	-----	-----	-----	0.077
1608	0.000	63.20	-----	-----	-----	-----	0.075	-----	-----	-----	-----	0.075
1609	0.000	63.20	-----	-----	-----	-----	0.073	-----	-----	-----	-----	0.074
1610	0.000	63.20	-----	-----	-----	-----	0.072	-----	-----	-----	-----	0.072
1611	0.000	63.20	-----	-----	-----	-----	0.070	-----	-----	-----	-----	0.070
1612	0.000	63.20	-----	-----	-----	-----	0.069	-----	-----	-----	-----	0.069
1613	0.000	63.20	-----	-----	-----	-----	0.067	-----	-----	-----	-----	0.067
1614	0.000	63.20	-----	-----	-----	-----	0.065	-----	-----	-----	-----	0.065
1615	0.000	63.20	-----	-----	-----	-----	0.064	-----	-----	-----	-----	0.064
1616	0.000	63.20	-----	-----	-----	-----	0.062	-----	-----	-----	-----	0.062
1617	0.000	63.20	-----	-----	-----	-----	0.061	-----	-----	-----	-----	0.061
1618	0.000	63.20	-----	-----	-----	-----	0.060	-----	-----	-----	-----	0.060
1619	0.000	63.20	-----	-----	-----	-----	0.058	-----	-----	-----	-----	0.058
1620	0.000	63.20	-----	-----	-----	-----	0.057	-----	-----	-----	-----	0.057
1621	0.000	63.20	-----	-----	-----	-----	0.056	-----	-----	-----	-----	0.056
1622	0.000	63.20	-----	-----	-----	-----	0.054	-----	-----	-----	-----	0.054
1623	0.000	63.20	-----	-----	-----	-----	0.053	-----	-----	-----	-----	0.053
1624	0.000	63.20	-----	-----	-----	-----	0.052	-----	-----	-----	-----	0.052
1625	0.000	63.20	-----	-----	-----	-----	0.051	-----	-----	-----	-----	0.051
1626	0.000	63.20	-----	-----	-----	-----	0.049	-----	-----	-----	-----	0.049
1627	0.000	63.20	-----	-----	-----	-----	0.048	-----	-----	-----	-----	0.048
1628	0.000	63.20	-----	-----	-----	-----	0.047	-----	-----	-----	-----	0.047
1629	0.000	63.20	-----	-----	-----	-----	0.046	-----	-----	-----	-----	0.046
1630	0.000	63.20	-----	-----	-----	-----	0.045	-----	-----	-----	-----	0.045
1631	0.000	63.20	-----	-----	-----	-----	0.044	-----	-----	-----	-----	0.044
1632	0.000	63.20	-----	-----	-----	-----	0.043	-----	-----	-----	-----	0.043
1633	0.000	63.20	-----	-----	-----	-----	0.042	-----	-----	-----	-----	0.042
1634	0.000	63.20	-----	-----	-----	-----	0.041	-----	-----	-----	-----	0.041
1635	0.000	63.20	-----	-----	-----	-----	0.040	-----	-----	-----	-----	0.040
1636	0.000	63.20	-----	-----	-----	-----	0.039	-----	-----	-----	-----	0.039
1637	0.000	63.20	-----	-----	-----	-----	0.038	-----	-----	-----	-----	0.038
1638	0.000	63.20	-----	-----	-----	-----	0.037	-----	-----	-----	-----	0.037
1639	0.000	63.20	-----	-----	-----	-----	0.037	-----	-----	-----	-----	0.036
1640	0.000	63.20	-----	-----	-----	-----	0.036	-----	-----	-----	-----	0.036
1641	0.000	63.20	-----	-----	-----	-----	0.035	-----	-----	-----	-----	0.035
1642	0.000	63.20	-----	-----	-----	-----	0.034	-----	-----	-----	-----	0.034
1643	0.000	63.20	-----	-----	-----	-----	0.033	-----	-----	-----	-----	0.033
1644	0.000	63.20	-----	-----	-----	-----	0.032	-----	-----	-----	-----	0.032
1645	0.000	63.20	-----	-----	-----	-----	0.032	-----	-----	-----	-----	0.032
1646	0.000	63.20	-----	-----	-----	-----	0.031	-----	-----	-----	-----	0.031
1647	0.000	63.20	-----	-----	-----	-----	0.030	-----	-----	-----	-----	0.030
1648	0.000	63.20	-----	-----	-----	-----	0.030	-----	-----	-----	-----	0.030
1649	0.000	63.20	-----	-----	-----	-----	0.029	-----	-----	-----	-----	0.029
1650	0.000	63.20	-----	-----	-----	-----	0.028	-----	-----	-----	-----	0.028

Continues on next page...

Detention pond outflow

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1651	0.000	63.20	-----	-----	-----	-----	0.028	-----	-----	-----	-----	0.028

...End

Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Hyd. No. 1

Developed site storm event

Hydrograph type	= SCS Runoff	Peak discharge	= 23.03 cfs
Storm frequency	= 100 yrs	Time to peak	= 495 min
Time interval	= 1 min	Hyd. volume	= 397,003 cuft
Drainage area	= 25.500 ac	Curve number	= 91
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 34.0 min
Total precip.	= 5.30 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 400

Hydrograph Discharge Table

(Printed values >= 1.00% of Qp.)

Time -- Outflow (min cfs)		Time -- Outflow (min cfs)		Time -- Outflow (min cfs)		Time -- Outflow (min cfs)	
133	0.243	172	0.955	211	1.536	250	2.213
134	0.258	173	0.972	212	1.549	251	2.232
135	0.274	174	0.990	213	1.564	252	2.250
136	0.290	175	1.007	214	1.578	253	2.268
137	0.306	176	1.024	215	1.592	254	2.286
138	0.323	177	1.041	216	1.607	255	2.304
139	0.340	178	1.057	217	1.622	256	2.322
140	0.358	179	1.074	218	1.637	257	2.340
141	0.375	180	1.090	219	1.653	258	2.357
142	0.393	181	1.107	220	1.668	259	2.375
143	0.411	182	1.123	221	1.684	260	2.392
144	0.429	183	1.139	222	1.700	261	2.409
145	0.448	184	1.155	223	1.717	262	2.427
146	0.467	185	1.170	224	1.733	263	2.444
147	0.485	186	1.186	225	1.750	264	2.461
148	0.504	187	1.201	226	1.767	265	2.478
149	0.523	188	1.216	227	1.784	266	2.495
150	0.543	189	1.231	228	1.802	267	2.512
151	0.562	190	1.246	229	1.820	268	2.529
152	0.581	191	1.260	230	1.838	269	2.547
153	0.600	192	1.275	231	1.856	270	2.564
154	0.620	193	1.289	232	1.874	271	2.581
155	0.639	194	1.304	233	1.893	272	2.598
156	0.659	195	1.318	234	1.912	273	2.616
157	0.678	196	1.332	235	1.930	274	2.633
158	0.697	197	1.345	236	1.949	275	2.650
159	0.716	198	1.359	237	1.968	276	2.668
160	0.736	199	1.373	238	1.987	277	2.685
161	0.755	200	1.386	239	2.006	278	2.703
162	0.774	201	1.400	240	2.025	279	2.720
163	0.792	202	1.413	241	2.044	280	2.738
164	0.811	203	1.427	242	2.063	281	2.756
165	0.830	204	1.440	243	2.082	282	2.774
166	0.848	205	1.454	244	2.101	283	2.792
167	0.866	206	1.467	245	2.120	284	2.810
168	0.884	207	1.481	246	2.139	285	2.829
169	0.902	208	1.494	247	2.158	286	2.847
170	0.920	209	1.508	248	2.176	287	2.866
171	0.938	210	1.522	249	2.195	288	2.885

Continues on next page...

Hydrograph Discharge Table

Time (min	Outflow cfs)	Time (min	Outflow cfs)	Time (min	Outflow cfs)	Time (min	Outflow cfs)
289	2.904	345	4.277	401	6.079	457	9.168
290	2.923	346	4.302	402	6.104	458	9.426
291	2.943	347	4.326	403	6.127	459	9.707
292	2.962	348	4.349	404	6.149	460	10.01
293	2.982	349	4.373	405	6.170	461	10.34
294	3.002	350	4.397	406	6.190	462	10.69
295	3.022	351	4.420	407	6.208	463	11.06
296	3.043	352	4.444	408	6.226	464	11.45
297	3.064	353	4.468	409	6.242	465	11.87
298	3.084	354	4.492	410	6.258	466	12.31
299	3.105	355	4.516	411	6.273	467	12.77
300	3.127	356	4.541	412	6.287	468	13.25
301	3.148	357	4.565	413	6.302	469	13.76
302	3.170	358	4.590	414	6.318	470	14.28
303	3.193	359	4.616	415	6.334	471	14.83
304	3.215	360	4.642	416	6.351	472	15.37
305	3.238	361	4.668	417	6.368	473	15.91
306	3.261	362	4.694	418	6.387	474	16.45
307	3.285	363	4.722	419	6.407	475	16.97
308	3.309	364	4.750	420	6.427	476	17.49
309	3.333	365	4.779	421	6.449	477	18.00
310	3.357	366	4.809	422	6.472	478	18.50
311	3.382	367	4.840	423	6.497	479	18.98
312	3.407	368	4.871	424	6.522	480	19.46
313	3.432	369	4.904	425	6.550	481	19.90
314	3.458	370	4.937	426	6.578	482	20.33
315	3.484	371	4.971	427	6.609	483	20.72
316	3.510	372	5.005	428	6.641	484	21.08
317	3.536	373	5.041	429	6.675	485	21.42
318	3.562	374	5.077	430	6.711	486	21.73
319	3.589	375	5.114	431	6.750	487	22.00
320	3.616	376	5.152	432	6.790	488	22.24
321	3.643	377	5.190	433	6.833	489	22.45
322	3.671	378	5.230	434	6.878	490	22.63
323	3.698	379	5.269	435	6.926	491	22.78
324	3.725	380	5.310	436	6.976	492	22.89
325	3.753	381	5.351	437	7.028	493	22.97
326	3.780	382	5.392	438	7.083	494	23.01
327	3.808	383	5.434	439	7.141	495	23.03 <<
328	3.835	384	5.475	440	7.201	496	23.00
329	3.863	385	5.516	441	7.265	497	22.95
330	3.890	386	5.557	442	7.331	498	22.86
331	3.917	387	5.598	443	7.400	499	22.74
332	3.945	388	5.638	444	7.472	500	22.59
333	3.971	389	5.679	445	7.547	501	22.40
334	3.998	390	5.718	446	7.625	502	22.20
335	4.025	391	5.758	447	7.705	503	21.98
336	4.051	392	5.796	448	7.790	504	21.75
337	4.077	393	5.832	449	7.877	505	21.50
338	4.103	394	5.868	450	7.967	506	21.25
339	4.128	395	5.902	451	8.076	507	20.97
340	4.154	396	5.935	452	8.206	508	20.69
341	4.179	397	5.966	453	8.355	509	20.39
342	4.204	398	5.996	454	8.526	510	20.09
343	4.229	399	6.025	455	8.718	511	19.78
344	4.253	400	6.053	456	8.932	512	19.46

Continues on next page...

Hydrograph Discharge Table

Time (min	Outflow cfs)	Time (min	Outflow cfs)	Time (min	Outflow cfs)	Time (min	Outflow cfs)
513	19.13	569	8.680	625	6.622	681	5.780
514	18.80	570	8.608	626	6.599	682	5.766
515	18.47	571	8.534	627	6.577	683	5.752
516	18.13	572	8.462	628	6.555	684	5.737
517	17.78	573	8.391	629	6.533	685	5.723
518	17.43	574	8.320	630	6.511	686	5.708
519	17.09	575	8.251	631	6.490	687	5.694
520	16.75	576	8.184	632	6.469	688	5.679
521	16.42	577	8.117	633	6.449	689	5.664
522	16.09	578	8.051	634	6.429	690	5.648
523	15.77	579	7.988	635	6.410	691	5.633
524	15.46	580	7.928	636	6.391	692	5.617
525	15.16	581	7.869	637	6.373	693	5.601
526	14.87	582	7.813	638	6.355	694	5.584
527	14.58	583	7.759	639	6.336	695	5.567
528	14.31	584	7.707	640	6.318	696	5.550
529	14.04	585	7.656	641	6.301	697	5.533
530	13.78	586	7.608	642	6.284	698	5.516
531	13.54	587	7.562	643	6.267	699	5.498
532	13.30	588	7.517	644	6.252	700	5.480
533	13.07	589	7.475	645	6.237	701	5.463
534	12.84	590	7.434	646	6.222	702	5.445
535	12.62	591	7.395	647	6.208	703	5.427
536	12.41	592	7.361	648	6.194	704	5.409
537	12.21	593	7.329	649	6.181	705	5.391
538	12.02	594	7.298	650	6.168	706	5.373
539	11.84	595	7.268	651	6.156	707	5.355
540	11.66	596	7.238	652	6.144	708	5.337
541	11.49	597	7.210	653	6.132	709	5.319
542	11.33	598	7.182	654	6.119	710	5.301
543	11.18	599	7.155	655	6.107	711	5.283
544	11.03	600	7.129	656	6.095	712	5.265
545	10.90	601	7.107	657	6.083	713	5.247
546	10.77	602	7.085	658	6.070	714	5.230
547	10.65	603	7.064	659	6.058	715	5.213
548	10.54	604	7.043	660	6.045	716	5.197
549	10.43	605	7.023	661	6.033	717	5.180
550	10.32	606	7.003	662	6.020	718	5.164
551	10.22	607	6.983	663	6.008	719	5.149
552	10.11	608	6.964	664	5.995	720	5.134
553	10.01	609	6.943	665	5.982	721	5.119
554	9.918	610	6.924	666	5.970	722	5.104
555	9.823	611	6.904	667	5.957	723	5.090
556	9.730	612	6.885	668	5.944	724	5.076
557	9.639	613	6.865	669	5.932	725	5.063
558	9.550	614	6.846	670	5.920	726	5.050
559	9.462	615	6.827	671	5.908	727	5.038
560	9.376	616	6.808	672	5.896	728	5.026
561	9.291	617	6.789	673	5.884	729	5.014
562	9.210	618	6.770	674	5.872	730	5.003
563	9.131	619	6.751	675	5.859	731	4.993
564	9.053	620	6.732	676	5.846	732	4.983
565	8.977	621	6.713	677	5.833	733	4.973
566	8.901	622	6.690	678	5.820	734	4.964
567	8.826	623	6.667	679	5.807	735	4.956
568	8.753	624	6.644	680	5.793	736	4.948

Continues on next page...

Hydrograph Discharge Table

Time (min	Outflow cfs)	Time (min	Outflow cfs)	Time (min	Outflow cfs)	Time (min	Outflow cfs)
737	4.941	793	4.756	849	4.484	905	4.333
738	4.934	794	4.753	850	4.479	906	4.330
739	4.927	795	4.751	851	4.474	907	4.327
740	4.922	796	4.749	852	4.470	908	4.324
741	4.917	797	4.747	853	4.466	909	4.321
742	4.912	798	4.745	854	4.461	910	4.318
743	4.908	799	4.743	855	4.458	911	4.315
744	4.905	800	4.742	856	4.454	912	4.312
745	4.902	801	4.740	857	4.451	913	4.309
746	4.900	802	4.739	858	4.448	914	4.306
747	4.898	803	4.737	859	4.445	915	4.302
748	4.897	804	4.734	860	4.442	916	4.299
749	4.897	805	4.731	861	4.439	917	4.296
750	4.897	806	4.728	862	4.437	918	4.293
751	4.897	807	4.725	863	4.434	919	4.290
752	4.898	808	4.721	864	4.432	920	4.287
753	4.898	809	4.717	865	4.429	921	4.284
754	4.899	810	4.713	866	4.427	922	4.281
755	4.899	811	4.708	867	4.425	923	4.278
756	4.900	812	4.704	868	4.423	924	4.275
757	4.900	813	4.699	869	4.420	925	4.271
758	4.901	814	4.695	870	4.418	926	4.268
759	4.901	815	4.690	871	4.416	927	4.265
760	4.900	816	4.685	872	4.414	928	4.262
761	4.900	817	4.680	873	4.412	929	4.259
762	4.899	818	4.675	874	4.410	930	4.256
763	4.897	819	4.670	875	4.408	931	4.253
764	4.895	820	4.665	876	4.405	932	4.250
765	4.893	821	4.660	877	4.403	933	4.247
766	4.890	822	4.654	878	4.401	934	4.243
767	4.887	823	4.648	879	4.399	935	4.240
768	4.883	824	4.643	880	4.397	936	4.237
769	4.878	825	4.637	881	4.395	937	4.234
770	4.873	826	4.630	882	4.393	938	4.231
771	4.867	827	4.624	883	4.390	939	4.228
772	4.861	828	4.618	884	4.388	940	4.225
773	4.855	829	4.612	885	4.386	941	4.222
774	4.848	830	4.605	886	4.384	942	4.219
775	4.842	831	4.599	887	4.381	943	4.215
776	4.836	832	4.592	888	4.379	944	4.212
777	4.829	833	4.585	889	4.377	945	4.209
778	4.823	834	4.579	890	4.374	946	4.206
779	4.816	835	4.572	891	4.372	947	4.203
780	4.810	836	4.565	892	4.369	948	4.200
781	4.804	837	4.559	893	4.367	949	4.197
782	4.798	838	4.552	894	4.364	950	4.194
783	4.793	839	4.545	895	4.361	951	4.191
784	4.788	840	4.539	896	4.359	952	4.187
785	4.783	841	4.532	897	4.356	953	4.184
786	4.779	842	4.526	898	4.353	954	4.181
787	4.775	843	4.519	899	4.351	955	4.178
788	4.771	844	4.513	900	4.348	956	4.175
789	4.767	845	4.507	901	4.345	957	4.172
790	4.764	846	4.501	902	4.342	958	4.169
791	4.761	847	4.495	903	4.339	959	4.165
792	4.758	848	4.490	904	4.336	960	4.162

Continues on next page...

Hydrograph Discharge Table

Time (min)	Outflow (cfs)	Time (min)	Outflow (cfs)	Time (min)	Outflow (cfs)	Time (min)	Outflow (cfs)
961	4.159	1017	3.983	1073	3.804	1129	3.624
962	4.156	1018	3.979	1074	3.801	1130	3.620
963	4.153	1019	3.976	1075	3.798	1131	3.617
964	4.150	1020	3.973	1076	3.794	1132	3.614
965	4.147	1021	3.970	1077	3.791	1133	3.611
966	4.144	1022	3.967	1078	3.788	1134	3.607
967	4.140	1023	3.964	1079	3.785	1135	3.604
968	4.137	1024	3.960	1080	3.782	1136	3.601
969	4.134	1025	3.957	1081	3.778	1137	3.598
970	4.131	1026	3.954	1082	3.775	1138	3.594
971	4.128	1027	3.951	1083	3.772	1139	3.591
972	4.125	1028	3.948	1084	3.769	1140	3.588
973	4.122	1029	3.945	1085	3.765	1141	3.585
974	4.118	1030	3.941	1086	3.762	1142	3.582
975	4.115	1031	3.938	1087	3.759	1143	3.578
976	4.112	1032	3.935	1088	3.756	1144	3.575
977	4.109	1033	3.932	1089	3.753	1145	3.572
978	4.106	1034	3.929	1090	3.749	1146	3.569
979	4.103	1035	3.925	1091	3.746	1147	3.565
980	4.100	1036	3.922	1092	3.743	1148	3.562
981	4.096	1037	3.919	1093	3.740	1149	3.559
982	4.093	1038	3.916	1094	3.737	1150	3.556
983	4.090	1039	3.913	1095	3.733	1151	3.552
984	4.087	1040	3.910	1096	3.730	1152	3.549
985	4.084	1041	3.906	1097	3.727	1153	3.546
986	4.081	1042	3.903	1098	3.724	1154	3.543
987	4.078	1043	3.900	1099	3.720	1155	3.539
988	4.074	1044	3.897	1100	3.717	1156	3.536
989	4.071	1045	3.894	1101	3.714	1157	3.533
990	4.068	1046	3.890	1102	3.711	1158	3.530
991	4.065	1047	3.887	1103	3.708	1159	3.526
992	4.062	1048	3.884	1104	3.704	1160	3.523
993	4.059	1049	3.881	1105	3.701	1161	3.520
994	4.055	1050	3.878	1106	3.698	1162	3.517
995	4.052	1051	3.874	1107	3.695	1163	3.513
996	4.049	1052	3.871	1108	3.691	1164	3.510
997	4.046	1053	3.868	1109	3.688	1165	3.507
998	4.043	1054	3.865	1110	3.685	1166	3.504
999	4.040	1055	3.862	1111	3.682	1167	3.500
1000	4.036	1056	3.858	1112	3.679	1168	3.497
1001	4.033	1057	3.855	1113	3.675	1169	3.494
1002	4.030	1058	3.852	1114	3.672	1170	3.491
1003	4.027	1059	3.849	1115	3.669	1171	3.487
1004	4.024	1060	3.846	1116	3.666	1172	3.484
1005	4.021	1061	3.842	1117	3.662	1173	3.481
1006	4.018	1062	3.839	1118	3.659	1174	3.478
1007	4.014	1063	3.836	1119	3.656	1175	3.474
1008	4.011	1064	3.833	1120	3.653	1176	3.471
1009	4.008	1065	3.830	1121	3.649	1177	3.468
1010	4.005	1066	3.826	1122	3.646	1178	3.465
1011	4.002	1067	3.823	1123	3.643	1179	3.461
1012	3.999	1068	3.820	1124	3.640	1180	3.458
1013	3.995	1069	3.817	1125	3.637	1181	3.455
1014	3.992	1070	3.814	1126	3.633	1182	3.452
1015	3.989	1071	3.810	1127	3.630	1183	3.448
1016	3.986	1072	3.807	1128	3.627	1184	3.445

Continues on next page...

Hydrograph Discharge Table

Time (min)	Outflow (cfs)	Time (min)	Outflow (cfs)	Time (min)	Outflow (cfs)	Time (min)	Outflow (cfs)
1185	3.442	1241	3.259	1297	3.075	1353	2.889
1186	3.439	1242	3.255	1298	3.071	1354	2.886
1187	3.435	1243	3.252	1299	3.068	1355	2.883
1188	3.432	1244	3.249	1300	3.065	1356	2.880
1189	3.429	1245	3.246	1301	3.061	1357	2.876
1190	3.425	1246	3.242	1302	3.058	1358	2.873
1191	3.422	1247	3.239	1303	3.055	1359	2.870
1192	3.419	1248	3.236	1304	3.051	1360	2.866
1193	3.416	1249	3.232	1305	3.048	1361	2.863
1194	3.412	1250	3.229	1306	3.045	1362	2.860
1195	3.409	1251	3.226	1307	3.042	1363	2.856
1196	3.406	1252	3.223	1308	3.038	1364	2.853
1197	3.403	1253	3.219	1309	3.035	1365	2.850
1198	3.399	1254	3.216	1310	3.032	1366	2.846
1199	3.396	1255	3.213	1311	3.028	1367	2.843
1200	3.393	1256	3.209	1312	3.025	1368	2.840
1201	3.390	1257	3.206	1313	3.022	1369	2.836
1202	3.386	1258	3.203	1314	3.018	1370	2.833
1203	3.383	1259	3.200	1315	3.015	1371	2.830
1204	3.380	1260	3.196	1316	3.012	1372	2.827
1205	3.377	1261	3.193	1317	3.009	1373	2.823
1206	3.373	1262	3.190	1318	3.005	1374	2.820
1207	3.370	1263	3.186	1319	3.002	1375	2.817
1208	3.367	1264	3.183	1320	2.999	1376	2.813
1209	3.363	1265	3.180	1321	2.995	1377	2.810
1210	3.360	1266	3.177	1322	2.992	1378	2.807
1211	3.357	1267	3.173	1323	2.989	1379	2.803
1212	3.354	1268	3.170	1324	2.985	1380	2.800
1213	3.350	1269	3.167	1325	2.982	1381	2.797
1214	3.347	1270	3.163	1326	2.979	1382	2.793
1215	3.344	1271	3.160	1327	2.975	1383	2.790
1216	3.341	1272	3.157	1328	2.972	1384	2.787
1217	3.337	1273	3.154	1329	2.969	1385	2.783
1218	3.334	1274	3.150	1330	2.966	1386	2.780
1219	3.331	1275	3.147	1331	2.962	1387	2.777
1220	3.327	1276	3.144	1332	2.959	1388	2.773
1221	3.324	1277	3.140	1333	2.956	1389	2.770
1222	3.321	1278	3.137	1334	2.952	1390	2.767
1223	3.318	1279	3.134	1335	2.949	1391	2.763
1224	3.314	1280	3.131	1336	2.946	1392	2.760
1225	3.311	1281	3.127	1337	2.942	1393	2.757
1226	3.308	1282	3.124	1338	2.939	1394	2.753
1227	3.305	1283	3.121	1339	2.936	1395	2.750
1228	3.301	1284	3.117	1340	2.933	1396	2.747
1229	3.298	1285	3.114	1341	2.929	1397	2.744
1230	3.295	1286	3.111	1342	2.926	1398	2.740
1231	3.291	1287	3.107	1343	2.923	1399	2.737
1232	3.288	1288	3.104	1344	2.919	1400	2.734
1233	3.285	1289	3.101	1345	2.916	1401	2.730
1234	3.282	1290	3.098	1346	2.913	1402	2.727
1235	3.278	1291	3.094	1347	2.909	1403	2.724
1236	3.275	1292	3.091	1348	2.906	1404	2.720
1237	3.272	1293	3.088	1349	2.903	1405	2.717
1238	3.269	1294	3.084	1350	2.899	1406	2.714
1239	3.265	1295	3.081	1351	2.896	1407	2.710
1240	3.262	1296	3.078	1352	2.893	1408	2.707

Continues on next page...

Developed site storm event

Hydrograph Discharge Table

Time (min	Outflow cfs)	Time (min	Outflow cfs)
1409	2.704	1465	1.441
1410	2.700	1466	1.374
1411	2.697	1467	1.308
1412	2.694	1468	1.243
1413	2.690	1469	1.181
1414	2.687	1470	1.120
1415	2.684	1471	1.060
1416	2.680	1472	1.002
1417	2.677	1473	0.946
1418	2.674	1474	0.892
1419	2.670	1475	0.839
1420	2.667	1476	0.788
1421	2.664	1477	0.738
1422	2.660	1478	0.690
1423	2.657	1479	0.644
1424	2.654	1480	0.599
1425	2.650	1481	0.556
1426	2.647	1482	0.515
1427	2.644	1483	0.475
1428	2.640	1484	0.437
1429	2.637	1485	0.400
1430	2.634	1486	0.365
1431	2.630	1487	0.332
1432	2.627	1488	0.300
1433	2.624	1489	0.270
1434	2.620	1490	0.242
1435	2.617		
1436	2.614	*...End*	
1437	2.610		
1438	2.607		
1439	2.604		
1440	2.600		
1441	2.594		
1442	2.583		
1443	2.570		
1444	2.552		
1445	2.531		
1446	2.507		
1447	2.479		
1448	2.448		
1449	2.413		
1450	2.375		
1451	2.334		
1452	2.289		
1453	2.240		
1454	2.188		
1455	2.133		
1456	2.074		
1457	2.012		
1458	1.946		
1459	1.877		
1460	1.804		
1461	1.728		
1462	1.654		
1463	1.581		
1464	1.511		

Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Hyd. No. 2

Detention pond outflow

Hydrograph type	= Reservoir	Peak discharge	= 6.197 cfs
Storm frequency	= 100 yrs	Time to peak	= 648 min
Time interval	= 1 min	Hyd. volume	= 223,992 cuft
Inflow hyd. No.	= 1 - Developed site storm event	Reservoir name	= Detention Pond
Max. Elevation	= 63.38 ft	Max. Storage	= 184,578 cuft

Storage Indication method used.

Hydrograph Discharge Table

(Printed values >= 1.00% of Qp.)

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
574	8.320	63.21	-----	-----	-----	-----	0.136	-----	-----	-----	-----	0.136
575	8.251	63.21	-----	-----	-----	-----	0.324	-----	-----	-----	-----	0.324
576	8.184	63.22	-----	-----	-----	-----	0.507	-----	-----	-----	-----	0.507
577	8.117	63.23	-----	-----	-----	-----	0.683	-----	-----	-----	-----	0.683
578	8.051	63.23	-----	-----	-----	-----	0.854	-----	-----	-----	-----	0.854
579	7.988	63.24	-----	-----	-----	-----	1.020	-----	-----	-----	-----	1.020
580	7.928	63.25	-----	-----	-----	-----	1.180	-----	-----	-----	-----	1.180
581	7.869	63.25	-----	-----	-----	-----	1.335	-----	-----	-----	-----	1.335
582	7.813	63.26	-----	-----	-----	-----	1.486	-----	-----	-----	-----	1.486
583	7.759	63.27	-----	-----	-----	-----	1.631	-----	-----	-----	-----	1.631
584	7.707	63.27	-----	-----	-----	-----	1.772	-----	-----	-----	-----	1.772
585	7.656	63.28	-----	-----	-----	-----	1.909	-----	-----	-----	-----	1.909
586	7.608	63.28	-----	-----	-----	-----	2.041	-----	-----	-----	-----	2.041
587	7.562	63.29	-----	-----	-----	-----	2.169	-----	-----	-----	-----	2.169
588	7.517	63.29	-----	-----	-----	-----	2.293	-----	-----	-----	-----	2.293
589	7.475	63.30	-----	-----	-----	-----	2.413	-----	-----	-----	-----	2.413
590	7.434	63.30	-----	-----	-----	-----	2.581	-----	-----	-----	-----	2.581
591	7.395	63.31	-----	-----	-----	-----	2.783	-----	-----	-----	-----	2.783
592	7.361	63.31	-----	-----	-----	-----	2.975	-----	-----	-----	-----	2.975
593	7.329	63.32	-----	-----	-----	-----	3.158	-----	-----	-----	-----	3.158
594	7.298	63.32	-----	-----	-----	-----	3.332	-----	-----	-----	-----	3.332
595	7.268	63.32	-----	-----	-----	-----	3.497	-----	-----	-----	-----	3.497
596	7.238	63.33	-----	-----	-----	-----	3.654	-----	-----	-----	-----	3.654
597	7.210	63.33	-----	-----	-----	-----	3.804	-----	-----	-----	-----	3.804
598	7.182	63.33	-----	-----	-----	-----	3.946	-----	-----	-----	-----	3.946
599	7.155	63.34	-----	-----	-----	-----	4.080	-----	-----	-----	-----	4.080
600	7.129	63.34	-----	-----	-----	-----	4.209	-----	-----	-----	-----	4.209
601	7.107	63.34	-----	-----	-----	-----	4.330	-----	-----	-----	-----	4.330
602	7.085	63.34	-----	-----	-----	-----	4.446	-----	-----	-----	-----	4.446
603	7.064	63.35	-----	-----	-----	-----	4.556	-----	-----	-----	-----	4.556
604	7.043	63.35	-----	-----	-----	-----	4.661	-----	-----	-----	-----	4.660
605	7.023	63.35	-----	-----	-----	-----	4.760	-----	-----	-----	-----	4.760
606	7.003	63.35	-----	-----	-----	-----	4.854	-----	-----	-----	-----	4.854
607	6.983	63.35	-----	-----	-----	-----	4.944	-----	-----	-----	-----	4.943
608	6.964	63.36	-----	-----	-----	-----	5.028	-----	-----	-----	-----	5.028
609	6.943	63.36	-----	-----	-----	-----	5.109	-----	-----	-----	-----	5.109
610	6.924	63.36	-----	-----	-----	-----	5.185	-----	-----	-----	-----	5.185
611	6.904	63.36	-----	-----	-----	-----	5.257	-----	-----	-----	-----	5.258
612	6.885	63.36	-----	-----	-----	-----	5.326	-----	-----	-----	-----	5.326
613	6.865	63.36	-----	-----	-----	-----	5.391	-----	-----	-----	-----	5.391
614	6.846	63.37	-----	-----	-----	-----	5.452	-----	-----	-----	-----	5.452
615	6.827	63.37	-----	-----	-----	-----	5.510	-----	-----	-----	-----	5.510

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
616	6.808	63.37	-----	-----	-----	-----	5.565	-----	-----	-----	-----	5.565
617	6.789	63.37	-----	-----	-----	-----	5.616	-----	-----	-----	-----	5.616
618	6.770	63.37	-----	-----	-----	-----	5.665	-----	-----	-----	-----	5.665
619	6.751	63.37	-----	-----	-----	-----	5.711	-----	-----	-----	-----	5.711
620	6.732	63.37	-----	-----	-----	-----	5.754	-----	-----	-----	-----	5.754
621	6.713	63.37	-----	-----	-----	-----	5.794	-----	-----	-----	-----	5.794
622	6.690	63.37	-----	-----	-----	-----	5.832	-----	-----	-----	-----	5.832
623	6.667	63.38	-----	-----	-----	-----	5.868	-----	-----	-----	-----	5.868
624	6.644	63.38	-----	-----	-----	-----	5.901	-----	-----	-----	-----	5.901
625	6.622	63.38	-----	-----	-----	-----	5.931	-----	-----	-----	-----	5.931
626	6.599	63.38	-----	-----	-----	-----	5.960	-----	-----	-----	-----	5.960
627	6.577	63.38	-----	-----	-----	-----	5.986	-----	-----	-----	-----	5.986
628	6.555	63.38	-----	-----	-----	-----	6.010	-----	-----	-----	-----	6.010
629	6.533	63.38	-----	-----	-----	-----	6.033	-----	-----	-----	-----	6.033
630	6.511	63.38	-----	-----	-----	-----	6.053	-----	-----	-----	-----	6.053
631	6.490	63.38	-----	-----	-----	-----	6.072	-----	-----	-----	-----	6.072
632	6.469	63.38	-----	-----	-----	-----	6.089	-----	-----	-----	-----	6.089
633	6.449	63.38	-----	-----	-----	-----	6.104	-----	-----	-----	-----	6.104
634	6.429	63.38	-----	-----	-----	-----	6.119	-----	-----	-----	-----	6.118
635	6.410	63.38	-----	-----	-----	-----	6.131	-----	-----	-----	-----	6.131
636	6.391	63.38	-----	-----	-----	-----	6.142	-----	-----	-----	-----	6.142
637	6.373	63.38	-----	-----	-----	-----	6.152	-----	-----	-----	-----	6.152
638	6.355	63.38	-----	-----	-----	-----	6.161	-----	-----	-----	-----	6.161
639	6.336	63.38	-----	-----	-----	-----	6.169	-----	-----	-----	-----	6.169
640	6.318	63.38	-----	-----	-----	-----	6.175	-----	-----	-----	-----	6.176
641	6.301	63.38	-----	-----	-----	-----	6.181	-----	-----	-----	-----	6.181
642	6.284	63.38	-----	-----	-----	-----	6.186	-----	-----	-----	-----	6.186
643	6.267	63.38	-----	-----	-----	-----	6.190	-----	-----	-----	-----	6.190
644	6.252	63.38	-----	-----	-----	-----	6.193	-----	-----	-----	-----	6.192
645	6.237	63.38	-----	-----	-----	-----	6.195	-----	-----	-----	-----	6.195
646	6.222	63.38	-----	-----	-----	-----	6.196	-----	-----	-----	-----	6.196
647	6.208	63.38	-----	-----	-----	-----	6.197	-----	-----	-----	-----	6.197
648	6.194	63.38 <<	-----	-----	-----	-----	6.197	-----	-----	-----	-----	6.197 <<
649	6.181	63.38	-----	-----	-----	-----	6.197	-----	-----	-----	-----	6.197
650	6.168	63.38	-----	-----	-----	-----	6.196	-----	-----	-----	-----	6.196
651	6.156	63.38	-----	-----	-----	-----	6.194	-----	-----	-----	-----	6.194
652	6.144	63.38	-----	-----	-----	-----	6.193	-----	-----	-----	-----	6.192
653	6.132	63.38	-----	-----	-----	-----	6.190	-----	-----	-----	-----	6.190
654	6.119	63.38	-----	-----	-----	-----	6.188	-----	-----	-----	-----	6.187
655	6.107	63.38	-----	-----	-----	-----	6.184	-----	-----	-----	-----	6.184
656	6.095	63.38	-----	-----	-----	-----	6.181	-----	-----	-----	-----	6.181
657	6.083	63.38	-----	-----	-----	-----	6.177	-----	-----	-----	-----	6.177
658	6.070	63.38	-----	-----	-----	-----	6.173	-----	-----	-----	-----	6.173
659	6.058	63.38	-----	-----	-----	-----	6.168	-----	-----	-----	-----	6.168
660	6.045	63.38	-----	-----	-----	-----	6.163	-----	-----	-----	-----	6.163
661	6.033	63.38	-----	-----	-----	-----	6.158	-----	-----	-----	-----	6.158
662	6.020	63.38	-----	-----	-----	-----	6.153	-----	-----	-----	-----	6.153
663	6.008	63.38	-----	-----	-----	-----	6.147	-----	-----	-----	-----	6.147
664	5.995	63.38	-----	-----	-----	-----	6.141	-----	-----	-----	-----	6.141
665	5.982	63.38	-----	-----	-----	-----	6.134	-----	-----	-----	-----	6.134
666	5.970	63.38	-----	-----	-----	-----	6.128	-----	-----	-----	-----	6.128
667	5.957	63.38	-----	-----	-----	-----	6.121	-----	-----	-----	-----	6.121
668	5.944	63.38	-----	-----	-----	-----	6.114	-----	-----	-----	-----	6.114
669	5.932	63.38	-----	-----	-----	-----	6.106	-----	-----	-----	-----	6.106
670	5.920	63.38	-----	-----	-----	-----	6.099	-----	-----	-----	-----	6.099
671	5.908	63.38	-----	-----	-----	-----	6.091	-----	-----	-----	-----	6.091

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
672	5.896	63.38	-----	-----	-----	-----	6.083	-----	-----	-----	-----	6.083
673	5.884	63.38	-----	-----	-----	-----	6.075	-----	-----	-----	-----	6.075
674	5.872	63.38	-----	-----	-----	-----	6.067	-----	-----	-----	-----	6.067
675	5.859	63.38	-----	-----	-----	-----	6.058	-----	-----	-----	-----	6.058
676	5.846	63.38	-----	-----	-----	-----	6.050	-----	-----	-----	-----	6.050
677	5.833	63.38	-----	-----	-----	-----	6.041	-----	-----	-----	-----	6.041
678	5.820	63.38	-----	-----	-----	-----	6.032	-----	-----	-----	-----	6.032
679	5.807	63.38	-----	-----	-----	-----	6.023	-----	-----	-----	-----	6.023
680	5.793	63.38	-----	-----	-----	-----	6.014	-----	-----	-----	-----	6.014
681	5.780	63.38	-----	-----	-----	-----	6.004	-----	-----	-----	-----	6.004
682	5.766	63.38	-----	-----	-----	-----	5.994	-----	-----	-----	-----	5.994
683	5.752	63.38	-----	-----	-----	-----	5.985	-----	-----	-----	-----	5.985
684	5.737	63.38	-----	-----	-----	-----	5.975	-----	-----	-----	-----	5.974
685	5.723	63.38	-----	-----	-----	-----	5.964	-----	-----	-----	-----	5.964
686	5.708	63.38	-----	-----	-----	-----	5.954	-----	-----	-----	-----	5.954
687	5.694	63.38	-----	-----	-----	-----	5.943	-----	-----	-----	-----	5.943
688	5.679	63.38	-----	-----	-----	-----	5.933	-----	-----	-----	-----	5.933
689	5.664	63.38	-----	-----	-----	-----	5.922	-----	-----	-----	-----	5.922
690	5.648	63.38	-----	-----	-----	-----	5.911	-----	-----	-----	-----	5.910
691	5.633	63.38	-----	-----	-----	-----	5.899	-----	-----	-----	-----	5.899
692	5.617	63.38	-----	-----	-----	-----	5.888	-----	-----	-----	-----	5.888
693	5.601	63.38	-----	-----	-----	-----	5.876	-----	-----	-----	-----	5.876
694	5.584	63.38	-----	-----	-----	-----	5.864	-----	-----	-----	-----	5.864
695	5.567	63.38	-----	-----	-----	-----	5.852	-----	-----	-----	-----	5.852
696	5.550	63.37	-----	-----	-----	-----	5.840	-----	-----	-----	-----	5.840
697	5.533	63.37	-----	-----	-----	-----	5.827	-----	-----	-----	-----	5.827
698	5.516	63.37	-----	-----	-----	-----	5.815	-----	-----	-----	-----	5.815
699	5.498	63.37	-----	-----	-----	-----	5.802	-----	-----	-----	-----	5.802
700	5.480	63.37	-----	-----	-----	-----	5.789	-----	-----	-----	-----	5.789
701	5.463	63.37	-----	-----	-----	-----	5.775	-----	-----	-----	-----	5.775
702	5.445	63.37	-----	-----	-----	-----	5.762	-----	-----	-----	-----	5.762
703	5.427	63.37	-----	-----	-----	-----	5.748	-----	-----	-----	-----	5.748
704	5.409	63.37	-----	-----	-----	-----	5.735	-----	-----	-----	-----	5.734
705	5.391	63.37	-----	-----	-----	-----	5.720	-----	-----	-----	-----	5.720
706	5.373	63.37	-----	-----	-----	-----	5.706	-----	-----	-----	-----	5.706
707	5.355	63.37	-----	-----	-----	-----	5.692	-----	-----	-----	-----	5.692
708	5.337	63.37	-----	-----	-----	-----	5.677	-----	-----	-----	-----	5.678
709	5.319	63.37	-----	-----	-----	-----	5.663	-----	-----	-----	-----	5.663
710	5.301	63.37	-----	-----	-----	-----	5.648	-----	-----	-----	-----	5.648
711	5.283	63.37	-----	-----	-----	-----	5.633	-----	-----	-----	-----	5.633
712	5.265	63.37	-----	-----	-----	-----	5.618	-----	-----	-----	-----	5.618
713	5.247	63.37	-----	-----	-----	-----	5.603	-----	-----	-----	-----	5.603
714	5.230	63.37	-----	-----	-----	-----	5.588	-----	-----	-----	-----	5.588
715	5.213	63.37	-----	-----	-----	-----	5.572	-----	-----	-----	-----	5.572
716	5.197	63.37	-----	-----	-----	-----	5.557	-----	-----	-----	-----	5.557
717	5.180	63.37	-----	-----	-----	-----	5.542	-----	-----	-----	-----	5.542
718	5.164	63.37	-----	-----	-----	-----	5.526	-----	-----	-----	-----	5.526
719	5.149	63.37	-----	-----	-----	-----	5.511	-----	-----	-----	-----	5.511
720	5.134	63.37	-----	-----	-----	-----	5.495	-----	-----	-----	-----	5.495
721	5.119	63.37	-----	-----	-----	-----	5.480	-----	-----	-----	-----	5.480
722	5.104	63.37	-----	-----	-----	-----	5.464	-----	-----	-----	-----	5.464
723	5.090	63.37	-----	-----	-----	-----	5.449	-----	-----	-----	-----	5.449
724	5.076	63.37	-----	-----	-----	-----	5.434	-----	-----	-----	-----	5.434
725	5.063	63.37	-----	-----	-----	-----	5.419	-----	-----	-----	-----	5.419
726	5.050	63.37	-----	-----	-----	-----	5.403	-----	-----	-----	-----	5.403
727	5.038	63.36	-----	-----	-----	-----	5.388	-----	-----	-----	-----	5.388

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
728	5.026	63.36	-----	-----	-----	-----	5.373	-----	-----	-----	-----	5.373
729	5.014	63.36	-----	-----	-----	-----	5.359	-----	-----	-----	-----	5.359
730	5.003	63.36	-----	-----	-----	-----	5.344	-----	-----	-----	-----	5.344
731	4.993	63.36	-----	-----	-----	-----	5.330	-----	-----	-----	-----	5.330
732	4.983	63.36	-----	-----	-----	-----	5.315	-----	-----	-----	-----	5.315
733	4.973	63.36	-----	-----	-----	-----	5.301	-----	-----	-----	-----	5.301
734	4.964	63.36	-----	-----	-----	-----	5.287	-----	-----	-----	-----	5.287
735	4.956	63.36	-----	-----	-----	-----	5.273	-----	-----	-----	-----	5.274
736	4.948	63.36	-----	-----	-----	-----	5.260	-----	-----	-----	-----	5.260
737	4.941	63.36	-----	-----	-----	-----	5.247	-----	-----	-----	-----	5.247
738	4.934	63.36	-----	-----	-----	-----	5.234	-----	-----	-----	-----	5.234
739	4.927	63.36	-----	-----	-----	-----	5.221	-----	-----	-----	-----	5.221
740	4.922	63.36	-----	-----	-----	-----	5.209	-----	-----	-----	-----	5.209
741	4.917	63.36	-----	-----	-----	-----	5.197	-----	-----	-----	-----	5.197
742	4.912	63.36	-----	-----	-----	-----	5.185	-----	-----	-----	-----	5.185
743	4.908	63.36	-----	-----	-----	-----	5.173	-----	-----	-----	-----	5.173
744	4.905	63.36	-----	-----	-----	-----	5.162	-----	-----	-----	-----	5.162
745	4.902	63.36	-----	-----	-----	-----	5.151	-----	-----	-----	-----	5.151
746	4.900	63.36	-----	-----	-----	-----	5.141	-----	-----	-----	-----	5.141
747	4.898	63.36	-----	-----	-----	-----	5.131	-----	-----	-----	-----	5.131
748	4.897	63.36	-----	-----	-----	-----	5.121	-----	-----	-----	-----	5.121
749	4.897	63.36	-----	-----	-----	-----	5.112	-----	-----	-----	-----	5.112
750	4.897	63.36	-----	-----	-----	-----	5.103	-----	-----	-----	-----	5.103
751	4.897	63.36	-----	-----	-----	-----	5.094	-----	-----	-----	-----	5.094
752	4.898	63.36	-----	-----	-----	-----	5.086	-----	-----	-----	-----	5.086
753	4.898	63.36	-----	-----	-----	-----	5.078	-----	-----	-----	-----	5.078
754	4.899	63.36	-----	-----	-----	-----	5.070	-----	-----	-----	-----	5.070
755	4.899	63.36	-----	-----	-----	-----	5.063	-----	-----	-----	-----	5.063
756	4.900	63.36	-----	-----	-----	-----	5.056	-----	-----	-----	-----	5.056
757	4.900	63.36	-----	-----	-----	-----	5.050	-----	-----	-----	-----	5.050
758	4.901	63.36	-----	-----	-----	-----	5.044	-----	-----	-----	-----	5.044
759	4.901	63.36	-----	-----	-----	-----	5.038	-----	-----	-----	-----	5.038
760	4.900	63.36	-----	-----	-----	-----	5.032	-----	-----	-----	-----	5.032
761	4.900	63.36	-----	-----	-----	-----	5.026	-----	-----	-----	-----	5.026
762	4.899	63.36	-----	-----	-----	-----	5.021	-----	-----	-----	-----	5.021
763	4.897	63.36	-----	-----	-----	-----	5.016	-----	-----	-----	-----	5.016
764	4.895	63.36	-----	-----	-----	-----	5.011	-----	-----	-----	-----	5.011
765	4.893	63.36	-----	-----	-----	-----	5.006	-----	-----	-----	-----	5.006
766	4.890	63.36	-----	-----	-----	-----	5.001	-----	-----	-----	-----	5.001
767	4.887	63.36	-----	-----	-----	-----	4.997	-----	-----	-----	-----	4.997
768	4.883	63.36	-----	-----	-----	-----	4.992	-----	-----	-----	-----	4.992
769	4.878	63.36	-----	-----	-----	-----	4.987	-----	-----	-----	-----	4.987
770	4.873	63.36	-----	-----	-----	-----	4.983	-----	-----	-----	-----	4.983
771	4.867	63.36	-----	-----	-----	-----	4.978	-----	-----	-----	-----	4.978
772	4.861	63.36	-----	-----	-----	-----	4.973	-----	-----	-----	-----	4.973
773	4.855	63.36	-----	-----	-----	-----	4.968	-----	-----	-----	-----	4.968
774	4.848	63.36	-----	-----	-----	-----	4.963	-----	-----	-----	-----	4.963
775	4.842	63.36	-----	-----	-----	-----	4.958	-----	-----	-----	-----	4.958
776	4.836	63.36	-----	-----	-----	-----	4.953	-----	-----	-----	-----	4.953
777	4.829	63.36	-----	-----	-----	-----	4.948	-----	-----	-----	-----	4.948
778	4.823	63.35	-----	-----	-----	-----	4.943	-----	-----	-----	-----	4.943
779	4.816	63.35	-----	-----	-----	-----	4.938	-----	-----	-----	-----	4.938
780	4.810	63.35	-----	-----	-----	-----	4.933	-----	-----	-----	-----	4.933
781	4.804	63.35	-----	-----	-----	-----	4.928	-----	-----	-----	-----	4.928
782	4.798	63.35	-----	-----	-----	-----	4.922	-----	-----	-----	-----	4.922
783	4.793	63.35	-----	-----	-----	-----	4.917	-----	-----	-----	-----	4.917

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
784	4.788	63.35	-----	-----	-----	-----	4.912	-----	-----	-----	-----	4.912
785	4.783	63.35	-----	-----	-----	-----	4.906	-----	-----	-----	-----	4.906
786	4.779	63.35	-----	-----	-----	-----	4.901	-----	-----	-----	-----	4.901
787	4.775	63.35	-----	-----	-----	-----	4.896	-----	-----	-----	-----	4.896
788	4.771	63.35	-----	-----	-----	-----	4.891	-----	-----	-----	-----	4.891
789	4.767	63.35	-----	-----	-----	-----	4.886	-----	-----	-----	-----	4.886
790	4.764	63.35	-----	-----	-----	-----	4.881	-----	-----	-----	-----	4.881
791	4.761	63.35	-----	-----	-----	-----	4.876	-----	-----	-----	-----	4.876
792	4.758	63.35	-----	-----	-----	-----	4.871	-----	-----	-----	-----	4.871
793	4.756	63.35	-----	-----	-----	-----	4.866	-----	-----	-----	-----	4.866
794	4.753	63.35	-----	-----	-----	-----	4.861	-----	-----	-----	-----	4.861
795	4.751	63.35	-----	-----	-----	-----	4.857	-----	-----	-----	-----	4.857
796	4.749	63.35	-----	-----	-----	-----	4.852	-----	-----	-----	-----	4.852
797	4.747	63.35	-----	-----	-----	-----	4.848	-----	-----	-----	-----	4.848
798	4.745	63.35	-----	-----	-----	-----	4.844	-----	-----	-----	-----	4.844
799	4.743	63.35	-----	-----	-----	-----	4.840	-----	-----	-----	-----	4.840
800	4.742	63.35	-----	-----	-----	-----	4.835	-----	-----	-----	-----	4.836
801	4.740	63.35	-----	-----	-----	-----	4.832	-----	-----	-----	-----	4.832
802	4.739	63.35	-----	-----	-----	-----	4.828	-----	-----	-----	-----	4.828
803	4.737	63.35	-----	-----	-----	-----	4.824	-----	-----	-----	-----	4.824
804	4.734	63.35	-----	-----	-----	-----	4.820	-----	-----	-----	-----	4.820
805	4.731	63.35	-----	-----	-----	-----	4.817	-----	-----	-----	-----	4.817
806	4.728	63.35	-----	-----	-----	-----	4.813	-----	-----	-----	-----	4.813
807	4.725	63.35	-----	-----	-----	-----	4.809	-----	-----	-----	-----	4.809
808	4.721	63.35	-----	-----	-----	-----	4.806	-----	-----	-----	-----	4.806
809	4.717	63.35	-----	-----	-----	-----	4.802	-----	-----	-----	-----	4.802
810	4.713	63.35	-----	-----	-----	-----	4.798	-----	-----	-----	-----	4.798
811	4.708	63.35	-----	-----	-----	-----	4.795	-----	-----	-----	-----	4.795
812	4.704	63.35	-----	-----	-----	-----	4.791	-----	-----	-----	-----	4.791
813	4.699	63.35	-----	-----	-----	-----	4.787	-----	-----	-----	-----	4.787
814	4.695	63.35	-----	-----	-----	-----	4.784	-----	-----	-----	-----	4.784
815	4.690	63.35	-----	-----	-----	-----	4.780	-----	-----	-----	-----	4.780
816	4.685	63.35	-----	-----	-----	-----	4.776	-----	-----	-----	-----	4.776
817	4.680	63.35	-----	-----	-----	-----	4.772	-----	-----	-----	-----	4.772
818	4.675	63.35	-----	-----	-----	-----	4.768	-----	-----	-----	-----	4.768
819	4.670	63.35	-----	-----	-----	-----	4.764	-----	-----	-----	-----	4.764
820	4.665	63.35	-----	-----	-----	-----	4.760	-----	-----	-----	-----	4.760
821	4.660	63.35	-----	-----	-----	-----	4.756	-----	-----	-----	-----	4.756
822	4.654	63.35	-----	-----	-----	-----	4.752	-----	-----	-----	-----	4.752
823	4.648	63.35	-----	-----	-----	-----	4.748	-----	-----	-----	-----	4.748
824	4.643	63.35	-----	-----	-----	-----	4.743	-----	-----	-----	-----	4.743
825	4.637	63.35	-----	-----	-----	-----	4.739	-----	-----	-----	-----	4.739
826	4.630	63.35	-----	-----	-----	-----	4.734	-----	-----	-----	-----	4.735
827	4.624	63.35	-----	-----	-----	-----	4.730	-----	-----	-----	-----	4.730
828	4.618	63.35	-----	-----	-----	-----	4.726	-----	-----	-----	-----	4.726
829	4.612	63.35	-----	-----	-----	-----	4.721	-----	-----	-----	-----	4.721
830	4.605	63.35	-----	-----	-----	-----	4.716	-----	-----	-----	-----	4.716
831	4.599	63.35	-----	-----	-----	-----	4.711	-----	-----	-----	-----	4.711
832	4.592	63.35	-----	-----	-----	-----	4.707	-----	-----	-----	-----	4.707
833	4.585	63.35	-----	-----	-----	-----	4.702	-----	-----	-----	-----	4.702
834	4.579	63.35	-----	-----	-----	-----	4.697	-----	-----	-----	-----	4.697
835	4.572	63.35	-----	-----	-----	-----	4.691	-----	-----	-----	-----	4.692
836	4.565	63.35	-----	-----	-----	-----	4.686	-----	-----	-----	-----	4.686
837	4.559	63.35	-----	-----	-----	-----	4.681	-----	-----	-----	-----	4.681
838	4.552	63.35	-----	-----	-----	-----	4.676	-----	-----	-----	-----	4.676
839	4.545	63.35	-----	-----	-----	-----	4.671	-----	-----	-----	-----	4.671

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
840	4.539	63.35	-----	-----	-----	-----	4.665	-----	-----	-----	-----	4.665
841	4.532	63.35	-----	-----	-----	-----	4.660	-----	-----	-----	-----	4.660
842	4.526	63.35	-----	-----	-----	-----	4.654	-----	-----	-----	-----	4.654
843	4.519	63.35	-----	-----	-----	-----	4.649	-----	-----	-----	-----	4.649
844	4.513	63.35	-----	-----	-----	-----	4.643	-----	-----	-----	-----	4.643
845	4.507	63.35	-----	-----	-----	-----	4.638	-----	-----	-----	-----	4.638
846	4.501	63.35	-----	-----	-----	-----	4.632	-----	-----	-----	-----	4.632
847	4.495	63.35	-----	-----	-----	-----	4.626	-----	-----	-----	-----	4.626
848	4.490	63.35	-----	-----	-----	-----	4.621	-----	-----	-----	-----	4.621
849	4.484	63.35	-----	-----	-----	-----	4.615	-----	-----	-----	-----	4.615
850	4.479	63.35	-----	-----	-----	-----	4.610	-----	-----	-----	-----	4.610
851	4.474	63.35	-----	-----	-----	-----	4.604	-----	-----	-----	-----	4.604
852	4.470	63.35	-----	-----	-----	-----	4.599	-----	-----	-----	-----	4.599
853	4.466	63.35	-----	-----	-----	-----	4.593	-----	-----	-----	-----	4.593
854	4.461	63.35	-----	-----	-----	-----	4.588	-----	-----	-----	-----	4.588
855	4.458	63.35	-----	-----	-----	-----	4.582	-----	-----	-----	-----	4.582
856	4.454	63.35	-----	-----	-----	-----	4.577	-----	-----	-----	-----	4.577
857	4.451	63.35	-----	-----	-----	-----	4.572	-----	-----	-----	-----	4.572
858	4.448	63.35	-----	-----	-----	-----	4.567	-----	-----	-----	-----	4.567
859	4.445	63.35	-----	-----	-----	-----	4.562	-----	-----	-----	-----	4.562
860	4.442	63.35	-----	-----	-----	-----	4.557	-----	-----	-----	-----	4.557
861	4.439	63.35	-----	-----	-----	-----	4.552	-----	-----	-----	-----	4.552
862	4.437	63.35	-----	-----	-----	-----	4.547	-----	-----	-----	-----	4.547
863	4.434	63.35	-----	-----	-----	-----	4.542	-----	-----	-----	-----	4.542
864	4.432	63.35	-----	-----	-----	-----	4.538	-----	-----	-----	-----	4.538
865	4.429	63.35	-----	-----	-----	-----	4.533	-----	-----	-----	-----	4.533
866	4.427	63.35	-----	-----	-----	-----	4.529	-----	-----	-----	-----	4.529
867	4.425	63.35	-----	-----	-----	-----	4.525	-----	-----	-----	-----	4.525
868	4.423	63.35	-----	-----	-----	-----	4.520	-----	-----	-----	-----	4.520
869	4.420	63.35	-----	-----	-----	-----	4.516	-----	-----	-----	-----	4.516
870	4.418	63.35	-----	-----	-----	-----	4.512	-----	-----	-----	-----	4.512
871	4.416	63.35	-----	-----	-----	-----	4.508	-----	-----	-----	-----	4.508
872	4.414	63.35	-----	-----	-----	-----	4.504	-----	-----	-----	-----	4.504
873	4.412	63.35	-----	-----	-----	-----	4.501	-----	-----	-----	-----	4.501
874	4.410	63.35	-----	-----	-----	-----	4.497	-----	-----	-----	-----	4.497
875	4.408	63.34	-----	-----	-----	-----	4.493	-----	-----	-----	-----	4.493
876	4.405	63.34	-----	-----	-----	-----	4.490	-----	-----	-----	-----	4.489
877	4.403	63.34	-----	-----	-----	-----	4.486	-----	-----	-----	-----	4.486
878	4.401	63.34	-----	-----	-----	-----	4.482	-----	-----	-----	-----	4.482
879	4.399	63.34	-----	-----	-----	-----	4.479	-----	-----	-----	-----	4.479
880	4.397	63.34	-----	-----	-----	-----	4.476	-----	-----	-----	-----	4.476
881	4.395	63.34	-----	-----	-----	-----	4.472	-----	-----	-----	-----	4.472
882	4.393	63.34	-----	-----	-----	-----	4.469	-----	-----	-----	-----	4.469
883	4.390	63.34	-----	-----	-----	-----	4.466	-----	-----	-----	-----	4.466
884	4.388	63.34	-----	-----	-----	-----	4.463	-----	-----	-----	-----	4.463
885	4.386	63.34	-----	-----	-----	-----	4.459	-----	-----	-----	-----	4.459
886	4.384	63.34	-----	-----	-----	-----	4.456	-----	-----	-----	-----	4.456
887	4.381	63.34	-----	-----	-----	-----	4.453	-----	-----	-----	-----	4.453
888	4.379	63.34	-----	-----	-----	-----	4.450	-----	-----	-----	-----	4.450
889	4.377	63.34	-----	-----	-----	-----	4.447	-----	-----	-----	-----	4.447
890	4.374	63.34	-----	-----	-----	-----	4.444	-----	-----	-----	-----	4.444
891	4.372	63.34	-----	-----	-----	-----	4.441	-----	-----	-----	-----	4.441
892	4.369	63.34	-----	-----	-----	-----	4.438	-----	-----	-----	-----	4.438
893	4.367	63.34	-----	-----	-----	-----	4.435	-----	-----	-----	-----	4.435
894	4.364	63.34	-----	-----	-----	-----	4.432	-----	-----	-----	-----	4.432
895	4.361	63.34	-----	-----	-----	-----	4.429	-----	-----	-----	-----	4.429

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
896	4.359	63.34	-----	-----	-----	-----	4.427	-----	-----	-----	-----	4.426
897	4.356	63.34	-----	-----	-----	-----	4.424	-----	-----	-----	-----	4.424
898	4.353	63.34	-----	-----	-----	-----	4.421	-----	-----	-----	-----	4.421
899	4.351	63.34	-----	-----	-----	-----	4.418	-----	-----	-----	-----	4.418
900	4.348	63.34	-----	-----	-----	-----	4.415	-----	-----	-----	-----	4.415
901	4.345	63.34	-----	-----	-----	-----	4.412	-----	-----	-----	-----	4.412
902	4.342	63.34	-----	-----	-----	-----	4.409	-----	-----	-----	-----	4.409
903	4.339	63.34	-----	-----	-----	-----	4.406	-----	-----	-----	-----	4.406
904	4.336	63.34	-----	-----	-----	-----	4.403	-----	-----	-----	-----	4.403
905	4.333	63.34	-----	-----	-----	-----	4.401	-----	-----	-----	-----	4.401
906	4.330	63.34	-----	-----	-----	-----	4.398	-----	-----	-----	-----	4.398
907	4.327	63.34	-----	-----	-----	-----	4.395	-----	-----	-----	-----	4.395
908	4.324	63.34	-----	-----	-----	-----	4.392	-----	-----	-----	-----	4.392
909	4.321	63.34	-----	-----	-----	-----	4.389	-----	-----	-----	-----	4.389
910	4.318	63.34	-----	-----	-----	-----	4.386	-----	-----	-----	-----	4.386
911	4.315	63.34	-----	-----	-----	-----	4.383	-----	-----	-----	-----	4.383
912	4.312	63.34	-----	-----	-----	-----	4.380	-----	-----	-----	-----	4.380
913	4.309	63.34	-----	-----	-----	-----	4.377	-----	-----	-----	-----	4.377
914	4.306	63.34	-----	-----	-----	-----	4.374	-----	-----	-----	-----	4.374
915	4.302	63.34	-----	-----	-----	-----	4.371	-----	-----	-----	-----	4.371
916	4.299	63.34	-----	-----	-----	-----	4.369	-----	-----	-----	-----	4.368
917	4.296	63.34	-----	-----	-----	-----	4.365	-----	-----	-----	-----	4.366
918	4.293	63.34	-----	-----	-----	-----	4.363	-----	-----	-----	-----	4.363
919	4.290	63.34	-----	-----	-----	-----	4.360	-----	-----	-----	-----	4.360
920	4.287	63.34	-----	-----	-----	-----	4.357	-----	-----	-----	-----	4.357
921	4.284	63.34	-----	-----	-----	-----	4.354	-----	-----	-----	-----	4.354
922	4.281	63.34	-----	-----	-----	-----	4.351	-----	-----	-----	-----	4.351
923	4.278	63.34	-----	-----	-----	-----	4.348	-----	-----	-----	-----	4.348
924	4.275	63.34	-----	-----	-----	-----	4.345	-----	-----	-----	-----	4.345
925	4.271	63.34	-----	-----	-----	-----	4.342	-----	-----	-----	-----	4.342
926	4.268	63.34	-----	-----	-----	-----	4.339	-----	-----	-----	-----	4.339
927	4.265	63.34	-----	-----	-----	-----	4.336	-----	-----	-----	-----	4.336
928	4.262	63.34	-----	-----	-----	-----	4.333	-----	-----	-----	-----	4.333
929	4.259	63.34	-----	-----	-----	-----	4.330	-----	-----	-----	-----	4.330
930	4.256	63.34	-----	-----	-----	-----	4.327	-----	-----	-----	-----	4.327
931	4.253	63.34	-----	-----	-----	-----	4.324	-----	-----	-----	-----	4.324
932	4.250	63.34	-----	-----	-----	-----	4.321	-----	-----	-----	-----	4.321
933	4.247	63.34	-----	-----	-----	-----	4.317	-----	-----	-----	-----	4.318
934	4.243	63.34	-----	-----	-----	-----	4.315	-----	-----	-----	-----	4.315
935	4.240	63.34	-----	-----	-----	-----	4.311	-----	-----	-----	-----	4.311
936	4.237	63.34	-----	-----	-----	-----	4.308	-----	-----	-----	-----	4.308
937	4.234	63.34	-----	-----	-----	-----	4.305	-----	-----	-----	-----	4.305
938	4.231	63.34	-----	-----	-----	-----	4.302	-----	-----	-----	-----	4.302
939	4.228	63.34	-----	-----	-----	-----	4.299	-----	-----	-----	-----	4.299
940	4.225	63.34	-----	-----	-----	-----	4.296	-----	-----	-----	-----	4.296
941	4.222	63.34	-----	-----	-----	-----	4.293	-----	-----	-----	-----	4.293
942	4.219	63.34	-----	-----	-----	-----	4.290	-----	-----	-----	-----	4.290
943	4.215	63.34	-----	-----	-----	-----	4.287	-----	-----	-----	-----	4.287
944	4.212	63.34	-----	-----	-----	-----	4.284	-----	-----	-----	-----	4.284
945	4.209	63.34	-----	-----	-----	-----	4.281	-----	-----	-----	-----	4.281
946	4.206	63.34	-----	-----	-----	-----	4.278	-----	-----	-----	-----	4.278
947	4.203	63.34	-----	-----	-----	-----	4.275	-----	-----	-----	-----	4.275
948	4.200	63.34	-----	-----	-----	-----	4.272	-----	-----	-----	-----	4.272
949	4.197	63.34	-----	-----	-----	-----	4.269	-----	-----	-----	-----	4.269
950	4.194	63.34	-----	-----	-----	-----	4.266	-----	-----	-----	-----	4.266
951	4.191	63.34	-----	-----	-----	-----	4.263	-----	-----	-----	-----	4.263

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
952	4.187	63.34	-----	-----	-----	-----	4.259	-----	-----	-----	-----	4.259
953	4.184	63.34	-----	-----	-----	-----	4.256	-----	-----	-----	-----	4.256
954	4.181	63.34	-----	-----	-----	-----	4.253	-----	-----	-----	-----	4.253
955	4.178	63.34	-----	-----	-----	-----	4.250	-----	-----	-----	-----	4.250
956	4.175	63.34	-----	-----	-----	-----	4.247	-----	-----	-----	-----	4.247
957	4.172	63.34	-----	-----	-----	-----	4.244	-----	-----	-----	-----	4.244
958	4.169	63.34	-----	-----	-----	-----	4.241	-----	-----	-----	-----	4.241
959	4.165	63.34	-----	-----	-----	-----	4.238	-----	-----	-----	-----	4.238
960	4.162	63.34	-----	-----	-----	-----	4.235	-----	-----	-----	-----	4.235
961	4.159	63.34	-----	-----	-----	-----	4.232	-----	-----	-----	-----	4.232
962	4.156	63.34	-----	-----	-----	-----	4.229	-----	-----	-----	-----	4.229
963	4.153	63.34	-----	-----	-----	-----	4.225	-----	-----	-----	-----	4.225
964	4.150	63.34	-----	-----	-----	-----	4.222	-----	-----	-----	-----	4.222
965	4.147	63.34	-----	-----	-----	-----	4.219	-----	-----	-----	-----	4.219
966	4.144	63.34	-----	-----	-----	-----	4.216	-----	-----	-----	-----	4.216
967	4.140	63.34	-----	-----	-----	-----	4.213	-----	-----	-----	-----	4.213
968	4.137	63.34	-----	-----	-----	-----	4.210	-----	-----	-----	-----	4.210
969	4.134	63.34	-----	-----	-----	-----	4.207	-----	-----	-----	-----	4.207
970	4.131	63.34	-----	-----	-----	-----	4.204	-----	-----	-----	-----	4.204
971	4.128	63.34	-----	-----	-----	-----	4.201	-----	-----	-----	-----	4.201
972	4.125	63.34	-----	-----	-----	-----	4.198	-----	-----	-----	-----	4.198
973	4.122	63.34	-----	-----	-----	-----	4.194	-----	-----	-----	-----	4.194
974	4.118	63.34	-----	-----	-----	-----	4.191	-----	-----	-----	-----	4.191
975	4.115	63.34	-----	-----	-----	-----	4.188	-----	-----	-----	-----	4.188
976	4.112	63.34	-----	-----	-----	-----	4.185	-----	-----	-----	-----	4.185
977	4.109	63.34	-----	-----	-----	-----	4.182	-----	-----	-----	-----	4.182
978	4.106	63.34	-----	-----	-----	-----	4.179	-----	-----	-----	-----	4.179
979	4.103	63.34	-----	-----	-----	-----	4.176	-----	-----	-----	-----	4.176
980	4.100	63.34	-----	-----	-----	-----	4.173	-----	-----	-----	-----	4.173
981	4.096	63.34	-----	-----	-----	-----	4.170	-----	-----	-----	-----	4.169
982	4.093	63.34	-----	-----	-----	-----	4.166	-----	-----	-----	-----	4.166
983	4.090	63.34	-----	-----	-----	-----	4.163	-----	-----	-----	-----	4.163
984	4.087	63.34	-----	-----	-----	-----	4.160	-----	-----	-----	-----	4.160
985	4.084	63.34	-----	-----	-----	-----	4.157	-----	-----	-----	-----	4.157
986	4.081	63.34	-----	-----	-----	-----	4.154	-----	-----	-----	-----	4.154
987	4.078	63.34	-----	-----	-----	-----	4.151	-----	-----	-----	-----	4.151
988	4.074	63.34	-----	-----	-----	-----	4.148	-----	-----	-----	-----	4.148
989	4.071	63.34	-----	-----	-----	-----	4.144	-----	-----	-----	-----	4.144
990	4.068	63.34	-----	-----	-----	-----	4.141	-----	-----	-----	-----	4.141
991	4.065	63.34	-----	-----	-----	-----	4.138	-----	-----	-----	-----	4.138
992	4.062	63.34	-----	-----	-----	-----	4.135	-----	-----	-----	-----	4.135
993	4.059	63.34	-----	-----	-----	-----	4.132	-----	-----	-----	-----	4.132
994	4.055	63.34	-----	-----	-----	-----	4.129	-----	-----	-----	-----	4.129
995	4.052	63.34	-----	-----	-----	-----	4.126	-----	-----	-----	-----	4.126
996	4.049	63.34	-----	-----	-----	-----	4.123	-----	-----	-----	-----	4.123
997	4.046	63.34	-----	-----	-----	-----	4.119	-----	-----	-----	-----	4.119
998	4.043	63.34	-----	-----	-----	-----	4.116	-----	-----	-----	-----	4.116
999	4.040	63.34	-----	-----	-----	-----	4.113	-----	-----	-----	-----	4.113
1000	4.036	63.34	-----	-----	-----	-----	4.110	-----	-----	-----	-----	4.110
1001	4.033	63.34	-----	-----	-----	-----	4.107	-----	-----	-----	-----	4.107
1002	4.030	63.34	-----	-----	-----	-----	4.104	-----	-----	-----	-----	4.104
1003	4.027	63.34	-----	-----	-----	-----	4.101	-----	-----	-----	-----	4.101
1004	4.024	63.34	-----	-----	-----	-----	4.097	-----	-----	-----	-----	4.097
1005	4.021	63.34	-----	-----	-----	-----	4.094	-----	-----	-----	-----	4.094
1006	4.018	63.34	-----	-----	-----	-----	4.091	-----	-----	-----	-----	4.091
1007	4.014	63.34	-----	-----	-----	-----	4.088	-----	-----	-----	-----	4.088

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1008	4.011	63.34	-----	-----	-----	-----	4.085	-----	-----	-----	-----	4.085
1009	4.008	63.34	-----	-----	-----	-----	4.082	-----	-----	-----	-----	4.082
1010	4.005	63.34	-----	-----	-----	-----	4.079	-----	-----	-----	-----	4.079
1011	4.002	63.34	-----	-----	-----	-----	4.075	-----	-----	-----	-----	4.075
1012	3.999	63.34	-----	-----	-----	-----	4.072	-----	-----	-----	-----	4.072
1013	3.995	63.34	-----	-----	-----	-----	4.069	-----	-----	-----	-----	4.069
1014	3.992	63.34	-----	-----	-----	-----	4.066	-----	-----	-----	-----	4.066
1015	3.989	63.34	-----	-----	-----	-----	4.063	-----	-----	-----	-----	4.063
1016	3.986	63.34	-----	-----	-----	-----	4.060	-----	-----	-----	-----	4.060
1017	3.983	63.34	-----	-----	-----	-----	4.056	-----	-----	-----	-----	4.056
1018	3.979	63.34	-----	-----	-----	-----	4.053	-----	-----	-----	-----	4.053
1019	3.976	63.34	-----	-----	-----	-----	4.050	-----	-----	-----	-----	4.050
1020	3.973	63.34	-----	-----	-----	-----	4.047	-----	-----	-----	-----	4.047
1021	3.970	63.33	-----	-----	-----	-----	4.044	-----	-----	-----	-----	4.044
1022	3.967	63.33	-----	-----	-----	-----	4.041	-----	-----	-----	-----	4.041
1023	3.964	63.33	-----	-----	-----	-----	4.038	-----	-----	-----	-----	4.037
1024	3.960	63.33	-----	-----	-----	-----	4.034	-----	-----	-----	-----	4.034
1025	3.957	63.33	-----	-----	-----	-----	4.031	-----	-----	-----	-----	4.031
1026	3.954	63.33	-----	-----	-----	-----	4.028	-----	-----	-----	-----	4.028
1027	3.951	63.33	-----	-----	-----	-----	4.025	-----	-----	-----	-----	4.025
1028	3.948	63.33	-----	-----	-----	-----	4.022	-----	-----	-----	-----	4.022
1029	3.945	63.33	-----	-----	-----	-----	4.018	-----	-----	-----	-----	4.018
1030	3.941	63.33	-----	-----	-----	-----	4.015	-----	-----	-----	-----	4.015
1031	3.938	63.33	-----	-----	-----	-----	4.012	-----	-----	-----	-----	4.012
1032	3.935	63.33	-----	-----	-----	-----	4.009	-----	-----	-----	-----	4.009
1033	3.932	63.33	-----	-----	-----	-----	4.006	-----	-----	-----	-----	4.006
1034	3.929	63.33	-----	-----	-----	-----	4.003	-----	-----	-----	-----	4.003
1035	3.925	63.33	-----	-----	-----	-----	4.000	-----	-----	-----	-----	3.999
1036	3.922	63.33	-----	-----	-----	-----	3.996	-----	-----	-----	-----	3.996
1037	3.919	63.33	-----	-----	-----	-----	3.993	-----	-----	-----	-----	3.993
1038	3.916	63.33	-----	-----	-----	-----	3.990	-----	-----	-----	-----	3.990
1039	3.913	63.33	-----	-----	-----	-----	3.987	-----	-----	-----	-----	3.987
1040	3.910	63.33	-----	-----	-----	-----	3.984	-----	-----	-----	-----	3.984
1041	3.906	63.33	-----	-----	-----	-----	3.980	-----	-----	-----	-----	3.980
1042	3.903	63.33	-----	-----	-----	-----	3.977	-----	-----	-----	-----	3.977
1043	3.900	63.33	-----	-----	-----	-----	3.974	-----	-----	-----	-----	3.974
1044	3.897	63.33	-----	-----	-----	-----	3.971	-----	-----	-----	-----	3.971
1045	3.894	63.33	-----	-----	-----	-----	3.968	-----	-----	-----	-----	3.968
1046	3.890	63.33	-----	-----	-----	-----	3.965	-----	-----	-----	-----	3.965
1047	3.887	63.33	-----	-----	-----	-----	3.962	-----	-----	-----	-----	3.961
1048	3.884	63.33	-----	-----	-----	-----	3.958	-----	-----	-----	-----	3.958
1049	3.881	63.33	-----	-----	-----	-----	3.955	-----	-----	-----	-----	3.955
1050	3.878	63.33	-----	-----	-----	-----	3.952	-----	-----	-----	-----	3.952
1051	3.874	63.33	-----	-----	-----	-----	3.949	-----	-----	-----	-----	3.949
1052	3.871	63.33	-----	-----	-----	-----	3.946	-----	-----	-----	-----	3.946
1053	3.868	63.33	-----	-----	-----	-----	3.942	-----	-----	-----	-----	3.942
1054	3.865	63.33	-----	-----	-----	-----	3.939	-----	-----	-----	-----	3.939
1055	3.862	63.33	-----	-----	-----	-----	3.936	-----	-----	-----	-----	3.936
1056	3.858	63.33	-----	-----	-----	-----	3.933	-----	-----	-----	-----	3.933
1057	3.855	63.33	-----	-----	-----	-----	3.930	-----	-----	-----	-----	3.930
1058	3.852	63.33	-----	-----	-----	-----	3.927	-----	-----	-----	-----	3.927
1059	3.849	63.33	-----	-----	-----	-----	3.923	-----	-----	-----	-----	3.923
1060	3.846	63.33	-----	-----	-----	-----	3.920	-----	-----	-----	-----	3.920
1061	3.842	63.33	-----	-----	-----	-----	3.917	-----	-----	-----	-----	3.917
1062	3.839	63.33	-----	-----	-----	-----	3.914	-----	-----	-----	-----	3.914
1063	3.836	63.33	-----	-----	-----	-----	3.911	-----	-----	-----	-----	3.911

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1064	3.833	63.33	-----	-----	-----	-----	3.908	-----	-----	-----	-----	3.907
1065	3.830	63.33	-----	-----	-----	-----	3.904	-----	-----	-----	-----	3.904
1066	3.826	63.33	-----	-----	-----	-----	3.901	-----	-----	-----	-----	3.901
1067	3.823	63.33	-----	-----	-----	-----	3.898	-----	-----	-----	-----	3.898
1068	3.820	63.33	-----	-----	-----	-----	3.895	-----	-----	-----	-----	3.895
1069	3.817	63.33	-----	-----	-----	-----	3.892	-----	-----	-----	-----	3.891
1070	3.814	63.33	-----	-----	-----	-----	3.888	-----	-----	-----	-----	3.888
1071	3.810	63.33	-----	-----	-----	-----	3.885	-----	-----	-----	-----	3.885
1072	3.807	63.33	-----	-----	-----	-----	3.882	-----	-----	-----	-----	3.882
1073	3.804	63.33	-----	-----	-----	-----	3.879	-----	-----	-----	-----	3.879
1074	3.801	63.33	-----	-----	-----	-----	3.876	-----	-----	-----	-----	3.876
1075	3.798	63.33	-----	-----	-----	-----	3.872	-----	-----	-----	-----	3.872
1076	3.794	63.33	-----	-----	-----	-----	3.869	-----	-----	-----	-----	3.869
1077	3.791	63.33	-----	-----	-----	-----	3.866	-----	-----	-----	-----	3.866
1078	3.788	63.33	-----	-----	-----	-----	3.863	-----	-----	-----	-----	3.863
1079	3.785	63.33	-----	-----	-----	-----	3.860	-----	-----	-----	-----	3.860
1080	3.782	63.33	-----	-----	-----	-----	3.856	-----	-----	-----	-----	3.856
1081	3.778	63.33	-----	-----	-----	-----	3.853	-----	-----	-----	-----	3.853
1082	3.775	63.33	-----	-----	-----	-----	3.850	-----	-----	-----	-----	3.850
1083	3.772	63.33	-----	-----	-----	-----	3.847	-----	-----	-----	-----	3.847
1084	3.769	63.33	-----	-----	-----	-----	3.844	-----	-----	-----	-----	3.844
1085	3.765	63.33	-----	-----	-----	-----	3.840	-----	-----	-----	-----	3.840
1086	3.762	63.33	-----	-----	-----	-----	3.837	-----	-----	-----	-----	3.837
1087	3.759	63.33	-----	-----	-----	-----	3.834	-----	-----	-----	-----	3.834
1088	3.756	63.33	-----	-----	-----	-----	3.831	-----	-----	-----	-----	3.831
1089	3.753	63.33	-----	-----	-----	-----	3.828	-----	-----	-----	-----	3.828
1090	3.749	63.33	-----	-----	-----	-----	3.824	-----	-----	-----	-----	3.824
1091	3.746	63.33	-----	-----	-----	-----	3.821	-----	-----	-----	-----	3.821
1092	3.743	63.33	-----	-----	-----	-----	3.818	-----	-----	-----	-----	3.818
1093	3.740	63.33	-----	-----	-----	-----	3.815	-----	-----	-----	-----	3.815
1094	3.737	63.33	-----	-----	-----	-----	3.812	-----	-----	-----	-----	3.812
1095	3.733	63.33	-----	-----	-----	-----	3.808	-----	-----	-----	-----	3.808
1096	3.730	63.33	-----	-----	-----	-----	3.805	-----	-----	-----	-----	3.805
1097	3.727	63.33	-----	-----	-----	-----	3.802	-----	-----	-----	-----	3.802
1098	3.724	63.33	-----	-----	-----	-----	3.799	-----	-----	-----	-----	3.799
1099	3.720	63.33	-----	-----	-----	-----	3.796	-----	-----	-----	-----	3.796
1100	3.717	63.33	-----	-----	-----	-----	3.792	-----	-----	-----	-----	3.792
1101	3.714	63.33	-----	-----	-----	-----	3.789	-----	-----	-----	-----	3.789
1102	3.711	63.33	-----	-----	-----	-----	3.786	-----	-----	-----	-----	3.786
1103	3.708	63.33	-----	-----	-----	-----	3.783	-----	-----	-----	-----	3.783
1104	3.704	63.33	-----	-----	-----	-----	3.780	-----	-----	-----	-----	3.779
1105	3.701	63.33	-----	-----	-----	-----	3.776	-----	-----	-----	-----	3.776
1106	3.698	63.33	-----	-----	-----	-----	3.773	-----	-----	-----	-----	3.773
1107	3.695	63.33	-----	-----	-----	-----	3.770	-----	-----	-----	-----	3.770
1108	3.691	63.33	-----	-----	-----	-----	3.767	-----	-----	-----	-----	3.767
1109	3.688	63.33	-----	-----	-----	-----	3.764	-----	-----	-----	-----	3.763
1110	3.685	63.33	-----	-----	-----	-----	3.760	-----	-----	-----	-----	3.760
1111	3.682	63.33	-----	-----	-----	-----	3.757	-----	-----	-----	-----	3.757
1112	3.679	63.33	-----	-----	-----	-----	3.754	-----	-----	-----	-----	3.754
1113	3.675	63.33	-----	-----	-----	-----	3.751	-----	-----	-----	-----	3.751
1114	3.672	63.33	-----	-----	-----	-----	3.747	-----	-----	-----	-----	3.747
1115	3.669	63.33	-----	-----	-----	-----	3.744	-----	-----	-----	-----	3.744
1116	3.666	63.33	-----	-----	-----	-----	3.741	-----	-----	-----	-----	3.741
1117	3.662	63.33	-----	-----	-----	-----	3.738	-----	-----	-----	-----	3.738
1118	3.659	63.33	-----	-----	-----	-----	3.734	-----	-----	-----	-----	3.734
1119	3.656	63.33	-----	-----	-----	-----	3.731	-----	-----	-----	-----	3.731

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1120	3.653	63.33	-----	-----	-----	-----	3.728	-----	-----	-----	-----	3.728
1121	3.649	63.33	-----	-----	-----	-----	3.725	-----	-----	-----	-----	3.725
1122	3.646	63.33	-----	-----	-----	-----	3.722	-----	-----	-----	-----	3.722
1123	3.643	63.33	-----	-----	-----	-----	3.718	-----	-----	-----	-----	3.718
1124	3.640	63.33	-----	-----	-----	-----	3.715	-----	-----	-----	-----	3.715
1125	3.637	63.33	-----	-----	-----	-----	3.712	-----	-----	-----	-----	3.712
1126	3.633	63.33	-----	-----	-----	-----	3.709	-----	-----	-----	-----	3.709
1127	3.630	63.33	-----	-----	-----	-----	3.706	-----	-----	-----	-----	3.706
1128	3.627	63.33	-----	-----	-----	-----	3.702	-----	-----	-----	-----	3.702
1129	3.624	63.33	-----	-----	-----	-----	3.699	-----	-----	-----	-----	3.699
1130	3.620	63.33	-----	-----	-----	-----	3.696	-----	-----	-----	-----	3.696
1131	3.617	63.33	-----	-----	-----	-----	3.693	-----	-----	-----	-----	3.693
1132	3.614	63.33	-----	-----	-----	-----	3.689	-----	-----	-----	-----	3.689
1133	3.611	63.33	-----	-----	-----	-----	3.686	-----	-----	-----	-----	3.686
1134	3.607	63.33	-----	-----	-----	-----	3.683	-----	-----	-----	-----	3.683
1135	3.604	63.33	-----	-----	-----	-----	3.680	-----	-----	-----	-----	3.680
1136	3.601	63.33	-----	-----	-----	-----	3.676	-----	-----	-----	-----	3.676
1137	3.598	63.33	-----	-----	-----	-----	3.673	-----	-----	-----	-----	3.673
1138	3.594	63.33	-----	-----	-----	-----	3.670	-----	-----	-----	-----	3.670
1139	3.591	63.33	-----	-----	-----	-----	3.667	-----	-----	-----	-----	3.667
1140	3.588	63.33	-----	-----	-----	-----	3.664	-----	-----	-----	-----	3.664
1141	3.585	63.33	-----	-----	-----	-----	3.660	-----	-----	-----	-----	3.660
1142	3.582	63.33	-----	-----	-----	-----	3.657	-----	-----	-----	-----	3.657
1143	3.578	63.33	-----	-----	-----	-----	3.654	-----	-----	-----	-----	3.654
1144	3.575	63.33	-----	-----	-----	-----	3.651	-----	-----	-----	-----	3.651
1145	3.572	63.33	-----	-----	-----	-----	3.647	-----	-----	-----	-----	3.647
1146	3.569	63.33	-----	-----	-----	-----	3.644	-----	-----	-----	-----	3.644
1147	3.565	63.33	-----	-----	-----	-----	3.641	-----	-----	-----	-----	3.641
1148	3.562	63.33	-----	-----	-----	-----	3.638	-----	-----	-----	-----	3.638
1149	3.559	63.33	-----	-----	-----	-----	3.634	-----	-----	-----	-----	3.634
1150	3.556	63.33	-----	-----	-----	-----	3.631	-----	-----	-----	-----	3.631
1151	3.552	63.33	-----	-----	-----	-----	3.628	-----	-----	-----	-----	3.628
1152	3.549	63.33	-----	-----	-----	-----	3.625	-----	-----	-----	-----	3.625
1153	3.546	63.33	-----	-----	-----	-----	3.622	-----	-----	-----	-----	3.622
1154	3.543	63.33	-----	-----	-----	-----	3.618	-----	-----	-----	-----	3.618
1155	3.539	63.33	-----	-----	-----	-----	3.615	-----	-----	-----	-----	3.615
1156	3.536	63.33	-----	-----	-----	-----	3.612	-----	-----	-----	-----	3.612
1157	3.533	63.33	-----	-----	-----	-----	3.609	-----	-----	-----	-----	3.609
1158	3.530	63.33	-----	-----	-----	-----	3.605	-----	-----	-----	-----	3.605
1159	3.526	63.33	-----	-----	-----	-----	3.602	-----	-----	-----	-----	3.602
1160	3.523	63.33	-----	-----	-----	-----	3.599	-----	-----	-----	-----	3.599
1161	3.520	63.33	-----	-----	-----	-----	3.596	-----	-----	-----	-----	3.596
1162	3.517	63.32	-----	-----	-----	-----	3.592	-----	-----	-----	-----	3.592
1163	3.513	63.32	-----	-----	-----	-----	3.589	-----	-----	-----	-----	3.589
1164	3.510	63.32	-----	-----	-----	-----	3.586	-----	-----	-----	-----	3.586
1165	3.507	63.32	-----	-----	-----	-----	3.583	-----	-----	-----	-----	3.583
1166	3.504	63.32	-----	-----	-----	-----	3.579	-----	-----	-----	-----	3.579
1167	3.500	63.32	-----	-----	-----	-----	3.576	-----	-----	-----	-----	3.576
1168	3.497	63.32	-----	-----	-----	-----	3.573	-----	-----	-----	-----	3.573
1169	3.494	63.32	-----	-----	-----	-----	3.570	-----	-----	-----	-----	3.570
1170	3.491	63.32	-----	-----	-----	-----	3.567	-----	-----	-----	-----	3.566
1171	3.487	63.32	-----	-----	-----	-----	3.563	-----	-----	-----	-----	3.563
1172	3.484	63.32	-----	-----	-----	-----	3.560	-----	-----	-----	-----	3.560
1173	3.481	63.32	-----	-----	-----	-----	3.557	-----	-----	-----	-----	3.557
1174	3.478	63.32	-----	-----	-----	-----	3.553	-----	-----	-----	-----	3.554
1175	3.474	63.32	-----	-----	-----	-----	3.550	-----	-----	-----	-----	3.550

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1176	3.471	63.32	-----	-----	-----	-----	3.547	-----	-----	-----	-----	3.547
1177	3.468	63.32	-----	-----	-----	-----	3.544	-----	-----	-----	-----	3.544
1178	3.465	63.32	-----	-----	-----	-----	3.541	-----	-----	-----	-----	3.541
1179	3.461	63.32	-----	-----	-----	-----	3.537	-----	-----	-----	-----	3.537
1180	3.458	63.32	-----	-----	-----	-----	3.534	-----	-----	-----	-----	3.534
1181	3.455	63.32	-----	-----	-----	-----	3.531	-----	-----	-----	-----	3.531
1182	3.452	63.32	-----	-----	-----	-----	3.528	-----	-----	-----	-----	3.528
1183	3.448	63.32	-----	-----	-----	-----	3.524	-----	-----	-----	-----	3.524
1184	3.445	63.32	-----	-----	-----	-----	3.521	-----	-----	-----	-----	3.521
1185	3.442	63.32	-----	-----	-----	-----	3.518	-----	-----	-----	-----	3.518
1186	3.439	63.32	-----	-----	-----	-----	3.515	-----	-----	-----	-----	3.515
1187	3.435	63.32	-----	-----	-----	-----	3.511	-----	-----	-----	-----	3.511
1188	3.432	63.32	-----	-----	-----	-----	3.508	-----	-----	-----	-----	3.508
1189	3.429	63.32	-----	-----	-----	-----	3.505	-----	-----	-----	-----	3.505
1190	3.425	63.32	-----	-----	-----	-----	3.501	-----	-----	-----	-----	3.502
1191	3.422	63.32	-----	-----	-----	-----	3.498	-----	-----	-----	-----	3.498
1192	3.419	63.32	-----	-----	-----	-----	3.495	-----	-----	-----	-----	3.495
1193	3.416	63.32	-----	-----	-----	-----	3.492	-----	-----	-----	-----	3.492
1194	3.412	63.32	-----	-----	-----	-----	3.489	-----	-----	-----	-----	3.489
1195	3.409	63.32	-----	-----	-----	-----	3.485	-----	-----	-----	-----	3.485
1196	3.406	63.32	-----	-----	-----	-----	3.482	-----	-----	-----	-----	3.482
1197	3.403	63.32	-----	-----	-----	-----	3.479	-----	-----	-----	-----	3.479
1198	3.399	63.32	-----	-----	-----	-----	3.476	-----	-----	-----	-----	3.476
1199	3.396	63.32	-----	-----	-----	-----	3.472	-----	-----	-----	-----	3.472
1200	3.393	63.32	-----	-----	-----	-----	3.469	-----	-----	-----	-----	3.469
1201	3.390	63.32	-----	-----	-----	-----	3.466	-----	-----	-----	-----	3.466
1202	3.386	63.32	-----	-----	-----	-----	3.462	-----	-----	-----	-----	3.463
1203	3.383	63.32	-----	-----	-----	-----	3.459	-----	-----	-----	-----	3.459
1204	3.380	63.32	-----	-----	-----	-----	3.456	-----	-----	-----	-----	3.456
1205	3.377	63.32	-----	-----	-----	-----	3.453	-----	-----	-----	-----	3.453
1206	3.373	63.32	-----	-----	-----	-----	3.450	-----	-----	-----	-----	3.450
1207	3.370	63.32	-----	-----	-----	-----	3.446	-----	-----	-----	-----	3.446
1208	3.367	63.32	-----	-----	-----	-----	3.443	-----	-----	-----	-----	3.443
1209	3.363	63.32	-----	-----	-----	-----	3.440	-----	-----	-----	-----	3.440
1210	3.360	63.32	-----	-----	-----	-----	3.436	-----	-----	-----	-----	3.436
1211	3.357	63.32	-----	-----	-----	-----	3.433	-----	-----	-----	-----	3.433
1212	3.354	63.32	-----	-----	-----	-----	3.430	-----	-----	-----	-----	3.430
1213	3.350	63.32	-----	-----	-----	-----	3.427	-----	-----	-----	-----	3.427
1214	3.347	63.32	-----	-----	-----	-----	3.423	-----	-----	-----	-----	3.423
1215	3.344	63.32	-----	-----	-----	-----	3.420	-----	-----	-----	-----	3.420
1216	3.341	63.32	-----	-----	-----	-----	3.417	-----	-----	-----	-----	3.417
1217	3.337	63.32	-----	-----	-----	-----	3.414	-----	-----	-----	-----	3.414
1218	3.334	63.32	-----	-----	-----	-----	3.410	-----	-----	-----	-----	3.410
1219	3.331	63.32	-----	-----	-----	-----	3.407	-----	-----	-----	-----	3.407
1220	3.327	63.32	-----	-----	-----	-----	3.404	-----	-----	-----	-----	3.404
1221	3.324	63.32	-----	-----	-----	-----	3.401	-----	-----	-----	-----	3.401
1222	3.321	63.32	-----	-----	-----	-----	3.397	-----	-----	-----	-----	3.397
1223	3.318	63.32	-----	-----	-----	-----	3.394	-----	-----	-----	-----	3.394
1224	3.314	63.32	-----	-----	-----	-----	3.391	-----	-----	-----	-----	3.391
1225	3.311	63.32	-----	-----	-----	-----	3.388	-----	-----	-----	-----	3.388
1226	3.308	63.32	-----	-----	-----	-----	3.384	-----	-----	-----	-----	3.384
1227	3.305	63.32	-----	-----	-----	-----	3.381	-----	-----	-----	-----	3.381
1228	3.301	63.32	-----	-----	-----	-----	3.378	-----	-----	-----	-----	3.378
1229	3.298	63.32	-----	-----	-----	-----	3.375	-----	-----	-----	-----	3.374
1230	3.295	63.32	-----	-----	-----	-----	3.371	-----	-----	-----	-----	3.371
1231	3.291	63.32	-----	-----	-----	-----	3.368	-----	-----	-----	-----	3.368

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1232	3.288	63.32	-----	-----	-----	-----	3.365	-----	-----	-----	-----	3.365
1233	3.285	63.32	-----	-----	-----	-----	3.361	-----	-----	-----	-----	3.361
1234	3.282	63.32	-----	-----	-----	-----	3.358	-----	-----	-----	-----	3.358
1235	3.278	63.32	-----	-----	-----	-----	3.355	-----	-----	-----	-----	3.355
1236	3.275	63.32	-----	-----	-----	-----	3.352	-----	-----	-----	-----	3.352
1237	3.272	63.32	-----	-----	-----	-----	3.348	-----	-----	-----	-----	3.348
1238	3.269	63.32	-----	-----	-----	-----	3.345	-----	-----	-----	-----	3.345
1239	3.265	63.32	-----	-----	-----	-----	3.342	-----	-----	-----	-----	3.342
1240	3.262	63.32	-----	-----	-----	-----	3.339	-----	-----	-----	-----	3.339
1241	3.259	63.32	-----	-----	-----	-----	3.335	-----	-----	-----	-----	3.335
1242	3.255	63.32	-----	-----	-----	-----	3.332	-----	-----	-----	-----	3.332
1243	3.252	63.32	-----	-----	-----	-----	3.329	-----	-----	-----	-----	3.329
1244	3.249	63.32	-----	-----	-----	-----	3.325	-----	-----	-----	-----	3.325
1245	3.246	63.32	-----	-----	-----	-----	3.322	-----	-----	-----	-----	3.322
1246	3.242	63.32	-----	-----	-----	-----	3.319	-----	-----	-----	-----	3.319
1247	3.239	63.32	-----	-----	-----	-----	3.316	-----	-----	-----	-----	3.316
1248	3.236	63.32	-----	-----	-----	-----	3.312	-----	-----	-----	-----	3.312
1249	3.232	63.32	-----	-----	-----	-----	3.309	-----	-----	-----	-----	3.309
1250	3.229	63.32	-----	-----	-----	-----	3.306	-----	-----	-----	-----	3.306
1251	3.226	63.32	-----	-----	-----	-----	3.302	-----	-----	-----	-----	3.303
1252	3.223	63.32	-----	-----	-----	-----	3.299	-----	-----	-----	-----	3.299
1253	3.219	63.32	-----	-----	-----	-----	3.296	-----	-----	-----	-----	3.296
1254	3.216	63.32	-----	-----	-----	-----	3.293	-----	-----	-----	-----	3.293
1255	3.213	63.32	-----	-----	-----	-----	3.289	-----	-----	-----	-----	3.289
1256	3.209	63.32	-----	-----	-----	-----	3.286	-----	-----	-----	-----	3.286
1257	3.206	63.32	-----	-----	-----	-----	3.283	-----	-----	-----	-----	3.283
1258	3.203	63.32	-----	-----	-----	-----	3.280	-----	-----	-----	-----	3.280
1259	3.200	63.32	-----	-----	-----	-----	3.276	-----	-----	-----	-----	3.276
1260	3.196	63.32	-----	-----	-----	-----	3.273	-----	-----	-----	-----	3.273
1261	3.193	63.32	-----	-----	-----	-----	3.270	-----	-----	-----	-----	3.270
1262	3.190	63.32	-----	-----	-----	-----	3.266	-----	-----	-----	-----	3.266
1263	3.186	63.32	-----	-----	-----	-----	3.263	-----	-----	-----	-----	3.263
1264	3.183	63.32	-----	-----	-----	-----	3.260	-----	-----	-----	-----	3.260
1265	3.180	63.32	-----	-----	-----	-----	3.257	-----	-----	-----	-----	3.257
1266	3.177	63.32	-----	-----	-----	-----	3.253	-----	-----	-----	-----	3.253
1267	3.173	63.32	-----	-----	-----	-----	3.250	-----	-----	-----	-----	3.250
1268	3.170	63.32	-----	-----	-----	-----	3.247	-----	-----	-----	-----	3.247
1269	3.167	63.32	-----	-----	-----	-----	3.243	-----	-----	-----	-----	3.243
1270	3.163	63.32	-----	-----	-----	-----	3.240	-----	-----	-----	-----	3.240
1271	3.160	63.32	-----	-----	-----	-----	3.237	-----	-----	-----	-----	3.237
1272	3.157	63.32	-----	-----	-----	-----	3.234	-----	-----	-----	-----	3.234
1273	3.154	63.32	-----	-----	-----	-----	3.230	-----	-----	-----	-----	3.230
1274	3.150	63.32	-----	-----	-----	-----	3.227	-----	-----	-----	-----	3.227
1275	3.147	63.32	-----	-----	-----	-----	3.224	-----	-----	-----	-----	3.224
1276	3.144	63.32	-----	-----	-----	-----	3.221	-----	-----	-----	-----	3.221
1277	3.140	63.32	-----	-----	-----	-----	3.217	-----	-----	-----	-----	3.217
1278	3.137	63.32	-----	-----	-----	-----	3.214	-----	-----	-----	-----	3.214
1279	3.134	63.32	-----	-----	-----	-----	3.211	-----	-----	-----	-----	3.211
1280	3.131	63.32	-----	-----	-----	-----	3.207	-----	-----	-----	-----	3.207
1281	3.127	63.32	-----	-----	-----	-----	3.204	-----	-----	-----	-----	3.204
1282	3.124	63.32	-----	-----	-----	-----	3.201	-----	-----	-----	-----	3.201
1283	3.121	63.32	-----	-----	-----	-----	3.198	-----	-----	-----	-----	3.198
1284	3.117	63.32	-----	-----	-----	-----	3.194	-----	-----	-----	-----	3.194
1285	3.114	63.32	-----	-----	-----	-----	3.191	-----	-----	-----	-----	3.191
1286	3.111	63.32	-----	-----	-----	-----	3.188	-----	-----	-----	-----	3.188
1287	3.107	63.32	-----	-----	-----	-----	3.184	-----	-----	-----	-----	3.184

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1288	3.104	63.32	-----	-----	-----	-----	3.181	-----	-----	-----	-----	3.181
1289	3.101	63.32	-----	-----	-----	-----	3.178	-----	-----	-----	-----	3.178
1290	3.098	63.32	-----	-----	-----	-----	3.174	-----	-----	-----	-----	3.175
1291	3.094	63.32	-----	-----	-----	-----	3.171	-----	-----	-----	-----	3.171
1292	3.091	63.32	-----	-----	-----	-----	3.168	-----	-----	-----	-----	3.168
1293	3.088	63.32	-----	-----	-----	-----	3.165	-----	-----	-----	-----	3.165
1294	3.084	63.32	-----	-----	-----	-----	3.161	-----	-----	-----	-----	3.161
1295	3.081	63.32	-----	-----	-----	-----	3.158	-----	-----	-----	-----	3.158
1296	3.078	63.32	-----	-----	-----	-----	3.155	-----	-----	-----	-----	3.155
1297	3.075	63.32	-----	-----	-----	-----	3.152	-----	-----	-----	-----	3.152
1298	3.071	63.32	-----	-----	-----	-----	3.148	-----	-----	-----	-----	3.148
1299	3.068	63.32	-----	-----	-----	-----	3.145	-----	-----	-----	-----	3.145
1300	3.065	63.31	-----	-----	-----	-----	3.142	-----	-----	-----	-----	3.142
1301	3.061	63.31	-----	-----	-----	-----	3.138	-----	-----	-----	-----	3.138
1302	3.058	63.31	-----	-----	-----	-----	3.135	-----	-----	-----	-----	3.135
1303	3.055	63.31	-----	-----	-----	-----	3.132	-----	-----	-----	-----	3.132
1304	3.051	63.31	-----	-----	-----	-----	3.129	-----	-----	-----	-----	3.128
1305	3.048	63.31	-----	-----	-----	-----	3.125	-----	-----	-----	-----	3.125
1306	3.045	63.31	-----	-----	-----	-----	3.122	-----	-----	-----	-----	3.122
1307	3.042	63.31	-----	-----	-----	-----	3.119	-----	-----	-----	-----	3.119
1308	3.038	63.31	-----	-----	-----	-----	3.115	-----	-----	-----	-----	3.115
1309	3.035	63.31	-----	-----	-----	-----	3.112	-----	-----	-----	-----	3.112
1310	3.032	63.31	-----	-----	-----	-----	3.109	-----	-----	-----	-----	3.109
1311	3.028	63.31	-----	-----	-----	-----	3.105	-----	-----	-----	-----	3.105
1312	3.025	63.31	-----	-----	-----	-----	3.102	-----	-----	-----	-----	3.102
1313	3.022	63.31	-----	-----	-----	-----	3.099	-----	-----	-----	-----	3.099
1314	3.018	63.31	-----	-----	-----	-----	3.095	-----	-----	-----	-----	3.096
1315	3.015	63.31	-----	-----	-----	-----	3.092	-----	-----	-----	-----	3.092
1316	3.012	63.31	-----	-----	-----	-----	3.089	-----	-----	-----	-----	3.089
1317	3.009	63.31	-----	-----	-----	-----	3.086	-----	-----	-----	-----	3.086
1318	3.005	63.31	-----	-----	-----	-----	3.082	-----	-----	-----	-----	3.082
1319	3.002	63.31	-----	-----	-----	-----	3.079	-----	-----	-----	-----	3.079
1320	2.999	63.31	-----	-----	-----	-----	3.076	-----	-----	-----	-----	3.076
1321	2.995	63.31	-----	-----	-----	-----	3.072	-----	-----	-----	-----	3.072
1322	2.992	63.31	-----	-----	-----	-----	3.069	-----	-----	-----	-----	3.069
1323	2.989	63.31	-----	-----	-----	-----	3.066	-----	-----	-----	-----	3.066
1324	2.985	63.31	-----	-----	-----	-----	3.063	-----	-----	-----	-----	3.063
1325	2.982	63.31	-----	-----	-----	-----	3.059	-----	-----	-----	-----	3.059
1326	2.979	63.31	-----	-----	-----	-----	3.056	-----	-----	-----	-----	3.056
1327	2.975	63.31	-----	-----	-----	-----	3.053	-----	-----	-----	-----	3.053
1328	2.972	63.31	-----	-----	-----	-----	3.049	-----	-----	-----	-----	3.049
1329	2.969	63.31	-----	-----	-----	-----	3.046	-----	-----	-----	-----	3.046
1330	2.966	63.31	-----	-----	-----	-----	3.043	-----	-----	-----	-----	3.043
1331	2.962	63.31	-----	-----	-----	-----	3.039	-----	-----	-----	-----	3.039
1332	2.959	63.31	-----	-----	-----	-----	3.036	-----	-----	-----	-----	3.036
1333	2.956	63.31	-----	-----	-----	-----	3.033	-----	-----	-----	-----	3.033
1334	2.952	63.31	-----	-----	-----	-----	3.030	-----	-----	-----	-----	3.030
1335	2.949	63.31	-----	-----	-----	-----	3.026	-----	-----	-----	-----	3.026
1336	2.946	63.31	-----	-----	-----	-----	3.023	-----	-----	-----	-----	3.023
1337	2.942	63.31	-----	-----	-----	-----	3.020	-----	-----	-----	-----	3.020
1338	2.939	63.31	-----	-----	-----	-----	3.016	-----	-----	-----	-----	3.016
1339	2.936	63.31	-----	-----	-----	-----	3.013	-----	-----	-----	-----	3.013
1340	2.933	63.31	-----	-----	-----	-----	3.010	-----	-----	-----	-----	3.010
1341	2.929	63.31	-----	-----	-----	-----	3.006	-----	-----	-----	-----	3.006
1342	2.926	63.31	-----	-----	-----	-----	3.003	-----	-----	-----	-----	3.003
1343	2.923	63.31	-----	-----	-----	-----	3.000	-----	-----	-----	-----	3.000

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1344	2.919	63.31	-----	-----	-----	-----	2.997	-----	-----	-----	-----	2.997
1345	2.916	63.31	-----	-----	-----	-----	2.993	-----	-----	-----	-----	2.993
1346	2.913	63.31	-----	-----	-----	-----	2.990	-----	-----	-----	-----	2.990
1347	2.909	63.31	-----	-----	-----	-----	2.987	-----	-----	-----	-----	2.987
1348	2.906	63.31	-----	-----	-----	-----	2.983	-----	-----	-----	-----	2.983
1349	2.903	63.31	-----	-----	-----	-----	2.980	-----	-----	-----	-----	2.980
1350	2.899	63.31	-----	-----	-----	-----	2.977	-----	-----	-----	-----	2.977
1351	2.896	63.31	-----	-----	-----	-----	2.974	-----	-----	-----	-----	2.973
1352	2.893	63.31	-----	-----	-----	-----	2.970	-----	-----	-----	-----	2.970
1353	2.889	63.31	-----	-----	-----	-----	2.967	-----	-----	-----	-----	2.967
1354	2.886	63.31	-----	-----	-----	-----	2.964	-----	-----	-----	-----	2.964
1355	2.883	63.31	-----	-----	-----	-----	2.960	-----	-----	-----	-----	2.960
1356	2.880	63.31	-----	-----	-----	-----	2.957	-----	-----	-----	-----	2.957
1357	2.876	63.31	-----	-----	-----	-----	2.954	-----	-----	-----	-----	2.954
1358	2.873	63.31	-----	-----	-----	-----	2.950	-----	-----	-----	-----	2.950
1359	2.870	63.31	-----	-----	-----	-----	2.947	-----	-----	-----	-----	2.947
1360	2.866	63.31	-----	-----	-----	-----	2.944	-----	-----	-----	-----	2.944
1361	2.863	63.31	-----	-----	-----	-----	2.940	-----	-----	-----	-----	2.940
1362	2.860	63.31	-----	-----	-----	-----	2.937	-----	-----	-----	-----	2.937
1363	2.856	63.31	-----	-----	-----	-----	2.934	-----	-----	-----	-----	2.934
1364	2.853	63.31	-----	-----	-----	-----	2.931	-----	-----	-----	-----	2.930
1365	2.850	63.31	-----	-----	-----	-----	2.927	-----	-----	-----	-----	2.927
1366	2.846	63.31	-----	-----	-----	-----	2.924	-----	-----	-----	-----	2.924
1367	2.843	63.31	-----	-----	-----	-----	2.921	-----	-----	-----	-----	2.921
1368	2.840	63.31	-----	-----	-----	-----	2.917	-----	-----	-----	-----	2.917
1369	2.836	63.31	-----	-----	-----	-----	2.914	-----	-----	-----	-----	2.914
1370	2.833	63.31	-----	-----	-----	-----	2.911	-----	-----	-----	-----	2.911
1371	2.830	63.31	-----	-----	-----	-----	2.907	-----	-----	-----	-----	2.907
1372	2.827	63.31	-----	-----	-----	-----	2.904	-----	-----	-----	-----	2.904
1373	2.823	63.31	-----	-----	-----	-----	2.901	-----	-----	-----	-----	2.901
1374	2.820	63.31	-----	-----	-----	-----	2.897	-----	-----	-----	-----	2.897
1375	2.817	63.31	-----	-----	-----	-----	2.894	-----	-----	-----	-----	2.894
1376	2.813	63.31	-----	-----	-----	-----	2.891	-----	-----	-----	-----	2.891
1377	2.810	63.31	-----	-----	-----	-----	2.887	-----	-----	-----	-----	2.887
1378	2.807	63.31	-----	-----	-----	-----	2.884	-----	-----	-----	-----	2.884
1379	2.803	63.31	-----	-----	-----	-----	2.881	-----	-----	-----	-----	2.881
1380	2.800	63.31	-----	-----	-----	-----	2.878	-----	-----	-----	-----	2.877
1381	2.797	63.31	-----	-----	-----	-----	2.874	-----	-----	-----	-----	2.874
1382	2.793	63.31	-----	-----	-----	-----	2.871	-----	-----	-----	-----	2.871
1383	2.790	63.31	-----	-----	-----	-----	2.868	-----	-----	-----	-----	2.868
1384	2.787	63.31	-----	-----	-----	-----	2.864	-----	-----	-----	-----	2.864
1385	2.783	63.31	-----	-----	-----	-----	2.861	-----	-----	-----	-----	2.861
1386	2.780	63.31	-----	-----	-----	-----	2.858	-----	-----	-----	-----	2.858
1387	2.777	63.31	-----	-----	-----	-----	2.854	-----	-----	-----	-----	2.854
1388	2.773	63.31	-----	-----	-----	-----	2.851	-----	-----	-----	-----	2.851
1389	2.770	63.31	-----	-----	-----	-----	2.848	-----	-----	-----	-----	2.848
1390	2.767	63.31	-----	-----	-----	-----	2.844	-----	-----	-----	-----	2.844
1391	2.763	63.31	-----	-----	-----	-----	2.841	-----	-----	-----	-----	2.841
1392	2.760	63.31	-----	-----	-----	-----	2.838	-----	-----	-----	-----	2.838
1393	2.757	63.31	-----	-----	-----	-----	2.834	-----	-----	-----	-----	2.834
1394	2.753	63.31	-----	-----	-----	-----	2.831	-----	-----	-----	-----	2.831
1395	2.750	63.31	-----	-----	-----	-----	2.828	-----	-----	-----	-----	2.828
1396	2.747	63.31	-----	-----	-----	-----	2.825	-----	-----	-----	-----	2.824
1397	2.744	63.31	-----	-----	-----	-----	2.821	-----	-----	-----	-----	2.821
1398	2.740	63.31	-----	-----	-----	-----	2.818	-----	-----	-----	-----	2.818
1399	2.737	63.31	-----	-----	-----	-----	2.815	-----	-----	-----	-----	2.815

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1400	2.734	63.31	-----	-----	-----	-----	2.811	-----	-----	-----	-----	2.811
1401	2.730	63.31	-----	-----	-----	-----	2.808	-----	-----	-----	-----	2.808
1402	2.727	63.31	-----	-----	-----	-----	2.805	-----	-----	-----	-----	2.805
1403	2.724	63.31	-----	-----	-----	-----	2.801	-----	-----	-----	-----	2.801
1404	2.720	63.31	-----	-----	-----	-----	2.798	-----	-----	-----	-----	2.798
1405	2.717	63.31	-----	-----	-----	-----	2.795	-----	-----	-----	-----	2.795
1406	2.714	63.31	-----	-----	-----	-----	2.791	-----	-----	-----	-----	2.791
1407	2.710	63.31	-----	-----	-----	-----	2.788	-----	-----	-----	-----	2.788
1408	2.707	63.31	-----	-----	-----	-----	2.785	-----	-----	-----	-----	2.785
1409	2.704	63.31	-----	-----	-----	-----	2.781	-----	-----	-----	-----	2.781
1410	2.700	63.31	-----	-----	-----	-----	2.778	-----	-----	-----	-----	2.778
1411	2.697	63.31	-----	-----	-----	-----	2.775	-----	-----	-----	-----	2.775
1412	2.694	63.31	-----	-----	-----	-----	2.771	-----	-----	-----	-----	2.771
1413	2.690	63.31	-----	-----	-----	-----	2.768	-----	-----	-----	-----	2.768
1414	2.687	63.31	-----	-----	-----	-----	2.765	-----	-----	-----	-----	2.765
1415	2.684	63.31	-----	-----	-----	-----	2.761	-----	-----	-----	-----	2.761
1416	2.680	63.31	-----	-----	-----	-----	2.758	-----	-----	-----	-----	2.758
1417	2.677	63.31	-----	-----	-----	-----	2.755	-----	-----	-----	-----	2.755
1418	2.674	63.31	-----	-----	-----	-----	2.751	-----	-----	-----	-----	2.751
1419	2.670	63.31	-----	-----	-----	-----	2.748	-----	-----	-----	-----	2.748
1420	2.667	63.31	-----	-----	-----	-----	2.745	-----	-----	-----	-----	2.745
1421	2.664	63.31	-----	-----	-----	-----	2.741	-----	-----	-----	-----	2.741
1422	2.660	63.31	-----	-----	-----	-----	2.738	-----	-----	-----	-----	2.738
1423	2.657	63.31	-----	-----	-----	-----	2.735	-----	-----	-----	-----	2.735
1424	2.654	63.31	-----	-----	-----	-----	2.731	-----	-----	-----	-----	2.732
1425	2.650	63.31	-----	-----	-----	-----	2.728	-----	-----	-----	-----	2.728
1426	2.647	63.31	-----	-----	-----	-----	2.725	-----	-----	-----	-----	2.725
1427	2.644	63.31	-----	-----	-----	-----	2.721	-----	-----	-----	-----	2.722
1428	2.640	63.31	-----	-----	-----	-----	2.718	-----	-----	-----	-----	2.718
1429	2.637	63.31	-----	-----	-----	-----	2.715	-----	-----	-----	-----	2.715
1430	2.634	63.31	-----	-----	-----	-----	2.712	-----	-----	-----	-----	2.712
1431	2.630	63.31	-----	-----	-----	-----	2.708	-----	-----	-----	-----	2.708
1432	2.627	63.31	-----	-----	-----	-----	2.705	-----	-----	-----	-----	2.705
1433	2.624	63.31	-----	-----	-----	-----	2.702	-----	-----	-----	-----	2.702
1434	2.620	63.31	-----	-----	-----	-----	2.698	-----	-----	-----	-----	2.698
1435	2.617	63.31	-----	-----	-----	-----	2.695	-----	-----	-----	-----	2.695
1436	2.614	63.30	-----	-----	-----	-----	2.692	-----	-----	-----	-----	2.692
1437	2.610	63.30	-----	-----	-----	-----	2.688	-----	-----	-----	-----	2.688
1438	2.607	63.30	-----	-----	-----	-----	2.685	-----	-----	-----	-----	2.685
1439	2.604	63.30	-----	-----	-----	-----	2.682	-----	-----	-----	-----	2.682
1440	2.600	63.30	-----	-----	-----	-----	2.678	-----	-----	-----	-----	2.678
1441	2.594	63.30	-----	-----	-----	-----	2.675	-----	-----	-----	-----	2.675
1442	2.583	63.30	-----	-----	-----	-----	2.671	-----	-----	-----	-----	2.671
1443	2.570	63.30	-----	-----	-----	-----	2.667	-----	-----	-----	-----	2.667
1444	2.552	63.30	-----	-----	-----	-----	2.663	-----	-----	-----	-----	2.663
1445	2.531	63.30	-----	-----	-----	-----	2.658	-----	-----	-----	-----	2.658
1446	2.507	63.30	-----	-----	-----	-----	2.652	-----	-----	-----	-----	2.652
1447	2.479	63.30	-----	-----	-----	-----	2.645	-----	-----	-----	-----	2.645
1448	2.448	63.30	-----	-----	-----	-----	2.638	-----	-----	-----	-----	2.638
1449	2.413	63.30	-----	-----	-----	-----	2.629	-----	-----	-----	-----	2.629
1450	2.375	63.30	-----	-----	-----	-----	2.619	-----	-----	-----	-----	2.619
1451	2.334	63.30	-----	-----	-----	-----	2.608	-----	-----	-----	-----	2.608
1452	2.289	63.30	-----	-----	-----	-----	2.596	-----	-----	-----	-----	2.596
1453	2.240	63.30	-----	-----	-----	-----	2.582	-----	-----	-----	-----	2.582
1454	2.188	63.30	-----	-----	-----	-----	2.566	-----	-----	-----	-----	2.567
1455	2.133	63.30	-----	-----	-----	-----	2.550	-----	-----	-----	-----	2.550

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1456	2.074	63.30	-----	-----	-----	-----	2.531	-----	-----	-----	-----	2.531
1457	2.012	63.30	-----	-----	-----	-----	2.510	-----	-----	-----	-----	2.510
1458	1.946	63.30	-----	-----	-----	-----	2.488	-----	-----	-----	-----	2.488
1459	1.877	63.30	-----	-----	-----	-----	2.465	-----	-----	-----	-----	2.465
1460	1.804	63.30	-----	-----	-----	-----	2.451	-----	-----	-----	-----	2.451
1461	1.728	63.30	-----	-----	-----	-----	2.435	-----	-----	-----	-----	2.435
1462	1.654	63.30	-----	-----	-----	-----	2.418	-----	-----	-----	-----	2.418
1463	1.581	63.30	-----	-----	-----	-----	2.399	-----	-----	-----	-----	2.399
1464	1.511	63.30	-----	-----	-----	-----	2.380	-----	-----	-----	-----	2.380
1465	1.441	63.30	-----	-----	-----	-----	2.359	-----	-----	-----	-----	2.359
1466	1.374	63.29	-----	-----	-----	-----	2.337	-----	-----	-----	-----	2.337
1467	1.308	63.29	-----	-----	-----	-----	2.314	-----	-----	-----	-----	2.314
1468	1.243	63.29	-----	-----	-----	-----	2.290	-----	-----	-----	-----	2.290
1469	1.181	63.29	-----	-----	-----	-----	2.265	-----	-----	-----	-----	2.265
1470	1.120	63.29	-----	-----	-----	-----	2.239	-----	-----	-----	-----	2.239
1471	1.060	63.29	-----	-----	-----	-----	2.212	-----	-----	-----	-----	2.212
1472	1.002	63.29	-----	-----	-----	-----	2.185	-----	-----	-----	-----	2.185
1473	0.946	63.29	-----	-----	-----	-----	2.157	-----	-----	-----	-----	2.157
1474	0.892	63.29	-----	-----	-----	-----	2.129	-----	-----	-----	-----	2.129
1475	0.839	63.29	-----	-----	-----	-----	2.099	-----	-----	-----	-----	2.099
1476	0.788	63.28	-----	-----	-----	-----	2.070	-----	-----	-----	-----	2.070
1477	0.738	63.28	-----	-----	-----	-----	2.040	-----	-----	-----	-----	2.040
1478	0.690	63.28	-----	-----	-----	-----	2.009	-----	-----	-----	-----	2.009
1479	0.644	63.28	-----	-----	-----	-----	1.978	-----	-----	-----	-----	1.978
1480	0.599	63.28	-----	-----	-----	-----	1.947	-----	-----	-----	-----	1.947
1481	0.556	63.28	-----	-----	-----	-----	1.915	-----	-----	-----	-----	1.915
1482	0.515	63.28	-----	-----	-----	-----	1.883	-----	-----	-----	-----	1.883
1483	0.475	63.28	-----	-----	-----	-----	1.851	-----	-----	-----	-----	1.851
1484	0.437	63.27	-----	-----	-----	-----	1.819	-----	-----	-----	-----	1.819
1485	0.400	63.27	-----	-----	-----	-----	1.787	-----	-----	-----	-----	1.786
1486	0.365	63.27	-----	-----	-----	-----	1.754	-----	-----	-----	-----	1.754
1487	0.332	63.27	-----	-----	-----	-----	1.722	-----	-----	-----	-----	1.722
1488	0.300	63.27	-----	-----	-----	-----	1.689	-----	-----	-----	-----	1.689
1489	0.270	63.27	-----	-----	-----	-----	1.657	-----	-----	-----	-----	1.657
1490	0.242	63.27	-----	-----	-----	-----	1.624	-----	-----	-----	-----	1.624
1491	0.215	63.26	-----	-----	-----	-----	1.592	-----	-----	-----	-----	1.592
1492	0.189	63.26	-----	-----	-----	-----	1.560	-----	-----	-----	-----	1.560
1493	0.166	63.26	-----	-----	-----	-----	1.528	-----	-----	-----	-----	1.528
1494	0.143	63.26	-----	-----	-----	-----	1.496	-----	-----	-----	-----	1.496
1495	0.123	63.26	-----	-----	-----	-----	1.465	-----	-----	-----	-----	1.465
1496	0.104	63.26	-----	-----	-----	-----	1.434	-----	-----	-----	-----	1.434
1497	0.087	63.26	-----	-----	-----	-----	1.403	-----	-----	-----	-----	1.403
1498	0.071	63.26	-----	-----	-----	-----	1.372	-----	-----	-----	-----	1.372
1499	0.057	63.25	-----	-----	-----	-----	1.342	-----	-----	-----	-----	1.342
1500	0.044	63.25	-----	-----	-----	-----	1.312	-----	-----	-----	-----	1.312
1501	0.033	63.25	-----	-----	-----	-----	1.283	-----	-----	-----	-----	1.283
1502	0.024	63.25	-----	-----	-----	-----	1.254	-----	-----	-----	-----	1.254
1503	0.016	63.25	-----	-----	-----	-----	1.225	-----	-----	-----	-----	1.225
1504	0.009	63.25	-----	-----	-----	-----	1.197	-----	-----	-----	-----	1.197
1505	0.005	63.25	-----	-----	-----	-----	1.170	-----	-----	-----	-----	1.170
1506	0.002	63.25	-----	-----	-----	-----	1.143	-----	-----	-----	-----	1.143
1507	0.000	63.25	-----	-----	-----	-----	1.116	-----	-----	-----	-----	1.116
1508	0.000	63.24	-----	-----	-----	-----	1.090	-----	-----	-----	-----	1.090
1509	0.000	63.24	-----	-----	-----	-----	1.065	-----	-----	-----	-----	1.065
1510	0.000	63.24	-----	-----	-----	-----	1.041	-----	-----	-----	-----	1.041
1511	0.000	63.24	-----	-----	-----	-----	1.017	-----	-----	-----	-----	1.017

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1512	0.000	63.24	-----	-----	-----	-----	0.993	-----	-----	-----	-----	0.993
1513	0.000	63.24	-----	-----	-----	-----	0.970	-----	-----	-----	-----	0.970
1514	0.000	63.24	-----	-----	-----	-----	0.948	-----	-----	-----	-----	0.948
1515	0.000	63.24	-----	-----	-----	-----	0.926	-----	-----	-----	-----	0.926
1516	0.000	63.24	-----	-----	-----	-----	0.905	-----	-----	-----	-----	0.904
1517	0.000	63.24	-----	-----	-----	-----	0.884	-----	-----	-----	-----	0.884
1518	0.000	63.24	-----	-----	-----	-----	0.863	-----	-----	-----	-----	0.863
1519	0.000	63.23	-----	-----	-----	-----	0.843	-----	-----	-----	-----	0.843
1520	0.000	63.23	-----	-----	-----	-----	0.824	-----	-----	-----	-----	0.824
1521	0.000	63.23	-----	-----	-----	-----	0.805	-----	-----	-----	-----	0.805
1522	0.000	63.23	-----	-----	-----	-----	0.786	-----	-----	-----	-----	0.786
1523	0.000	63.23	-----	-----	-----	-----	0.768	-----	-----	-----	-----	0.768
1524	0.000	63.23	-----	-----	-----	-----	0.750	-----	-----	-----	-----	0.750
1525	0.000	63.23	-----	-----	-----	-----	0.733	-----	-----	-----	-----	0.733
1526	0.000	63.23	-----	-----	-----	-----	0.716	-----	-----	-----	-----	0.716
1527	0.000	63.23	-----	-----	-----	-----	0.699	-----	-----	-----	-----	0.699
1528	0.000	63.23	-----	-----	-----	-----	0.683	-----	-----	-----	-----	0.683
1529	0.000	63.23	-----	-----	-----	-----	0.667	-----	-----	-----	-----	0.667
1530	0.000	63.23	-----	-----	-----	-----	0.652	-----	-----	-----	-----	0.652
1531	0.000	63.23	-----	-----	-----	-----	0.637	-----	-----	-----	-----	0.637
1532	0.000	63.23	-----	-----	-----	-----	0.622	-----	-----	-----	-----	0.622
1533	0.000	63.22	-----	-----	-----	-----	0.608	-----	-----	-----	-----	0.608
1534	0.000	63.22	-----	-----	-----	-----	0.594	-----	-----	-----	-----	0.594
1535	0.000	63.22	-----	-----	-----	-----	0.580	-----	-----	-----	-----	0.580
1536	0.000	63.22	-----	-----	-----	-----	0.567	-----	-----	-----	-----	0.567
1537	0.000	63.22	-----	-----	-----	-----	0.554	-----	-----	-----	-----	0.554
1538	0.000	63.22	-----	-----	-----	-----	0.541	-----	-----	-----	-----	0.541
1539	0.000	63.22	-----	-----	-----	-----	0.528	-----	-----	-----	-----	0.528
1540	0.000	63.22	-----	-----	-----	-----	0.516	-----	-----	-----	-----	0.516
1541	0.000	63.22	-----	-----	-----	-----	0.504	-----	-----	-----	-----	0.504
1542	0.000	63.22	-----	-----	-----	-----	0.493	-----	-----	-----	-----	0.493
1543	0.000	63.22	-----	-----	-----	-----	0.481	-----	-----	-----	-----	0.481
1544	0.000	63.22	-----	-----	-----	-----	0.470	-----	-----	-----	-----	0.470
1545	0.000	63.22	-----	-----	-----	-----	0.459	-----	-----	-----	-----	0.459
1546	0.000	63.22	-----	-----	-----	-----	0.449	-----	-----	-----	-----	0.449
1547	0.000	63.22	-----	-----	-----	-----	0.438	-----	-----	-----	-----	0.438
1548	0.000	63.22	-----	-----	-----	-----	0.428	-----	-----	-----	-----	0.428
1549	0.000	63.22	-----	-----	-----	-----	0.418	-----	-----	-----	-----	0.418
1550	0.000	63.22	-----	-----	-----	-----	0.409	-----	-----	-----	-----	0.409
1551	0.000	63.22	-----	-----	-----	-----	0.399	-----	-----	-----	-----	0.399
1552	0.000	63.22	-----	-----	-----	-----	0.390	-----	-----	-----	-----	0.390
1553	0.000	63.22	-----	-----	-----	-----	0.381	-----	-----	-----	-----	0.381
1554	0.000	63.22	-----	-----	-----	-----	0.372	-----	-----	-----	-----	0.372
1555	0.000	63.21	-----	-----	-----	-----	0.363	-----	-----	-----	-----	0.364
1556	0.000	63.21	-----	-----	-----	-----	0.355	-----	-----	-----	-----	0.355
1557	0.000	63.21	-----	-----	-----	-----	0.347	-----	-----	-----	-----	0.347
1558	0.000	63.21	-----	-----	-----	-----	0.339	-----	-----	-----	-----	0.339
1559	0.000	63.21	-----	-----	-----	-----	0.331	-----	-----	-----	-----	0.331
1560	0.000	63.21	-----	-----	-----	-----	0.323	-----	-----	-----	-----	0.323
1561	0.000	63.21	-----	-----	-----	-----	0.316	-----	-----	-----	-----	0.316
1562	0.000	63.21	-----	-----	-----	-----	0.309	-----	-----	-----	-----	0.309
1563	0.000	63.21	-----	-----	-----	-----	0.301	-----	-----	-----	-----	0.302
1564	0.000	63.21	-----	-----	-----	-----	0.295	-----	-----	-----	-----	0.295
1565	0.000	63.21	-----	-----	-----	-----	0.288	-----	-----	-----	-----	0.288
1566	0.000	63.21	-----	-----	-----	-----	0.281	-----	-----	-----	-----	0.281
1567	0.000	63.21	-----	-----	-----	-----	0.275	-----	-----	-----	-----	0.275

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1568	0.000	63.21	-----	-----	-----	-----	0.268	-----	-----	-----	-----	0.268
1569	0.000	63.21	-----	-----	-----	-----	0.262	-----	-----	-----	-----	0.262
1570	0.000	63.21	-----	-----	-----	-----	0.256	-----	-----	-----	-----	0.256
1571	0.000	63.21	-----	-----	-----	-----	0.250	-----	-----	-----	-----	0.250
1572	0.000	63.21	-----	-----	-----	-----	0.244	-----	-----	-----	-----	0.244
1573	0.000	63.21	-----	-----	-----	-----	0.239	-----	-----	-----	-----	0.239
1574	0.000	63.21	-----	-----	-----	-----	0.233	-----	-----	-----	-----	0.233
1575	0.000	63.21	-----	-----	-----	-----	0.228	-----	-----	-----	-----	0.228
1576	0.000	63.21	-----	-----	-----	-----	0.223	-----	-----	-----	-----	0.222
1577	0.000	63.21	-----	-----	-----	-----	0.217	-----	-----	-----	-----	0.217
1578	0.000	63.21	-----	-----	-----	-----	0.212	-----	-----	-----	-----	0.212
1579	0.000	63.21	-----	-----	-----	-----	0.207	-----	-----	-----	-----	0.207
1580	0.000	63.21	-----	-----	-----	-----	0.203	-----	-----	-----	-----	0.203
1581	0.000	63.21	-----	-----	-----	-----	0.198	-----	-----	-----	-----	0.198
1582	0.000	63.21	-----	-----	-----	-----	0.193	-----	-----	-----	-----	0.193
1583	0.000	63.21	-----	-----	-----	-----	0.189	-----	-----	-----	-----	0.189
1584	0.000	63.21	-----	-----	-----	-----	0.185	-----	-----	-----	-----	0.185
1585	0.000	63.21	-----	-----	-----	-----	0.180	-----	-----	-----	-----	0.180
1586	0.000	63.21	-----	-----	-----	-----	0.176	-----	-----	-----	-----	0.176
1587	0.000	63.21	-----	-----	-----	-----	0.172	-----	-----	-----	-----	0.172
1588	0.000	63.21	-----	-----	-----	-----	0.168	-----	-----	-----	-----	0.168
1589	0.000	63.21	-----	-----	-----	-----	0.164	-----	-----	-----	-----	0.164
1590	0.000	63.21	-----	-----	-----	-----	0.160	-----	-----	-----	-----	0.160
1591	0.000	63.21	-----	-----	-----	-----	0.157	-----	-----	-----	-----	0.157
1592	0.000	63.21	-----	-----	-----	-----	0.153	-----	-----	-----	-----	0.153
1593	0.000	63.21	-----	-----	-----	-----	0.150	-----	-----	-----	-----	0.150
1594	0.000	63.21	-----	-----	-----	-----	0.146	-----	-----	-----	-----	0.146
1595	0.000	63.21	-----	-----	-----	-----	0.143	-----	-----	-----	-----	0.143
1596	0.000	63.21	-----	-----	-----	-----	0.139	-----	-----	-----	-----	0.139
1597	0.000	63.21	-----	-----	-----	-----	0.136	-----	-----	-----	-----	0.136
1598	0.000	63.21	-----	-----	-----	-----	0.133	-----	-----	-----	-----	0.133
1599	0.000	63.21	-----	-----	-----	-----	0.130	-----	-----	-----	-----	0.130
1600	0.000	63.21	-----	-----	-----	-----	0.127	-----	-----	-----	-----	0.127
1601	0.000	63.21	-----	-----	-----	-----	0.124	-----	-----	-----	-----	0.124
1602	0.000	63.20	-----	-----	-----	-----	0.121	-----	-----	-----	-----	0.121
1603	0.000	63.20	-----	-----	-----	-----	0.118	-----	-----	-----	-----	0.118
1604	0.000	63.20	-----	-----	-----	-----	0.116	-----	-----	-----	-----	0.116
1605	0.000	63.20	-----	-----	-----	-----	0.113	-----	-----	-----	-----	0.113
1606	0.000	63.20	-----	-----	-----	-----	0.110	-----	-----	-----	-----	0.110
1607	0.000	63.20	-----	-----	-----	-----	0.108	-----	-----	-----	-----	0.108
1608	0.000	63.20	-----	-----	-----	-----	0.105	-----	-----	-----	-----	0.105
1609	0.000	63.20	-----	-----	-----	-----	0.103	-----	-----	-----	-----	0.103
1610	0.000	63.20	-----	-----	-----	-----	0.100	-----	-----	-----	-----	0.101
1611	0.000	63.20	-----	-----	-----	-----	0.098	-----	-----	-----	-----	0.098
1612	0.000	63.20	-----	-----	-----	-----	0.096	-----	-----	-----	-----	0.096
1613	0.000	63.20	-----	-----	-----	-----	0.094	-----	-----	-----	-----	0.094
1614	0.000	63.20	-----	-----	-----	-----	0.092	-----	-----	-----	-----	0.092
1615	0.000	63.20	-----	-----	-----	-----	0.089	-----	-----	-----	-----	0.089
1616	0.000	63.20	-----	-----	-----	-----	0.087	-----	-----	-----	-----	0.087
1617	0.000	63.20	-----	-----	-----	-----	0.085	-----	-----	-----	-----	0.085
1618	0.000	63.20	-----	-----	-----	-----	0.083	-----	-----	-----	-----	0.083
1619	0.000	63.20	-----	-----	-----	-----	0.081	-----	-----	-----	-----	0.081
1620	0.000	63.20	-----	-----	-----	-----	0.080	-----	-----	-----	-----	0.080
1621	0.000	63.20	-----	-----	-----	-----	0.078	-----	-----	-----	-----	0.078
1622	0.000	63.20	-----	-----	-----	-----	0.076	-----	-----	-----	-----	0.076
1623	0.000	63.20	-----	-----	-----	-----	0.074	-----	-----	-----	-----	0.074

Continues on next page...

Detention pond outflow

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1624	0.000	63.20	-----	-----	-----	-----	0.072	-----	-----	-----	-----	0.072
1625	0.000	63.20	-----	-----	-----	-----	0.071	-----	-----	-----	-----	0.071
1626	0.000	63.20	-----	-----	-----	-----	0.069	-----	-----	-----	-----	0.069
1627	0.000	63.20	-----	-----	-----	-----	0.068	-----	-----	-----	-----	0.068
1628	0.000	63.20	-----	-----	-----	-----	0.066	-----	-----	-----	-----	0.066
1629	0.000	63.20	-----	-----	-----	-----	0.064	-----	-----	-----	-----	0.064
1630	0.000	63.20	-----	-----	-----	-----	0.063	-----	-----	-----	-----	0.063

...End

EMERGENCY RELEASE THROUGH 30’ BROAD CRESTED WEIR MODEL CALCULATIONS

Watershed Model Schematic

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

Legend

Hyd.	Origin	Description
1	SCS Runoff	Developed site storm event
2	Reservoir	Detention pond outflow

Project: Proposed site SCS 06-25-09 Broad crested weir emergency.gpw

Thursday, Jul 2, 2009

Hydrograph Return Period Recap

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

Hyd. No.	Hydrograph type (origin)	Inflow Hyd(s)	Peak Outflow (cfs)								Hydrograph description
			1-Yr	2-Yr	3-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr	
1	SCS Runoff	------	-------	7.792	-------	11.97	14.81	18.23	20.66	23.03	Developed site storm event
2	Reservoir	1	-------	0.000	-------	1.838	2.737	3.816	4.911	6.197	Detention pond outflow

Hydrograph Summary Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	SCS Runoff	14.81	1	495	257,225	------	------	------	Developed site storm event
2	Reservoir	2.737	1	1012	84,215	1	63.31	179,719	Detention pond outflow

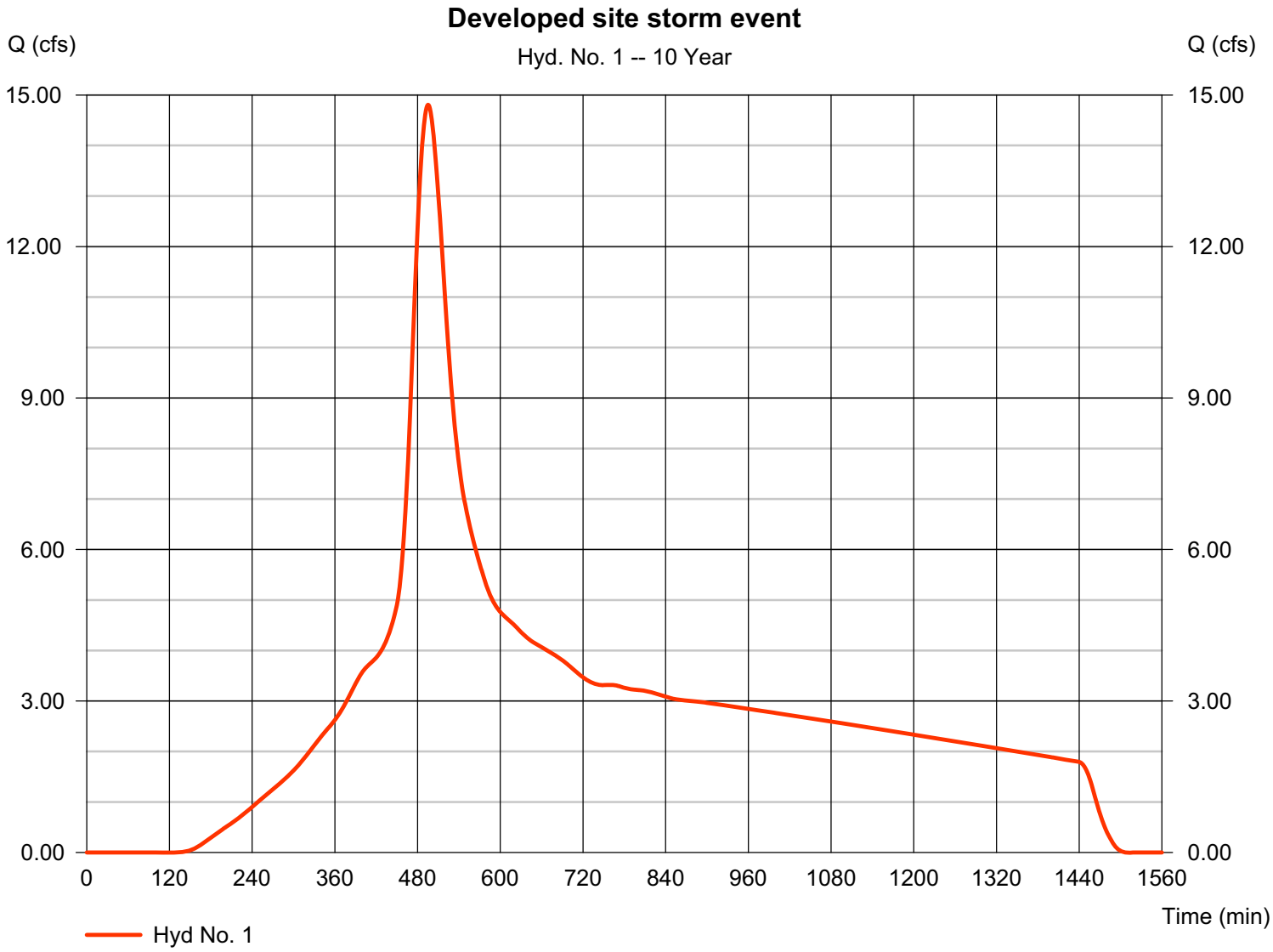
Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Hyd. No. 1

Developed site storm event

Hydrograph type	=	SCS Runoff	Peak discharge	=	14.81 cfs
Storm frequency	=	10 yrs	Time to peak	=	495 min
Time interval	=	1 min	Hyd. volume	=	257,225 cuft
Drainage area	=	25.500 ac	Curve number	=	91
Basin Slope	=	0.0 %	Hydraulic length	=	0 ft
Tc method	=	TR55	Time of conc. (Tc)	=	34.00 min
Total precip.	=	3.74 in	Distribution	=	Type IA
Storm duration	=	24 hrs	Shape factor	=	400



TR55 Tc Worksheet

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

Hyd. No. 1

Developed site storm event

Description		A		B		C		Totals
Sheet Flow								
Manning's n-value	=	0.240		0.011		0.011		
Flow length (ft)	=	180.0		0.0		0.0		
Two-year 24-hr precip. (in)	=	2.39		0.00		0.00		
Land slope (%)	=	1.50		0.00		0.00		
Travel Time (min)	**=**	**29.65**	**+**	**0.00**	**+**	**0.00**	**=**	**29.65**
Shallow Concentrated Flow								
Flow length (ft)	=	0.00		0.00		0.00		
Watercourse slope (%)	=	0.00		0.00		0.00		
Surface description	=	Paved		Paved		Paved		
Average velocity (ft/s)	=	0.00		0.00		0.00		
Travel Time (min)	**=**	**0.00**	**+**	**0.00**	**+**	**0.00**	**=**	**0.00**
Channel Flow								
X sectional flow area (sqft)	=	18.00		0.00		0.00		
Wetted perimeter (ft)	=	13.40		0.00		0.00		
Channel slope (%)	=	0.25		0.00		0.00		
Manning's n-value	=	0.025		0.015		0.015		
Velocity (ft/s)	=	3.63		0.00		0.00		
Flow length (ft)	=	950.0		0.0		0.0		
Travel Time (min)	**=**	**4.36**	**+**	**0.00**	**+**	**0.00**	**=**	**4.36**

Total Travel Time, Tc ..... 34.00 min

Hydrograph Report

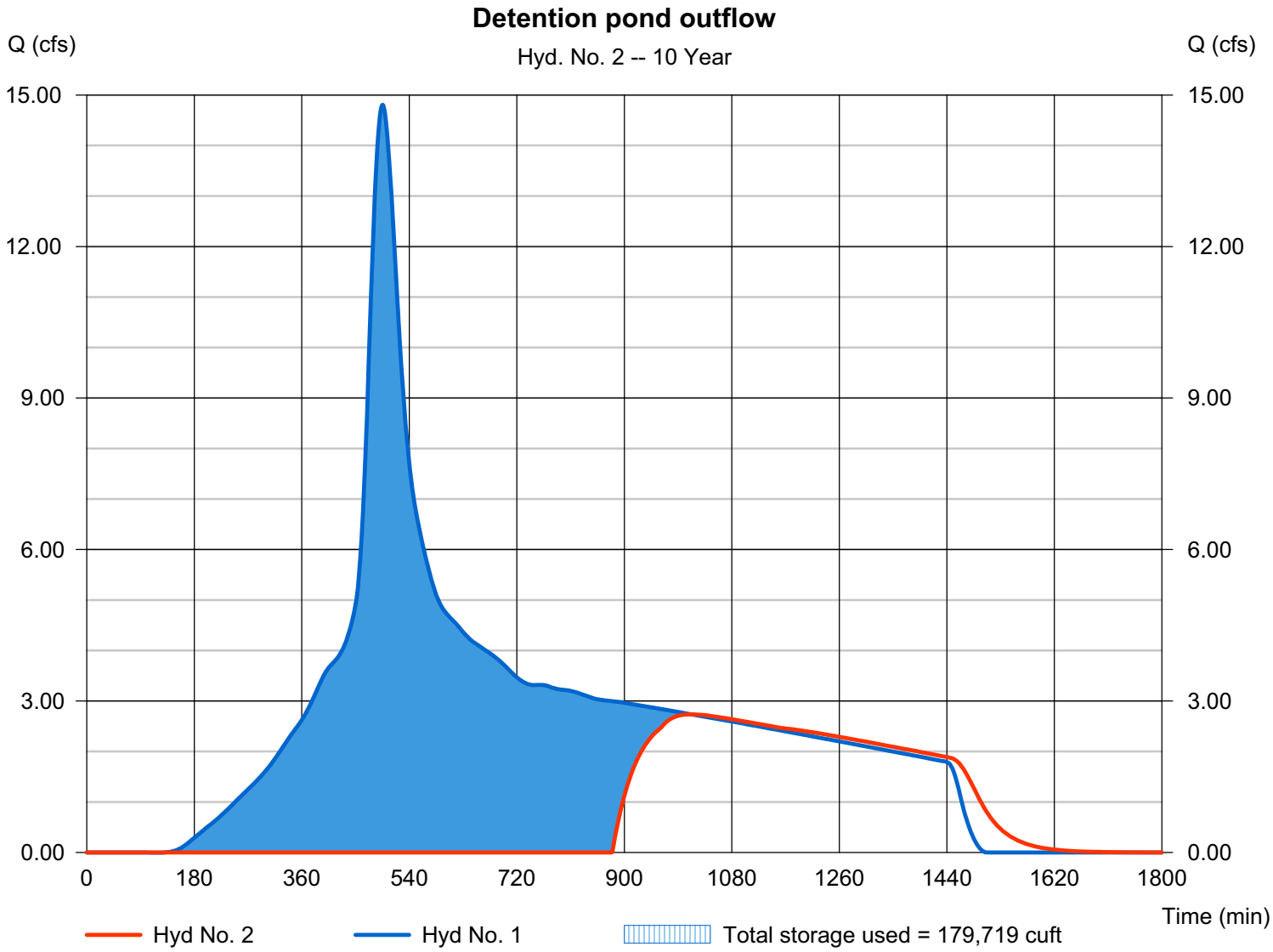
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Hyd. No. 2

Detention pond outflow

Hydrograph type	=	Reservoir	Peak discharge	=	2.737 cfs
Storm frequency	=	10 yrs	Time to peak	=	1012 min
Time interval	=	1 min	Hyd. volume	=	84,215 cuft
Inflow hyd. No.	=	1 - Developed site storm event	Max. Elevation	=	63.31 ft
Reservoir name	=	Detention Pond	Max. Storage	=	179,719 cuft

Storage Indication method used.



Pond Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Pond No. 1 - Detention Pond

Pond Data

Contours - User-defined contour areas. Average end area method used for volume calculation. Begining Elevation = 59.00 ft

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	59.00	10	0	0
1.00	60.00	24,253	12,132	12,132
1.70	60.70	46,955	24,923	37,054
2.00	61.00	48,669	14,344	51,398
3.00	62.00	54,448	51,559	102,956
4.00	63.00	60,328	57,388	160,344
5.00	64.00	66,309	63,319	223,663

Culvert / Orifice Structures

	[A]	[B]	[C]	[PrfRsr]
Rise (in)	Inactive	Inactive	Inactive	Inactive
Span (in)	= 0.00	0.00	0.00	0.00
No. Barrels	= 1	1	0	0
Invert El. (ft)	= 0.00	0.00	0.00	0.00
Length (ft)	= 0.00	0.00	0.00	0.00
Slope (%)	= 0.00	0.00	0.00	n/a
N-Value	= .013	.013	.013	n/a
Orifice Coeff.	= 0.60	0.60	0.60	0.60
Multi-Stage	= n/a	Yes	Yes	Yes

Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 30.00	0.00	0.00	0.00
Crest El. (ft)	= 63.20	0.00	0.00	0.00
Weir Coeff.	= 2.60	2.60	3.33	3.33
Weir Type	= Broad	---	---	---
Multi-Stage	= No	No	No	No

Exfil.(in/hr) = 0.000 (by Wet area)

TW Elev. (ft) = 61.20

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0	59.00	---	---	---	---	0.00	---	---	---	---	---	0.000
0.10	1,213	59.10	---	---	---	---	0.00	---	---	---	---	---	0.000
0.20	2,426	59.20	---	---	---	---	0.00	---	---	---	---	---	0.000
0.30	3,639	59.30	---	---	---	---	0.00	---	---	---	---	---	0.000
0.40	4,853	59.40	---	---	---	---	0.00	---	---	---	---	---	0.000
0.50	6,066	59.50	---	---	---	---	0.00	---	---	---	---	---	0.000
0.60	7,279	59.60	---	---	---	---	0.00	---	---	---	---	---	0.000
0.70	8,492	59.70	---	---	---	---	0.00	---	---	---	---	---	0.000
0.80	9,705	59.80	---	---	---	---	0.00	---	---	---	---	---	0.000
0.90	10,918	59.90	---	---	---	---	0.00	---	---	---	---	---	0.000
1.00	12,132	60.00	---	---	---	---	0.00	---	---	---	---	---	0.000
1.07	14,624	60.07	---	---	---	---	0.00	---	---	---	---	---	0.000
1.14	17,116	60.14	---	---	---	---	0.00	---	---	---	---	---	0.000
1.21	19,608	60.21	---	---	---	---	0.00	---	---	---	---	---	0.000
1.28	22,101	60.28	---	---	---	---	0.00	---	---	---	---	---	0.000
1.35	24,593	60.35	---	---	---	---	0.00	---	---	---	---	---	0.000
1.42	27,085	60.42	---	---	---	---	0.00	---	---	---	---	---	0.000
1.49	29,577	60.49	---	---	---	---	0.00	---	---	---	---	---	0.000
1.56	32,070	60.56	---	---	---	---	0.00	---	---	---	---	---	0.000
1.63	34,562	60.63	---	---	---	---	0.00	---	---	---	---	---	0.000
1.70	37,054	60.70	---	---	---	---	0.00	---	---	---	---	---	0.000
1.73	38,489	60.73	---	---	---	---	0.00	---	---	---	---	---	0.000
1.76	39,923	60.76	---	---	---	---	0.00	---	---	---	---	---	0.000
1.79	41,357	60.79	---	---	---	---	0.00	---	---	---	---	---	0.000
1.82	42,792	60.82	---	---	---	---	0.00	---	---	---	---	---	0.000
1.85	44,226	60.85	---	---	---	---	0.00	---	---	---	---	---	0.000
1.88	45,660	60.88	---	---	---	---	0.00	---	---	---	---	---	0.000
1.91	47,095	60.91	---	---	---	---	0.00	---	---	---	---	---	0.000
1.94	48,529	60.94	---	---	---	---	0.00	---	---	---	---	---	0.000
1.97	49,964	60.97	---	---	---	---	0.00	---	---	---	---	---	0.000
2.00	51,398	61.00	---	---	---	---	0.00	---	---	---	---	---	0.000
2.10	56,554	61.10	---	---	---	---	0.00	---	---	---	---	---	0.000
2.20	61,710	61.20	---	---	---	---	0.00	---	---	---	---	---	0.000
2.30	66,865	61.30	---	---	---	---	0.00	---	---	---	---	---	0.000
2.40	72,021	61.40	---	---	---	---	0.00	---	---	---	---	---	0.000
2.50	77,177	61.50	---	---	---	---	0.00	---	---	---	---	---	0.000
2.60	82,333	61.60	---	---	---	---	0.00	---	---	---	---	---	0.000
2.70	87,489	61.70	---	---	---	---	0.00	---	---	---	---	---	0.000

Continues on next page...

Detention Pond

Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
2.80	92,645	61.80	---	---	---	---	0.00	---	---	---	---	---	0.000
2.90	97,801	61.90	---	---	---	---	0.00	---	---	---	---	---	0.000
3.00	102,956	62.00	---	---	---	---	0.00	---	---	---	---	---	0.000
3.10	108,695	62.10	---	---	---	---	0.00	---	---	---	---	---	0.000
3.20	114,434	62.20	---	---	---	---	0.00	---	---	---	---	---	0.000
3.30	120,173	62.30	---	---	---	---	0.00	---	---	---	---	---	0.000
3.40	125,912	62.40	---	---	---	---	0.00	---	---	---	---	---	0.000
3.50	131,650	62.50	---	---	---	---	0.00	---	---	---	---	---	0.000
3.60	137,389	62.60	---	---	---	---	0.00	---	---	---	---	---	0.000
3.70	143,128	62.70	---	---	---	---	0.00	---	---	---	---	---	0.000
3.80	148,867	62.80	---	---	---	---	0.00	---	---	---	---	---	0.000
3.90	154,606	62.90	---	---	---	---	0.00	---	---	---	---	---	0.000
4.00	160,344	63.00	---	---	---	---	0.00	---	---	---	---	---	0.000
4.10	166,676	63.10	---	---	---	---	0.00	---	---	---	---	---	0.000
4.20	173,008	63.20	---	---	---	---	0.00	---	---	---	---	---	0.000
4.30	179,340	63.30	---	---	---	---	2.47	---	---	---	---	---	2.467
4.40	185,672	63.40	---	---	---	---	6.98	---	---	---	---	---	6.976
4.50	192,004	63.50	---	---	---	---	12.82	---	---	---	---	---	12.82
4.60	198,336	63.60	---	---	---	---	19.73	---	---	---	---	---	19.73
4.70	204,667	63.70	---	---	---	---	27.58	---	---	---	---	---	27.58
4.80	210,999	63.80	---	---	---	---	36.25	---	---	---	---	---	36.25
4.90	217,331	63.90	---	---	---	---	45.68	---	---	---	---	---	45.68
5.00	223,663	64.00	---	---	---	---	55.81	---	---	---	---	---	55.81

...End

Hydrograph Summary Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	SCS Runoff	23.03	1	495	397,003	------	------	------	Developed site storm event
2	Reservoir	6.197	1	648	223,992	1	63.38	184,578	Detention pond outflow

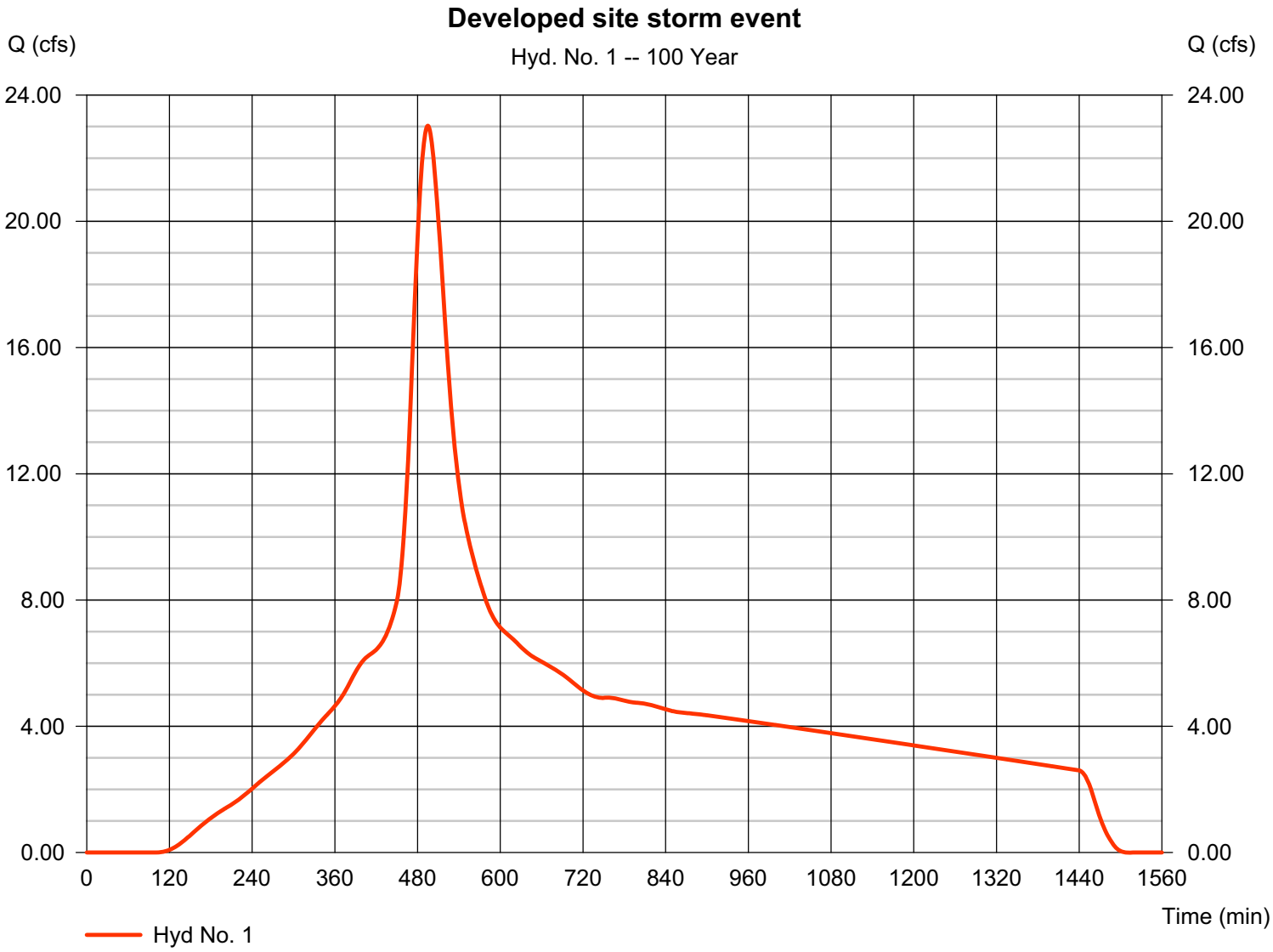
Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Hyd. No. 1

Developed site storm event

Hydrograph type	=	SCS Runoff	Peak discharge	=	23.03 cfs
Storm frequency	=	100 yrs	Time to peak	=	495 min
Time interval	=	1 min	Hyd. volume	=	397,003 cuft
Drainage area	=	25.500 ac	Curve number	=	91
Basin Slope	=	0.0 %	Hydraulic length	=	0 ft
Tc method	=	TR55	Time of conc. (Tc)	=	34.00 min
Total precip.	=	5.30 in	Distribution	=	Type IA
Storm duration	=	24 hrs	Shape factor	=	400



Hydrograph Report

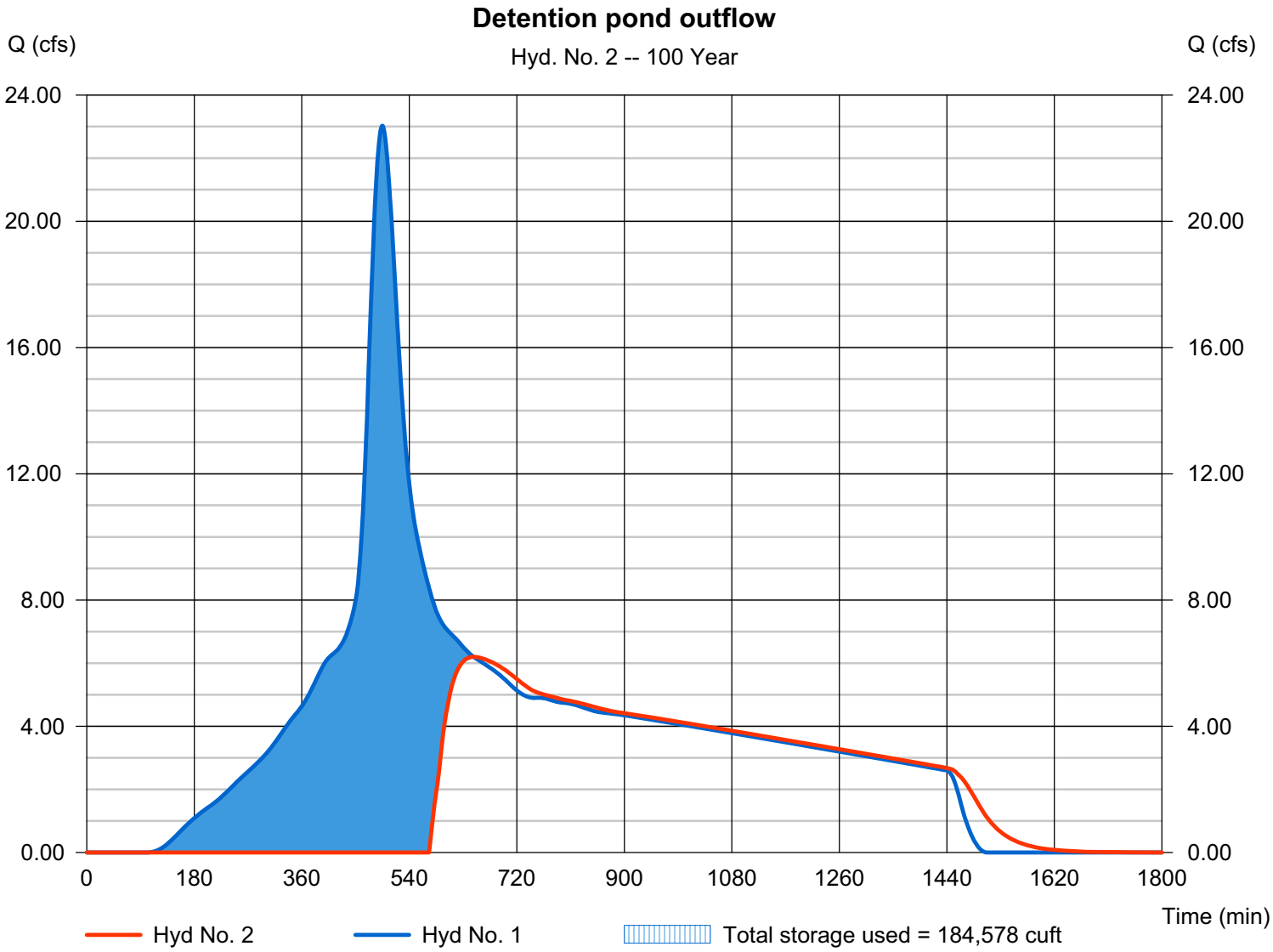
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Hyd. No. 2

Detention pond outflow

Hydrograph type	=	Reservoir	Peak discharge	=	6.197 cfs
Storm frequency	=	100 yrs	Time to peak	=	648 min
Time interval	=	1 min	Hyd. volume	=	223,992 cuft
Inflow hyd. No.	=	1 - Developed site storm event	Max. Elevation	=	63.38 ft
Reservoir name	=	Detention Pond	Max. Storage	=	184,578 cuft

Storage Indication method used.



Hydraflow Rainfall Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Return Period (Yrs)	Intensity-Duration-Frequency Equation Coefficients (FHA)			
	B	D	E	(N/A)
1	0.0000	0.0000	0.0000	--------
2	6.1078	0.1000	0.5625	--------
3	0.0000	0.0000	0.0000	--------
5	8.7423	0.3000	0.5773	--------
10	9.7582	0.1000	0.5661	--------
25	11.5209	0.1000	0.5690	--------
50	12.8436	0.1000	0.5707	--------
100	14.8890	0.3000	0.5856	--------

File name: Vacaville_ISO_22.IDF

Intensity = B / (Tc + D)^E

Return Period (Yrs)	Intensity Values (in/hr)											
	5 min	10	15	20	25	30	35	40	45	50	55	60
1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	2.44	1.66	1.33	1.13	1.00	0.90	0.83	0.77	0.72	0.68	0.64	0.61
3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5	3.34	2.27	1.81	1.54	1.35	1.22	1.12	1.03	0.97	0.91	0.86	0.82
10	3.88	2.63	2.10	1.78	1.57	1.42	1.30	1.21	1.13	1.06	1.01	0.96
25	4.56	3.09	2.46	2.09	1.84	1.66	1.52	1.41	1.32	1.24	1.18	1.12
50	5.07	3.43	2.73	2.32	2.04	1.84	1.69	1.56	1.46	1.38	1.30	1.24
100	5.61	3.80	3.01	2.55	2.24	2.02	1.85	1.71	1.60	1.50	1.42	1.35

Tc = time in minutes. Values may exceed 60.

Precip. file name: Sample.pcp

Storm Distribution	Rainfall Precipitation Table (in)							
	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr
SCS 24-hour	0.00	2.39	0.00	3.20	3.74	4.39	4.85	5.30
SCS 6-Hr	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-1st	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-2nd	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-3rd	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-4th	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-Indy	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Custom	0.00	2.39	0.00	3.20	3.74	4.39	4.85	5.30

Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Hyd. No. 1

Developed site storm event

Hydrograph type	= SCS Runoff	Peak discharge	= 14.81 cfs
Storm frequency	= 10 yrs	Time to peak	= 495 min
Time interval	= 1 min	Hyd. volume	= 257,225 cuft
Drainage area	= 25.500 ac	Curve number	= 91
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 34.0 min
Total precip.	= 3.74 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 400

Hydrograph Discharge Table

(Printed values >= 1.00% of Qp.)

Time -- Outflow (min cfs)		Time -- Outflow (min cfs)		Time -- Outflow (min cfs)		Time -- Outflow (min cfs)	
165	0.148	204	0.526	243	0.938	282	1.390
166	0.157	205	0.535	244	0.950	283	1.403
167	0.166	206	0.544	245	0.962	284	1.415
168	0.175	207	0.553	246	0.974	285	1.427
169	0.184	208	0.563	247	0.986	286	1.439
170	0.193	209	0.572	248	0.998	287	1.452
171	0.202	210	0.581	249	1.009	288	1.464
172	0.212	211	0.591	250	1.021	289	1.477
173	0.221	212	0.600	251	1.033	290	1.490
174	0.231	213	0.610	252	1.045	291	1.503
175	0.241	214	0.619	253	1.056	292	1.516
176	0.251	215	0.629	254	1.068	293	1.529
177	0.260	216	0.639	255	1.079	294	1.542
178	0.270	217	0.649	256	1.091	295	1.555
179	0.280	218	0.659	257	1.103	296	1.569
180	0.291	219	0.669	258	1.114	297	1.582
181	0.301	220	0.679	259	1.125	298	1.596
182	0.311	221	0.689	260	1.137	299	1.610
183	0.321	222	0.699	261	1.148	300	1.624
184	0.331	223	0.710	262	1.159	301	1.638
185	0.341	224	0.720	263	1.171	302	1.652
186	0.351	225	0.731	264	1.182	303	1.667
187	0.361	226	0.742	265	1.193	304	1.682
188	0.371	227	0.753	266	1.205	305	1.696
189	0.382	228	0.764	267	1.216	306	1.712
190	0.392	229	0.775	268	1.227	307	1.727
191	0.401	230	0.786	269	1.239	308	1.742
192	0.411	231	0.797	270	1.250	309	1.758
193	0.421	232	0.809	271	1.262	310	1.774
194	0.431	233	0.821	272	1.273	311	1.790
195	0.441	234	0.832	273	1.285	312	1.806
196	0.450	235	0.844	274	1.296	313	1.822
197	0.460	236	0.855	275	1.308	314	1.839
198	0.469	237	0.867	276	1.319	315	1.856
199	0.479	238	0.879	277	1.331	316	1.873
200	0.488	239	0.891	278	1.343	317	1.890
201	0.498	240	0.903	279	1.355	318	1.907
202	0.507	241	0.915	280	1.367	319	1.924
203	0.516	242	0.927	281	1.378	320	1.941

Continues on next page...

Hydrograph Discharge Table

Time (min	-- Outflow cfs)	Time (min	-- Outflow cfs)	Time (min	-- Outflow cfs)	Time (min	-- Outflow cfs)
321	1.959	377	2.995	433	4.148	489	14.38
322	1.977	378	3.021	434	4.178	490	14.50
323	1.994	379	3.048	435	4.211	491	14.61
324	2.012	380	3.074	436	4.245	492	14.69
325	2.030	381	3.101	437	4.280	493	14.75
326	2.048	382	3.129	438	4.317	494	14.79
327	2.066	383	3.156	439	4.356	495	14.81 <<
328	2.084	384	3.183	440	4.396	496	14.80
329	2.102	385	3.210	441	4.438	497	14.78
330	2.120	386	3.238	442	4.482	498	14.73
331	2.138	387	3.265	443	4.528	499	14.66
332	2.155	388	3.292	444	4.576	500	14.57
333	2.173	389	3.318	445	4.625	501	14.46
334	2.191	390	3.345	446	4.676	502	14.34
335	2.208	391	3.371	447	4.730	503	14.21
336	2.226	392	3.397	448	4.785	504	14.07
337	2.243	393	3.422	449	4.843	505	13.92
338	2.260	394	3.446	450	4.902	506	13.76
339	2.277	395	3.469	451	4.973	507	13.59
340	2.294	396	3.492	452	5.057	508	13.41
341	2.311	397	3.513	453	5.154	509	13.23
342	2.328	398	3.534	454	5.264	510	13.04
343	2.345	399	3.555	455	5.388	511	12.84
344	2.361	400	3.574	456	5.526	512	12.64
345	2.378	401	3.593	457	5.678	513	12.44
346	2.394	402	3.610	458	5.844	514	12.23
347	2.411	403	3.628	459	6.025	515	12.02
348	2.427	404	3.644	460	6.220	516	11.81
349	2.443	405	3.659	461	6.430	517	11.59
350	2.460	406	3.674	462	6.654	518	11.37
351	2.476	407	3.689	463	6.894	519	11.15
352	2.492	408	3.702	464	7.147	520	10.94
353	2.508	409	3.715	465	7.416	521	10.73
354	2.525	410	3.727	466	7.699	522	10.52
355	2.542	411	3.739	467	7.997	523	10.32
356	2.559	412	3.751	468	8.309	524	10.12
357	2.576	413	3.763	469	8.635	525	9.930
358	2.593	414	3.776	470	8.976	526	9.743
359	2.610	415	3.788	471	9.330	527	9.561
360	2.628	416	3.802	472	9.683	528	9.386
361	2.646	417	3.815	473	10.03	529	9.217
362	2.664	418	3.830	474	10.38	530	9.054
363	2.683	419	3.845	475	10.73	531	8.898
364	2.702	420	3.860	476	11.07	532	8.744
365	2.721	421	3.877	477	11.40	533	8.595
366	2.742	422	3.894	478	11.73	534	8.451
367	2.762	423	3.911	479	12.05	535	8.312
368	2.783	424	3.930	480	12.36	536	8.178
369	2.805	425	3.950	481	12.65	537	8.049
370	2.827	426	3.971	482	12.93	538	7.926
371	2.850	427	3.992	483	13.20	539	7.808
372	2.873	428	4.015	484	13.44	540	7.695
373	2.896	429	4.039	485	13.67	541	7.586
374	2.920	430	4.064	486	13.88	542	7.482
375	2.945	431	4.091	487	14.06	543	7.384
376	2.970	432	4.118	488	14.23	544	7.291

Continues on next page...

Hydrograph Discharge Table

Time (min	Outflow cfs)	Time (min	Outflow cfs)	Time (min	Outflow cfs)	Time (min	Outflow cfs)
545	7.203	601	4.749	657	4.090	713	3.544
546	7.120	602	4.735	658	4.082	714	3.532
547	7.043	603	4.721	659	4.074	715	3.521
548	6.970	604	4.708	660	4.066	716	3.510
549	6.899	605	4.695	661	4.058	717	3.500
550	6.831	606	4.682	662	4.050	718	3.489
551	6.764	607	4.670	663	4.042	719	3.479
552	6.698	608	4.657	664	4.033	720	3.469
553	6.634	609	4.644	665	4.025	721	3.459
554	6.572	610	4.632	666	4.017	722	3.449
555	6.510	611	4.619	667	4.009	723	3.440
556	6.450	612	4.607	668	4.000	724	3.431
557	6.392	613	4.594	669	3.993	725	3.422
558	6.334	614	4.582	670	3.985	726	3.414
559	6.277	615	4.570	671	3.977	727	3.405
560	6.221	616	4.558	672	3.970	728	3.398
561	6.166	617	4.545	673	3.962	729	3.390
562	6.114	618	4.533	674	3.954	730	3.383
563	6.062	619	4.521	675	3.945	731	3.376
564	6.012	620	4.509	676	3.937	732	3.369
565	5.962	621	4.497	677	3.929	733	3.363
566	5.913	622	4.482	678	3.920	734	3.357
567	5.865	623	4.467	679	3.912	735	3.352
568	5.817	624	4.452	680	3.903	736	3.347
569	5.770	625	4.437	681	3.894	737	3.342
570	5.723	626	4.423	682	3.885	738	3.337
571	5.675	627	4.408	683	3.876	739	3.333
572	5.628	628	4.394	684	3.866	740	3.330
573	5.582	629	4.380	685	3.857	741	3.326
574	5.536	630	4.366	686	3.848	742	3.324
575	5.491	631	4.352	687	3.838	743	3.321
576	5.447	632	4.339	688	3.828	744	3.319
577	5.403	633	4.326	689	3.818	745	3.317
578	5.360	634	4.313	690	3.808	746	3.316
579	5.320	635	4.300	691	3.798	747	3.315
580	5.280	636	4.288	692	3.788	748	3.315
581	5.242	637	4.276	693	3.777	749	3.315
582	5.206	638	4.265	694	3.766	750	3.315
583	5.170	639	4.253	695	3.755	751	3.315
584	5.136	640	4.241	696	3.744	752	3.316
585	5.104	641	4.230	697	3.733	753	3.317
586	5.072	642	4.219	698	3.721	754	3.317
587	5.042	643	4.208	699	3.709	755	3.318
588	5.013	644	4.198	700	3.698	756	3.318
589	4.986	645	4.188	701	3.686	757	3.319
590	4.959	646	4.179	702	3.674	758	3.319
591	4.934	647	4.170	703	3.662	759	3.319
592	4.912	648	4.161	704	3.651	760	3.319
593	4.892	649	4.153	705	3.639	761	3.319
594	4.872	650	4.144	706	3.627	762	3.318
595	4.852	651	4.137	707	3.615	763	3.318
596	4.833	652	4.129	708	3.603	764	3.317
597	4.815	653	4.121	709	3.591	765	3.315
598	4.797	654	4.113	710	3.579	766	3.314
599	4.780	655	4.105	711	3.567	767	3.312
600	4.763	656	4.097	712	3.555	768	3.309

Continues on next page...

Hydrograph Discharge Table

Time -- Outflow (min cfs)		Time -- Outflow (min cfs)		Time -- Outflow (min cfs)		Time -- Outflow (min cfs)	
769	3.306	825	3.151	881	2.994	937	2.891
770	3.303	826	3.147	882	2.993	938	2.889
771	3.299	827	3.143	883	2.991	939	2.887
772	3.295	828	3.139	884	2.990	940	2.885
773	3.291	829	3.135	885	2.988	941	2.883
774	3.286	830	3.130	886	2.987	942	2.881
775	3.282	831	3.126	887	2.986	943	2.879
776	3.278	832	3.122	888	2.984	944	2.877
777	3.274	833	3.117	889	2.983	945	2.874
778	3.270	834	3.113	890	2.981	946	2.872
779	3.266	835	3.109	891	2.980	947	2.870
780	3.262	836	3.104	892	2.978	948	2.868
781	3.258	837	3.100	893	2.976	949	2.866
782	3.254	838	3.095	894	2.975	950	2.864
783	3.251	839	3.091	895	2.973	951	2.862
784	3.247	840	3.087	896	2.971	952	2.860
785	3.244	841	3.082	897	2.970	953	2.858
786	3.242	842	3.078	898	2.968	954	2.856
787	3.239	843	3.074	899	2.966	955	2.854
788	3.236	844	3.070	900	2.964	956	2.852
789	3.234	845	3.066	901	2.962	957	2.850
790	3.232	846	3.062	902	2.961	958	2.848
791	3.230	847	3.058	903	2.959	959	2.846
792	3.228	848	3.054	904	2.957	960	2.844
793	3.227	849	3.051	905	2.955	961	2.842
794	3.225	850	3.048	906	2.953	962	2.840
795	3.224	851	3.044	907	2.951	963	2.838
796	3.223	852	3.041	908	2.949	964	2.836
797	3.222	853	3.039	909	2.947	965	2.834
798	3.221	854	3.036	910	2.945	966	2.832
799	3.220	855	3.034	911	2.943	967	2.830
800	3.219	856	3.031	912	2.941	968	2.828
801	3.218	857	3.029	913	2.939	969	2.825
802	3.217	858	3.027	914	2.937	970	2.823
803	3.216	859	3.025	915	2.935	971	2.821
804	3.214	860	3.024	916	2.933	972	2.819
805	3.212	861	3.022	917	2.931	973	2.817
806	3.210	862	3.020	918	2.929	974	2.815
807	3.208	863	3.019	919	2.927	975	2.813
808	3.206	864	3.017	920	2.925	976	2.811
809	3.203	865	3.016	921	2.923	977	2.809
810	3.201	866	3.014	922	2.921	978	2.807
811	3.198	867	3.013	923	2.919	979	2.805
812	3.195	868	3.011	924	2.917	980	2.803
813	3.192	869	3.010	925	2.915	981	2.801
814	3.189	870	3.009	926	2.913	982	2.799
815	3.186	871	3.007	927	2.911	983	2.797
816	3.183	872	3.006	928	2.909	984	2.795
817	3.180	873	3.005	929	2.907	985	2.793
818	3.176	874	3.003	930	2.905	986	2.790
819	3.173	875	3.002	931	2.903	987	2.788
820	3.170	876	3.001	932	2.901	988	2.786
821	3.166	877	2.999	933	2.899	989	2.784
822	3.163	878	2.998	934	2.897	990	2.782
823	3.159	879	2.997	935	2.895	991	2.780
824	3.155	880	2.995	936	2.893	992	2.778

Continues on next page...

Hydrograph Discharge Table

Time -- Outflow (min	cfs)	Time -- Outflow (min	cfs)	Time -- Outflow (min	cfs)	Time -- Outflow (min	cfs)
993	2.776	1049	2.659	1105	2.539	1161	2.418
994	2.774	1050	2.657	1106	2.537	1162	2.416
995	2.772	1051	2.654	1107	2.535	1163	2.414
996	2.770	1052	2.652	1108	2.533	1164	2.411
997	2.768	1053	2.650	1109	2.531	1165	2.409
998	2.766	1054	2.648	1110	2.528	1166	2.407
999	2.764	1055	2.646	1111	2.526	1167	2.405
1000	2.761	1056	2.644	1112	2.524	1168	2.403
1001	2.759	1057	2.642	1113	2.522	1169	2.400
1002	2.757	1058	2.640	1114	2.520	1170	2.398
1003	2.755	1059	2.637	1115	2.518	1171	2.396
1004	2.753	1060	2.635	1116	2.515	1172	2.394
1005	2.751	1061	2.633	1117	2.513	1173	2.392
1006	2.749	1062	2.631	1118	2.511	1174	2.389
1007	2.747	1063	2.629	1119	2.509	1175	2.387
1008	2.745	1064	2.627	1120	2.507	1176	2.385
1009	2.743	1065	2.625	1121	2.505	1177	2.383
1010	2.741	1066	2.623	1122	2.503	1178	2.381
1011	2.739	1067	2.620	1123	2.500	1179	2.379
1012	2.736	1068	2.618	1124	2.498	1180	2.376
1013	2.734	1069	2.616	1125	2.496	1181	2.374
1014	2.732	1070	2.614	1126	2.494	1182	2.372
1015	2.730	1071	2.612	1127	2.492	1183	2.370
1016	2.728	1072	2.610	1128	2.490	1184	2.368
1017	2.726	1073	2.608	1129	2.487	1185	2.365
1018	2.724	1074	2.606	1130	2.485	1186	2.363
1019	2.722	1075	2.603	1131	2.483	1187	2.361
1020	2.720	1076	2.601	1132	2.481	1188	2.359
1021	2.718	1077	2.599	1133	2.479	1189	2.357
1022	2.716	1078	2.597	1134	2.477	1190	2.354
1023	2.713	1079	2.595	1135	2.474	1191	2.352
1024	2.711	1080	2.593	1136	2.472	1192	2.350
1025	2.709	1081	2.591	1137	2.470	1193	2.348
1026	2.707	1082	2.588	1138	2.468	1194	2.346
1027	2.705	1083	2.586	1139	2.466	1195	2.343
1028	2.703	1084	2.584	1140	2.464	1196	2.341
1029	2.701	1085	2.582	1141	2.461	1197	2.339
1030	2.699	1086	2.580	1142	2.459	1198	2.337
1031	2.697	1087	2.578	1143	2.457	1199	2.335
1032	2.695	1088	2.576	1144	2.455	1200	2.332
1033	2.692	1089	2.574	1145	2.453	1201	2.330
1034	2.690	1090	2.571	1146	2.451	1202	2.328
1035	2.688	1091	2.569	1147	2.448	1203	2.326
1036	2.686	1092	2.567	1148	2.446	1204	2.324
1037	2.684	1093	2.565	1149	2.444	1205	2.321
1038	2.682	1094	2.563	1150	2.442	1206	2.319
1039	2.680	1095	2.561	1151	2.440	1207	2.317
1040	2.678	1096	2.559	1152	2.437	1208	2.315
1041	2.676	1097	2.556	1153	2.435	1209	2.313
1042	2.673	1098	2.554	1154	2.433	1210	2.310
1043	2.671	1099	2.552	1155	2.431	1211	2.308
1044	2.669	1100	2.550	1156	2.429	1212	2.306
1045	2.667	1101	2.548	1157	2.427	1213	2.304
1046	2.665	1102	2.546	1158	2.424	1214	2.302
1047	2.663	1103	2.543	1159	2.422	1215	2.299
1048	2.661	1104	2.541	1160	2.420	1216	2.297

Continues on next page...

Hydrograph Discharge Table

Time (min	Outflow cfs)	Time (min	Outflow cfs)	Time (min	Outflow cfs)	Time (min	Outflow cfs)
1217	2.295	1273	2.171	1329	2.046	1385	1.919
1218	2.293	1274	2.169	1330	2.043	1386	1.917
1219	2.291	1275	2.166	1331	2.041	1387	1.915
1220	2.288	1276	2.164	1332	2.039	1388	1.912
1221	2.286	1277	2.162	1333	2.037	1389	1.910
1222	2.284	1278	2.160	1334	2.034	1390	1.908
1223	2.282	1279	2.157	1335	2.032	1391	1.906
1224	2.280	1280	2.155	1336	2.030	1392	1.903
1225	2.277	1281	2.153	1337	2.028	1393	1.901
1226	2.275	1282	2.151	1338	2.025	1394	1.899
1227	2.273	1283	2.149	1339	2.023	1395	1.897
1228	2.271	1284	2.146	1340	2.021	1396	1.894
1229	2.269	1285	2.144	1341	2.019	1397	1.892
1230	2.266	1286	2.142	1342	2.016	1398	1.890
1231	2.264	1287	2.140	1343	2.014	1399	1.888
1232	2.262	1288	2.137	1344	2.012	1400	1.885
1233	2.260	1289	2.135	1345	2.010	1401	1.883
1234	2.257	1290	2.133	1346	2.007	1402	1.881
1235	2.255	1291	2.131	1347	2.005	1403	1.878
1236	2.253	1292	2.128	1348	2.003	1404	1.876
1237	2.251	1293	2.126	1349	2.001	1405	1.874
1238	2.249	1294	2.124	1350	1.998	1406	1.872
1239	2.246	1295	2.122	1351	1.996	1407	1.869
1240	2.244	1296	2.120	1352	1.994	1408	1.867
1241	2.242	1297	2.117	1353	1.992	1409	1.865
1242	2.240	1298	2.115	1354	1.989	1410	1.863
1243	2.238	1299	2.113	1355	1.987	1411	1.860
1244	2.235	1300	2.111	1356	1.985	1412	1.858
1245	2.233	1301	2.108	1357	1.982	1413	1.856
1246	2.231	1302	2.106	1358	1.980	1414	1.853
1247	2.229	1303	2.104	1359	1.978	1415	1.851
1248	2.226	1304	2.102	1360	1.976	1416	1.849
1249	2.224	1305	2.099	1361	1.973	1417	1.847
1250	2.222	1306	2.097	1362	1.971	1418	1.844
1251	2.220	1307	2.095	1363	1.969	1419	1.842
1252	2.218	1308	2.093	1364	1.967	1420	1.840
1253	2.215	1309	2.090	1365	1.964	1421	1.838
1254	2.213	1310	2.088	1366	1.962	1422	1.835
1255	2.211	1311	2.086	1367	1.960	1423	1.833
1256	2.209	1312	2.084	1368	1.958	1424	1.831
1257	2.206	1313	2.081	1369	1.955	1425	1.828
1258	2.204	1314	2.079	1370	1.953	1426	1.826
1259	2.202	1315	2.077	1371	1.951	1427	1.824
1260	2.200	1316	2.075	1372	1.949	1428	1.822
1261	2.198	1317	2.072	1373	1.946	1429	1.819
1262	2.195	1318	2.070	1374	1.944	1430	1.817
1263	2.193	1319	2.068	1375	1.942	1431	1.815
1264	2.191	1320	2.066	1376	1.940	1432	1.813
1265	2.189	1321	2.063	1377	1.937	1433	1.810
1266	2.186	1322	2.061	1378	1.935	1434	1.808
1267	2.184	1323	2.059	1379	1.933	1435	1.806
1268	2.182	1324	2.057	1380	1.931	1436	1.803
1269	2.180	1325	2.055	1381	1.928	1437	1.801
1270	2.178	1326	2.052	1382	1.926	1438	1.799
1271	2.175	1327	2.050	1383	1.924	1439	1.797
1272	2.173	1328	2.048	1384	1.921	1440	1.794

Continues on next page...

Developed site storm event

Hydrograph Discharge Table

Time -- (min	Outflow cfs)
1441	1.790
1442	1.783
1443	1.773
1444	1.761
1445	1.747
1446	1.730
1447	1.711
1448	1.689
1449	1.665
1450	1.639
1451	1.610
1452	1.579
1453	1.546
1454	1.510
1455	1.472
1456	1.431
1457	1.388
1458	1.343
1459	1.295
1460	1.245
1461	1.193
1462	1.142
1463	1.091
1464	1.042
1465	0.995
1466	0.948
1467	0.902
1468	0.858
1469	0.815
1470	0.773
1471	0.732
1472	0.692
1473	0.653
1474	0.616
1475	0.579
1476	0.544
1477	0.510
1478	0.476
1479	0.445
1480	0.414
1481	0.384
1482	0.355
1483	0.328
1484	0.302
1485	0.276
1486	0.252
1487	0.229
1488	0.207
1489	0.186
1490	0.167
1491	0.148

...End

Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Hyd. No. 2

Detention pond outflow

Hydrograph type	= Reservoir	Peak discharge	= 2.990 cfs
Storm frequency	= 10 yrs	Time to peak	= 884 min
Time interval	= 1 min	Hyd. volume	= 114,093 cuft
Inflow hyd. No.	= 1 - Developed site storm event	Reservoir name	= Detention Pond
Max. Elevation	= 62.87 ft	Max. Storage	= 152,824 cuft

Storage Indication method used.

Hydrograph Discharge Table

(Printed values >= 1.00% of Qp.)

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
725	3.422	62.70	0.046	-----	-----	-----	0.046	-----	-----	-----	-----	0.046
726	3.414	62.71	0.092	-----	-----	-----	0.092	-----	-----	-----	-----	0.092
727	3.405	62.71	0.138	-----	-----	-----	0.138	-----	-----	-----	-----	0.138
728	3.398	62.71	0.183	-----	-----	-----	0.182	-----	-----	-----	-----	0.182
729	3.390	62.72	0.227	-----	-----	-----	0.226	-----	-----	-----	-----	0.226
730	3.383	62.72	0.270	-----	-----	-----	0.270	-----	-----	-----	-----	0.270
731	3.376	62.72	0.313	-----	-----	-----	0.313	-----	-----	-----	-----	0.313
732	3.369	62.73	0.355	-----	-----	-----	0.355	-----	-----	-----	-----	0.355
733	3.363	62.73	0.397	-----	-----	-----	0.396	-----	-----	-----	-----	0.396
734	3.357	62.73	0.437	-----	-----	-----	0.437	-----	-----	-----	-----	0.437
735	3.352	62.74	0.478	-----	-----	-----	0.477	-----	-----	-----	-----	0.477
736	3.347	62.74	0.517	-----	-----	-----	0.516	-----	-----	-----	-----	0.516
737	3.342	62.74	0.556	-----	-----	-----	0.555	-----	-----	-----	-----	0.555
738	3.337	62.74	0.594	-----	-----	-----	0.593	-----	-----	-----	-----	0.593
739	3.333	62.75	0.632	-----	-----	-----	0.631	-----	-----	-----	-----	0.631
740	3.330	62.75	0.669	-----	-----	-----	0.668	-----	-----	-----	-----	0.668
741	3.326	62.75	0.706	-----	-----	-----	0.704	-----	-----	-----	-----	0.704
742	3.324	62.76	0.742	-----	-----	-----	0.740	-----	-----	-----	-----	0.740
743	3.321	62.76	0.777	-----	-----	-----	0.776	-----	-----	-----	-----	0.776
744	3.319	62.76	0.812	-----	-----	-----	0.811	-----	-----	-----	-----	0.811
745	3.317	62.76	0.847	-----	-----	-----	0.845	-----	-----	-----	-----	0.845
746	3.316	62.77	0.881	-----	-----	-----	0.879	-----	-----	-----	-----	0.879
747	3.315	62.77	0.914	-----	-----	-----	0.913	-----	-----	-----	-----	0.913
748	3.315	62.77	0.947	-----	-----	-----	0.946	-----	-----	-----	-----	0.946
749	3.315	62.77	0.980	-----	-----	-----	0.978	-----	-----	-----	-----	0.978
750	3.315	62.78	1.012	-----	-----	-----	1.010	-----	-----	-----	-----	1.010
751	3.315	62.78	1.044	-----	-----	-----	1.042	-----	-----	-----	-----	1.042
752	3.316	62.78	1.075	-----	-----	-----	1.073	-----	-----	-----	-----	1.073
753	3.317	62.78	1.106	-----	-----	-----	1.104	-----	-----	-----	-----	1.104
754	3.317	62.79	1.137	-----	-----	-----	1.134	-----	-----	-----	-----	1.134
755	3.318	62.79	1.167	-----	-----	-----	1.164	-----	-----	-----	-----	1.164
756	3.318	62.79	1.196	-----	-----	-----	1.194	-----	-----	-----	-----	1.194
757	3.319	62.79	1.225	-----	-----	-----	1.223	-----	-----	-----	-----	1.223
758	3.319	62.79	1.254	-----	-----	-----	1.252	-----	-----	-----	-----	1.252
759	3.319	62.80	1.283	-----	-----	-----	1.280	-----	-----	-----	-----	1.280
760	3.319	62.80	1.311	-----	-----	-----	1.308	-----	-----	-----	-----	1.308
761	3.319	62.80	1.349	-----	-----	-----	1.347	-----	-----	-----	-----	1.347
762	3.318	62.80	1.399	-----	-----	-----	1.396	-----	-----	-----	-----	1.396
763	3.318	62.81	1.447	-----	-----	-----	1.444	-----	-----	-----	-----	1.444
764	3.317	62.81	1.493	-----	-----	-----	1.491	-----	-----	-----	-----	1.491
765	3.315	62.81	1.539	-----	-----	-----	1.536	-----	-----	-----	-----	1.536
766	3.314	62.81	1.583	-----	-----	-----	1.581	-----	-----	-----	-----	1.581

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
767	3.312	62.81	1.626	-----	-----	-----	1.624	-----	-----	-----	-----	1.624
768	3.309	62.81	1.668	-----	-----	-----	1.666	-----	-----	-----	-----	1.666
769	3.306	62.82	1.710	-----	-----	-----	1.707	-----	-----	-----	-----	1.707
770	3.303	62.82	1.749	-----	-----	-----	1.747	-----	-----	-----	-----	1.747
771	3.299	62.82	1.788	-----	-----	-----	1.786	-----	-----	-----	-----	1.786
772	3.295	62.82	1.826	-----	-----	-----	1.823	-----	-----	-----	-----	1.823
773	3.291	62.82	1.862	-----	-----	-----	1.860	-----	-----	-----	-----	1.860
774	3.286	62.82	1.898	-----	-----	-----	1.896	-----	-----	-----	-----	1.896
775	3.282	62.83	1.933	-----	-----	-----	1.930	-----	-----	-----	-----	1.930
776	3.278	62.83	1.967	-----	-----	-----	1.964	-----	-----	-----	-----	1.964
777	3.274	62.83	1.999	-----	-----	-----	1.997	-----	-----	-----	-----	1.997
778	3.270	62.83	2.031	-----	-----	-----	2.029	-----	-----	-----	-----	2.029
779	3.266	62.83	2.062	-----	-----	-----	2.060	-----	-----	-----	-----	2.060
780	3.262	62.83	2.092	-----	-----	-----	2.090	-----	-----	-----	-----	2.090
781	3.258	62.83	2.121	-----	-----	-----	2.119	-----	-----	-----	-----	2.119
782	3.254	62.83	2.150	-----	-----	-----	2.147	-----	-----	-----	-----	2.147
783	3.251	62.84	2.177	-----	-----	-----	2.175	-----	-----	-----	-----	2.175
784	3.247	62.84	2.204	-----	-----	-----	2.202	-----	-----	-----	-----	2.202
785	3.244	62.84	2.230	-----	-----	-----	2.228	-----	-----	-----	-----	2.228
786	3.242	62.84	2.255	-----	-----	-----	2.253	-----	-----	-----	-----	2.253
787	3.239	62.84	2.280	-----	-----	-----	2.278	-----	-----	-----	-----	2.278
788	3.236	62.84	2.304	-----	-----	-----	2.302	-----	-----	-----	-----	2.302
789	3.234	62.84	2.327	-----	-----	-----	2.325	-----	-----	-----	-----	2.325
790	3.232	62.84	2.350	-----	-----	-----	2.348	-----	-----	-----	-----	2.348
791	3.230	62.84	2.372	-----	-----	-----	2.370	-----	-----	-----	-----	2.370
792	3.228	62.84	2.393	-----	-----	-----	2.391	-----	-----	-----	-----	2.391
793	3.227	62.85	2.414	-----	-----	-----	2.412	-----	-----	-----	-----	2.412
794	3.225	62.85	2.435	-----	-----	-----	2.432	-----	-----	-----	-----	2.432
795	3.224	62.85	2.454	-----	-----	-----	2.452	-----	-----	-----	-----	2.452
796	3.223	62.85	2.474	-----	-----	-----	2.471	-----	-----	-----	-----	2.471
797	3.222	62.85	2.492	-----	-----	-----	2.490	-----	-----	-----	-----	2.490
798	3.221	62.85	2.511	-----	-----	-----	2.508	-----	-----	-----	-----	2.508
799	3.220	62.85	2.528	-----	-----	-----	2.526	-----	-----	-----	-----	2.526
800	3.219	62.85	2.546	-----	-----	-----	2.544	-----	-----	-----	-----	2.544
801	3.218	62.85	2.563	-----	-----	-----	2.560	-----	-----	-----	-----	2.560
802	3.217	62.85	2.579	-----	-----	-----	2.577	-----	-----	-----	-----	2.577
803	3.216	62.85	2.595	-----	-----	-----	2.593	-----	-----	-----	-----	2.593
804	3.214	62.85	2.610	-----	-----	-----	2.608	-----	-----	-----	-----	2.608
805	3.212	62.85	2.626	-----	-----	-----	2.623	-----	-----	-----	-----	2.623
806	3.210	62.85	2.640	-----	-----	-----	2.638	-----	-----	-----	-----	2.638
807	3.208	62.85	2.654	-----	-----	-----	2.652	-----	-----	-----	-----	2.652
808	3.206	62.86	2.668	-----	-----	-----	2.666	-----	-----	-----	-----	2.666
809	3.203	62.86	2.682	-----	-----	-----	2.680	-----	-----	-----	-----	2.680
810	3.201	62.86	2.695	-----	-----	-----	2.693	-----	-----	-----	-----	2.693
811	3.198	62.86	2.707	-----	-----	-----	2.705	-----	-----	-----	-----	2.705
812	3.195	62.86	2.720	-----	-----	-----	2.718	-----	-----	-----	-----	2.718
813	3.192	62.86	2.732	-----	-----	-----	2.729	-----	-----	-----	-----	2.729
814	3.189	62.86	2.743	-----	-----	-----	2.741	-----	-----	-----	-----	2.741
815	3.186	62.86	2.754	-----	-----	-----	2.752	-----	-----	-----	-----	2.752
816	3.183	62.86	2.765	-----	-----	-----	2.763	-----	-----	-----	-----	2.763
817	3.180	62.86	2.775	-----	-----	-----	2.773	-----	-----	-----	-----	2.773
818	3.176	62.86	2.786	-----	-----	-----	2.783	-----	-----	-----	-----	2.783
819	3.173	62.86	2.795	-----	-----	-----	2.793	-----	-----	-----	-----	2.793
820	3.170	62.86	2.805	-----	-----	-----	2.803	-----	-----	-----	-----	2.803
821	3.166	62.86	2.814	-----	-----	-----	2.812	-----	-----	-----	-----	2.812
822	3.163	62.86	2.823	-----	-----	-----	2.821	-----	-----	-----	-----	2.821

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
823	3.159	62.86	2.831	-----	-----	-----	2.829	-----	-----	-----	-----	2.829
824	3.155	62.86	2.839	-----	-----	-----	2.837	-----	-----	-----	-----	2.837
825	3.151	62.86	2.847	-----	-----	-----	2.845	-----	-----	-----	-----	2.845
826	3.147	62.86	2.855	-----	-----	-----	2.853	-----	-----	-----	-----	2.853
827	3.143	62.86	2.862	-----	-----	-----	2.860	-----	-----	-----	-----	2.860
828	3.139	62.86	2.869	-----	-----	-----	2.867	-----	-----	-----	-----	2.867
829	3.135	62.86	2.876	-----	-----	-----	2.874	-----	-----	-----	-----	2.874
830	3.130	62.86	2.882	-----	-----	-----	2.880	-----	-----	-----	-----	2.880
831	3.126	62.86	2.888	-----	-----	-----	2.886	-----	-----	-----	-----	2.886
832	3.122	62.86	2.894	-----	-----	-----	2.892	-----	-----	-----	-----	2.892
833	3.117	62.87	2.900	-----	-----	-----	2.898	-----	-----	-----	-----	2.898
834	3.113	62.87	2.906	-----	-----	-----	2.903	-----	-----	-----	-----	2.903
835	3.109	62.87	2.911	-----	-----	-----	2.909	-----	-----	-----	-----	2.909
836	3.104	62.87	2.916	-----	-----	-----	2.914	-----	-----	-----	-----	2.914
837	3.100	62.87	2.920	-----	-----	-----	2.918	-----	-----	-----	-----	2.918
838	3.095	62.87	2.925	-----	-----	-----	2.923	-----	-----	-----	-----	2.923
839	3.091	62.87	2.929	-----	-----	-----	2.927	-----	-----	-----	-----	2.927
840	3.087	62.87	2.933	-----	-----	-----	2.931	-----	-----	-----	-----	2.931
841	3.082	62.87	2.937	-----	-----	-----	2.935	-----	-----	-----	-----	2.935
842	3.078	62.87	2.941	-----	-----	-----	2.939	-----	-----	-----	-----	2.939
843	3.074	62.87	2.944	-----	-----	-----	2.942	-----	-----	-----	-----	2.942
844	3.070	62.87	2.947	-----	-----	-----	2.945	-----	-----	-----	-----	2.945
845	3.066	62.87	2.950	-----	-----	-----	2.948	-----	-----	-----	-----	2.948
846	3.062	62.87	2.953	-----	-----	-----	2.951	-----	-----	-----	-----	2.951
847	3.058	62.87	2.956	-----	-----	-----	2.954	-----	-----	-----	-----	2.954
848	3.054	62.87	2.958	-----	-----	-----	2.956	-----	-----	-----	-----	2.956
849	3.051	62.87	2.961	-----	-----	-----	2.959	-----	-----	-----	-----	2.959
850	3.048	62.87	2.963	-----	-----	-----	2.961	-----	-----	-----	-----	2.961
851	3.044	62.87	2.965	-----	-----	-----	2.963	-----	-----	-----	-----	2.963
852	3.041	62.87	2.967	-----	-----	-----	2.965	-----	-----	-----	-----	2.965
853	3.039	62.87	2.969	-----	-----	-----	2.967	-----	-----	-----	-----	2.967
854	3.036	62.87	2.971	-----	-----	-----	2.969	-----	-----	-----	-----	2.969
855	3.034	62.87	2.972	-----	-----	-----	2.970	-----	-----	-----	-----	2.970
856	3.031	62.87	2.974	-----	-----	-----	2.972	-----	-----	-----	-----	2.972
857	3.029	62.87	2.976	-----	-----	-----	2.973	-----	-----	-----	-----	2.973
858	3.027	62.87	2.977	-----	-----	-----	2.975	-----	-----	-----	-----	2.975
859	3.025	62.87	2.978	-----	-----	-----	2.976	-----	-----	-----	-----	2.976
860	3.024	62.87	2.979	-----	-----	-----	2.977	-----	-----	-----	-----	2.977
861	3.022	62.87	2.980	-----	-----	-----	2.978	-----	-----	-----	-----	2.978
862	3.020	62.87	2.981	-----	-----	-----	2.979	-----	-----	-----	-----	2.980
863	3.019	62.87	2.983	-----	-----	-----	2.981	-----	-----	-----	-----	2.981
864	3.017	62.87	2.983	-----	-----	-----	2.981	-----	-----	-----	-----	2.981
865	3.016	62.87	2.984	-----	-----	-----	2.982	-----	-----	-----	-----	2.982
866	3.014	62.87	2.985	-----	-----	-----	2.983	-----	-----	-----	-----	2.983
867	3.013	62.87	2.986	-----	-----	-----	2.984	-----	-----	-----	-----	2.984
868	3.011	62.87	2.987	-----	-----	-----	2.985	-----	-----	-----	-----	2.985
869	3.010	62.87	2.987	-----	-----	-----	2.985	-----	-----	-----	-----	2.985
870	3.009	62.87	2.988	-----	-----	-----	2.986	-----	-----	-----	-----	2.986
871	3.007	62.87	2.988	-----	-----	-----	2.986	-----	-----	-----	-----	2.986
872	3.006	62.87	2.989	-----	-----	-----	2.987	-----	-----	-----	-----	2.987
873	3.005	62.87	2.989	-----	-----	-----	2.987	-----	-----	-----	-----	2.987
874	3.003	62.87	2.990	-----	-----	-----	2.988	-----	-----	-----	-----	2.988
875	3.002	62.87	2.990	-----	-----	-----	2.988	-----	-----	-----	-----	2.988
876	3.001	62.87	2.991	-----	-----	-----	2.989	-----	-----	-----	-----	2.989
877	2.999	62.87	2.991	-----	-----	-----	2.989	-----	-----	-----	-----	2.989
878	2.998	62.87	2.991	-----	-----	-----	2.989	-----	-----	-----	-----	2.989

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
879	2.997	62.87	2.991	-----	-----	-----	2.989	-----	-----	-----	-----	2.989
880	2.995	62.87	2.991	-----	-----	-----	2.989	-----	-----	-----	-----	2.989
881	2.994	62.87	2.992	-----	-----	-----	2.990	-----	-----	-----	-----	2.990
882	2.993	62.87	2.992	-----	-----	-----	2.990	-----	-----	-----	-----	2.990
883	2.991	62.87	2.992	-----	-----	-----	2.990	-----	-----	-----	-----	2.990
884	2.990	62.87 <<	2.992	-----	-----	-----	2.990	-----	-----	-----	-----	2.990 <<
885	2.988	62.87	2.992	-----	-----	-----	2.990	-----	-----	-----	-----	2.990
886	2.987	62.87	2.992	-----	-----	-----	2.990	-----	-----	-----	-----	2.990
887	2.986	62.87	2.992	-----	-----	-----	2.990	-----	-----	-----	-----	2.990
888	2.984	62.87	2.991	-----	-----	-----	2.989	-----	-----	-----	-----	2.989
889	2.983	62.87	2.991	-----	-----	-----	2.989	-----	-----	-----	-----	2.989
890	2.981	62.87	2.991	-----	-----	-----	2.989	-----	-----	-----	-----	2.989
891	2.980	62.87	2.991	-----	-----	-----	2.989	-----	-----	-----	-----	2.989
892	2.978	62.87	2.991	-----	-----	-----	2.989	-----	-----	-----	-----	2.989
893	2.976	62.87	2.990	-----	-----	-----	2.988	-----	-----	-----	-----	2.988
894	2.975	62.87	2.990	-----	-----	-----	2.988	-----	-----	-----	-----	2.988
895	2.973	62.87	2.990	-----	-----	-----	2.988	-----	-----	-----	-----	2.988
896	2.971	62.87	2.989	-----	-----	-----	2.987	-----	-----	-----	-----	2.987
897	2.970	62.87	2.989	-----	-----	-----	2.987	-----	-----	-----	-----	2.987
898	2.968	62.87	2.988	-----	-----	-----	2.986	-----	-----	-----	-----	2.986
899	2.966	62.87	2.988	-----	-----	-----	2.986	-----	-----	-----	-----	2.986
900	2.964	62.87	2.987	-----	-----	-----	2.985	-----	-----	-----	-----	2.985
901	2.962	62.87	2.987	-----	-----	-----	2.985	-----	-----	-----	-----	2.985
902	2.961	62.87	2.986	-----	-----	-----	2.984	-----	-----	-----	-----	2.984
903	2.959	62.87	2.986	-----	-----	-----	2.984	-----	-----	-----	-----	2.984
904	2.957	62.87	2.985	-----	-----	-----	2.983	-----	-----	-----	-----	2.983
905	2.955	62.87	2.984	-----	-----	-----	2.982	-----	-----	-----	-----	2.982
906	2.953	62.87	2.984	-----	-----	-----	2.982	-----	-----	-----	-----	2.982
907	2.951	62.87	2.983	-----	-----	-----	2.981	-----	-----	-----	-----	2.981
908	2.949	62.87	2.982	-----	-----	-----	2.980	-----	-----	-----	-----	2.980
909	2.947	62.87	2.981	-----	-----	-----	2.979	-----	-----	-----	-----	2.979
910	2.945	62.87	2.980	-----	-----	-----	2.978	-----	-----	-----	-----	2.978
911	2.943	62.87	2.980	-----	-----	-----	2.978	-----	-----	-----	-----	2.978
912	2.941	62.87	2.979	-----	-----	-----	2.977	-----	-----	-----	-----	2.977
913	2.939	62.87	2.978	-----	-----	-----	2.976	-----	-----	-----	-----	2.976
914	2.937	62.87	2.977	-----	-----	-----	2.975	-----	-----	-----	-----	2.975
915	2.935	62.87	2.976	-----	-----	-----	2.974	-----	-----	-----	-----	2.974
916	2.933	62.87	2.975	-----	-----	-----	2.973	-----	-----	-----	-----	2.973
917	2.931	62.87	2.974	-----	-----	-----	2.972	-----	-----	-----	-----	2.972
918	2.929	62.87	2.973	-----	-----	-----	2.971	-----	-----	-----	-----	2.971
919	2.927	62.87	2.972	-----	-----	-----	2.970	-----	-----	-----	-----	2.970
920	2.925	62.87	2.971	-----	-----	-----	2.969	-----	-----	-----	-----	2.969
921	2.923	62.87	2.970	-----	-----	-----	2.968	-----	-----	-----	-----	2.968
922	2.921	62.87	2.968	-----	-----	-----	2.966	-----	-----	-----	-----	2.966
923	2.919	62.87	2.967	-----	-----	-----	2.965	-----	-----	-----	-----	2.965
924	2.917	62.87	2.966	-----	-----	-----	2.964	-----	-----	-----	-----	2.964
925	2.915	62.87	2.965	-----	-----	-----	2.963	-----	-----	-----	-----	2.963
926	2.913	62.87	2.964	-----	-----	-----	2.962	-----	-----	-----	-----	2.962
927	2.911	62.87	2.962	-----	-----	-----	2.960	-----	-----	-----	-----	2.960
928	2.909	62.87	2.961	-----	-----	-----	2.959	-----	-----	-----	-----	2.959
929	2.907	62.87	2.960	-----	-----	-----	2.958	-----	-----	-----	-----	2.958
930	2.905	62.87	2.959	-----	-----	-----	2.957	-----	-----	-----	-----	2.957
931	2.903	62.87	2.957	-----	-----	-----	2.955	-----	-----	-----	-----	2.955
932	2.901	62.87	2.956	-----	-----	-----	2.954	-----	-----	-----	-----	2.954
933	2.899	62.87	2.955	-----	-----	-----	2.953	-----	-----	-----	-----	2.953
934	2.897	62.87	2.953	-----	-----	-----	2.951	-----	-----	-----	-----	2.951

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
935	2.895	62.87	2.952	-----	-----	-----	2.950	-----	-----	-----	-----	2.950
936	2.893	62.87	2.950	-----	-----	-----	2.948	-----	-----	-----	-----	2.948
937	2.891	62.87	2.949	-----	-----	-----	2.947	-----	-----	-----	-----	2.947
938	2.889	62.87	2.948	-----	-----	-----	2.946	-----	-----	-----	-----	2.946
939	2.887	62.87	2.946	-----	-----	-----	2.944	-----	-----	-----	-----	2.944
940	2.885	62.87	2.945	-----	-----	-----	2.943	-----	-----	-----	-----	2.943
941	2.883	62.87	2.943	-----	-----	-----	2.941	-----	-----	-----	-----	2.941
942	2.881	62.87	2.942	-----	-----	-----	2.940	-----	-----	-----	-----	2.940
943	2.879	62.87	2.940	-----	-----	-----	2.938	-----	-----	-----	-----	2.938
944	2.877	62.87	2.939	-----	-----	-----	2.937	-----	-----	-----	-----	2.937
945	2.874	62.87	2.937	-----	-----	-----	2.935	-----	-----	-----	-----	2.935
946	2.872	62.87	2.936	-----	-----	-----	2.934	-----	-----	-----	-----	2.934
947	2.870	62.87	2.934	-----	-----	-----	2.932	-----	-----	-----	-----	2.932
948	2.868	62.87	2.933	-----	-----	-----	2.931	-----	-----	-----	-----	2.931
949	2.866	62.87	2.931	-----	-----	-----	2.929	-----	-----	-----	-----	2.929
950	2.864	62.87	2.929	-----	-----	-----	2.927	-----	-----	-----	-----	2.927
951	2.862	62.87	2.928	-----	-----	-----	2.926	-----	-----	-----	-----	2.926
952	2.860	62.87	2.926	-----	-----	-----	2.924	-----	-----	-----	-----	2.924
953	2.858	62.87	2.925	-----	-----	-----	2.922	-----	-----	-----	-----	2.923
954	2.856	62.87	2.923	-----	-----	-----	2.921	-----	-----	-----	-----	2.921
955	2.854	62.87	2.921	-----	-----	-----	2.919	-----	-----	-----	-----	2.919
956	2.852	62.87	2.920	-----	-----	-----	2.918	-----	-----	-----	-----	2.918
957	2.850	62.87	2.918	-----	-----	-----	2.916	-----	-----	-----	-----	2.916
958	2.848	62.87	2.916	-----	-----	-----	2.914	-----	-----	-----	-----	2.914
959	2.846	62.87	2.915	-----	-----	-----	2.913	-----	-----	-----	-----	2.913
960	2.844	62.87	2.913	-----	-----	-----	2.911	-----	-----	-----	-----	2.911
961	2.842	62.87	2.911	-----	-----	-----	2.909	-----	-----	-----	-----	2.909
962	2.840	62.87	2.910	-----	-----	-----	2.908	-----	-----	-----	-----	2.907
963	2.838	62.87	2.908	-----	-----	-----	2.906	-----	-----	-----	-----	2.906
964	2.836	62.87	2.906	-----	-----	-----	2.904	-----	-----	-----	-----	2.904
965	2.834	62.87	2.904	-----	-----	-----	2.902	-----	-----	-----	-----	2.902
966	2.832	62.87	2.903	-----	-----	-----	2.901	-----	-----	-----	-----	2.901
967	2.830	62.87	2.901	-----	-----	-----	2.899	-----	-----	-----	-----	2.899
968	2.828	62.87	2.899	-----	-----	-----	2.897	-----	-----	-----	-----	2.897
969	2.825	62.87	2.897	-----	-----	-----	2.895	-----	-----	-----	-----	2.895
970	2.823	62.86	2.896	-----	-----	-----	2.894	-----	-----	-----	-----	2.894
971	2.821	62.86	2.894	-----	-----	-----	2.892	-----	-----	-----	-----	2.892
972	2.819	62.86	2.892	-----	-----	-----	2.890	-----	-----	-----	-----	2.890
973	2.817	62.86	2.890	-----	-----	-----	2.888	-----	-----	-----	-----	2.888
974	2.815	62.86	2.888	-----	-----	-----	2.886	-----	-----	-----	-----	2.886
975	2.813	62.86	2.887	-----	-----	-----	2.885	-----	-----	-----	-----	2.885
976	2.811	62.86	2.885	-----	-----	-----	2.883	-----	-----	-----	-----	2.883
977	2.809	62.86	2.883	-----	-----	-----	2.881	-----	-----	-----	-----	2.881
978	2.807	62.86	2.881	-----	-----	-----	2.879	-----	-----	-----	-----	2.879
979	2.805	62.86	2.879	-----	-----	-----	2.877	-----	-----	-----	-----	2.877
980	2.803	62.86	2.878	-----	-----	-----	2.876	-----	-----	-----	-----	2.875
981	2.801	62.86	2.876	-----	-----	-----	2.874	-----	-----	-----	-----	2.874
982	2.799	62.86	2.874	-----	-----	-----	2.872	-----	-----	-----	-----	2.872
983	2.797	62.86	2.872	-----	-----	-----	2.870	-----	-----	-----	-----	2.870
984	2.795	62.86	2.870	-----	-----	-----	2.868	-----	-----	-----	-----	2.868
985	2.793	62.86	2.868	-----	-----	-----	2.866	-----	-----	-----	-----	2.866
986	2.790	62.86	2.866	-----	-----	-----	2.864	-----	-----	-----	-----	2.864
987	2.788	62.86	2.865	-----	-----	-----	2.863	-----	-----	-----	-----	2.863
988	2.786	62.86	2.863	-----	-----	-----	2.861	-----	-----	-----	-----	2.861
989	2.784	62.86	2.861	-----	-----	-----	2.859	-----	-----	-----	-----	2.859
990	2.782	62.86	2.859	-----	-----	-----	2.857	-----	-----	-----	-----	2.857

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
991	2.780	62.86	2.857	-----	-----	-----	2.855	-----	-----	-----	-----	2.855
992	2.778	62.86	2.855	-----	-----	-----	2.853	-----	-----	-----	-----	2.853
993	2.776	62.86	2.853	-----	-----	-----	2.851	-----	-----	-----	-----	2.851
994	2.774	62.86	2.851	-----	-----	-----	2.849	-----	-----	-----	-----	2.849
995	2.772	62.86	2.849	-----	-----	-----	2.847	-----	-----	-----	-----	2.847
996	2.770	62.86	2.848	-----	-----	-----	2.845	-----	-----	-----	-----	2.845
997	2.768	62.86	2.846	-----	-----	-----	2.844	-----	-----	-----	-----	2.844
998	2.766	62.86	2.844	-----	-----	-----	2.842	-----	-----	-----	-----	2.842
999	2.764	62.86	2.842	-----	-----	-----	2.840	-----	-----	-----	-----	2.840
1000	2.761	62.86	2.840	-----	-----	-----	2.838	-----	-----	-----	-----	2.838
1001	2.759	62.86	2.838	-----	-----	-----	2.836	-----	-----	-----	-----	2.836
1002	2.757	62.86	2.836	-----	-----	-----	2.834	-----	-----	-----	-----	2.834
1003	2.755	62.86	2.834	-----	-----	-----	2.832	-----	-----	-----	-----	2.832
1004	2.753	62.86	2.832	-----	-----	-----	2.830	-----	-----	-----	-----	2.830
1005	2.751	62.86	2.830	-----	-----	-----	2.828	-----	-----	-----	-----	2.828
1006	2.749	62.86	2.828	-----	-----	-----	2.826	-----	-----	-----	-----	2.826
1007	2.747	62.86	2.826	-----	-----	-----	2.824	-----	-----	-----	-----	2.824
1008	2.745	62.86	2.824	-----	-----	-----	2.822	-----	-----	-----	-----	2.822
1009	2.743	62.86	2.822	-----	-----	-----	2.820	-----	-----	-----	-----	2.820
1010	2.741	62.86	2.820	-----	-----	-----	2.818	-----	-----	-----	-----	2.818
1011	2.739	62.86	2.818	-----	-----	-----	2.816	-----	-----	-----	-----	2.816
1012	2.736	62.86	2.816	-----	-----	-----	2.814	-----	-----	-----	-----	2.814
1013	2.734	62.86	2.814	-----	-----	-----	2.812	-----	-----	-----	-----	2.812
1014	2.732	62.86	2.812	-----	-----	-----	2.810	-----	-----	-----	-----	2.810
1015	2.730	62.86	2.811	-----	-----	-----	2.808	-----	-----	-----	-----	2.808
1016	2.728	62.86	2.809	-----	-----	-----	2.806	-----	-----	-----	-----	2.806
1017	2.726	62.86	2.807	-----	-----	-----	2.804	-----	-----	-----	-----	2.804
1018	2.724	62.86	2.805	-----	-----	-----	2.802	-----	-----	-----	-----	2.802
1019	2.722	62.86	2.803	-----	-----	-----	2.801	-----	-----	-----	-----	2.801
1020	2.720	62.86	2.801	-----	-----	-----	2.798	-----	-----	-----	-----	2.799
1021	2.718	62.86	2.799	-----	-----	-----	2.797	-----	-----	-----	-----	2.797
1022	2.716	62.86	2.797	-----	-----	-----	2.795	-----	-----	-----	-----	2.795
1023	2.713	62.86	2.795	-----	-----	-----	2.792	-----	-----	-----	-----	2.793
1024	2.711	62.86	2.793	-----	-----	-----	2.791	-----	-----	-----	-----	2.791
1025	2.709	62.86	2.791	-----	-----	-----	2.789	-----	-----	-----	-----	2.789
1026	2.707	62.86	2.789	-----	-----	-----	2.787	-----	-----	-----	-----	2.787
1027	2.705	62.86	2.787	-----	-----	-----	2.784	-----	-----	-----	-----	2.784
1028	2.703	62.86	2.785	-----	-----	-----	2.783	-----	-----	-----	-----	2.782
1029	2.701	62.86	2.783	-----	-----	-----	2.781	-----	-----	-----	-----	2.780
1030	2.699	62.86	2.781	-----	-----	-----	2.778	-----	-----	-----	-----	2.778
1031	2.697	62.86	2.779	-----	-----	-----	2.776	-----	-----	-----	-----	2.776
1032	2.695	62.86	2.777	-----	-----	-----	2.774	-----	-----	-----	-----	2.774
1033	2.692	62.86	2.774	-----	-----	-----	2.772	-----	-----	-----	-----	2.772
1034	2.690	62.86	2.772	-----	-----	-----	2.770	-----	-----	-----	-----	2.770
1035	2.688	62.86	2.770	-----	-----	-----	2.768	-----	-----	-----	-----	2.768
1036	2.686	62.86	2.768	-----	-----	-----	2.766	-----	-----	-----	-----	2.766
1037	2.684	62.86	2.766	-----	-----	-----	2.764	-----	-----	-----	-----	2.764
1038	2.682	62.86	2.764	-----	-----	-----	2.762	-----	-----	-----	-----	2.762
1039	2.680	62.86	2.762	-----	-----	-----	2.760	-----	-----	-----	-----	2.760
1040	2.678	62.86	2.760	-----	-----	-----	2.758	-----	-----	-----	-----	2.758
1041	2.676	62.86	2.758	-----	-----	-----	2.756	-----	-----	-----	-----	2.756
1042	2.673	62.86	2.756	-----	-----	-----	2.754	-----	-----	-----	-----	2.754
1043	2.671	62.86	2.754	-----	-----	-----	2.752	-----	-----	-----	-----	2.752
1044	2.669	62.86	2.752	-----	-----	-----	2.750	-----	-----	-----	-----	2.750
1045	2.667	62.86	2.750	-----	-----	-----	2.748	-----	-----	-----	-----	2.748
1046	2.665	62.86	2.748	-----	-----	-----	2.746	-----	-----	-----	-----	2.746

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1047	2.663	62.86	2.746	-----	-----	-----	2.744	-----	-----	-----	-----	2.744
1048	2.661	62.86	2.744	-----	-----	-----	2.742	-----	-----	-----	-----	2.742
1049	2.659	62.86	2.742	-----	-----	-----	2.740	-----	-----	-----	-----	2.740
1050	2.657	62.86	2.740	-----	-----	-----	2.738	-----	-----	-----	-----	2.738
1051	2.654	62.86	2.738	-----	-----	-----	2.736	-----	-----	-----	-----	2.736
1052	2.652	62.86	2.736	-----	-----	-----	2.734	-----	-----	-----	-----	2.734
1053	2.650	62.86	2.734	-----	-----	-----	2.732	-----	-----	-----	-----	2.732
1054	2.648	62.86	2.732	-----	-----	-----	2.729	-----	-----	-----	-----	2.730
1055	2.646	62.86	2.730	-----	-----	-----	2.727	-----	-----	-----	-----	2.727
1056	2.644	62.86	2.728	-----	-----	-----	2.725	-----	-----	-----	-----	2.725
1057	2.642	62.86	2.725	-----	-----	-----	2.723	-----	-----	-----	-----	2.723
1058	2.640	62.86	2.723	-----	-----	-----	2.721	-----	-----	-----	-----	2.721
1059	2.637	62.86	2.721	-----	-----	-----	2.719	-----	-----	-----	-----	2.719
1060	2.635	62.86	2.719	-----	-----	-----	2.717	-----	-----	-----	-----	2.717
1061	2.633	62.86	2.717	-----	-----	-----	2.715	-----	-----	-----	-----	2.715
1062	2.631	62.86	2.715	-----	-----	-----	2.713	-----	-----	-----	-----	2.713
1063	2.629	62.86	2.713	-----	-----	-----	2.711	-----	-----	-----	-----	2.711
1064	2.627	62.86	2.711	-----	-----	-----	2.709	-----	-----	-----	-----	2.709
1065	2.625	62.86	2.709	-----	-----	-----	2.707	-----	-----	-----	-----	2.707
1066	2.623	62.86	2.707	-----	-----	-----	2.705	-----	-----	-----	-----	2.705
1067	2.620	62.86	2.705	-----	-----	-----	2.703	-----	-----	-----	-----	2.703
1068	2.618	62.86	2.703	-----	-----	-----	2.701	-----	-----	-----	-----	2.701
1069	2.616	62.86	2.701	-----	-----	-----	2.698	-----	-----	-----	-----	2.698
1070	2.614	62.86	2.698	-----	-----	-----	2.696	-----	-----	-----	-----	2.696
1071	2.612	62.86	2.696	-----	-----	-----	2.694	-----	-----	-----	-----	2.694
1072	2.610	62.86	2.694	-----	-----	-----	2.692	-----	-----	-----	-----	2.692
1073	2.608	62.86	2.692	-----	-----	-----	2.690	-----	-----	-----	-----	2.690
1074	2.606	62.86	2.690	-----	-----	-----	2.688	-----	-----	-----	-----	2.688
1075	2.603	62.86	2.688	-----	-----	-----	2.686	-----	-----	-----	-----	2.686
1076	2.601	62.86	2.686	-----	-----	-----	2.684	-----	-----	-----	-----	2.684
1077	2.599	62.86	2.684	-----	-----	-----	2.682	-----	-----	-----	-----	2.682
1078	2.597	62.86	2.682	-----	-----	-----	2.680	-----	-----	-----	-----	2.680
1079	2.595	62.86	2.680	-----	-----	-----	2.678	-----	-----	-----	-----	2.678
1080	2.593	62.86	2.678	-----	-----	-----	2.676	-----	-----	-----	-----	2.676
1081	2.591	62.86	2.676	-----	-----	-----	2.673	-----	-----	-----	-----	2.673
1082	2.588	62.86	2.674	-----	-----	-----	2.671	-----	-----	-----	-----	2.671
1083	2.586	62.86	2.671	-----	-----	-----	2.669	-----	-----	-----	-----	2.669
1084	2.584	62.86	2.669	-----	-----	-----	2.667	-----	-----	-----	-----	2.667
1085	2.582	62.86	2.667	-----	-----	-----	2.665	-----	-----	-----	-----	2.665
1086	2.580	62.86	2.665	-----	-----	-----	2.663	-----	-----	-----	-----	2.663
1087	2.578	62.86	2.663	-----	-----	-----	2.661	-----	-----	-----	-----	2.661
1088	2.576	62.86	2.661	-----	-----	-----	2.659	-----	-----	-----	-----	2.659
1089	2.574	62.86	2.659	-----	-----	-----	2.657	-----	-----	-----	-----	2.657
1090	2.571	62.86	2.657	-----	-----	-----	2.655	-----	-----	-----	-----	2.655
1091	2.569	62.85	2.655	-----	-----	-----	2.652	-----	-----	-----	-----	2.652
1092	2.567	62.85	2.652	-----	-----	-----	2.650	-----	-----	-----	-----	2.650
1093	2.565	62.85	2.650	-----	-----	-----	2.648	-----	-----	-----	-----	2.648
1094	2.563	62.85	2.648	-----	-----	-----	2.646	-----	-----	-----	-----	2.646
1095	2.561	62.85	2.646	-----	-----	-----	2.644	-----	-----	-----	-----	2.644
1096	2.559	62.85	2.644	-----	-----	-----	2.642	-----	-----	-----	-----	2.642
1097	2.556	62.85	2.642	-----	-----	-----	2.640	-----	-----	-----	-----	2.640
1098	2.554	62.85	2.640	-----	-----	-----	2.638	-----	-----	-----	-----	2.638
1099	2.552	62.85	2.638	-----	-----	-----	2.636	-----	-----	-----	-----	2.636
1100	2.550	62.85	2.636	-----	-----	-----	2.633	-----	-----	-----	-----	2.633
1101	2.548	62.85	2.633	-----	-----	-----	2.631	-----	-----	-----	-----	2.631
1102	2.546	62.85	2.631	-----	-----	-----	2.629	-----	-----	-----	-----	2.629

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1103	2.543	62.85	2.629	-----	-----	-----	2.627	-----	-----	-----	-----	2.627
1104	2.541	62.85	2.627	-----	-----	-----	2.625	-----	-----	-----	-----	2.625
1105	2.539	62.85	2.625	-----	-----	-----	2.623	-----	-----	-----	-----	2.623
1106	2.537	62.85	2.623	-----	-----	-----	2.621	-----	-----	-----	-----	2.621
1107	2.535	62.85	2.621	-----	-----	-----	2.619	-----	-----	-----	-----	2.619
1108	2.533	62.85	2.619	-----	-----	-----	2.617	-----	-----	-----	-----	2.617
1109	2.531	62.85	2.617	-----	-----	-----	2.614	-----	-----	-----	-----	2.614
1110	2.528	62.85	2.614	-----	-----	-----	2.612	-----	-----	-----	-----	2.612
1111	2.526	62.85	2.612	-----	-----	-----	2.610	-----	-----	-----	-----	2.610
1112	2.524	62.85	2.610	-----	-----	-----	2.608	-----	-----	-----	-----	2.608
1113	2.522	62.85	2.608	-----	-----	-----	2.606	-----	-----	-----	-----	2.606
1114	2.520	62.85	2.606	-----	-----	-----	2.604	-----	-----	-----	-----	2.604
1115	2.518	62.85	2.604	-----	-----	-----	2.602	-----	-----	-----	-----	2.602
1116	2.515	62.85	2.602	-----	-----	-----	2.600	-----	-----	-----	-----	2.600
1117	2.513	62.85	2.600	-----	-----	-----	2.597	-----	-----	-----	-----	2.597
1118	2.511	62.85	2.598	-----	-----	-----	2.595	-----	-----	-----	-----	2.595
1119	2.509	62.85	2.595	-----	-----	-----	2.593	-----	-----	-----	-----	2.593
1120	2.507	62.85	2.593	-----	-----	-----	2.591	-----	-----	-----	-----	2.591
1121	2.505	62.85	2.591	-----	-----	-----	2.589	-----	-----	-----	-----	2.589
1122	2.503	62.85	2.589	-----	-----	-----	2.587	-----	-----	-----	-----	2.587
1123	2.500	62.85	2.587	-----	-----	-----	2.585	-----	-----	-----	-----	2.585
1124	2.498	62.85	2.585	-----	-----	-----	2.583	-----	-----	-----	-----	2.583
1125	2.496	62.85	2.583	-----	-----	-----	2.580	-----	-----	-----	-----	2.580
1126	2.494	62.85	2.580	-----	-----	-----	2.578	-----	-----	-----	-----	2.578
1127	2.492	62.85	2.578	-----	-----	-----	2.576	-----	-----	-----	-----	2.576
1128	2.490	62.85	2.576	-----	-----	-----	2.574	-----	-----	-----	-----	2.574
1129	2.487	62.85	2.574	-----	-----	-----	2.572	-----	-----	-----	-----	2.572
1130	2.485	62.85	2.572	-----	-----	-----	2.570	-----	-----	-----	-----	2.570
1131	2.483	62.85	2.570	-----	-----	-----	2.568	-----	-----	-----	-----	2.568
1132	2.481	62.85	2.568	-----	-----	-----	2.565	-----	-----	-----	-----	2.565
1133	2.479	62.85	2.566	-----	-----	-----	2.563	-----	-----	-----	-----	2.563
1134	2.477	62.85	2.563	-----	-----	-----	2.561	-----	-----	-----	-----	2.561
1135	2.474	62.85	2.561	-----	-----	-----	2.559	-----	-----	-----	-----	2.559
1136	2.472	62.85	2.559	-----	-----	-----	2.557	-----	-----	-----	-----	2.557
1137	2.470	62.85	2.557	-----	-----	-----	2.555	-----	-----	-----	-----	2.555
1138	2.468	62.85	2.555	-----	-----	-----	2.553	-----	-----	-----	-----	2.553
1139	2.466	62.85	2.553	-----	-----	-----	2.551	-----	-----	-----	-----	2.551
1140	2.464	62.85	2.550	-----	-----	-----	2.548	-----	-----	-----	-----	2.548
1141	2.461	62.85	2.548	-----	-----	-----	2.546	-----	-----	-----	-----	2.546
1142	2.459	62.85	2.546	-----	-----	-----	2.544	-----	-----	-----	-----	2.544
1143	2.457	62.85	2.544	-----	-----	-----	2.542	-----	-----	-----	-----	2.542
1144	2.455	62.85	2.542	-----	-----	-----	2.540	-----	-----	-----	-----	2.540
1145	2.453	62.85	2.540	-----	-----	-----	2.538	-----	-----	-----	-----	2.538
1146	2.451	62.85	2.538	-----	-----	-----	2.535	-----	-----	-----	-----	2.535
1147	2.448	62.85	2.536	-----	-----	-----	2.533	-----	-----	-----	-----	2.533
1148	2.446	62.85	2.533	-----	-----	-----	2.531	-----	-----	-----	-----	2.531
1149	2.444	62.85	2.531	-----	-----	-----	2.529	-----	-----	-----	-----	2.529
1150	2.442	62.85	2.529	-----	-----	-----	2.527	-----	-----	-----	-----	2.527
1151	2.440	62.85	2.527	-----	-----	-----	2.525	-----	-----	-----	-----	2.525
1152	2.437	62.85	2.525	-----	-----	-----	2.523	-----	-----	-----	-----	2.523
1153	2.435	62.85	2.523	-----	-----	-----	2.520	-----	-----	-----	-----	2.520
1154	2.433	62.85	2.520	-----	-----	-----	2.518	-----	-----	-----	-----	2.518
1155	2.431	62.85	2.518	-----	-----	-----	2.516	-----	-----	-----	-----	2.516
1156	2.429	62.85	2.516	-----	-----	-----	2.514	-----	-----	-----	-----	2.514
1157	2.427	62.85	2.514	-----	-----	-----	2.512	-----	-----	-----	-----	2.512
1158	2.424	62.85	2.512	-----	-----	-----	2.510	-----	-----	-----	-----	2.510

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1159	2.422	62.85	2.510	-----	-----	-----	2.508	-----	-----	-----	-----	2.508
1160	2.420	62.85	2.508	-----	-----	-----	2.505	-----	-----	-----	-----	2.505
1161	2.418	62.85	2.505	-----	-----	-----	2.503	-----	-----	-----	-----	2.503
1162	2.416	62.85	2.503	-----	-----	-----	2.501	-----	-----	-----	-----	2.501
1163	2.414	62.85	2.501	-----	-----	-----	2.499	-----	-----	-----	-----	2.499
1164	2.411	62.85	2.499	-----	-----	-----	2.497	-----	-----	-----	-----	2.497
1165	2.409	62.85	2.497	-----	-----	-----	2.495	-----	-----	-----	-----	2.495
1166	2.407	62.85	2.495	-----	-----	-----	2.492	-----	-----	-----	-----	2.492
1167	2.405	62.85	2.492	-----	-----	-----	2.490	-----	-----	-----	-----	2.490
1168	2.403	62.85	2.490	-----	-----	-----	2.488	-----	-----	-----	-----	2.488
1169	2.400	62.85	2.488	-----	-----	-----	2.486	-----	-----	-----	-----	2.486
1170	2.398	62.85	2.486	-----	-----	-----	2.484	-----	-----	-----	-----	2.484
1171	2.396	62.85	2.484	-----	-----	-----	2.482	-----	-----	-----	-----	2.482
1172	2.394	62.85	2.482	-----	-----	-----	2.479	-----	-----	-----	-----	2.479
1173	2.392	62.85	2.479	-----	-----	-----	2.477	-----	-----	-----	-----	2.477
1174	2.389	62.85	2.477	-----	-----	-----	2.475	-----	-----	-----	-----	2.475
1175	2.387	62.85	2.475	-----	-----	-----	2.473	-----	-----	-----	-----	2.473
1176	2.385	62.85	2.473	-----	-----	-----	2.471	-----	-----	-----	-----	2.471
1177	2.383	62.85	2.471	-----	-----	-----	2.469	-----	-----	-----	-----	2.469
1178	2.381	62.85	2.469	-----	-----	-----	2.466	-----	-----	-----	-----	2.466
1179	2.379	62.85	2.466	-----	-----	-----	2.464	-----	-----	-----	-----	2.464
1180	2.376	62.85	2.464	-----	-----	-----	2.462	-----	-----	-----	-----	2.462
1181	2.374	62.85	2.462	-----	-----	-----	2.460	-----	-----	-----	-----	2.460
1182	2.372	62.85	2.460	-----	-----	-----	2.458	-----	-----	-----	-----	2.458
1183	2.370	62.85	2.458	-----	-----	-----	2.456	-----	-----	-----	-----	2.456
1184	2.368	62.85	2.456	-----	-----	-----	2.453	-----	-----	-----	-----	2.453
1185	2.365	62.85	2.453	-----	-----	-----	2.451	-----	-----	-----	-----	2.451
1186	2.363	62.85	2.451	-----	-----	-----	2.449	-----	-----	-----	-----	2.449
1187	2.361	62.85	2.449	-----	-----	-----	2.447	-----	-----	-----	-----	2.447
1188	2.359	62.85	2.447	-----	-----	-----	2.445	-----	-----	-----	-----	2.445
1189	2.357	62.85	2.445	-----	-----	-----	2.443	-----	-----	-----	-----	2.443
1190	2.354	62.85	2.443	-----	-----	-----	2.440	-----	-----	-----	-----	2.440
1191	2.352	62.85	2.440	-----	-----	-----	2.438	-----	-----	-----	-----	2.438
1192	2.350	62.85	2.438	-----	-----	-----	2.436	-----	-----	-----	-----	2.436
1193	2.348	62.85	2.436	-----	-----	-----	2.434	-----	-----	-----	-----	2.434
1194	2.346	62.85	2.434	-----	-----	-----	2.432	-----	-----	-----	-----	2.432
1195	2.343	62.85	2.432	-----	-----	-----	2.430	-----	-----	-----	-----	2.430
1196	2.341	62.85	2.430	-----	-----	-----	2.427	-----	-----	-----	-----	2.427
1197	2.339	62.85	2.427	-----	-----	-----	2.425	-----	-----	-----	-----	2.425
1198	2.337	62.85	2.425	-----	-----	-----	2.423	-----	-----	-----	-----	2.423
1199	2.335	62.85	2.423	-----	-----	-----	2.421	-----	-----	-----	-----	2.421
1200	2.332	62.85	2.421	-----	-----	-----	2.419	-----	-----	-----	-----	2.419
1201	2.330	62.85	2.419	-----	-----	-----	2.416	-----	-----	-----	-----	2.416
1202	2.328	62.85	2.417	-----	-----	-----	2.414	-----	-----	-----	-----	2.414
1203	2.326	62.85	2.414	-----	-----	-----	2.412	-----	-----	-----	-----	2.412
1204	2.324	62.84	2.412	-----	-----	-----	2.410	-----	-----	-----	-----	2.410
1205	2.321	62.84	2.410	-----	-----	-----	2.408	-----	-----	-----	-----	2.408
1206	2.319	62.84	2.408	-----	-----	-----	2.406	-----	-----	-----	-----	2.406
1207	2.317	62.84	2.406	-----	-----	-----	2.403	-----	-----	-----	-----	2.403
1208	2.315	62.84	2.403	-----	-----	-----	2.401	-----	-----	-----	-----	2.401
1209	2.313	62.84	2.401	-----	-----	-----	2.399	-----	-----	-----	-----	2.399
1210	2.310	62.84	2.399	-----	-----	-----	2.397	-----	-----	-----	-----	2.397
1211	2.308	62.84	2.397	-----	-----	-----	2.395	-----	-----	-----	-----	2.395
1212	2.306	62.84	2.395	-----	-----	-----	2.392	-----	-----	-----	-----	2.392
1213	2.304	62.84	2.393	-----	-----	-----	2.390	-----	-----	-----	-----	2.390
1214	2.302	62.84	2.390	-----	-----	-----	2.388	-----	-----	-----	-----	2.388

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1215	2.299	62.84	2.388	-----	-----	-----	2.386	-----	-----	-----	-----	2.386
1216	2.297	62.84	2.386	-----	-----	-----	2.384	-----	-----	-----	-----	2.384
1217	2.295	62.84	2.384	-----	-----	-----	2.382	-----	-----	-----	-----	2.382
1218	2.293	62.84	2.382	-----	-----	-----	2.379	-----	-----	-----	-----	2.379
1219	2.291	62.84	2.379	-----	-----	-----	2.377	-----	-----	-----	-----	2.377
1220	2.288	62.84	2.377	-----	-----	-----	2.375	-----	-----	-----	-----	2.375
1221	2.286	62.84	2.375	-----	-----	-----	2.373	-----	-----	-----	-----	2.373
1222	2.284	62.84	2.373	-----	-----	-----	2.371	-----	-----	-----	-----	2.371
1223	2.282	62.84	2.371	-----	-----	-----	2.368	-----	-----	-----	-----	2.368
1224	2.280	62.84	2.368	-----	-----	-----	2.366	-----	-----	-----	-----	2.366
1225	2.277	62.84	2.366	-----	-----	-----	2.364	-----	-----	-----	-----	2.364
1226	2.275	62.84	2.364	-----	-----	-----	2.362	-----	-----	-----	-----	2.362
1227	2.273	62.84	2.362	-----	-----	-----	2.360	-----	-----	-----	-----	2.360
1228	2.271	62.84	2.360	-----	-----	-----	2.357	-----	-----	-----	-----	2.357
1229	2.269	62.84	2.357	-----	-----	-----	2.355	-----	-----	-----	-----	2.355
1230	2.266	62.84	2.355	-----	-----	-----	2.353	-----	-----	-----	-----	2.353
1231	2.264	62.84	2.353	-----	-----	-----	2.351	-----	-----	-----	-----	2.351
1232	2.262	62.84	2.351	-----	-----	-----	2.349	-----	-----	-----	-----	2.349
1233	2.260	62.84	2.349	-----	-----	-----	2.346	-----	-----	-----	-----	2.346
1234	2.257	62.84	2.347	-----	-----	-----	2.344	-----	-----	-----	-----	2.344
1235	2.255	62.84	2.344	-----	-----	-----	2.342	-----	-----	-----	-----	2.342
1236	2.253	62.84	2.342	-----	-----	-----	2.340	-----	-----	-----	-----	2.340
1237	2.251	62.84	2.340	-----	-----	-----	2.338	-----	-----	-----	-----	2.338
1238	2.249	62.84	2.338	-----	-----	-----	2.336	-----	-----	-----	-----	2.335
1239	2.246	62.84	2.336	-----	-----	-----	2.333	-----	-----	-----	-----	2.333
1240	2.244	62.84	2.333	-----	-----	-----	2.331	-----	-----	-----	-----	2.331
1241	2.242	62.84	2.331	-----	-----	-----	2.329	-----	-----	-----	-----	2.329
1242	2.240	62.84	2.329	-----	-----	-----	2.327	-----	-----	-----	-----	2.327
1243	2.238	62.84	2.327	-----	-----	-----	2.325	-----	-----	-----	-----	2.325
1244	2.235	62.84	2.325	-----	-----	-----	2.322	-----	-----	-----	-----	2.322
1245	2.233	62.84	2.322	-----	-----	-----	2.320	-----	-----	-----	-----	2.320
1246	2.231	62.84	2.320	-----	-----	-----	2.318	-----	-----	-----	-----	2.318
1247	2.229	62.84	2.318	-----	-----	-----	2.316	-----	-----	-----	-----	2.316
1248	2.226	62.84	2.316	-----	-----	-----	2.314	-----	-----	-----	-----	2.314
1249	2.224	62.84	2.314	-----	-----	-----	2.311	-----	-----	-----	-----	2.311
1250	2.222	62.84	2.311	-----	-----	-----	2.309	-----	-----	-----	-----	2.309
1251	2.220	62.84	2.309	-----	-----	-----	2.307	-----	-----	-----	-----	2.307
1252	2.218	62.84	2.307	-----	-----	-----	2.305	-----	-----	-----	-----	2.305
1253	2.215	62.84	2.305	-----	-----	-----	2.302	-----	-----	-----	-----	2.303
1254	2.213	62.84	2.303	-----	-----	-----	2.300	-----	-----	-----	-----	2.300
1255	2.211	62.84	2.300	-----	-----	-----	2.298	-----	-----	-----	-----	2.298
1256	2.209	62.84	2.298	-----	-----	-----	2.296	-----	-----	-----	-----	2.296
1257	2.206	62.84	2.296	-----	-----	-----	2.294	-----	-----	-----	-----	2.294
1258	2.204	62.84	2.294	-----	-----	-----	2.292	-----	-----	-----	-----	2.291
1259	2.202	62.84	2.292	-----	-----	-----	2.289	-----	-----	-----	-----	2.289
1260	2.200	62.84	2.289	-----	-----	-----	2.287	-----	-----	-----	-----	2.287
1261	2.198	62.84	2.287	-----	-----	-----	2.285	-----	-----	-----	-----	2.285
1262	2.195	62.84	2.285	-----	-----	-----	2.283	-----	-----	-----	-----	2.283
1263	2.193	62.84	2.283	-----	-----	-----	2.280	-----	-----	-----	-----	2.280
1264	2.191	62.84	2.280	-----	-----	-----	2.278	-----	-----	-----	-----	2.278
1265	2.189	62.84	2.278	-----	-----	-----	2.276	-----	-----	-----	-----	2.276
1266	2.186	62.84	2.276	-----	-----	-----	2.274	-----	-----	-----	-----	2.274
1267	2.184	62.84	2.274	-----	-----	-----	2.272	-----	-----	-----	-----	2.272
1268	2.182	62.84	2.272	-----	-----	-----	2.269	-----	-----	-----	-----	2.269
1269	2.180	62.84	2.269	-----	-----	-----	2.267	-----	-----	-----	-----	2.267
1270	2.178	62.84	2.267	-----	-----	-----	2.265	-----	-----	-----	-----	2.265

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1271	2.175	62.84	2.265	-----	-----	-----	2.263	-----	-----	-----	-----	2.263
1272	2.173	62.84	2.263	-----	-----	-----	2.261	-----	-----	-----	-----	2.261
1273	2.171	62.84	2.261	-----	-----	-----	2.258	-----	-----	-----	-----	2.258
1274	2.169	62.84	2.258	-----	-----	-----	2.256	-----	-----	-----	-----	2.256
1275	2.166	62.84	2.256	-----	-----	-----	2.254	-----	-----	-----	-----	2.254
1276	2.164	62.84	2.254	-----	-----	-----	2.252	-----	-----	-----	-----	2.252
1277	2.162	62.84	2.252	-----	-----	-----	2.250	-----	-----	-----	-----	2.249
1278	2.160	62.84	2.250	-----	-----	-----	2.247	-----	-----	-----	-----	2.247
1279	2.157	62.84	2.247	-----	-----	-----	2.245	-----	-----	-----	-----	2.245
1280	2.155	62.84	2.245	-----	-----	-----	2.243	-----	-----	-----	-----	2.243
1281	2.153	62.84	2.243	-----	-----	-----	2.241	-----	-----	-----	-----	2.241
1282	2.151	62.84	2.241	-----	-----	-----	2.238	-----	-----	-----	-----	2.238
1283	2.149	62.84	2.238	-----	-----	-----	2.236	-----	-----	-----	-----	2.236
1284	2.146	62.84	2.236	-----	-----	-----	2.234	-----	-----	-----	-----	2.234
1285	2.144	62.84	2.234	-----	-----	-----	2.232	-----	-----	-----	-----	2.232
1286	2.142	62.84	2.232	-----	-----	-----	2.230	-----	-----	-----	-----	2.230
1287	2.140	62.84	2.230	-----	-----	-----	2.227	-----	-----	-----	-----	2.227
1288	2.137	62.84	2.227	-----	-----	-----	2.225	-----	-----	-----	-----	2.225
1289	2.135	62.84	2.225	-----	-----	-----	2.223	-----	-----	-----	-----	2.223
1290	2.133	62.84	2.223	-----	-----	-----	2.221	-----	-----	-----	-----	2.221
1291	2.131	62.84	2.221	-----	-----	-----	2.218	-----	-----	-----	-----	2.218
1292	2.128	62.84	2.219	-----	-----	-----	2.216	-----	-----	-----	-----	2.216
1293	2.126	62.84	2.216	-----	-----	-----	2.214	-----	-----	-----	-----	2.214
1294	2.124	62.84	2.214	-----	-----	-----	2.212	-----	-----	-----	-----	2.212
1295	2.122	62.84	2.212	-----	-----	-----	2.210	-----	-----	-----	-----	2.210
1296	2.120	62.84	2.210	-----	-----	-----	2.207	-----	-----	-----	-----	2.207
1297	2.117	62.84	2.207	-----	-----	-----	2.205	-----	-----	-----	-----	2.205
1298	2.115	62.84	2.205	-----	-----	-----	2.203	-----	-----	-----	-----	2.203
1299	2.113	62.84	2.203	-----	-----	-----	2.201	-----	-----	-----	-----	2.201
1300	2.111	62.84	2.201	-----	-----	-----	2.199	-----	-----	-----	-----	2.198
1301	2.108	62.84	2.199	-----	-----	-----	2.196	-----	-----	-----	-----	2.196
1302	2.106	62.84	2.196	-----	-----	-----	2.194	-----	-----	-----	-----	2.194
1303	2.104	62.84	2.194	-----	-----	-----	2.192	-----	-----	-----	-----	2.192
1304	2.102	62.84	2.192	-----	-----	-----	2.190	-----	-----	-----	-----	2.190
1305	2.099	62.84	2.190	-----	-----	-----	2.187	-----	-----	-----	-----	2.187
1306	2.097	62.84	2.187	-----	-----	-----	2.185	-----	-----	-----	-----	2.185
1307	2.095	62.84	2.185	-----	-----	-----	2.183	-----	-----	-----	-----	2.183
1308	2.093	62.84	2.183	-----	-----	-----	2.181	-----	-----	-----	-----	2.181
1309	2.090	62.84	2.181	-----	-----	-----	2.178	-----	-----	-----	-----	2.178
1310	2.088	62.84	2.178	-----	-----	-----	2.176	-----	-----	-----	-----	2.176
1311	2.086	62.84	2.176	-----	-----	-----	2.174	-----	-----	-----	-----	2.174
1312	2.084	62.84	2.174	-----	-----	-----	2.172	-----	-----	-----	-----	2.172
1313	2.081	62.84	2.172	-----	-----	-----	2.170	-----	-----	-----	-----	2.170
1314	2.079	62.83	2.170	-----	-----	-----	2.167	-----	-----	-----	-----	2.167
1315	2.077	62.83	2.167	-----	-----	-----	2.165	-----	-----	-----	-----	2.165
1316	2.075	62.83	2.165	-----	-----	-----	2.163	-----	-----	-----	-----	2.163
1317	2.072	62.83	2.163	-----	-----	-----	2.161	-----	-----	-----	-----	2.161
1318	2.070	62.83	2.161	-----	-----	-----	2.158	-----	-----	-----	-----	2.158
1319	2.068	62.83	2.158	-----	-----	-----	2.156	-----	-----	-----	-----	2.156
1320	2.066	62.83	2.156	-----	-----	-----	2.154	-----	-----	-----	-----	2.154
1321	2.063	62.83	2.154	-----	-----	-----	2.152	-----	-----	-----	-----	2.152
1322	2.061	62.83	2.152	-----	-----	-----	2.149	-----	-----	-----	-----	2.149
1323	2.059	62.83	2.150	-----	-----	-----	2.147	-----	-----	-----	-----	2.147
1324	2.057	62.83	2.147	-----	-----	-----	2.145	-----	-----	-----	-----	2.145
1325	2.055	62.83	2.145	-----	-----	-----	2.143	-----	-----	-----	-----	2.143
1326	2.052	62.83	2.143	-----	-----	-----	2.141	-----	-----	-----	-----	2.141

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1327	2.050	62.83	2.141	-----	-----	-----	2.138	-----	-----	-----	-----	2.138
1328	2.048	62.83	2.138	-----	-----	-----	2.136	-----	-----	-----	-----	2.136
1329	2.046	62.83	2.136	-----	-----	-----	2.134	-----	-----	-----	-----	2.134
1330	2.043	62.83	2.134	-----	-----	-----	2.132	-----	-----	-----	-----	2.132
1331	2.041	62.83	2.132	-----	-----	-----	2.129	-----	-----	-----	-----	2.129
1332	2.039	62.83	2.129	-----	-----	-----	2.127	-----	-----	-----	-----	2.127
1333	2.037	62.83	2.127	-----	-----	-----	2.125	-----	-----	-----	-----	2.125
1334	2.034	62.83	2.125	-----	-----	-----	2.123	-----	-----	-----	-----	2.123
1335	2.032	62.83	2.123	-----	-----	-----	2.120	-----	-----	-----	-----	2.120
1336	2.030	62.83	2.121	-----	-----	-----	2.118	-----	-----	-----	-----	2.118
1337	2.028	62.83	2.118	-----	-----	-----	2.116	-----	-----	-----	-----	2.116
1338	2.025	62.83	2.116	-----	-----	-----	2.114	-----	-----	-----	-----	2.114
1339	2.023	62.83	2.114	-----	-----	-----	2.112	-----	-----	-----	-----	2.112
1340	2.021	62.83	2.112	-----	-----	-----	2.109	-----	-----	-----	-----	2.109
1341	2.019	62.83	2.109	-----	-----	-----	2.107	-----	-----	-----	-----	2.107
1342	2.016	62.83	2.107	-----	-----	-----	2.105	-----	-----	-----	-----	2.105
1343	2.014	62.83	2.105	-----	-----	-----	2.103	-----	-----	-----	-----	2.103
1344	2.012	62.83	2.103	-----	-----	-----	2.100	-----	-----	-----	-----	2.100
1345	2.010	62.83	2.100	-----	-----	-----	2.098	-----	-----	-----	-----	2.098
1346	2.007	62.83	2.098	-----	-----	-----	2.096	-----	-----	-----	-----	2.096
1347	2.005	62.83	2.096	-----	-----	-----	2.094	-----	-----	-----	-----	2.094
1348	2.003	62.83	2.094	-----	-----	-----	2.091	-----	-----	-----	-----	2.091
1349	2.001	62.83	2.091	-----	-----	-----	2.089	-----	-----	-----	-----	2.089
1350	1.998	62.83	2.089	-----	-----	-----	2.087	-----	-----	-----	-----	2.087
1351	1.996	62.83	2.087	-----	-----	-----	2.085	-----	-----	-----	-----	2.085
1352	1.994	62.83	2.085	-----	-----	-----	2.082	-----	-----	-----	-----	2.082
1353	1.992	62.83	2.083	-----	-----	-----	2.080	-----	-----	-----	-----	2.080
1354	1.989	62.83	2.080	-----	-----	-----	2.078	-----	-----	-----	-----	2.078
1355	1.987	62.83	2.078	-----	-----	-----	2.076	-----	-----	-----	-----	2.076
1356	1.985	62.83	2.076	-----	-----	-----	2.073	-----	-----	-----	-----	2.073
1357	1.982	62.83	2.074	-----	-----	-----	2.071	-----	-----	-----	-----	2.071
1358	1.980	62.83	2.071	-----	-----	-----	2.069	-----	-----	-----	-----	2.069
1359	1.978	62.83	2.069	-----	-----	-----	2.067	-----	-----	-----	-----	2.067
1360	1.976	62.83	2.067	-----	-----	-----	2.064	-----	-----	-----	-----	2.064
1361	1.973	62.83	2.065	-----	-----	-----	2.062	-----	-----	-----	-----	2.062
1362	1.971	62.83	2.062	-----	-----	-----	2.060	-----	-----	-----	-----	2.060
1363	1.969	62.83	2.060	-----	-----	-----	2.058	-----	-----	-----	-----	2.058
1364	1.967	62.83	2.058	-----	-----	-----	2.056	-----	-----	-----	-----	2.055
1365	1.964	62.83	2.056	-----	-----	-----	2.053	-----	-----	-----	-----	2.053
1366	1.962	62.83	2.053	-----	-----	-----	2.051	-----	-----	-----	-----	2.051
1367	1.960	62.83	2.051	-----	-----	-----	2.049	-----	-----	-----	-----	2.049
1368	1.958	62.83	2.049	-----	-----	-----	2.046	-----	-----	-----	-----	2.047
1369	1.955	62.83	2.047	-----	-----	-----	2.044	-----	-----	-----	-----	2.044
1370	1.953	62.83	2.044	-----	-----	-----	2.042	-----	-----	-----	-----	2.042
1371	1.951	62.83	2.042	-----	-----	-----	2.040	-----	-----	-----	-----	2.040
1372	1.949	62.83	2.040	-----	-----	-----	2.038	-----	-----	-----	-----	2.038
1373	1.946	62.83	2.038	-----	-----	-----	2.035	-----	-----	-----	-----	2.035
1374	1.944	62.83	2.035	-----	-----	-----	2.033	-----	-----	-----	-----	2.033
1375	1.942	62.83	2.033	-----	-----	-----	2.031	-----	-----	-----	-----	2.031
1376	1.940	62.83	2.031	-----	-----	-----	2.029	-----	-----	-----	-----	2.029
1377	1.937	62.83	2.029	-----	-----	-----	2.026	-----	-----	-----	-----	2.026
1378	1.935	62.83	2.026	-----	-----	-----	2.024	-----	-----	-----	-----	2.024
1379	1.933	62.83	2.024	-----	-----	-----	2.022	-----	-----	-----	-----	2.022
1380	1.931	62.83	2.022	-----	-----	-----	2.020	-----	-----	-----	-----	2.020
1381	1.928	62.83	2.020	-----	-----	-----	2.017	-----	-----	-----	-----	2.017
1382	1.926	62.83	2.017	-----	-----	-----	2.015	-----	-----	-----	-----	2.015

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1383	1.924	62.83	2.015	-----	-----	-----	2.013	-----	-----	-----	-----	2.013
1384	1.921	62.83	2.013	-----	-----	-----	2.011	-----	-----	-----	-----	2.011
1385	1.919	62.83	2.011	-----	-----	-----	2.008	-----	-----	-----	-----	2.008
1386	1.917	62.83	2.008	-----	-----	-----	2.006	-----	-----	-----	-----	2.006
1387	1.915	62.83	2.006	-----	-----	-----	2.004	-----	-----	-----	-----	2.004
1388	1.912	62.83	2.004	-----	-----	-----	2.001	-----	-----	-----	-----	2.002
1389	1.910	62.83	2.002	-----	-----	-----	1.999	-----	-----	-----	-----	1.999
1390	1.908	62.83	1.999	-----	-----	-----	1.997	-----	-----	-----	-----	1.997
1391	1.906	62.83	1.997	-----	-----	-----	1.995	-----	-----	-----	-----	1.995
1392	1.903	62.83	1.995	-----	-----	-----	1.993	-----	-----	-----	-----	1.993
1393	1.901	62.83	1.993	-----	-----	-----	1.990	-----	-----	-----	-----	1.990
1394	1.899	62.83	1.990	-----	-----	-----	1.988	-----	-----	-----	-----	1.988
1395	1.897	62.83	1.988	-----	-----	-----	1.986	-----	-----	-----	-----	1.986
1396	1.894	62.83	1.986	-----	-----	-----	1.983	-----	-----	-----	-----	1.983
1397	1.892	62.83	1.984	-----	-----	-----	1.981	-----	-----	-----	-----	1.981
1398	1.890	62.83	1.981	-----	-----	-----	1.979	-----	-----	-----	-----	1.979
1399	1.888	62.83	1.979	-----	-----	-----	1.977	-----	-----	-----	-----	1.977
1400	1.885	62.83	1.977	-----	-----	-----	1.974	-----	-----	-----	-----	1.974
1401	1.883	62.83	1.975	-----	-----	-----	1.972	-----	-----	-----	-----	1.972
1402	1.881	62.83	1.972	-----	-----	-----	1.970	-----	-----	-----	-----	1.970
1403	1.878	62.83	1.970	-----	-----	-----	1.968	-----	-----	-----	-----	1.968
1404	1.876	62.83	1.968	-----	-----	-----	1.965	-----	-----	-----	-----	1.965
1405	1.874	62.83	1.966	-----	-----	-----	1.963	-----	-----	-----	-----	1.963
1406	1.872	62.83	1.963	-----	-----	-----	1.961	-----	-----	-----	-----	1.961
1407	1.869	62.83	1.961	-----	-----	-----	1.959	-----	-----	-----	-----	1.959
1408	1.867	62.83	1.959	-----	-----	-----	1.956	-----	-----	-----	-----	1.956
1409	1.865	62.83	1.957	-----	-----	-----	1.954	-----	-----	-----	-----	1.954
1410	1.863	62.83	1.954	-----	-----	-----	1.952	-----	-----	-----	-----	1.952
1411	1.860	62.83	1.952	-----	-----	-----	1.950	-----	-----	-----	-----	1.950
1412	1.858	62.83	1.950	-----	-----	-----	1.947	-----	-----	-----	-----	1.947
1413	1.856	62.83	1.948	-----	-----	-----	1.945	-----	-----	-----	-----	1.945
1414	1.853	62.83	1.945	-----	-----	-----	1.943	-----	-----	-----	-----	1.943
1415	1.851	62.83	1.943	-----	-----	-----	1.941	-----	-----	-----	-----	1.941
1416	1.849	62.83	1.941	-----	-----	-----	1.938	-----	-----	-----	-----	1.938
1417	1.847	62.83	1.938	-----	-----	-----	1.936	-----	-----	-----	-----	1.936
1418	1.844	62.83	1.936	-----	-----	-----	1.934	-----	-----	-----	-----	1.934
1419	1.842	62.83	1.934	-----	-----	-----	1.932	-----	-----	-----	-----	1.932
1420	1.840	62.83	1.932	-----	-----	-----	1.929	-----	-----	-----	-----	1.929
1421	1.838	62.82	1.929	-----	-----	-----	1.927	-----	-----	-----	-----	1.927
1422	1.835	62.82	1.927	-----	-----	-----	1.925	-----	-----	-----	-----	1.925
1423	1.833	62.82	1.925	-----	-----	-----	1.923	-----	-----	-----	-----	1.923
1424	1.831	62.82	1.923	-----	-----	-----	1.920	-----	-----	-----	-----	1.920
1425	1.828	62.82	1.920	-----	-----	-----	1.918	-----	-----	-----	-----	1.918
1426	1.826	62.82	1.918	-----	-----	-----	1.916	-----	-----	-----	-----	1.916
1427	1.824	62.82	1.916	-----	-----	-----	1.913	-----	-----	-----	-----	1.913
1428	1.822	62.82	1.914	-----	-----	-----	1.911	-----	-----	-----	-----	1.911
1429	1.819	62.82	1.911	-----	-----	-----	1.909	-----	-----	-----	-----	1.909
1430	1.817	62.82	1.909	-----	-----	-----	1.907	-----	-----	-----	-----	1.907
1431	1.815	62.82	1.907	-----	-----	-----	1.904	-----	-----	-----	-----	1.904
1432	1.813	62.82	1.905	-----	-----	-----	1.902	-----	-----	-----	-----	1.902
1433	1.810	62.82	1.902	-----	-----	-----	1.900	-----	-----	-----	-----	1.900
1434	1.808	62.82	1.900	-----	-----	-----	1.898	-----	-----	-----	-----	1.898
1435	1.806	62.82	1.898	-----	-----	-----	1.895	-----	-----	-----	-----	1.895
1436	1.803	62.82	1.895	-----	-----	-----	1.893	-----	-----	-----	-----	1.893
1437	1.801	62.82	1.893	-----	-----	-----	1.891	-----	-----	-----	-----	1.891
1438	1.799	62.82	1.891	-----	-----	-----	1.889	-----	-----	-----	-----	1.889

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1439	1.797	62.82	1.889	-----	-----	-----	1.886	-----	-----	-----	-----	1.886
1440	1.794	62.82	1.886	-----	-----	-----	1.884	-----	-----	-----	-----	1.884
1441	1.790	62.82	1.884	-----	-----	-----	1.882	-----	-----	-----	-----	1.882
1442	1.783	62.82	1.882	-----	-----	-----	1.879	-----	-----	-----	-----	1.879
1443	1.773	62.82	1.879	-----	-----	-----	1.877	-----	-----	-----	-----	1.877
1444	1.761	62.82	1.876	-----	-----	-----	1.874	-----	-----	-----	-----	1.874
1445	1.747	62.82	1.873	-----	-----	-----	1.871	-----	-----	-----	-----	1.871
1446	1.730	62.82	1.870	-----	-----	-----	1.868	-----	-----	-----	-----	1.868
1447	1.711	62.82	1.867	-----	-----	-----	1.864	-----	-----	-----	-----	1.864
1448	1.689	62.82	1.862	-----	-----	-----	1.860	-----	-----	-----	-----	1.860
1449	1.665	62.82	1.858	-----	-----	-----	1.855	-----	-----	-----	-----	1.855
1450	1.639	62.82	1.853	-----	-----	-----	1.850	-----	-----	-----	-----	1.850
1451	1.610	62.82	1.847	-----	-----	-----	1.845	-----	-----	-----	-----	1.845
1452	1.579	62.82	1.841	-----	-----	-----	1.838	-----	-----	-----	-----	1.838
1453	1.546	62.82	1.834	-----	-----	-----	1.832	-----	-----	-----	-----	1.832
1454	1.510	62.82	1.826	-----	-----	-----	1.824	-----	-----	-----	-----	1.824
1455	1.472	62.82	1.818	-----	-----	-----	1.816	-----	-----	-----	-----	1.816
1456	1.431	62.82	1.809	-----	-----	-----	1.807	-----	-----	-----	-----	1.807
1457	1.388	62.82	1.799	-----	-----	-----	1.797	-----	-----	-----	-----	1.797
1458	1.343	62.82	1.788	-----	-----	-----	1.786	-----	-----	-----	-----	1.786
1459	1.295	62.82	1.777	-----	-----	-----	1.774	-----	-----	-----	-----	1.774
1460	1.245	62.82	1.764	-----	-----	-----	1.762	-----	-----	-----	-----	1.762
1461	1.193	62.82	1.751	-----	-----	-----	1.748	-----	-----	-----	-----	1.748
1462	1.142	62.82	1.736	-----	-----	-----	1.734	-----	-----	-----	-----	1.734
1463	1.091	62.82	1.721	-----	-----	-----	1.718	-----	-----	-----	-----	1.718
1464	1.042	62.82	1.704	-----	-----	-----	1.702	-----	-----	-----	-----	1.702
1465	0.995	62.81	1.687	-----	-----	-----	1.685	-----	-----	-----	-----	1.685
1466	0.948	62.81	1.670	-----	-----	-----	1.667	-----	-----	-----	-----	1.667
1467	0.902	62.81	1.651	-----	-----	-----	1.649	-----	-----	-----	-----	1.649
1468	0.858	62.81	1.632	-----	-----	-----	1.629	-----	-----	-----	-----	1.629
1469	0.815	62.81	1.612	-----	-----	-----	1.610	-----	-----	-----	-----	1.610
1470	0.773	62.81	1.592	-----	-----	-----	1.589	-----	-----	-----	-----	1.589
1471	0.732	62.81	1.571	-----	-----	-----	1.568	-----	-----	-----	-----	1.568
1472	0.692	62.81	1.550	-----	-----	-----	1.547	-----	-----	-----	-----	1.547
1473	0.653	62.81	1.528	-----	-----	-----	1.525	-----	-----	-----	-----	1.525
1474	0.616	62.81	1.505	-----	-----	-----	1.503	-----	-----	-----	-----	1.503
1475	0.579	62.81	1.483	-----	-----	-----	1.480	-----	-----	-----	-----	1.480
1476	0.544	62.81	1.460	-----	-----	-----	1.457	-----	-----	-----	-----	1.457
1477	0.510	62.80	1.437	-----	-----	-----	1.434	-----	-----	-----	-----	1.434
1478	0.476	62.80	1.413	-----	-----	-----	1.411	-----	-----	-----	-----	1.411
1479	0.445	62.80	1.389	-----	-----	-----	1.387	-----	-----	-----	-----	1.387
1480	0.414	62.80	1.366	-----	-----	-----	1.363	-----	-----	-----	-----	1.363
1481	0.384	62.80	1.341	-----	-----	-----	1.339	-----	-----	-----	-----	1.339
1482	0.355	62.80	1.321	-----	-----	-----	1.318	-----	-----	-----	-----	1.318
1483	0.328	62.80	1.307	-----	-----	-----	1.305	-----	-----	-----	-----	1.305
1484	0.302	62.80	1.294	-----	-----	-----	1.291	-----	-----	-----	-----	1.291
1485	0.276	62.80	1.280	-----	-----	-----	1.277	-----	-----	-----	-----	1.277
1486	0.252	62.80	1.266	-----	-----	-----	1.263	-----	-----	-----	-----	1.263
1487	0.229	62.79	1.252	-----	-----	-----	1.249	-----	-----	-----	-----	1.249
1488	0.207	62.79	1.238	-----	-----	-----	1.235	-----	-----	-----	-----	1.235
1489	0.186	62.79	1.223	-----	-----	-----	1.221	-----	-----	-----	-----	1.221
1490	0.167	62.79	1.209	-----	-----	-----	1.207	-----	-----	-----	-----	1.207
1491	0.148	62.79	1.195	-----	-----	-----	1.192	-----	-----	-----	-----	1.192
1492	0.131	62.79	1.180	-----	-----	-----	1.178	-----	-----	-----	-----	1.178
1493	0.114	62.79	1.166	-----	-----	-----	1.163	-----	-----	-----	-----	1.163
1494	0.099	62.79	1.151	-----	-----	-----	1.149	-----	-----	-----	-----	1.149

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1495	0.085	62.79	1.137	-----	-----	-----	1.134	-----	-----	-----	-----	1.134
1496	0.072	62.78	1.122	-----	-----	-----	1.120	-----	-----	-----	-----	1.120
1497	0.060	62.78	1.108	-----	-----	-----	1.105	-----	-----	-----	-----	1.105
1498	0.049	62.78	1.093	-----	-----	-----	1.091	-----	-----	-----	-----	1.091
1499	0.039	62.78	1.079	-----	-----	-----	1.077	-----	-----	-----	-----	1.077
1500	0.030	62.78	1.064	-----	-----	-----	1.062	-----	-----	-----	-----	1.062
1501	0.023	62.78	1.050	-----	-----	-----	1.048	-----	-----	-----	-----	1.048
1502	0.016	62.78	1.036	-----	-----	-----	1.034	-----	-----	-----	-----	1.034
1503	0.011	62.78	1.022	-----	-----	-----	1.020	-----	-----	-----	-----	1.020
1504	0.006	62.78	1.008	-----	-----	-----	1.006	-----	-----	-----	-----	1.006
1505	0.003	62.78	0.994	-----	-----	-----	0.992	-----	-----	-----	-----	0.992
1506	0.001	62.77	0.981	-----	-----	-----	0.979	-----	-----	-----	-----	0.979
1507	0.000	62.77	0.967	-----	-----	-----	0.965	-----	-----	-----	-----	0.965
1508	0.000	62.77	0.954	-----	-----	-----	0.952	-----	-----	-----	-----	0.952
1509	0.000	62.77	0.941	-----	-----	-----	0.939	-----	-----	-----	-----	0.939
1510	0.000	62.77	0.928	-----	-----	-----	0.926	-----	-----	-----	-----	0.926
1511	0.000	62.77	0.915	-----	-----	-----	0.913	-----	-----	-----	-----	0.913
1512	0.000	62.77	0.902	-----	-----	-----	0.901	-----	-----	-----	-----	0.901
1513	0.000	62.77	0.890	-----	-----	-----	0.888	-----	-----	-----	-----	0.888
1514	0.000	62.77	0.878	-----	-----	-----	0.876	-----	-----	-----	-----	0.876
1515	0.000	62.77	0.866	-----	-----	-----	0.864	-----	-----	-----	-----	0.864
1516	0.000	62.76	0.854	-----	-----	-----	0.852	-----	-----	-----	-----	0.852
1517	0.000	62.76	0.842	-----	-----	-----	0.841	-----	-----	-----	-----	0.841
1518	0.000	62.76	0.831	-----	-----	-----	0.829	-----	-----	-----	-----	0.829
1519	0.000	62.76	0.819	-----	-----	-----	0.818	-----	-----	-----	-----	0.818
1520	0.000	62.76	0.808	-----	-----	-----	0.806	-----	-----	-----	-----	0.806
1521	0.000	62.76	0.797	-----	-----	-----	0.795	-----	-----	-----	-----	0.795
1522	0.000	62.76	0.786	-----	-----	-----	0.784	-----	-----	-----	-----	0.784
1523	0.000	62.76	0.775	-----	-----	-----	0.774	-----	-----	-----	-----	0.774
1524	0.000	62.76	0.765	-----	-----	-----	0.763	-----	-----	-----	-----	0.763
1525	0.000	62.76	0.754	-----	-----	-----	0.753	-----	-----	-----	-----	0.753
1526	0.000	62.76	0.744	-----	-----	-----	0.742	-----	-----	-----	-----	0.742
1527	0.000	62.76	0.733	-----	-----	-----	0.732	-----	-----	-----	-----	0.732
1528	0.000	62.75	0.723	-----	-----	-----	0.722	-----	-----	-----	-----	0.722
1529	0.000	62.75	0.713	-----	-----	-----	0.712	-----	-----	-----	-----	0.712
1530	0.000	62.75	0.704	-----	-----	-----	0.702	-----	-----	-----	-----	0.702
1531	0.000	62.75	0.694	-----	-----	-----	0.693	-----	-----	-----	-----	0.693
1532	0.000	62.75	0.684	-----	-----	-----	0.683	-----	-----	-----	-----	0.683
1533	0.000	62.75	0.675	-----	-----	-----	0.674	-----	-----	-----	-----	0.674
1534	0.000	62.75	0.666	-----	-----	-----	0.664	-----	-----	-----	-----	0.664
1535	0.000	62.75	0.657	-----	-----	-----	0.655	-----	-----	-----	-----	0.655
1536	0.000	62.75	0.648	-----	-----	-----	0.646	-----	-----	-----	-----	0.646
1537	0.000	62.75	0.639	-----	-----	-----	0.637	-----	-----	-----	-----	0.637
1538	0.000	62.75	0.630	-----	-----	-----	0.629	-----	-----	-----	-----	0.629
1539	0.000	62.75	0.621	-----	-----	-----	0.620	-----	-----	-----	-----	0.620
1540	0.000	62.75	0.613	-----	-----	-----	0.612	-----	-----	-----	-----	0.612
1541	0.000	62.75	0.604	-----	-----	-----	0.603	-----	-----	-----	-----	0.603
1542	0.000	62.74	0.596	-----	-----	-----	0.595	-----	-----	-----	-----	0.595
1543	0.000	62.74	0.588	-----	-----	-----	0.587	-----	-----	-----	-----	0.587
1544	0.000	62.74	0.580	-----	-----	-----	0.579	-----	-----	-----	-----	0.579
1545	0.000	62.74	0.572	-----	-----	-----	0.571	-----	-----	-----	-----	0.571
1546	0.000	62.74	0.564	-----	-----	-----	0.563	-----	-----	-----	-----	0.563
1547	0.000	62.74	0.556	-----	-----	-----	0.555	-----	-----	-----	-----	0.555
1548	0.000	62.74	0.549	-----	-----	-----	0.548	-----	-----	-----	-----	0.548
1549	0.000	62.74	0.541	-----	-----	-----	0.540	-----	-----	-----	-----	0.540
1550	0.000	62.74	0.534	-----	-----	-----	0.533	-----	-----	-----	-----	0.533

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1551	0.000	62.74	0.526	-----	-----	-----	0.525	-----	-----	-----	-----	0.525
1552	0.000	62.74	0.519	-----	-----	-----	0.518	-----	-----	-----	-----	0.518
1553	0.000	62.74	0.512	-----	-----	-----	0.511	-----	-----	-----	-----	0.511
1554	0.000	62.74	0.505	-----	-----	-----	0.504	-----	-----	-----	-----	0.504
1555	0.000	62.74	0.498	-----	-----	-----	0.497	-----	-----	-----	-----	0.497
1556	0.000	62.74	0.491	-----	-----	-----	0.490	-----	-----	-----	-----	0.490
1557	0.000	62.74	0.484	-----	-----	-----	0.483	-----	-----	-----	-----	0.483
1558	0.000	62.74	0.478	-----	-----	-----	0.477	-----	-----	-----	-----	0.477
1559	0.000	62.74	0.471	-----	-----	-----	0.470	-----	-----	-----	-----	0.470
1560	0.000	62.74	0.465	-----	-----	-----	0.464	-----	-----	-----	-----	0.464
1561	0.000	62.73	0.458	-----	-----	-----	0.457	-----	-----	-----	-----	0.457
1562	0.000	62.73	0.452	-----	-----	-----	0.451	-----	-----	-----	-----	0.451
1563	0.000	62.73	0.446	-----	-----	-----	0.445	-----	-----	-----	-----	0.445
1564	0.000	62.73	0.440	-----	-----	-----	0.439	-----	-----	-----	-----	0.439
1565	0.000	62.73	0.434	-----	-----	-----	0.433	-----	-----	-----	-----	0.433
1566	0.000	62.73	0.428	-----	-----	-----	0.427	-----	-----	-----	-----	0.427
1567	0.000	62.73	0.422	-----	-----	-----	0.421	-----	-----	-----	-----	0.421
1568	0.000	62.73	0.416	-----	-----	-----	0.415	-----	-----	-----	-----	0.415
1569	0.000	62.73	0.410	-----	-----	-----	0.410	-----	-----	-----	-----	0.410
1570	0.000	62.73	0.405	-----	-----	-----	0.404	-----	-----	-----	-----	0.404
1571	0.000	62.73	0.399	-----	-----	-----	0.398	-----	-----	-----	-----	0.398
1572	0.000	62.73	0.394	-----	-----	-----	0.393	-----	-----	-----	-----	0.393
1573	0.000	62.73	0.388	-----	-----	-----	0.388	-----	-----	-----	-----	0.388
1574	0.000	62.73	0.383	-----	-----	-----	0.382	-----	-----	-----	-----	0.382
1575	0.000	62.73	0.378	-----	-----	-----	0.377	-----	-----	-----	-----	0.377
1576	0.000	62.73	0.373	-----	-----	-----	0.372	-----	-----	-----	-----	0.372
1577	0.000	62.73	0.367	-----	-----	-----	0.367	-----	-----	-----	-----	0.367
1578	0.000	62.73	0.362	-----	-----	-----	0.362	-----	-----	-----	-----	0.362
1579	0.000	62.73	0.357	-----	-----	-----	0.357	-----	-----	-----	-----	0.357
1580	0.000	62.73	0.352	-----	-----	-----	0.352	-----	-----	-----	-----	0.352
1581	0.000	62.73	0.348	-----	-----	-----	0.347	-----	-----	-----	-----	0.347
1582	0.000	62.73	0.343	-----	-----	-----	0.342	-----	-----	-----	-----	0.342
1583	0.000	62.73	0.338	-----	-----	-----	0.337	-----	-----	-----	-----	0.337
1584	0.000	62.73	0.334	-----	-----	-----	0.333	-----	-----	-----	-----	0.333
1585	0.000	62.72	0.329	-----	-----	-----	0.328	-----	-----	-----	-----	0.328
1586	0.000	62.72	0.324	-----	-----	-----	0.324	-----	-----	-----	-----	0.324
1587	0.000	62.72	0.320	-----	-----	-----	0.319	-----	-----	-----	-----	0.319
1588	0.000	62.72	0.316	-----	-----	-----	0.315	-----	-----	-----	-----	0.315
1589	0.000	62.72	0.311	-----	-----	-----	0.311	-----	-----	-----	-----	0.311
1590	0.000	62.72	0.307	-----	-----	-----	0.306	-----	-----	-----	-----	0.306
1591	0.000	62.72	0.303	-----	-----	-----	0.302	-----	-----	-----	-----	0.302
1592	0.000	62.72	0.299	-----	-----	-----	0.298	-----	-----	-----	-----	0.298
1593	0.000	62.72	0.294	-----	-----	-----	0.294	-----	-----	-----	-----	0.294
1594	0.000	62.72	0.290	-----	-----	-----	0.290	-----	-----	-----	-----	0.290
1595	0.000	62.72	0.286	-----	-----	-----	0.286	-----	-----	-----	-----	0.286
1596	0.000	62.72	0.283	-----	-----	-----	0.282	-----	-----	-----	-----	0.282
1597	0.000	62.72	0.279	-----	-----	-----	0.278	-----	-----	-----	-----	0.278
1598	0.000	62.72	0.275	-----	-----	-----	0.274	-----	-----	-----	-----	0.274
1599	0.000	62.72	0.271	-----	-----	-----	0.270	-----	-----	-----	-----	0.270
1600	0.000	62.72	0.267	-----	-----	-----	0.267	-----	-----	-----	-----	0.267
1601	0.000	62.72	0.264	-----	-----	-----	0.263	-----	-----	-----	-----	0.263
1602	0.000	62.72	0.260	-----	-----	-----	0.259	-----	-----	-----	-----	0.260
1603	0.000	62.72	0.256	-----	-----	-----	0.256	-----	-----	-----	-----	0.256
1604	0.000	62.72	0.253	-----	-----	-----	0.252	-----	-----	-----	-----	0.252
1605	0.000	62.72	0.249	-----	-----	-----	0.249	-----	-----	-----	-----	0.249
1606	0.000	62.72	0.246	-----	-----	-----	0.246	-----	-----	-----	-----	0.246

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1607	0.000	62.72	0.243	-----	-----	-----	0.242	-----	-----	-----	-----	0.242
1608	0.000	62.72	0.239	-----	-----	-----	0.239	-----	-----	-----	-----	0.239
1609	0.000	62.72	0.236	-----	-----	-----	0.236	-----	-----	-----	-----	0.236
1610	0.000	62.72	0.233	-----	-----	-----	0.232	-----	-----	-----	-----	0.232
1611	0.000	62.72	0.230	-----	-----	-----	0.229	-----	-----	-----	-----	0.229
1612	0.000	62.72	0.226	-----	-----	-----	0.226	-----	-----	-----	-----	0.226
1613	0.000	62.72	0.223	-----	-----	-----	0.223	-----	-----	-----	-----	0.223
1614	0.000	62.72	0.220	-----	-----	-----	0.220	-----	-----	-----	-----	0.220
1615	0.000	62.72	0.217	-----	-----	-----	0.217	-----	-----	-----	-----	0.217
1616	0.000	62.72	0.214	-----	-----	-----	0.214	-----	-----	-----	-----	0.214
1617	0.000	62.72	0.211	-----	-----	-----	0.211	-----	-----	-----	-----	0.211
1618	0.000	62.72	0.208	-----	-----	-----	0.208	-----	-----	-----	-----	0.208
1619	0.000	62.72	0.206	-----	-----	-----	0.205	-----	-----	-----	-----	0.205
1620	0.000	62.72	0.203	-----	-----	-----	0.202	-----	-----	-----	-----	0.202
1621	0.000	62.72	0.200	-----	-----	-----	0.200	-----	-----	-----	-----	0.200
1622	0.000	62.71	0.197	-----	-----	-----	0.197	-----	-----	-----	-----	0.197
1623	0.000	62.71	0.195	-----	-----	-----	0.194	-----	-----	-----	-----	0.194
1624	0.000	62.71	0.192	-----	-----	-----	0.191	-----	-----	-----	-----	0.191
1625	0.000	62.71	0.189	-----	-----	-----	0.189	-----	-----	-----	-----	0.189
1626	0.000	62.71	0.187	-----	-----	-----	0.186	-----	-----	-----	-----	0.186
1627	0.000	62.71	0.184	-----	-----	-----	0.184	-----	-----	-----	-----	0.184
1628	0.000	62.71	0.182	-----	-----	-----	0.181	-----	-----	-----	-----	0.181
1629	0.000	62.71	0.179	-----	-----	-----	0.179	-----	-----	-----	-----	0.179
1630	0.000	62.71	0.177	-----	-----	-----	0.176	-----	-----	-----	-----	0.176
1631	0.000	62.71	0.174	-----	-----	-----	0.174	-----	-----	-----	-----	0.174
1632	0.000	62.71	0.172	-----	-----	-----	0.171	-----	-----	-----	-----	0.171
1633	0.000	62.71	0.169	-----	-----	-----	0.169	-----	-----	-----	-----	0.169
1634	0.000	62.71	0.167	-----	-----	-----	0.167	-----	-----	-----	-----	0.167
1635	0.000	62.71	0.165	-----	-----	-----	0.164	-----	-----	-----	-----	0.164
1636	0.000	62.71	0.163	-----	-----	-----	0.162	-----	-----	-----	-----	0.162
1637	0.000	62.71	0.160	-----	-----	-----	0.160	-----	-----	-----	-----	0.160
1638	0.000	62.71	0.158	-----	-----	-----	0.158	-----	-----	-----	-----	0.158
1639	0.000	62.71	0.156	-----	-----	-----	0.156	-----	-----	-----	-----	0.156
1640	0.000	62.71	0.154	-----	-----	-----	0.153	-----	-----	-----	-----	0.153
1641	0.000	62.71	0.152	-----	-----	-----	0.151	-----	-----	-----	-----	0.151
1642	0.000	62.71	0.150	-----	-----	-----	0.149	-----	-----	-----	-----	0.149
1643	0.000	62.71	0.147	-----	-----	-----	0.147	-----	-----	-----	-----	0.147
1644	0.000	62.71	0.145	-----	-----	-----	0.145	-----	-----	-----	-----	0.145
1645	0.000	62.71	0.143	-----	-----	-----	0.143	-----	-----	-----	-----	0.143
1646	0.000	62.71	0.142	-----	-----	-----	0.141	-----	-----	-----	-----	0.141
1647	0.000	62.71	0.140	-----	-----	-----	0.139	-----	-----	-----	-----	0.139
1648	0.000	62.71	0.138	-----	-----	-----	0.137	-----	-----	-----	-----	0.137
1649	0.000	62.71	0.136	-----	-----	-----	0.135	-----	-----	-----	-----	0.135
1650	0.000	62.71	0.134	-----	-----	-----	0.134	-----	-----	-----	-----	0.134
1651	0.000	62.71	0.132	-----	-----	-----	0.132	-----	-----	-----	-----	0.132
1652	0.000	62.71	0.130	-----	-----	-----	0.130	-----	-----	-----	-----	0.130
1653	0.000	62.71	0.128	-----	-----	-----	0.128	-----	-----	-----	-----	0.128
1654	0.000	62.71	0.127	-----	-----	-----	0.126	-----	-----	-----	-----	0.126
1655	0.000	62.71	0.125	-----	-----	-----	0.125	-----	-----	-----	-----	0.125
1656	0.000	62.71	0.123	-----	-----	-----	0.123	-----	-----	-----	-----	0.123
1657	0.000	62.71	0.122	-----	-----	-----	0.121	-----	-----	-----	-----	0.121
1658	0.000	62.71	0.120	-----	-----	-----	0.120	-----	-----	-----	-----	0.120
1659	0.000	62.71	0.118	-----	-----	-----	0.118	-----	-----	-----	-----	0.118
1660	0.000	62.71	0.117	-----	-----	-----	0.116	-----	-----	-----	-----	0.116
1661	0.000	62.71	0.115	-----	-----	-----	0.115	-----	-----	-----	-----	0.115
1662	0.000	62.71	0.113	-----	-----	-----	0.113	-----	-----	-----	-----	0.113

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1663	0.000	62.71	0.112	-----	-----	-----	0.112	-----	-----	-----	-----	0.112
1664	0.000	62.71	0.110	-----	-----	-----	0.110	-----	-----	-----	-----	0.110
1665	0.000	62.71	0.109	-----	-----	-----	0.109	-----	-----	-----	-----	0.109
1666	0.000	62.71	0.107	-----	-----	-----	0.107	-----	-----	-----	-----	0.107
1667	0.000	62.71	0.106	-----	-----	-----	0.106	-----	-----	-----	-----	0.106
1668	0.000	62.71	0.104	-----	-----	-----	0.104	-----	-----	-----	-----	0.104
1669	0.000	62.71	0.103	-----	-----	-----	0.103	-----	-----	-----	-----	0.103
1670	0.000	62.71	0.102	-----	-----	-----	0.101	-----	-----	-----	-----	0.101
1671	0.000	62.71	0.100	-----	-----	-----	0.100	-----	-----	-----	-----	0.100
1672	0.000	62.71	0.099	-----	-----	-----	0.099	-----	-----	-----	-----	0.099
1673	0.000	62.71	0.097	-----	-----	-----	0.097	-----	-----	-----	-----	0.097
1674	0.000	62.71	0.096	-----	-----	-----	0.096	-----	-----	-----	-----	0.096
1675	0.000	62.71	0.095	-----	-----	-----	0.095	-----	-----	-----	-----	0.095
1676	0.000	62.71	0.093	-----	-----	-----	0.093	-----	-----	-----	-----	0.093
1677	0.000	62.71	0.092	-----	-----	-----	0.092	-----	-----	-----	-----	0.092
1678	0.000	62.71	0.091	-----	-----	-----	0.091	-----	-----	-----	-----	0.091
1679	0.000	62.71	0.090	-----	-----	-----	0.089	-----	-----	-----	-----	0.089
1680	0.000	62.71	0.088	-----	-----	-----	0.088	-----	-----	-----	-----	0.088
1681	0.000	62.71	0.087	-----	-----	-----	0.087	-----	-----	-----	-----	0.087
1682	0.000	62.71	0.086	-----	-----	-----	0.086	-----	-----	-----	-----	0.086
1683	0.000	62.71	0.085	-----	-----	-----	0.085	-----	-----	-----	-----	0.085
1684	0.000	62.71	0.084	-----	-----	-----	0.083	-----	-----	-----	-----	0.084
1685	0.000	62.71	0.083	-----	-----	-----	0.082	-----	-----	-----	-----	0.082
1686	0.000	62.71	0.081	-----	-----	-----	0.081	-----	-----	-----	-----	0.081
1687	0.000	62.71	0.080	-----	-----	-----	0.080	-----	-----	-----	-----	0.080
1688	0.000	62.71	0.079	-----	-----	-----	0.079	-----	-----	-----	-----	0.079
1689	0.000	62.71	0.078	-----	-----	-----	0.078	-----	-----	-----	-----	0.078
1690	0.000	62.71	0.077	-----	-----	-----	0.077	-----	-----	-----	-----	0.077
1691	0.000	62.71	0.076	-----	-----	-----	0.076	-----	-----	-----	-----	0.076
1692	0.000	62.71	0.075	-----	-----	-----	0.075	-----	-----	-----	-----	0.075
1693	0.000	62.71	0.074	-----	-----	-----	0.074	-----	-----	-----	-----	0.074
1694	0.000	62.71	0.073	-----	-----	-----	0.073	-----	-----	-----	-----	0.073
1695	0.000	62.71	0.072	-----	-----	-----	0.072	-----	-----	-----	-----	0.072
1696	0.000	62.71	0.071	-----	-----	-----	0.071	-----	-----	-----	-----	0.071
1697	0.000	62.71	0.070	-----	-----	-----	0.070	-----	-----	-----	-----	0.070
1698	0.000	62.71	0.069	-----	-----	-----	0.069	-----	-----	-----	-----	0.069
1699	0.000	62.71	0.068	-----	-----	-----	0.068	-----	-----	-----	-----	0.068
1700	0.000	62.71	0.067	-----	-----	-----	0.067	-----	-----	-----	-----	0.067
1701	0.000	62.70	0.066	-----	-----	-----	0.066	-----	-----	-----	-----	0.066
1702	0.000	62.70	0.065	-----	-----	-----	0.065	-----	-----	-----	-----	0.065
1703	0.000	62.70	0.064	-----	-----	-----	0.064	-----	-----	-----	-----	0.064
1704	0.000	62.70	0.063	-----	-----	-----	0.063	-----	-----	-----	-----	0.063
1705	0.000	62.70	0.063	-----	-----	-----	0.062	-----	-----	-----	-----	0.062
1706	0.000	62.70	0.062	-----	-----	-----	0.062	-----	-----	-----	-----	0.062
1707	0.000	62.70	0.061	-----	-----	-----	0.061	-----	-----	-----	-----	0.061
1708	0.000	62.70	0.060	-----	-----	-----	0.060	-----	-----	-----	-----	0.060
1709	0.000	62.70	0.059	-----	-----	-----	0.059	-----	-----	-----	-----	0.059
1710	0.000	62.70	0.058	-----	-----	-----	0.058	-----	-----	-----	-----	0.058
1711	0.000	62.70	0.058	-----	-----	-----	0.058	-----	-----	-----	-----	0.057
1712	0.000	62.70	0.057	-----	-----	-----	0.057	-----	-----	-----	-----	0.057
1713	0.000	62.70	0.056	-----	-----	-----	0.056	-----	-----	-----	-----	0.056
1714	0.000	62.70	0.055	-----	-----	-----	0.055	-----	-----	-----	-----	0.055
1715	0.000	62.70	0.054	-----	-----	-----	0.054	-----	-----	-----	-----	0.054
1716	0.000	62.70	0.054	-----	-----	-----	0.054	-----	-----	-----	-----	0.054
1717	0.000	62.70	0.053	-----	-----	-----	0.053	-----	-----	-----	-----	0.053
1718	0.000	62.70	0.052	-----	-----	-----	0.052	-----	-----	-----	-----	0.052

Continues on next page...

Detention pond outflow

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1719	0.000	62.70	0.052	-----	-----	-----	0.051	-----	-----	-----	-----	0.051
1720	0.000	62.70	0.051	-----	-----	-----	0.051	-----	-----	-----	-----	0.051
1721	0.000	62.70	0.050	-----	-----	-----	0.050	-----	-----	-----	-----	0.050
1722	0.000	62.70	0.049	-----	-----	-----	0.049	-----	-----	-----	-----	0.049
1723	0.000	62.70	0.049	-----	-----	-----	0.049	-----	-----	-----	-----	0.049
1724	0.000	62.70	0.048	-----	-----	-----	0.048	-----	-----	-----	-----	0.048
1725	0.000	62.70	0.047	-----	-----	-----	0.047	-----	-----	-----	-----	0.047
1726	0.000	62.70	0.047	-----	-----	-----	0.047	-----	-----	-----	-----	0.047
1727	0.000	62.70	0.046	-----	-----	-----	0.046	-----	-----	-----	-----	0.046
1728	0.000	62.70	0.046	-----	-----	-----	0.045	-----	-----	-----	-----	0.045
1729	0.000	62.70	0.045	-----	-----	-----	0.045	-----	-----	-----	-----	0.045
1730	0.000	62.70	0.044	-----	-----	-----	0.044	-----	-----	-----	-----	0.044
1731	0.000	62.70	0.044	-----	-----	-----	0.044	-----	-----	-----	-----	0.044
1732	0.000	62.70	0.043	-----	-----	-----	0.043	-----	-----	-----	-----	0.043
1733	0.000	62.70	0.043	-----	-----	-----	0.042	-----	-----	-----	-----	0.042
1734	0.000	62.70	0.042	-----	-----	-----	0.042	-----	-----	-----	-----	0.042
1735	0.000	62.70	0.041	-----	-----	-----	0.041	-----	-----	-----	-----	0.041
1736	0.000	62.70	0.041	-----	-----	-----	0.041	-----	-----	-----	-----	0.041
1737	0.000	62.70	0.040	-----	-----	-----	0.040	-----	-----	-----	-----	0.040
1738	0.000	62.70	0.040	-----	-----	-----	0.040	-----	-----	-----	-----	0.040
1739	0.000	62.70	0.039	-----	-----	-----	0.039	-----	-----	-----	-----	0.039
1740	0.000	62.70	0.039	-----	-----	-----	0.038	-----	-----	-----	-----	0.038
1741	0.000	62.70	0.038	-----	-----	-----	0.038	-----	-----	-----	-----	0.038
1742	0.000	62.70	0.038	-----	-----	-----	0.037	-----	-----	-----	-----	0.037
1743	0.000	62.70	0.037	-----	-----	-----	0.037	-----	-----	-----	-----	0.037
1744	0.000	62.70	0.036	-----	-----	-----	0.036	-----	-----	-----	-----	0.036
1745	0.000	62.70	0.036	-----	-----	-----	0.036	-----	-----	-----	-----	0.036
1746	0.000	62.70	0.035	-----	-----	-----	0.035	-----	-----	-----	-----	0.035
1747	0.000	62.70	0.035	-----	-----	-----	0.035	-----	-----	-----	-----	0.035
1748	0.000	62.70	0.035	-----	-----	-----	0.034	-----	-----	-----	-----	0.034
1749	0.000	62.70	0.034	-----	-----	-----	0.034	-----	-----	-----	-----	0.034
1750	0.000	62.70	0.034	-----	-----	-----	0.034	-----	-----	-----	-----	0.034
1751	0.000	62.70	0.033	-----	-----	-----	0.033	-----	-----	-----	-----	0.033
1752	0.000	62.70	0.033	-----	-----	-----	0.033	-----	-----	-----	-----	0.033
1753	0.000	62.70	0.032	-----	-----	-----	0.032	-----	-----	-----	-----	0.032
1754	0.000	62.70	0.032	-----	-----	-----	0.032	-----	-----	-----	-----	0.032
1755	0.000	62.70	0.031	-----	-----	-----	0.031	-----	-----	-----	-----	0.031
1756	0.000	62.70	0.031	-----	-----	-----	0.031	-----	-----	-----	-----	0.031
1757	0.000	62.70	0.030	-----	-----	-----	0.030	-----	-----	-----	-----	0.030
1758	0.000	62.70	0.030	-----	-----	-----	0.030	-----	-----	-----	-----	0.030

...End

Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Hyd. No. 1

Developed site storm event

Hydrograph type	= SCS Runoff	Peak discharge	= 23.03 cfs
Storm frequency	= 100 yrs	Time to peak	= 495 min
Time interval	= 1 min	Hyd. volume	= 397,003 cuft
Drainage area	= 25.500 ac	Curve number	= 91
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 34.0 min
Total precip.	= 5.30 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 400

Hydrograph Discharge Table

(Printed values >= 1.00% of Qp.)

Time -- Outflow (min cfs)		Time -- Outflow (min cfs)		Time -- Outflow (min cfs)		Time -- Outflow (min cfs)	
133	0.243	172	0.955	211	1.536	250	2.213
134	0.258	173	0.972	212	1.549	251	2.232
135	0.274	174	0.990	213	1.564	252	2.250
136	0.290	175	1.007	214	1.578	253	2.268
137	0.306	176	1.024	215	1.592	254	2.286
138	0.323	177	1.041	216	1.607	255	2.304
139	0.340	178	1.057	217	1.622	256	2.322
140	0.358	179	1.074	218	1.637	257	2.340
141	0.375	180	1.090	219	1.653	258	2.357
142	0.393	181	1.107	220	1.668	259	2.375
143	0.411	182	1.123	221	1.684	260	2.392
144	0.429	183	1.139	222	1.700	261	2.409
145	0.448	184	1.155	223	1.717	262	2.427
146	0.467	185	1.170	224	1.733	263	2.444
147	0.485	186	1.186	225	1.750	264	2.461
148	0.504	187	1.201	226	1.767	265	2.478
149	0.523	188	1.216	227	1.784	266	2.495
150	0.543	189	1.231	228	1.802	267	2.512
151	0.562	190	1.246	229	1.820	268	2.529
152	0.581	191	1.260	230	1.838	269	2.547
153	0.600	192	1.275	231	1.856	270	2.564
154	0.620	193	1.289	232	1.874	271	2.581
155	0.639	194	1.304	233	1.893	272	2.598
156	0.659	195	1.318	234	1.912	273	2.616
157	0.678	196	1.332	235	1.930	274	2.633
158	0.697	197	1.345	236	1.949	275	2.650
159	0.716	198	1.359	237	1.968	276	2.668
160	0.736	199	1.373	238	1.987	277	2.685
161	0.755	200	1.386	239	2.006	278	2.703
162	0.774	201	1.400	240	2.025	279	2.720
163	0.792	202	1.413	241	2.044	280	2.738
164	0.811	203	1.427	242	2.063	281	2.756
165	0.830	204	1.440	243	2.082	282	2.774
166	0.848	205	1.454	244	2.101	283	2.792
167	0.866	206	1.467	245	2.120	284	2.810
168	0.884	207	1.481	246	2.139	285	2.829
169	0.902	208	1.494	247	2.158	286	2.847
170	0.920	209	1.508	248	2.176	287	2.866
171	0.938	210	1.522	249	2.195	288	2.885

Continues on next page...

Hydrograph Discharge Table

Time (min	Outflow cfs)	Time (min	Outflow cfs)	Time (min	Outflow cfs)	Time (min	Outflow cfs)
289	2.904	345	4.277	401	6.079	457	9.168
290	2.923	346	4.302	402	6.104	458	9.426
291	2.943	347	4.326	403	6.127	459	9.707
292	2.962	348	4.349	404	6.149	460	10.01
293	2.982	349	4.373	405	6.170	461	10.34
294	3.002	350	4.397	406	6.190	462	10.69
295	3.022	351	4.420	407	6.208	463	11.06
296	3.043	352	4.444	408	6.226	464	11.45
297	3.064	353	4.468	409	6.242	465	11.87
298	3.084	354	4.492	410	6.258	466	12.31
299	3.105	355	4.516	411	6.273	467	12.77
300	3.127	356	4.541	412	6.287	468	13.25
301	3.148	357	4.565	413	6.302	469	13.76
302	3.170	358	4.590	414	6.318	470	14.28
303	3.193	359	4.616	415	6.334	471	14.83
304	3.215	360	4.642	416	6.351	472	15.37
305	3.238	361	4.668	417	6.368	473	15.91
306	3.261	362	4.694	418	6.387	474	16.45
307	3.285	363	4.722	419	6.407	475	16.97
308	3.309	364	4.750	420	6.427	476	17.49
309	3.333	365	4.779	421	6.449	477	18.00
310	3.357	366	4.809	422	6.472	478	18.50
311	3.382	367	4.840	423	6.497	479	18.98
312	3.407	368	4.871	424	6.522	480	19.46
313	3.432	369	4.904	425	6.550	481	19.90
314	3.458	370	4.937	426	6.578	482	20.33
315	3.484	371	4.971	427	6.609	483	20.72
316	3.510	372	5.005	428	6.641	484	21.08
317	3.536	373	5.041	429	6.675	485	21.42
318	3.562	374	5.077	430	6.711	486	21.73
319	3.589	375	5.114	431	6.750	487	22.00
320	3.616	376	5.152	432	6.790	488	22.24
321	3.643	377	5.190	433	6.833	489	22.45
322	3.671	378	5.230	434	6.878	490	22.63
323	3.698	379	5.269	435	6.926	491	22.78
324	3.725	380	5.310	436	6.976	492	22.89
325	3.753	381	5.351	437	7.028	493	22.97
326	3.780	382	5.392	438	7.083	494	23.01
327	3.808	383	5.434	439	7.141	495	23.03 <<
328	3.835	384	5.475	440	7.201	496	23.00
329	3.863	385	5.516	441	7.265	497	22.95
330	3.890	386	5.557	442	7.331	498	22.86
331	3.917	387	5.598	443	7.400	499	22.74
332	3.945	388	5.638	444	7.472	500	22.59
333	3.971	389	5.679	445	7.547	501	22.40
334	3.998	390	5.718	446	7.625	502	22.20
335	4.025	391	5.758	447	7.705	503	21.98
336	4.051	392	5.796	448	7.790	504	21.75
337	4.077	393	5.832	449	7.877	505	21.50
338	4.103	394	5.868	450	7.967	506	21.25
339	4.128	395	5.902	451	8.076	507	20.97
340	4.154	396	5.935	452	8.206	508	20.69
341	4.179	397	5.966	453	8.355	509	20.39
342	4.204	398	5.996	454	8.526	510	20.09
343	4.229	399	6.025	455	8.718	511	19.78
344	4.253	400	6.053	456	8.932	512	19.46

Continues on next page...

Hydrograph Discharge Table

Time (min	Outflow cfs)	Time (min	Outflow cfs)	Time (min	Outflow cfs)	Time (min	Outflow cfs)
513	19.13	569	8.680	625	6.622	681	5.780
514	18.80	570	8.608	626	6.599	682	5.766
515	18.47	571	8.534	627	6.577	683	5.752
516	18.13	572	8.462	628	6.555	684	5.737
517	17.78	573	8.391	629	6.533	685	5.723
518	17.43	574	8.320	630	6.511	686	5.708
519	17.09	575	8.251	631	6.490	687	5.694
520	16.75	576	8.184	632	6.469	688	5.679
521	16.42	577	8.117	633	6.449	689	5.664
522	16.09	578	8.051	634	6.429	690	5.648
523	15.77	579	7.988	635	6.410	691	5.633
524	15.46	580	7.928	636	6.391	692	5.617
525	15.16	581	7.869	637	6.373	693	5.601
526	14.87	582	7.813	638	6.355	694	5.584
527	14.58	583	7.759	639	6.336	695	5.567
528	14.31	584	7.707	640	6.318	696	5.550
529	14.04	585	7.656	641	6.301	697	5.533
530	13.78	586	7.608	642	6.284	698	5.516
531	13.54	587	7.562	643	6.267	699	5.498
532	13.30	588	7.517	644	6.252	700	5.480
533	13.07	589	7.475	645	6.237	701	5.463
534	12.84	590	7.434	646	6.222	702	5.445
535	12.62	591	7.395	647	6.208	703	5.427
536	12.41	592	7.361	648	6.194	704	5.409
537	12.21	593	7.329	649	6.181	705	5.391
538	12.02	594	7.298	650	6.168	706	5.373
539	11.84	595	7.268	651	6.156	707	5.355
540	11.66	596	7.238	652	6.144	708	5.337
541	11.49	597	7.210	653	6.132	709	5.319
542	11.33	598	7.182	654	6.119	710	5.301
543	11.18	599	7.155	655	6.107	711	5.283
544	11.03	600	7.129	656	6.095	712	5.265
545	10.90	601	7.107	657	6.083	713	5.247
546	10.77	602	7.085	658	6.070	714	5.230
547	10.65	603	7.064	659	6.058	715	5.213
548	10.54	604	7.043	660	6.045	716	5.197
549	10.43	605	7.023	661	6.033	717	5.180
550	10.32	606	7.003	662	6.020	718	5.164
551	10.22	607	6.983	663	6.008	719	5.149
552	10.11	608	6.964	664	5.995	720	5.134
553	10.01	609	6.943	665	5.982	721	5.119
554	9.918	610	6.924	666	5.970	722	5.104
555	9.823	611	6.904	667	5.957	723	5.090
556	9.730	612	6.885	668	5.944	724	5.076
557	9.639	613	6.865	669	5.932	725	5.063
558	9.550	614	6.846	670	5.920	726	5.050
559	9.462	615	6.827	671	5.908	727	5.038
560	9.376	616	6.808	672	5.896	728	5.026
561	9.291	617	6.789	673	5.884	729	5.014
562	9.210	618	6.770	674	5.872	730	5.003
563	9.131	619	6.751	675	5.859	731	4.993
564	9.053	620	6.732	676	5.846	732	4.983
565	8.977	621	6.713	677	5.833	733	4.973
566	8.901	622	6.690	678	5.820	734	4.964
567	8.826	623	6.667	679	5.807	735	4.956
568	8.753	624	6.644	680	5.793	736	4.948

Continues on next page...

Hydrograph Discharge Table

Time (min	Outflow cfs)	Time (min	Outflow cfs)	Time (min	Outflow cfs)	Time (min	Outflow cfs)
737	4.941	793	4.756	849	4.484	905	4.333
738	4.934	794	4.753	850	4.479	906	4.330
739	4.927	795	4.751	851	4.474	907	4.327
740	4.922	796	4.749	852	4.470	908	4.324
741	4.917	797	4.747	853	4.466	909	4.321
742	4.912	798	4.745	854	4.461	910	4.318
743	4.908	799	4.743	855	4.458	911	4.315
744	4.905	800	4.742	856	4.454	912	4.312
745	4.902	801	4.740	857	4.451	913	4.309
746	4.900	802	4.739	858	4.448	914	4.306
747	4.898	803	4.737	859	4.445	915	4.302
748	4.897	804	4.734	860	4.442	916	4.299
749	4.897	805	4.731	861	4.439	917	4.296
750	4.897	806	4.728	862	4.437	918	4.293
751	4.897	807	4.725	863	4.434	919	4.290
752	4.898	808	4.721	864	4.432	920	4.287
753	4.898	809	4.717	865	4.429	921	4.284
754	4.899	810	4.713	866	4.427	922	4.281
755	4.899	811	4.708	867	4.425	923	4.278
756	4.900	812	4.704	868	4.423	924	4.275
757	4.900	813	4.699	869	4.420	925	4.271
758	4.901	814	4.695	870	4.418	926	4.268
759	4.901	815	4.690	871	4.416	927	4.265
760	4.900	816	4.685	872	4.414	928	4.262
761	4.900	817	4.680	873	4.412	929	4.259
762	4.899	818	4.675	874	4.410	930	4.256
763	4.897	819	4.670	875	4.408	931	4.253
764	4.895	820	4.665	876	4.405	932	4.250
765	4.893	821	4.660	877	4.403	933	4.247
766	4.890	822	4.654	878	4.401	934	4.243
767	4.887	823	4.648	879	4.399	935	4.240
768	4.883	824	4.643	880	4.397	936	4.237
769	4.878	825	4.637	881	4.395	937	4.234
770	4.873	826	4.630	882	4.393	938	4.231
771	4.867	827	4.624	883	4.390	939	4.228
772	4.861	828	4.618	884	4.388	940	4.225
773	4.855	829	4.612	885	4.386	941	4.222
774	4.848	830	4.605	886	4.384	942	4.219
775	4.842	831	4.599	887	4.381	943	4.215
776	4.836	832	4.592	888	4.379	944	4.212
777	4.829	833	4.585	889	4.377	945	4.209
778	4.823	834	4.579	890	4.374	946	4.206
779	4.816	835	4.572	891	4.372	947	4.203
780	4.810	836	4.565	892	4.369	948	4.200
781	4.804	837	4.559	893	4.367	949	4.197
782	4.798	838	4.552	894	4.364	950	4.194
783	4.793	839	4.545	895	4.361	951	4.191
784	4.788	840	4.539	896	4.359	952	4.187
785	4.783	841	4.532	897	4.356	953	4.184
786	4.779	842	4.526	898	4.353	954	4.181
787	4.775	843	4.519	899	4.351	955	4.178
788	4.771	844	4.513	900	4.348	956	4.175
789	4.767	845	4.507	901	4.345	957	4.172
790	4.764	846	4.501	902	4.342	958	4.169
791	4.761	847	4.495	903	4.339	959	4.165
792	4.758	848	4.490	904	4.336	960	4.162

Continues on next page...

Hydrograph Discharge Table

Time (min)	Outflow (cfs)	Time (min)	Outflow (cfs)	Time (min)	Outflow (cfs)	Time (min)	Outflow (cfs)
961	4.159	1017	3.983	1073	3.804	1129	3.624
962	4.156	1018	3.979	1074	3.801	1130	3.620
963	4.153	1019	3.976	1075	3.798	1131	3.617
964	4.150	1020	3.973	1076	3.794	1132	3.614
965	4.147	1021	3.970	1077	3.791	1133	3.611
966	4.144	1022	3.967	1078	3.788	1134	3.607
967	4.140	1023	3.964	1079	3.785	1135	3.604
968	4.137	1024	3.960	1080	3.782	1136	3.601
969	4.134	1025	3.957	1081	3.778	1137	3.598
970	4.131	1026	3.954	1082	3.775	1138	3.594
971	4.128	1027	3.951	1083	3.772	1139	3.591
972	4.125	1028	3.948	1084	3.769	1140	3.588
973	4.122	1029	3.945	1085	3.765	1141	3.585
974	4.118	1030	3.941	1086	3.762	1142	3.582
975	4.115	1031	3.938	1087	3.759	1143	3.578
976	4.112	1032	3.935	1088	3.756	1144	3.575
977	4.109	1033	3.932	1089	3.753	1145	3.572
978	4.106	1034	3.929	1090	3.749	1146	3.569
979	4.103	1035	3.925	1091	3.746	1147	3.565
980	4.100	1036	3.922	1092	3.743	1148	3.562
981	4.096	1037	3.919	1093	3.740	1149	3.559
982	4.093	1038	3.916	1094	3.737	1150	3.556
983	4.090	1039	3.913	1095	3.733	1151	3.552
984	4.087	1040	3.910	1096	3.730	1152	3.549
985	4.084	1041	3.906	1097	3.727	1153	3.546
986	4.081	1042	3.903	1098	3.724	1154	3.543
987	4.078	1043	3.900	1099	3.720	1155	3.539
988	4.074	1044	3.897	1100	3.717	1156	3.536
989	4.071	1045	3.894	1101	3.714	1157	3.533
990	4.068	1046	3.890	1102	3.711	1158	3.530
991	4.065	1047	3.887	1103	3.708	1159	3.526
992	4.062	1048	3.884	1104	3.704	1160	3.523
993	4.059	1049	3.881	1105	3.701	1161	3.520
994	4.055	1050	3.878	1106	3.698	1162	3.517
995	4.052	1051	3.874	1107	3.695	1163	3.513
996	4.049	1052	3.871	1108	3.691	1164	3.510
997	4.046	1053	3.868	1109	3.688	1165	3.507
998	4.043	1054	3.865	1110	3.685	1166	3.504
999	4.040	1055	3.862	1111	3.682	1167	3.500
1000	4.036	1056	3.858	1112	3.679	1168	3.497
1001	4.033	1057	3.855	1113	3.675	1169	3.494
1002	4.030	1058	3.852	1114	3.672	1170	3.491
1003	4.027	1059	3.849	1115	3.669	1171	3.487
1004	4.024	1060	3.846	1116	3.666	1172	3.484
1005	4.021	1061	3.842	1117	3.662	1173	3.481
1006	4.018	1062	3.839	1118	3.659	1174	3.478
1007	4.014	1063	3.836	1119	3.656	1175	3.474
1008	4.011	1064	3.833	1120	3.653	1176	3.471
1009	4.008	1065	3.830	1121	3.649	1177	3.468
1010	4.005	1066	3.826	1122	3.646	1178	3.465
1011	4.002	1067	3.823	1123	3.643	1179	3.461
1012	3.999	1068	3.820	1124	3.640	1180	3.458
1013	3.995	1069	3.817	1125	3.637	1181	3.455
1014	3.992	1070	3.814	1126	3.633	1182	3.452
1015	3.989	1071	3.810	1127	3.630	1183	3.448
1016	3.986	1072	3.807	1128	3.627	1184	3.445

Continues on next page...

Hydrograph Discharge Table

Time (min)	Outflow (cfs)	Time (min)	Outflow (cfs)	Time (min)	Outflow (cfs)	Time (min)	Outflow (cfs)
1185	3.442	1241	3.259	1297	3.075	1353	2.889
1186	3.439	1242	3.255	1298	3.071	1354	2.886
1187	3.435	1243	3.252	1299	3.068	1355	2.883
1188	3.432	1244	3.249	1300	3.065	1356	2.880
1189	3.429	1245	3.246	1301	3.061	1357	2.876
1190	3.425	1246	3.242	1302	3.058	1358	2.873
1191	3.422	1247	3.239	1303	3.055	1359	2.870
1192	3.419	1248	3.236	1304	3.051	1360	2.866
1193	3.416	1249	3.232	1305	3.048	1361	2.863
1194	3.412	1250	3.229	1306	3.045	1362	2.860
1195	3.409	1251	3.226	1307	3.042	1363	2.856
1196	3.406	1252	3.223	1308	3.038	1364	2.853
1197	3.403	1253	3.219	1309	3.035	1365	2.850
1198	3.399	1254	3.216	1310	3.032	1366	2.846
1199	3.396	1255	3.213	1311	3.028	1367	2.843
1200	3.393	1256	3.209	1312	3.025	1368	2.840
1201	3.390	1257	3.206	1313	3.022	1369	2.836
1202	3.386	1258	3.203	1314	3.018	1370	2.833
1203	3.383	1259	3.200	1315	3.015	1371	2.830
1204	3.380	1260	3.196	1316	3.012	1372	2.827
1205	3.377	1261	3.193	1317	3.009	1373	2.823
1206	3.373	1262	3.190	1318	3.005	1374	2.820
1207	3.370	1263	3.186	1319	3.002	1375	2.817
1208	3.367	1264	3.183	1320	2.999	1376	2.813
1209	3.363	1265	3.180	1321	2.995	1377	2.810
1210	3.360	1266	3.177	1322	2.992	1378	2.807
1211	3.357	1267	3.173	1323	2.989	1379	2.803
1212	3.354	1268	3.170	1324	2.985	1380	2.800
1213	3.350	1269	3.167	1325	2.982	1381	2.797
1214	3.347	1270	3.163	1326	2.979	1382	2.793
1215	3.344	1271	3.160	1327	2.975	1383	2.790
1216	3.341	1272	3.157	1328	2.972	1384	2.787
1217	3.337	1273	3.154	1329	2.969	1385	2.783
1218	3.334	1274	3.150	1330	2.966	1386	2.780
1219	3.331	1275	3.147	1331	2.962	1387	2.777
1220	3.327	1276	3.144	1332	2.959	1388	2.773
1221	3.324	1277	3.140	1333	2.956	1389	2.770
1222	3.321	1278	3.137	1334	2.952	1390	2.767
1223	3.318	1279	3.134	1335	2.949	1391	2.763
1224	3.314	1280	3.131	1336	2.946	1392	2.760
1225	3.311	1281	3.127	1337	2.942	1393	2.757
1226	3.308	1282	3.124	1338	2.939	1394	2.753
1227	3.305	1283	3.121	1339	2.936	1395	2.750
1228	3.301	1284	3.117	1340	2.933	1396	2.747
1229	3.298	1285	3.114	1341	2.929	1397	2.744
1230	3.295	1286	3.111	1342	2.926	1398	2.740
1231	3.291	1287	3.107	1343	2.923	1399	2.737
1232	3.288	1288	3.104	1344	2.919	1400	2.734
1233	3.285	1289	3.101	1345	2.916	1401	2.730
1234	3.282	1290	3.098	1346	2.913	1402	2.727
1235	3.278	1291	3.094	1347	2.909	1403	2.724
1236	3.275	1292	3.091	1348	2.906	1404	2.720
1237	3.272	1293	3.088	1349	2.903	1405	2.717
1238	3.269	1294	3.084	1350	2.899	1406	2.714
1239	3.265	1295	3.081	1351	2.896	1407	2.710
1240	3.262	1296	3.078	1352	2.893	1408	2.707

Continues on next page...

Developed site storm event

Hydrograph Discharge Table

Time (min	Outflow cfs)	Time (min	Outflow cfs)
1409	2.704	1465	1.441
1410	2.700	1466	1.374
1411	2.697	1467	1.308
1412	2.694	1468	1.243
1413	2.690	1469	1.181
1414	2.687	1470	1.120
1415	2.684	1471	1.060
1416	2.680	1472	1.002
1417	2.677	1473	0.946
1418	2.674	1474	0.892
1419	2.670	1475	0.839
1420	2.667	1476	0.788
1421	2.664	1477	0.738
1422	2.660	1478	0.690
1423	2.657	1479	0.644
1424	2.654	1480	0.599
1425	2.650	1481	0.556
1426	2.647	1482	0.515
1427	2.644	1483	0.475
1428	2.640	1484	0.437
1429	2.637	1485	0.400
1430	2.634	1486	0.365
1431	2.630	1487	0.332
1432	2.627	1488	0.300
1433	2.624	1489	0.270
1434	2.620	1490	0.242
1435	2.617		
1436	2.614	*...End*	
1437	2.610		
1438	2.607		
1439	2.604		
1440	2.600		
1441	2.594		
1442	2.583		
1443	2.570		
1444	2.552		
1445	2.531		
1446	2.507		
1447	2.479		
1448	2.448		
1449	2.413		
1450	2.375		
1451	2.334		
1452	2.289		
1453	2.240		
1454	2.188		
1455	2.133		
1456	2.074		
1457	2.012		
1458	1.946		
1459	1.877		
1460	1.804		
1461	1.728		
1462	1.654		
1463	1.581		
1464	1.511		

Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066 Thursday, Jul 2, 2009

Hyd. No. 2

Detention pond outflow

Hydrograph type	= Reservoir	Peak discharge	= 7.458 cfs
Storm frequency	= 100 yrs	Time to peak	= 589 min
Time interval	= 1 min	Hyd. volume	= 253,870 cuft
Inflow hyd. No.	= 1 - Developed site storm event	Reservoir name	= Detention Pond
Max. Elevation	= 63.02 ft	Max. Storage	= 161,345 cuft

Storage Indication method used.

Hydrograph Discharge Table

(Printed values >= 1.00% of Qp.)

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
528	14.31	62.72	0.246	-----	-----	-----	0.246	-----	-----	-----	-----	0.246
529	14.04	62.73	0.438	-----	-----	-----	0.437	-----	-----	-----	-----	0.437
530	13.78	62.75	0.623	-----	-----	-----	0.622	-----	-----	-----	-----	0.622
531	13.54	62.76	0.803	-----	-----	-----	0.801	-----	-----	-----	-----	0.801
532	13.30	62.77	0.976	-----	-----	-----	0.974	-----	-----	-----	-----	0.974
533	13.07	62.79	1.144	-----	-----	-----	1.142	-----	-----	-----	-----	1.142
534	12.84	62.80	1.307	-----	-----	-----	1.304	-----	-----	-----	-----	1.304
535	12.62	62.81	1.577	-----	-----	-----	1.575	-----	-----	-----	-----	1.575
536	12.41	62.82	1.850	-----	-----	-----	1.848	-----	-----	-----	-----	1.848
537	12.21	62.83	2.111	-----	-----	-----	2.109	-----	-----	-----	-----	2.109
538	12.02	62.84	2.361	-----	-----	-----	2.359	-----	-----	-----	-----	2.359
539	11.84	62.85	2.600	-----	-----	-----	2.598	-----	-----	-----	-----	2.598
540	11.66	62.86	2.829	-----	-----	-----	2.826	-----	-----	-----	-----	2.826
541	11.49	62.87	3.047	-----	-----	-----	3.045	-----	-----	-----	-----	3.045
542	11.33	62.88	3.256	-----	-----	-----	3.254	-----	-----	-----	-----	3.254
543	11.18	62.89	3.455	-----	-----	-----	3.454	-----	-----	-----	-----	3.454
544	11.03	62.90	3.646	-----	-----	-----	3.645	-----	-----	-----	-----	3.645
545	10.90	62.90	3.854	-----	-----	-----	3.853	-----	-----	-----	-----	3.853
546	10.77	62.91	4.079	-----	-----	-----	4.077	-----	-----	-----	-----	4.077
547	10.65	62.92	4.293	-----	-----	-----	4.291	-----	-----	-----	-----	4.291
548	10.54	62.92	4.495	-----	-----	-----	4.494	-----	-----	-----	-----	4.494
549	10.43	62.93	4.688	-----	-----	-----	4.687	-----	-----	-----	-----	4.687
550	10.32	62.94	4.871	-----	-----	-----	4.870	-----	-----	-----	-----	4.870
551	10.22	62.94	5.045	-----	-----	-----	5.044	-----	-----	-----	-----	5.044
552	10.11	62.95	5.210	-----	-----	-----	5.209	-----	-----	-----	-----	5.209
553	10.01	62.95	5.366	-----	-----	-----	5.365	-----	-----	-----	-----	5.365
554	9.918	62.96	5.514	-----	-----	-----	5.514	-----	-----	-----	-----	5.514
555	9.823	62.96	5.655	-----	-----	-----	5.654	-----	-----	-----	-----	5.654
556	9.730	62.97	5.788	-----	-----	-----	5.787	-----	-----	-----	-----	5.787
557	9.639	62.97	5.913	-----	-----	-----	5.912	-----	-----	-----	-----	5.912
558	9.550	62.97	6.032	-----	-----	-----	6.031	-----	-----	-----	-----	6.031
559	9.462	62.98	6.144	-----	-----	-----	6.143	-----	-----	-----	-----	6.143
560	9.376	62.98	6.249	-----	-----	-----	6.248	-----	-----	-----	-----	6.248
561	9.291	62.98	6.348	-----	-----	-----	6.348	-----	-----	-----	-----	6.348
562	9.210	62.99	6.442	-----	-----	-----	6.441	-----	-----	-----	-----	6.441
563	9.131	62.99	6.530	-----	-----	-----	6.529	-----	-----	-----	-----	6.529
564	9.053	62.99	6.612	-----	-----	-----	6.612	-----	-----	-----	-----	6.612
565	8.977	62.99	6.690	-----	-----	-----	6.689	-----	-----	-----	-----	6.689
566	8.901	63.00	6.762	-----	-----	-----	6.762	-----	-----	-----	-----	6.762
567	8.826	63.00	6.830	-----	-----	-----	6.829	-----	-----	-----	-----	6.829
568	8.753	63.00	6.894	-----	-----	-----	6.894	-----	-----	-----	-----	6.894
569	8.680	63.00	6.957	-----	-----	-----	6.957	-----	-----	-----	-----	6.957

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
570	8.608	63.00	7.016	-----	-----	-----	7.015	-----	-----	-----	-----	7.015
571	8.534	63.01	7.069	-----	-----	-----	7.069	-----	-----	-----	-----	7.069
572	8.462	63.01	7.119	-----	-----	-----	7.118	-----	-----	-----	-----	7.118
573	8.391	63.01	7.164	-----	-----	-----	7.163	-----	-----	-----	-----	7.163
574	8.320	63.01	7.205	-----	-----	-----	7.205	-----	-----	-----	-----	7.205
575	8.251	63.01	7.242	-----	-----	-----	7.242	-----	-----	-----	-----	7.242
576	8.184	63.01	7.276	-----	-----	-----	7.276	-----	-----	-----	-----	7.276
577	8.117	63.01	7.306	-----	-----	-----	7.306	-----	-----	-----	-----	7.306
578	8.051	63.01	7.333	-----	-----	-----	7.333	-----	-----	-----	-----	7.333
579	7.988	63.01	7.357	-----	-----	-----	7.356	-----	-----	-----	-----	7.356
580	7.928	63.01	7.378	-----	-----	-----	7.377	-----	-----	-----	-----	7.377
581	7.869	63.01	7.396	-----	-----	-----	7.395	-----	-----	-----	-----	7.395
582	7.813	63.01	7.411	-----	-----	-----	7.411	-----	-----	-----	-----	7.411
583	7.759	63.01	7.424	-----	-----	-----	7.424	-----	-----	-----	-----	7.424
584	7.707	63.02	7.435	-----	-----	-----	7.434	-----	-----	-----	-----	7.434
585	7.656	63.02	7.443	-----	-----	-----	7.443	-----	-----	-----	-----	7.443
586	7.608	63.02	7.450	-----	-----	-----	7.449	-----	-----	-----	-----	7.449
587	7.562	63.02	7.454	-----	-----	-----	7.454	-----	-----	-----	-----	7.454
588	7.517	63.02	7.457	-----	-----	-----	7.457	-----	-----	-----	-----	7.457
589	7.475	63.02 <<	7.459	-----	-----	-----	7.458	-----	-----	-----	-----	7.458 <<
590	7.434	63.02	7.459	-----	-----	-----	7.458	-----	-----	-----	-----	7.458
591	7.395	63.02	7.457	-----	-----	-----	7.457	-----	-----	-----	-----	7.457
592	7.361	63.02	7.454	-----	-----	-----	7.454	-----	-----	-----	-----	7.454
593	7.329	63.02	7.451	-----	-----	-----	7.450	-----	-----	-----	-----	7.450
594	7.298	63.02	7.446	-----	-----	-----	7.445	-----	-----	-----	-----	7.445
595	7.268	63.02	7.440	-----	-----	-----	7.440	-----	-----	-----	-----	7.440
596	7.238	63.02	7.434	-----	-----	-----	7.433	-----	-----	-----	-----	7.433
597	7.210	63.01	7.427	-----	-----	-----	7.426	-----	-----	-----	-----	7.426
598	7.182	63.01	7.419	-----	-----	-----	7.418	-----	-----	-----	-----	7.418
599	7.155	63.01	7.410	-----	-----	-----	7.410	-----	-----	-----	-----	7.410
600	7.129	63.01	7.401	-----	-----	-----	7.400	-----	-----	-----	-----	7.400
601	7.107	63.01	7.391	-----	-----	-----	7.391	-----	-----	-----	-----	7.391
602	7.085	63.01	7.381	-----	-----	-----	7.380	-----	-----	-----	-----	7.380
603	7.064	63.01	7.370	-----	-----	-----	7.370	-----	-----	-----	-----	7.370
604	7.043	63.01	7.359	-----	-----	-----	7.359	-----	-----	-----	-----	7.359
605	7.023	63.01	7.348	-----	-----	-----	7.348	-----	-----	-----	-----	7.348
606	7.003	63.01	7.336	-----	-----	-----	7.336	-----	-----	-----	-----	7.336
607	6.983	63.01	7.325	-----	-----	-----	7.324	-----	-----	-----	-----	7.324
608	6.964	63.01	7.313	-----	-----	-----	7.312	-----	-----	-----	-----	7.312
609	6.943	63.01	7.300	-----	-----	-----	7.300	-----	-----	-----	-----	7.300
610	6.924	63.01	7.287	-----	-----	-----	7.287	-----	-----	-----	-----	7.287
611	6.904	63.01	7.275	-----	-----	-----	7.274	-----	-----	-----	-----	7.274
612	6.885	63.01	7.261	-----	-----	-----	7.261	-----	-----	-----	-----	7.261
613	6.865	63.01	7.248	-----	-----	-----	7.248	-----	-----	-----	-----	7.248
614	6.846	63.01	7.235	-----	-----	-----	7.234	-----	-----	-----	-----	7.234
615	6.827	63.01	7.221	-----	-----	-----	7.220	-----	-----	-----	-----	7.220
616	6.808	63.01	7.207	-----	-----	-----	7.206	-----	-----	-----	-----	7.207
617	6.789	63.01	7.193	-----	-----	-----	7.192	-----	-----	-----	-----	7.192
618	6.770	63.01	7.179	-----	-----	-----	7.178	-----	-----	-----	-----	7.178
619	6.751	63.01	7.164	-----	-----	-----	7.164	-----	-----	-----	-----	7.164
620	6.732	63.01	7.150	-----	-----	-----	7.149	-----	-----	-----	-----	7.149
621	6.713	63.01	7.135	-----	-----	-----	7.134	-----	-----	-----	-----	7.134
622	6.690	63.01	7.120	-----	-----	-----	7.119	-----	-----	-----	-----	7.120
623	6.667	63.01	7.105	-----	-----	-----	7.104	-----	-----	-----	-----	7.104
624	6.644	63.01	7.089	-----	-----	-----	7.089	-----	-----	-----	-----	7.089
625	6.622	63.01	7.073	-----	-----	-----	7.073	-----	-----	-----	-----	7.073

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
626	6.599	63.00	7.057	-----	-----	-----	7.057	-----	-----	-----	-----	7.057
627	6.577	63.00	7.041	-----	-----	-----	7.041	-----	-----	-----	-----	7.041
628	6.555	63.00	7.025	-----	-----	-----	7.024	-----	-----	-----	-----	7.024
629	6.533	63.00	7.008	-----	-----	-----	7.008	-----	-----	-----	-----	7.008
630	6.511	63.00	6.992	-----	-----	-----	6.991	-----	-----	-----	-----	6.991
631	6.490	63.00	6.975	-----	-----	-----	6.974	-----	-----	-----	-----	6.974
632	6.469	63.00	6.957	-----	-----	-----	6.957	-----	-----	-----	-----	6.957
633	6.449	63.00	6.940	-----	-----	-----	6.940	-----	-----	-----	-----	6.940
634	6.429	63.00	6.923	-----	-----	-----	6.923	-----	-----	-----	-----	6.923
635	6.410	63.00	6.906	-----	-----	-----	6.905	-----	-----	-----	-----	6.905
636	6.391	63.00	6.888	-----	-----	-----	6.888	-----	-----	-----	-----	6.888
637	6.373	63.00	6.871	-----	-----	-----	6.870	-----	-----	-----	-----	6.871
638	6.355	63.00	6.855	-----	-----	-----	6.854	-----	-----	-----	-----	6.854
639	6.336	63.00	6.838	-----	-----	-----	6.838	-----	-----	-----	-----	6.838
640	6.318	63.00	6.822	-----	-----	-----	6.821	-----	-----	-----	-----	6.821
641	6.301	63.00	6.805	-----	-----	-----	6.805	-----	-----	-----	-----	6.805
642	6.284	63.00	6.789	-----	-----	-----	6.788	-----	-----	-----	-----	6.788
643	6.267	63.00	6.772	-----	-----	-----	6.772	-----	-----	-----	-----	6.772
644	6.252	63.00	6.756	-----	-----	-----	6.755	-----	-----	-----	-----	6.755
645	6.237	63.00	6.739	-----	-----	-----	6.739	-----	-----	-----	-----	6.739
646	6.222	63.00	6.723	-----	-----	-----	6.722	-----	-----	-----	-----	6.722
647	6.208	62.99	6.707	-----	-----	-----	6.706	-----	-----	-----	-----	6.706
648	6.194	62.99	6.690	-----	-----	-----	6.690	-----	-----	-----	-----	6.690
649	6.181	62.99	6.674	-----	-----	-----	6.674	-----	-----	-----	-----	6.674
650	6.168	62.99	6.658	-----	-----	-----	6.658	-----	-----	-----	-----	6.658
651	6.156	62.99	6.642	-----	-----	-----	6.642	-----	-----	-----	-----	6.642
652	6.144	62.99	6.626	-----	-----	-----	6.626	-----	-----	-----	-----	6.626
653	6.132	62.99	6.611	-----	-----	-----	6.610	-----	-----	-----	-----	6.610
654	6.119	62.99	6.595	-----	-----	-----	6.594	-----	-----	-----	-----	6.594
655	6.107	62.99	6.579	-----	-----	-----	6.579	-----	-----	-----	-----	6.579
656	6.095	62.99	6.564	-----	-----	-----	6.564	-----	-----	-----	-----	6.564
657	6.083	62.99	6.549	-----	-----	-----	6.548	-----	-----	-----	-----	6.548
658	6.070	62.99	6.533	-----	-----	-----	6.533	-----	-----	-----	-----	6.533
659	6.058	62.99	6.518	-----	-----	-----	6.518	-----	-----	-----	-----	6.518
660	6.045	62.99	6.503	-----	-----	-----	6.503	-----	-----	-----	-----	6.503
661	6.033	62.99	6.488	-----	-----	-----	6.488	-----	-----	-----	-----	6.488
662	6.020	62.99	6.474	-----	-----	-----	6.473	-----	-----	-----	-----	6.473
663	6.008	62.99	6.459	-----	-----	-----	6.458	-----	-----	-----	-----	6.458
664	5.995	62.99	6.444	-----	-----	-----	6.444	-----	-----	-----	-----	6.444
665	5.982	62.99	6.429	-----	-----	-----	6.429	-----	-----	-----	-----	6.429
666	5.970	62.99	6.415	-----	-----	-----	6.414	-----	-----	-----	-----	6.414
667	5.957	62.98	6.400	-----	-----	-----	6.400	-----	-----	-----	-----	6.400
668	5.944	62.98	6.386	-----	-----	-----	6.385	-----	-----	-----	-----	6.385
669	5.932	62.98	6.371	-----	-----	-----	6.371	-----	-----	-----	-----	6.371
670	5.920	62.98	6.357	-----	-----	-----	6.357	-----	-----	-----	-----	6.357
671	5.908	62.98	6.343	-----	-----	-----	6.342	-----	-----	-----	-----	6.342
672	5.896	62.98	6.329	-----	-----	-----	6.328	-----	-----	-----	-----	6.328
673	5.884	62.98	6.315	-----	-----	-----	6.314	-----	-----	-----	-----	6.314
674	5.872	62.98	6.301	-----	-----	-----	6.300	-----	-----	-----	-----	6.300
675	5.859	62.98	6.287	-----	-----	-----	6.286	-----	-----	-----	-----	6.286
676	5.846	62.98	6.273	-----	-----	-----	6.272	-----	-----	-----	-----	6.272
677	5.833	62.98	6.259	-----	-----	-----	6.258	-----	-----	-----	-----	6.258
678	5.820	62.98	6.245	-----	-----	-----	6.244	-----	-----	-----	-----	6.244
679	5.807	62.98	6.231	-----	-----	-----	6.230	-----	-----	-----	-----	6.230
680	5.793	62.98	6.217	-----	-----	-----	6.216	-----	-----	-----	-----	6.216
681	5.780	62.98	6.203	-----	-----	-----	6.203	-----	-----	-----	-----	6.203

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
682	5.766	62.98	6.189	-----	-----	-----	6.189	-----	-----	-----	-----	6.189
683	5.752	62.98	6.176	-----	-----	-----	6.175	-----	-----	-----	-----	6.175
684	5.737	62.98	6.162	-----	-----	-----	6.161	-----	-----	-----	-----	6.161
685	5.723	62.98	6.148	-----	-----	-----	6.147	-----	-----	-----	-----	6.147
686	5.708	62.98	6.134	-----	-----	-----	6.133	-----	-----	-----	-----	6.133
687	5.694	62.98	6.120	-----	-----	-----	6.119	-----	-----	-----	-----	6.119
688	5.679	62.98	6.106	-----	-----	-----	6.105	-----	-----	-----	-----	6.105
689	5.664	62.98	6.092	-----	-----	-----	6.091	-----	-----	-----	-----	6.091
690	5.648	62.97	6.078	-----	-----	-----	6.077	-----	-----	-----	-----	6.077
691	5.633	62.97	6.064	-----	-----	-----	6.063	-----	-----	-----	-----	6.063
692	5.617	62.97	6.050	-----	-----	-----	6.049	-----	-----	-----	-----	6.049
693	5.601	62.97	6.036	-----	-----	-----	6.035	-----	-----	-----	-----	6.035
694	5.584	62.97	6.021	-----	-----	-----	6.021	-----	-----	-----	-----	6.021
695	5.567	62.97	6.007	-----	-----	-----	6.006	-----	-----	-----	-----	6.006
696	5.550	62.97	5.993	-----	-----	-----	5.992	-----	-----	-----	-----	5.992
697	5.533	62.97	5.978	-----	-----	-----	5.977	-----	-----	-----	-----	5.977
698	5.516	62.97	5.964	-----	-----	-----	5.963	-----	-----	-----	-----	5.963
699	5.498	62.97	5.949	-----	-----	-----	5.948	-----	-----	-----	-----	5.948
700	5.480	62.97	5.934	-----	-----	-----	5.933	-----	-----	-----	-----	5.933
701	5.463	62.97	5.919	-----	-----	-----	5.918	-----	-----	-----	-----	5.918
702	5.445	62.97	5.904	-----	-----	-----	5.903	-----	-----	-----	-----	5.903
703	5.427	62.97	5.889	-----	-----	-----	5.888	-----	-----	-----	-----	5.888
704	5.409	62.97	5.874	-----	-----	-----	5.873	-----	-----	-----	-----	5.873
705	5.391	62.97	5.859	-----	-----	-----	5.858	-----	-----	-----	-----	5.858
706	5.373	62.97	5.843	-----	-----	-----	5.843	-----	-----	-----	-----	5.843
707	5.355	62.97	5.828	-----	-----	-----	5.827	-----	-----	-----	-----	5.827
708	5.337	62.97	5.813	-----	-----	-----	5.812	-----	-----	-----	-----	5.812
709	5.319	62.97	5.797	-----	-----	-----	5.796	-----	-----	-----	-----	5.796
710	5.301	62.97	5.781	-----	-----	-----	5.780	-----	-----	-----	-----	5.780
711	5.283	62.96	5.766	-----	-----	-----	5.765	-----	-----	-----	-----	5.765
712	5.265	62.96	5.750	-----	-----	-----	5.749	-----	-----	-----	-----	5.749
713	5.247	62.96	5.734	-----	-----	-----	5.733	-----	-----	-----	-----	5.733
714	5.230	62.96	5.718	-----	-----	-----	5.717	-----	-----	-----	-----	5.717
715	5.213	62.96	5.702	-----	-----	-----	5.701	-----	-----	-----	-----	5.701
716	5.197	62.96	5.686	-----	-----	-----	5.685	-----	-----	-----	-----	5.685
717	5.180	62.96	5.670	-----	-----	-----	5.669	-----	-----	-----	-----	5.669
718	5.164	62.96	5.654	-----	-----	-----	5.653	-----	-----	-----	-----	5.653
719	5.149	62.96	5.638	-----	-----	-----	5.637	-----	-----	-----	-----	5.637
720	5.134	62.96	5.622	-----	-----	-----	5.621	-----	-----	-----	-----	5.621
721	5.119	62.96	5.606	-----	-----	-----	5.605	-----	-----	-----	-----	5.605
722	5.104	62.96	5.590	-----	-----	-----	5.589	-----	-----	-----	-----	5.589
723	5.090	62.96	5.574	-----	-----	-----	5.573	-----	-----	-----	-----	5.573
724	5.076	62.96	5.559	-----	-----	-----	5.558	-----	-----	-----	-----	5.558
725	5.063	62.96	5.543	-----	-----	-----	5.542	-----	-----	-----	-----	5.542
726	5.050	62.96	5.527	-----	-----	-----	5.526	-----	-----	-----	-----	5.526
727	5.038	62.96	5.512	-----	-----	-----	5.511	-----	-----	-----	-----	5.511
728	5.026	62.96	5.496	-----	-----	-----	5.495	-----	-----	-----	-----	5.495
729	5.014	62.96	5.481	-----	-----	-----	5.480	-----	-----	-----	-----	5.480
730	5.003	62.96	5.466	-----	-----	-----	5.465	-----	-----	-----	-----	5.465
731	4.993	62.95	5.451	-----	-----	-----	5.450	-----	-----	-----	-----	5.450
732	4.983	62.95	5.436	-----	-----	-----	5.435	-----	-----	-----	-----	5.435
733	4.973	62.95	5.421	-----	-----	-----	5.420	-----	-----	-----	-----	5.420
734	4.964	62.95	5.407	-----	-----	-----	5.406	-----	-----	-----	-----	5.406
735	4.956	62.95	5.392	-----	-----	-----	5.391	-----	-----	-----	-----	5.391
736	4.948	62.95	5.378	-----	-----	-----	5.377	-----	-----	-----	-----	5.377
737	4.941	62.95	5.364	-----	-----	-----	5.363	-----	-----	-----	-----	5.363

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
738	4.934	62.95	5.351	-----	-----	-----	5.350	-----	-----	-----	-----	5.349
739	4.927	62.95	5.337	-----	-----	-----	5.336	-----	-----	-----	-----	5.336
740	4.922	62.95	5.324	-----	-----	-----	5.323	-----	-----	-----	-----	5.323
741	4.917	62.95	5.311	-----	-----	-----	5.310	-----	-----	-----	-----	5.310
742	4.912	62.95	5.298	-----	-----	-----	5.297	-----	-----	-----	-----	5.297
743	4.908	62.95	5.286	-----	-----	-----	5.285	-----	-----	-----	-----	5.285
744	4.905	62.95	5.273	-----	-----	-----	5.272	-----	-----	-----	-----	5.272
745	4.902	62.95	5.261	-----	-----	-----	5.260	-----	-----	-----	-----	5.260
746	4.900	62.95	5.250	-----	-----	-----	5.249	-----	-----	-----	-----	5.249
747	4.898	62.95	5.239	-----	-----	-----	5.238	-----	-----	-----	-----	5.238
748	4.897	62.95	5.228	-----	-----	-----	5.227	-----	-----	-----	-----	5.227
749	4.897	62.95	5.217	-----	-----	-----	5.216	-----	-----	-----	-----	5.216
750	4.897	62.95	5.207	-----	-----	-----	5.206	-----	-----	-----	-----	5.206
751	4.897	62.95	5.197	-----	-----	-----	5.196	-----	-----	-----	-----	5.196
752	4.898	62.95	5.187	-----	-----	-----	5.186	-----	-----	-----	-----	5.186
753	4.898	62.95	5.178	-----	-----	-----	5.177	-----	-----	-----	-----	5.177
754	4.899	62.95	5.169	-----	-----	-----	5.168	-----	-----	-----	-----	5.168
755	4.899	62.95	5.160	-----	-----	-----	5.159	-----	-----	-----	-----	5.159
756	4.900	62.95	5.152	-----	-----	-----	5.151	-----	-----	-----	-----	5.151
757	4.900	62.94	5.144	-----	-----	-----	5.143	-----	-----	-----	-----	5.143
758	4.901	62.94	5.136	-----	-----	-----	5.135	-----	-----	-----	-----	5.135
759	4.901	62.94	5.129	-----	-----	-----	5.127	-----	-----	-----	-----	5.127
760	4.900	62.94	5.121	-----	-----	-----	5.120	-----	-----	-----	-----	5.120
761	4.900	62.94	5.114	-----	-----	-----	5.113	-----	-----	-----	-----	5.113
762	4.899	62.94	5.107	-----	-----	-----	5.106	-----	-----	-----	-----	5.106
763	4.897	62.94	5.101	-----	-----	-----	5.099	-----	-----	-----	-----	5.099
764	4.895	62.94	5.094	-----	-----	-----	5.093	-----	-----	-----	-----	5.093
765	4.893	62.94	5.088	-----	-----	-----	5.086	-----	-----	-----	-----	5.087
766	4.890	62.94	5.081	-----	-----	-----	5.080	-----	-----	-----	-----	5.080
767	4.887	62.94	5.075	-----	-----	-----	5.074	-----	-----	-----	-----	5.074
768	4.883	62.94	5.069	-----	-----	-----	5.068	-----	-----	-----	-----	5.068
769	4.878	62.94	5.063	-----	-----	-----	5.062	-----	-----	-----	-----	5.062
770	4.873	62.94	5.057	-----	-----	-----	5.056	-----	-----	-----	-----	5.056
771	4.867	62.94	5.051	-----	-----	-----	5.050	-----	-----	-----	-----	5.050
772	4.861	62.94	5.045	-----	-----	-----	5.044	-----	-----	-----	-----	5.044
773	4.855	62.94	5.039	-----	-----	-----	5.038	-----	-----	-----	-----	5.038
774	4.848	62.94	5.033	-----	-----	-----	5.032	-----	-----	-----	-----	5.032
775	4.842	62.94	5.027	-----	-----	-----	5.026	-----	-----	-----	-----	5.026
776	4.836	62.94	5.021	-----	-----	-----	5.020	-----	-----	-----	-----	5.020
777	4.829	62.94	5.015	-----	-----	-----	5.014	-----	-----	-----	-----	5.014
778	4.823	62.94	5.009	-----	-----	-----	5.008	-----	-----	-----	-----	5.008
779	4.816	62.94	5.003	-----	-----	-----	5.002	-----	-----	-----	-----	5.002
780	4.810	62.94	4.997	-----	-----	-----	4.996	-----	-----	-----	-----	4.996
781	4.804	62.94	4.991	-----	-----	-----	4.990	-----	-----	-----	-----	4.990
782	4.798	62.94	4.985	-----	-----	-----	4.983	-----	-----	-----	-----	4.984
783	4.793	62.94	4.979	-----	-----	-----	4.978	-----	-----	-----	-----	4.977
784	4.788	62.94	4.973	-----	-----	-----	4.971	-----	-----	-----	-----	4.971
785	4.783	62.94	4.967	-----	-----	-----	4.965	-----	-----	-----	-----	4.965
786	4.779	62.94	4.961	-----	-----	-----	4.959	-----	-----	-----	-----	4.960
787	4.775	62.94	4.955	-----	-----	-----	4.954	-----	-----	-----	-----	4.954
788	4.771	62.94	4.949	-----	-----	-----	4.948	-----	-----	-----	-----	4.948
789	4.767	62.94	4.943	-----	-----	-----	4.942	-----	-----	-----	-----	4.942
790	4.764	62.94	4.938	-----	-----	-----	4.936	-----	-----	-----	-----	4.936
791	4.761	62.94	4.932	-----	-----	-----	4.931	-----	-----	-----	-----	4.931
792	4.758	62.94	4.927	-----	-----	-----	4.925	-----	-----	-----	-----	4.925
793	4.756	62.94	4.921	-----	-----	-----	4.920	-----	-----	-----	-----	4.920

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
794	4.753	62.94	4.916	-----	-----	-----	4.915	-----	-----	-----	-----	4.915
795	4.751	62.94	4.911	-----	-----	-----	4.909	-----	-----	-----	-----	4.909
796	4.749	62.94	4.905	-----	-----	-----	4.904	-----	-----	-----	-----	4.904
797	4.747	62.94	4.900	-----	-----	-----	4.899	-----	-----	-----	-----	4.899
798	4.745	62.94	4.895	-----	-----	-----	4.894	-----	-----	-----	-----	4.894
799	4.743	62.94	4.891	-----	-----	-----	4.889	-----	-----	-----	-----	4.889
800	4.742	62.94	4.886	-----	-----	-----	4.885	-----	-----	-----	-----	4.885
801	4.740	62.94	4.881	-----	-----	-----	4.880	-----	-----	-----	-----	4.880
802	4.739	62.94	4.877	-----	-----	-----	4.875	-----	-----	-----	-----	4.875
803	4.737	62.94	4.872	-----	-----	-----	4.871	-----	-----	-----	-----	4.871
804	4.734	62.94	4.868	-----	-----	-----	4.867	-----	-----	-----	-----	4.867
805	4.731	62.94	4.864	-----	-----	-----	4.862	-----	-----	-----	-----	4.862
806	4.728	62.94	4.859	-----	-----	-----	4.858	-----	-----	-----	-----	4.858
807	4.725	62.94	4.855	-----	-----	-----	4.854	-----	-----	-----	-----	4.854
808	4.721	62.94	4.851	-----	-----	-----	4.850	-----	-----	-----	-----	4.850
809	4.717	62.94	4.847	-----	-----	-----	4.845	-----	-----	-----	-----	4.845
810	4.713	62.94	4.842	-----	-----	-----	4.841	-----	-----	-----	-----	4.841
811	4.708	62.94	4.838	-----	-----	-----	4.837	-----	-----	-----	-----	4.837
812	4.704	62.93	4.834	-----	-----	-----	4.833	-----	-----	-----	-----	4.833
813	4.699	62.93	4.830	-----	-----	-----	4.829	-----	-----	-----	-----	4.829
814	4.695	62.93	4.825	-----	-----	-----	4.824	-----	-----	-----	-----	4.824
815	4.690	62.93	4.821	-----	-----	-----	4.820	-----	-----	-----	-----	4.820
816	4.685	62.93	4.817	-----	-----	-----	4.816	-----	-----	-----	-----	4.816
817	4.680	62.93	4.813	-----	-----	-----	4.811	-----	-----	-----	-----	4.811
818	4.675	62.93	4.808	-----	-----	-----	4.807	-----	-----	-----	-----	4.807
819	4.670	62.93	4.804	-----	-----	-----	4.803	-----	-----	-----	-----	4.803
820	4.665	62.93	4.800	-----	-----	-----	4.799	-----	-----	-----	-----	4.799
821	4.660	62.93	4.795	-----	-----	-----	4.794	-----	-----	-----	-----	4.794
822	4.654	62.93	4.791	-----	-----	-----	4.790	-----	-----	-----	-----	4.790
823	4.648	62.93	4.786	-----	-----	-----	4.785	-----	-----	-----	-----	4.785
824	4.643	62.93	4.782	-----	-----	-----	4.781	-----	-----	-----	-----	4.781
825	4.637	62.93	4.777	-----	-----	-----	4.776	-----	-----	-----	-----	4.776
826	4.630	62.93	4.773	-----	-----	-----	4.772	-----	-----	-----	-----	4.772
827	4.624	62.93	4.768	-----	-----	-----	4.767	-----	-----	-----	-----	4.767
828	4.618	62.93	4.764	-----	-----	-----	4.762	-----	-----	-----	-----	4.762
829	4.612	62.93	4.759	-----	-----	-----	4.757	-----	-----	-----	-----	4.758
830	4.605	62.93	4.754	-----	-----	-----	4.753	-----	-----	-----	-----	4.753
831	4.599	62.93	4.749	-----	-----	-----	4.748	-----	-----	-----	-----	4.748
832	4.592	62.93	4.744	-----	-----	-----	4.743	-----	-----	-----	-----	4.743
833	4.585	62.93	4.739	-----	-----	-----	4.738	-----	-----	-----	-----	4.738
834	4.579	62.93	4.734	-----	-----	-----	4.733	-----	-----	-----	-----	4.733
835	4.572	62.93	4.729	-----	-----	-----	4.728	-----	-----	-----	-----	4.728
836	4.565	62.93	4.724	-----	-----	-----	4.723	-----	-----	-----	-----	4.723
837	4.559	62.93	4.719	-----	-----	-----	4.718	-----	-----	-----	-----	4.718
838	4.552	62.93	4.714	-----	-----	-----	4.712	-----	-----	-----	-----	4.712
839	4.545	62.93	4.708	-----	-----	-----	4.707	-----	-----	-----	-----	4.707
840	4.539	62.93	4.703	-----	-----	-----	4.702	-----	-----	-----	-----	4.702
841	4.532	62.93	4.698	-----	-----	-----	4.696	-----	-----	-----	-----	4.696
842	4.526	62.93	4.692	-----	-----	-----	4.691	-----	-----	-----	-----	4.691
843	4.519	62.93	4.687	-----	-----	-----	4.686	-----	-----	-----	-----	4.686
844	4.513	62.93	4.681	-----	-----	-----	4.680	-----	-----	-----	-----	4.680
845	4.507	62.93	4.676	-----	-----	-----	4.675	-----	-----	-----	-----	4.675
846	4.501	62.93	4.670	-----	-----	-----	4.669	-----	-----	-----	-----	4.669
847	4.495	62.93	4.665	-----	-----	-----	4.664	-----	-----	-----	-----	4.664
848	4.490	62.93	4.659	-----	-----	-----	4.658	-----	-----	-----	-----	4.658
849	4.484	62.93	4.654	-----	-----	-----	4.653	-----	-----	-----	-----	4.653

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
850	4.479	62.93	4.648	-----	-----	-----	4.647	-----	-----	-----	-----	4.647
851	4.474	62.93	4.643	-----	-----	-----	4.642	-----	-----	-----	-----	4.642
852	4.470	62.93	4.637	-----	-----	-----	4.636	-----	-----	-----	-----	4.636
853	4.466	62.93	4.632	-----	-----	-----	4.631	-----	-----	-----	-----	4.631
854	4.461	62.93	4.627	-----	-----	-----	4.625	-----	-----	-----	-----	4.625
855	4.458	62.93	4.621	-----	-----	-----	4.620	-----	-----	-----	-----	4.620
856	4.454	62.93	4.616	-----	-----	-----	4.615	-----	-----	-----	-----	4.615
857	4.451	62.93	4.611	-----	-----	-----	4.609	-----	-----	-----	-----	4.609
858	4.448	62.93	4.606	-----	-----	-----	4.604	-----	-----	-----	-----	4.604
859	4.445	62.93	4.601	-----	-----	-----	4.599	-----	-----	-----	-----	4.599
860	4.442	62.93	4.596	-----	-----	-----	4.594	-----	-----	-----	-----	4.594
861	4.439	62.93	4.591	-----	-----	-----	4.589	-----	-----	-----	-----	4.589
862	4.437	62.93	4.586	-----	-----	-----	4.584	-----	-----	-----	-----	4.584
863	4.434	62.93	4.581	-----	-----	-----	4.580	-----	-----	-----	-----	4.580
864	4.432	62.93	4.576	-----	-----	-----	4.575	-----	-----	-----	-----	4.575
865	4.429	62.93	4.572	-----	-----	-----	4.570	-----	-----	-----	-----	4.570
866	4.427	62.93	4.567	-----	-----	-----	4.566	-----	-----	-----	-----	4.566
867	4.425	62.93	4.562	-----	-----	-----	4.561	-----	-----	-----	-----	4.561
868	4.423	62.93	4.558	-----	-----	-----	4.557	-----	-----	-----	-----	4.557
869	4.420	62.93	4.554	-----	-----	-----	4.552	-----	-----	-----	-----	4.552
870	4.418	62.93	4.549	-----	-----	-----	4.548	-----	-----	-----	-----	4.548
871	4.416	62.93	4.545	-----	-----	-----	4.544	-----	-----	-----	-----	4.544
872	4.414	62.93	4.541	-----	-----	-----	4.540	-----	-----	-----	-----	4.540
873	4.412	62.93	4.537	-----	-----	-----	4.536	-----	-----	-----	-----	4.536
874	4.410	62.93	4.533	-----	-----	-----	4.532	-----	-----	-----	-----	4.532
875	4.408	62.93	4.529	-----	-----	-----	4.528	-----	-----	-----	-----	4.528
876	4.405	62.93	4.525	-----	-----	-----	4.524	-----	-----	-----	-----	4.524
877	4.403	62.92	4.521	-----	-----	-----	4.520	-----	-----	-----	-----	4.520
878	4.401	62.92	4.518	-----	-----	-----	4.516	-----	-----	-----	-----	4.516
879	4.399	62.92	4.514	-----	-----	-----	4.512	-----	-----	-----	-----	4.512
880	4.397	62.92	4.510	-----	-----	-----	4.509	-----	-----	-----	-----	4.509
881	4.395	62.92	4.506	-----	-----	-----	4.505	-----	-----	-----	-----	4.505
882	4.393	62.92	4.503	-----	-----	-----	4.501	-----	-----	-----	-----	4.501
883	4.390	62.92	4.499	-----	-----	-----	4.498	-----	-----	-----	-----	4.498
884	4.388	62.92	4.496	-----	-----	-----	4.494	-----	-----	-----	-----	4.494
885	4.386	62.92	4.492	-----	-----	-----	4.491	-----	-----	-----	-----	4.491
886	4.384	62.92	4.489	-----	-----	-----	4.488	-----	-----	-----	-----	4.488
887	4.381	62.92	4.486	-----	-----	-----	4.484	-----	-----	-----	-----	4.484
888	4.379	62.92	4.482	-----	-----	-----	4.481	-----	-----	-----	-----	4.481
889	4.377	62.92	4.479	-----	-----	-----	4.477	-----	-----	-----	-----	4.477
890	4.374	62.92	4.476	-----	-----	-----	4.474	-----	-----	-----	-----	4.474
891	4.372	62.92	4.472	-----	-----	-----	4.471	-----	-----	-----	-----	4.471
892	4.369	62.92	4.469	-----	-----	-----	4.468	-----	-----	-----	-----	4.468
893	4.367	62.92	4.466	-----	-----	-----	4.464	-----	-----	-----	-----	4.464
894	4.364	62.92	4.463	-----	-----	-----	4.461	-----	-----	-----	-----	4.461
895	4.361	62.92	4.460	-----	-----	-----	4.458	-----	-----	-----	-----	4.458
896	4.359	62.92	4.456	-----	-----	-----	4.455	-----	-----	-----	-----	4.455
897	4.356	62.92	4.453	-----	-----	-----	4.452	-----	-----	-----	-----	4.452
898	4.353	62.92	4.450	-----	-----	-----	4.449	-----	-----	-----	-----	4.449
899	4.351	62.92	4.447	-----	-----	-----	4.446	-----	-----	-----	-----	4.446
900	4.348	62.92	4.444	-----	-----	-----	4.442	-----	-----	-----	-----	4.442
901	4.345	62.92	4.441	-----	-----	-----	4.439	-----	-----	-----	-----	4.439
902	4.342	62.92	4.438	-----	-----	-----	4.436	-----	-----	-----	-----	4.436
903	4.339	62.92	4.435	-----	-----	-----	4.433	-----	-----	-----	-----	4.433
904	4.336	62.92	4.432	-----	-----	-----	4.430	-----	-----	-----	-----	4.430
905	4.333	62.92	4.428	-----	-----	-----	4.427	-----	-----	-----	-----	4.427

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
906	4.330	62.92	4.425	-----	-----	-----	4.424	-----	-----	-----	-----	4.424
907	4.327	62.92	4.422	-----	-----	-----	4.421	-----	-----	-----	-----	4.421
908	4.324	62.92	4.419	-----	-----	-----	4.418	-----	-----	-----	-----	4.418
909	4.321	62.92	4.416	-----	-----	-----	4.415	-----	-----	-----	-----	4.415
910	4.318	62.92	4.413	-----	-----	-----	4.412	-----	-----	-----	-----	4.412
911	4.315	62.92	4.410	-----	-----	-----	4.409	-----	-----	-----	-----	4.409
912	4.312	62.92	4.407	-----	-----	-----	4.406	-----	-----	-----	-----	4.406
913	4.309	62.92	4.404	-----	-----	-----	4.402	-----	-----	-----	-----	4.402
914	4.306	62.92	4.401	-----	-----	-----	4.399	-----	-----	-----	-----	4.399
915	4.302	62.92	4.398	-----	-----	-----	4.396	-----	-----	-----	-----	4.396
916	4.299	62.92	4.395	-----	-----	-----	4.393	-----	-----	-----	-----	4.393
917	4.296	62.92	4.392	-----	-----	-----	4.390	-----	-----	-----	-----	4.390
918	4.293	62.92	4.389	-----	-----	-----	4.387	-----	-----	-----	-----	4.387
919	4.290	62.92	4.385	-----	-----	-----	4.384	-----	-----	-----	-----	4.384
920	4.287	62.92	4.382	-----	-----	-----	4.381	-----	-----	-----	-----	4.381
921	4.284	62.92	4.379	-----	-----	-----	4.378	-----	-----	-----	-----	4.378
922	4.281	62.92	4.376	-----	-----	-----	4.375	-----	-----	-----	-----	4.375
923	4.278	62.92	4.373	-----	-----	-----	4.372	-----	-----	-----	-----	4.372
924	4.275	62.92	4.370	-----	-----	-----	4.369	-----	-----	-----	-----	4.369
925	4.271	62.92	4.367	-----	-----	-----	4.366	-----	-----	-----	-----	4.366
926	4.268	62.92	4.364	-----	-----	-----	4.362	-----	-----	-----	-----	4.362
927	4.265	62.92	4.361	-----	-----	-----	4.359	-----	-----	-----	-----	4.359
928	4.262	62.92	4.358	-----	-----	-----	4.356	-----	-----	-----	-----	4.356
929	4.259	62.92	4.355	-----	-----	-----	4.353	-----	-----	-----	-----	4.353
930	4.256	62.92	4.352	-----	-----	-----	4.350	-----	-----	-----	-----	4.350
931	4.253	62.92	4.348	-----	-----	-----	4.347	-----	-----	-----	-----	4.347
932	4.250	62.92	4.345	-----	-----	-----	4.344	-----	-----	-----	-----	4.344
933	4.247	62.92	4.342	-----	-----	-----	4.341	-----	-----	-----	-----	4.341
934	4.243	62.92	4.339	-----	-----	-----	4.338	-----	-----	-----	-----	4.338
935	4.240	62.92	4.336	-----	-----	-----	4.335	-----	-----	-----	-----	4.335
936	4.237	62.92	4.333	-----	-----	-----	4.332	-----	-----	-----	-----	4.332
937	4.234	62.92	4.330	-----	-----	-----	4.328	-----	-----	-----	-----	4.329
938	4.231	62.92	4.327	-----	-----	-----	4.325	-----	-----	-----	-----	4.325
939	4.228	62.92	4.324	-----	-----	-----	4.322	-----	-----	-----	-----	4.322
940	4.225	62.92	4.321	-----	-----	-----	4.319	-----	-----	-----	-----	4.319
941	4.222	62.92	4.318	-----	-----	-----	4.316	-----	-----	-----	-----	4.316
942	4.219	62.92	4.315	-----	-----	-----	4.313	-----	-----	-----	-----	4.313
943	4.215	62.92	4.311	-----	-----	-----	4.310	-----	-----	-----	-----	4.310
944	4.212	62.92	4.308	-----	-----	-----	4.307	-----	-----	-----	-----	4.307
945	4.209	62.92	4.305	-----	-----	-----	4.304	-----	-----	-----	-----	4.304
946	4.206	62.92	4.302	-----	-----	-----	4.301	-----	-----	-----	-----	4.301
947	4.203	62.92	4.299	-----	-----	-----	4.298	-----	-----	-----	-----	4.298
948	4.200	62.92	4.296	-----	-----	-----	4.294	-----	-----	-----	-----	4.294
949	4.197	62.92	4.293	-----	-----	-----	4.291	-----	-----	-----	-----	4.291
950	4.194	62.92	4.290	-----	-----	-----	4.288	-----	-----	-----	-----	4.288
951	4.191	62.92	4.287	-----	-----	-----	4.285	-----	-----	-----	-----	4.285
952	4.187	62.92	4.284	-----	-----	-----	4.282	-----	-----	-----	-----	4.282
953	4.184	62.92	4.281	-----	-----	-----	4.279	-----	-----	-----	-----	4.279
954	4.181	62.92	4.277	-----	-----	-----	4.276	-----	-----	-----	-----	4.276
955	4.178	62.92	4.274	-----	-----	-----	4.273	-----	-----	-----	-----	4.273
956	4.175	62.92	4.271	-----	-----	-----	4.270	-----	-----	-----	-----	4.270
957	4.172	62.92	4.268	-----	-----	-----	4.267	-----	-----	-----	-----	4.267
958	4.169	62.92	4.265	-----	-----	-----	4.263	-----	-----	-----	-----	4.263
959	4.165	62.92	4.262	-----	-----	-----	4.260	-----	-----	-----	-----	4.260
960	4.162	62.92	4.259	-----	-----	-----	4.257	-----	-----	-----	-----	4.257
961	4.159	62.92	4.256	-----	-----	-----	4.254	-----	-----	-----	-----	4.254

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
962	4.156	62.92	4.253	-----	-----	-----	4.251	-----	-----	-----	-----	4.251
963	4.153	62.92	4.249	-----	-----	-----	4.248	-----	-----	-----	-----	4.248
964	4.150	62.92	4.246	-----	-----	-----	4.245	-----	-----	-----	-----	4.245
965	4.147	62.92	4.243	-----	-----	-----	4.242	-----	-----	-----	-----	4.242
966	4.144	62.92	4.240	-----	-----	-----	4.239	-----	-----	-----	-----	4.239
967	4.140	62.92	4.237	-----	-----	-----	4.235	-----	-----	-----	-----	4.235
968	4.137	62.92	4.234	-----	-----	-----	4.232	-----	-----	-----	-----	4.232
969	4.134	62.92	4.231	-----	-----	-----	4.229	-----	-----	-----	-----	4.229
970	4.131	62.92	4.228	-----	-----	-----	4.226	-----	-----	-----	-----	4.226
971	4.128	62.92	4.225	-----	-----	-----	4.223	-----	-----	-----	-----	4.223
972	4.125	62.92	4.221	-----	-----	-----	4.220	-----	-----	-----	-----	4.220
973	4.122	62.92	4.218	-----	-----	-----	4.217	-----	-----	-----	-----	4.217
974	4.118	62.92	4.215	-----	-----	-----	4.214	-----	-----	-----	-----	4.214
975	4.115	62.92	4.212	-----	-----	-----	4.211	-----	-----	-----	-----	4.211
976	4.112	62.91	4.209	-----	-----	-----	4.207	-----	-----	-----	-----	4.207
977	4.109	62.91	4.206	-----	-----	-----	4.204	-----	-----	-----	-----	4.204
978	4.106	62.91	4.203	-----	-----	-----	4.201	-----	-----	-----	-----	4.201
979	4.103	62.91	4.200	-----	-----	-----	4.198	-----	-----	-----	-----	4.198
980	4.100	62.91	4.196	-----	-----	-----	4.195	-----	-----	-----	-----	4.195
981	4.096	62.91	4.193	-----	-----	-----	4.192	-----	-----	-----	-----	4.192
982	4.093	62.91	4.190	-----	-----	-----	4.189	-----	-----	-----	-----	4.189
983	4.090	62.91	4.187	-----	-----	-----	4.186	-----	-----	-----	-----	4.186
984	4.087	62.91	4.184	-----	-----	-----	4.183	-----	-----	-----	-----	4.182
985	4.084	62.91	4.181	-----	-----	-----	4.179	-----	-----	-----	-----	4.179
986	4.081	62.91	4.178	-----	-----	-----	4.176	-----	-----	-----	-----	4.176
987	4.078	62.91	4.175	-----	-----	-----	4.173	-----	-----	-----	-----	4.173
988	4.074	62.91	4.171	-----	-----	-----	4.170	-----	-----	-----	-----	4.170
989	4.071	62.91	4.168	-----	-----	-----	4.167	-----	-----	-----	-----	4.167
990	4.068	62.91	4.165	-----	-----	-----	4.164	-----	-----	-----	-----	4.164
991	4.065	62.91	4.162	-----	-----	-----	4.161	-----	-----	-----	-----	4.161
992	4.062	62.91	4.159	-----	-----	-----	4.157	-----	-----	-----	-----	4.157
993	4.059	62.91	4.156	-----	-----	-----	4.154	-----	-----	-----	-----	4.154
994	4.055	62.91	4.153	-----	-----	-----	4.151	-----	-----	-----	-----	4.151
995	4.052	62.91	4.150	-----	-----	-----	4.148	-----	-----	-----	-----	4.148
996	4.049	62.91	4.146	-----	-----	-----	4.145	-----	-----	-----	-----	4.145
997	4.046	62.91	4.143	-----	-----	-----	4.142	-----	-----	-----	-----	4.142
998	4.043	62.91	4.140	-----	-----	-----	4.139	-----	-----	-----	-----	4.139
999	4.040	62.91	4.137	-----	-----	-----	4.135	-----	-----	-----	-----	4.135
1000	4.036	62.91	4.134	-----	-----	-----	4.132	-----	-----	-----	-----	4.132
1001	4.033	62.91	4.131	-----	-----	-----	4.129	-----	-----	-----	-----	4.129
1002	4.030	62.91	4.128	-----	-----	-----	4.126	-----	-----	-----	-----	4.126
1003	4.027	62.91	4.124	-----	-----	-----	4.123	-----	-----	-----	-----	4.123
1004	4.024	62.91	4.121	-----	-----	-----	4.120	-----	-----	-----	-----	4.120
1005	4.021	62.91	4.118	-----	-----	-----	4.117	-----	-----	-----	-----	4.117
1006	4.018	62.91	4.115	-----	-----	-----	4.113	-----	-----	-----	-----	4.113
1007	4.014	62.91	4.112	-----	-----	-----	4.110	-----	-----	-----	-----	4.110
1008	4.011	62.91	4.109	-----	-----	-----	4.107	-----	-----	-----	-----	4.107
1009	4.008	62.91	4.106	-----	-----	-----	4.104	-----	-----	-----	-----	4.104
1010	4.005	62.91	4.102	-----	-----	-----	4.101	-----	-----	-----	-----	4.101
1011	4.002	62.91	4.099	-----	-----	-----	4.098	-----	-----	-----	-----	4.098
1012	3.999	62.91	4.096	-----	-----	-----	4.095	-----	-----	-----	-----	4.095
1013	3.995	62.91	4.093	-----	-----	-----	4.091	-----	-----	-----	-----	4.091
1014	3.992	62.91	4.090	-----	-----	-----	4.088	-----	-----	-----	-----	4.088
1015	3.989	62.91	4.087	-----	-----	-----	4.085	-----	-----	-----	-----	4.085
1016	3.986	62.91	4.084	-----	-----	-----	4.082	-----	-----	-----	-----	4.082
1017	3.983	62.91	4.080	-----	-----	-----	4.079	-----	-----	-----	-----	4.079

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1018	3.979	62.91	4.077	-----	-----	-----	4.076	-----	-----	-----	-----	4.076
1019	3.976	62.91	4.074	-----	-----	-----	4.072	-----	-----	-----	-----	4.073
1020	3.973	62.91	4.071	-----	-----	-----	4.069	-----	-----	-----	-----	4.069
1021	3.970	62.91	4.068	-----	-----	-----	4.066	-----	-----	-----	-----	4.066
1022	3.967	62.91	4.065	-----	-----	-----	4.063	-----	-----	-----	-----	4.063
1023	3.964	62.91	4.062	-----	-----	-----	4.060	-----	-----	-----	-----	4.060
1024	3.960	62.91	4.058	-----	-----	-----	4.057	-----	-----	-----	-----	4.057
1025	3.957	62.91	4.055	-----	-----	-----	4.054	-----	-----	-----	-----	4.054
1026	3.954	62.91	4.052	-----	-----	-----	4.050	-----	-----	-----	-----	4.050
1027	3.951	62.91	4.049	-----	-----	-----	4.047	-----	-----	-----	-----	4.047
1028	3.948	62.91	4.046	-----	-----	-----	4.044	-----	-----	-----	-----	4.044
1029	3.945	62.91	4.043	-----	-----	-----	4.041	-----	-----	-----	-----	4.041
1030	3.941	62.91	4.039	-----	-----	-----	4.038	-----	-----	-----	-----	4.038
1031	3.938	62.91	4.036	-----	-----	-----	4.035	-----	-----	-----	-----	4.035
1032	3.935	62.91	4.033	-----	-----	-----	4.032	-----	-----	-----	-----	4.031
1033	3.932	62.91	4.030	-----	-----	-----	4.028	-----	-----	-----	-----	4.028
1034	3.929	62.91	4.027	-----	-----	-----	4.025	-----	-----	-----	-----	4.025
1035	3.925	62.91	4.024	-----	-----	-----	4.022	-----	-----	-----	-----	4.022
1036	3.922	62.91	4.020	-----	-----	-----	4.019	-----	-----	-----	-----	4.019
1037	3.919	62.91	4.017	-----	-----	-----	4.016	-----	-----	-----	-----	4.016
1038	3.916	62.91	4.014	-----	-----	-----	4.013	-----	-----	-----	-----	4.012
1039	3.913	62.91	4.011	-----	-----	-----	4.009	-----	-----	-----	-----	4.009
1040	3.910	62.91	4.008	-----	-----	-----	4.006	-----	-----	-----	-----	4.006
1041	3.906	62.91	4.005	-----	-----	-----	4.003	-----	-----	-----	-----	4.003
1042	3.903	62.91	4.001	-----	-----	-----	4.000	-----	-----	-----	-----	4.000
1043	3.900	62.91	3.998	-----	-----	-----	3.997	-----	-----	-----	-----	3.997
1044	3.897	62.91	3.995	-----	-----	-----	3.994	-----	-----	-----	-----	3.994
1045	3.894	62.91	3.992	-----	-----	-----	3.990	-----	-----	-----	-----	3.990
1046	3.890	62.91	3.989	-----	-----	-----	3.987	-----	-----	-----	-----	3.987
1047	3.887	62.91	3.986	-----	-----	-----	3.984	-----	-----	-----	-----	3.984
1048	3.884	62.91	3.982	-----	-----	-----	3.981	-----	-----	-----	-----	3.981
1049	3.881	62.91	3.979	-----	-----	-----	3.978	-----	-----	-----	-----	3.978
1050	3.878	62.91	3.976	-----	-----	-----	3.975	-----	-----	-----	-----	3.974
1051	3.874	62.91	3.973	-----	-----	-----	3.971	-----	-----	-----	-----	3.971
1052	3.871	62.91	3.970	-----	-----	-----	3.968	-----	-----	-----	-----	3.968
1053	3.868	62.91	3.967	-----	-----	-----	3.965	-----	-----	-----	-----	3.965
1054	3.865	62.91	3.963	-----	-----	-----	3.962	-----	-----	-----	-----	3.962
1055	3.862	62.91	3.960	-----	-----	-----	3.959	-----	-----	-----	-----	3.959
1056	3.858	62.91	3.957	-----	-----	-----	3.955	-----	-----	-----	-----	3.955
1057	3.855	62.91	3.954	-----	-----	-----	3.952	-----	-----	-----	-----	3.952
1058	3.852	62.91	3.951	-----	-----	-----	3.949	-----	-----	-----	-----	3.949
1059	3.849	62.91	3.948	-----	-----	-----	3.946	-----	-----	-----	-----	3.946
1060	3.846	62.91	3.944	-----	-----	-----	3.943	-----	-----	-----	-----	3.943
1061	3.842	62.91	3.941	-----	-----	-----	3.940	-----	-----	-----	-----	3.940
1062	3.839	62.91	3.938	-----	-----	-----	3.936	-----	-----	-----	-----	3.936
1063	3.836	62.91	3.935	-----	-----	-----	3.933	-----	-----	-----	-----	3.933
1064	3.833	62.91	3.932	-----	-----	-----	3.930	-----	-----	-----	-----	3.930
1065	3.830	62.91	3.929	-----	-----	-----	3.927	-----	-----	-----	-----	3.927
1066	3.826	62.91	3.925	-----	-----	-----	3.924	-----	-----	-----	-----	3.924
1067	3.823	62.91	3.922	-----	-----	-----	3.921	-----	-----	-----	-----	3.920
1068	3.820	62.91	3.919	-----	-----	-----	3.917	-----	-----	-----	-----	3.917
1069	3.817	62.91	3.916	-----	-----	-----	3.914	-----	-----	-----	-----	3.914
1070	3.814	62.91	3.913	-----	-----	-----	3.911	-----	-----	-----	-----	3.911
1071	3.810	62.91	3.909	-----	-----	-----	3.908	-----	-----	-----	-----	3.908
1072	3.807	62.91	3.906	-----	-----	-----	3.905	-----	-----	-----	-----	3.905
1073	3.804	62.91	3.903	-----	-----	-----	3.901	-----	-----	-----	-----	3.901

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1074	3.801	62.91	3.900	-----	-----	-----	3.898	-----	-----	-----	-----	3.898
1075	3.798	62.90	3.897	-----	-----	-----	3.895	-----	-----	-----	-----	3.895
1076	3.794	62.90	3.894	-----	-----	-----	3.892	-----	-----	-----	-----	3.892
1077	3.791	62.90	3.890	-----	-----	-----	3.889	-----	-----	-----	-----	3.889
1078	3.788	62.90	3.887	-----	-----	-----	3.885	-----	-----	-----	-----	3.885
1079	3.785	62.90	3.884	-----	-----	-----	3.882	-----	-----	-----	-----	3.882
1080	3.782	62.90	3.881	-----	-----	-----	3.879	-----	-----	-----	-----	3.879
1081	3.778	62.90	3.878	-----	-----	-----	3.876	-----	-----	-----	-----	3.876
1082	3.775	62.90	3.874	-----	-----	-----	3.873	-----	-----	-----	-----	3.873
1083	3.772	62.90	3.871	-----	-----	-----	3.870	-----	-----	-----	-----	3.869
1084	3.769	62.90	3.868	-----	-----	-----	3.866	-----	-----	-----	-----	3.866
1085	3.765	62.90	3.865	-----	-----	-----	3.863	-----	-----	-----	-----	3.863
1086	3.762	62.90	3.862	-----	-----	-----	3.860	-----	-----	-----	-----	3.860
1087	3.759	62.90	3.858	-----	-----	-----	3.857	-----	-----	-----	-----	3.857
1088	3.756	62.90	3.855	-----	-----	-----	3.854	-----	-----	-----	-----	3.854
1089	3.753	62.90	3.852	-----	-----	-----	3.850	-----	-----	-----	-----	3.850
1090	3.749	62.90	3.849	-----	-----	-----	3.847	-----	-----	-----	-----	3.847
1091	3.746	62.90	3.846	-----	-----	-----	3.844	-----	-----	-----	-----	3.844
1092	3.743	62.90	3.842	-----	-----	-----	3.841	-----	-----	-----	-----	3.841
1093	3.740	62.90	3.839	-----	-----	-----	3.838	-----	-----	-----	-----	3.838
1094	3.737	62.90	3.836	-----	-----	-----	3.834	-----	-----	-----	-----	3.834
1095	3.733	62.90	3.833	-----	-----	-----	3.831	-----	-----	-----	-----	3.831
1096	3.730	62.90	3.830	-----	-----	-----	3.828	-----	-----	-----	-----	3.828
1097	3.727	62.90	3.826	-----	-----	-----	3.825	-----	-----	-----	-----	3.825
1098	3.724	62.90	3.823	-----	-----	-----	3.821	-----	-----	-----	-----	3.822
1099	3.720	62.90	3.820	-----	-----	-----	3.818	-----	-----	-----	-----	3.818
1100	3.717	62.90	3.817	-----	-----	-----	3.815	-----	-----	-----	-----	3.815
1101	3.714	62.90	3.814	-----	-----	-----	3.812	-----	-----	-----	-----	3.812
1102	3.711	62.90	3.810	-----	-----	-----	3.809	-----	-----	-----	-----	3.809
1103	3.708	62.90	3.807	-----	-----	-----	3.805	-----	-----	-----	-----	3.805
1104	3.704	62.90	3.804	-----	-----	-----	3.802	-----	-----	-----	-----	3.802
1105	3.701	62.90	3.801	-----	-----	-----	3.799	-----	-----	-----	-----	3.799
1106	3.698	62.90	3.798	-----	-----	-----	3.796	-----	-----	-----	-----	3.796
1107	3.695	62.90	3.794	-----	-----	-----	3.793	-----	-----	-----	-----	3.793
1108	3.691	62.90	3.791	-----	-----	-----	3.789	-----	-----	-----	-----	3.789
1109	3.688	62.90	3.788	-----	-----	-----	3.786	-----	-----	-----	-----	3.786
1110	3.685	62.90	3.785	-----	-----	-----	3.783	-----	-----	-----	-----	3.783
1111	3.682	62.90	3.782	-----	-----	-----	3.780	-----	-----	-----	-----	3.780
1112	3.679	62.90	3.778	-----	-----	-----	3.777	-----	-----	-----	-----	3.777
1113	3.675	62.90	3.775	-----	-----	-----	3.773	-----	-----	-----	-----	3.773
1114	3.672	62.90	3.772	-----	-----	-----	3.770	-----	-----	-----	-----	3.770
1115	3.669	62.90	3.769	-----	-----	-----	3.767	-----	-----	-----	-----	3.767
1116	3.666	62.90	3.766	-----	-----	-----	3.764	-----	-----	-----	-----	3.764
1117	3.662	62.90	3.762	-----	-----	-----	3.761	-----	-----	-----	-----	3.761
1118	3.659	62.90	3.759	-----	-----	-----	3.757	-----	-----	-----	-----	3.757
1119	3.656	62.90	3.756	-----	-----	-----	3.754	-----	-----	-----	-----	3.754
1120	3.653	62.90	3.753	-----	-----	-----	3.751	-----	-----	-----	-----	3.751
1121	3.649	62.90	3.749	-----	-----	-----	3.748	-----	-----	-----	-----	3.748
1122	3.646	62.90	3.746	-----	-----	-----	3.744	-----	-----	-----	-----	3.744
1123	3.643	62.90	3.743	-----	-----	-----	3.741	-----	-----	-----	-----	3.741
1124	3.640	62.90	3.740	-----	-----	-----	3.739	-----	-----	-----	-----	3.739
1125	3.637	62.90	3.738	-----	-----	-----	3.736	-----	-----	-----	-----	3.736
1126	3.633	62.90	3.735	-----	-----	-----	3.734	-----	-----	-----	-----	3.734
1127	3.630	62.90	3.733	-----	-----	-----	3.731	-----	-----	-----	-----	3.731
1128	3.627	62.90	3.730	-----	-----	-----	3.728	-----	-----	-----	-----	3.728
1129	3.624	62.90	3.728	-----	-----	-----	3.726	-----	-----	-----	-----	3.726

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1130	3.620	62.90	3.725	-----	-----	-----	3.723	-----	-----	-----	-----	3.723
1131	3.617	62.90	3.722	-----	-----	-----	3.721	-----	-----	-----	-----	3.721
1132	3.614	62.90	3.720	-----	-----	-----	3.718	-----	-----	-----	-----	3.718
1133	3.611	62.90	3.717	-----	-----	-----	3.715	-----	-----	-----	-----	3.715
1134	3.607	62.90	3.715	-----	-----	-----	3.713	-----	-----	-----	-----	3.713
1135	3.604	62.90	3.712	-----	-----	-----	3.710	-----	-----	-----	-----	3.710
1136	3.601	62.90	3.709	-----	-----	-----	3.707	-----	-----	-----	-----	3.707
1137	3.598	62.90	3.706	-----	-----	-----	3.705	-----	-----	-----	-----	3.705
1138	3.594	62.90	3.704	-----	-----	-----	3.702	-----	-----	-----	-----	3.702
1139	3.591	62.90	3.701	-----	-----	-----	3.699	-----	-----	-----	-----	3.699
1140	3.588	62.90	3.698	-----	-----	-----	3.697	-----	-----	-----	-----	3.697
1141	3.585	62.90	3.696	-----	-----	-----	3.694	-----	-----	-----	-----	3.694
1142	3.582	62.90	3.693	-----	-----	-----	3.691	-----	-----	-----	-----	3.691
1143	3.578	62.90	3.690	-----	-----	-----	3.688	-----	-----	-----	-----	3.688
1144	3.575	62.90	3.687	-----	-----	-----	3.685	-----	-----	-----	-----	3.685
1145	3.572	62.90	3.684	-----	-----	-----	3.683	-----	-----	-----	-----	3.683
1146	3.569	62.90	3.682	-----	-----	-----	3.680	-----	-----	-----	-----	3.680
1147	3.565	62.90	3.679	-----	-----	-----	3.677	-----	-----	-----	-----	3.677
1148	3.562	62.90	3.676	-----	-----	-----	3.674	-----	-----	-----	-----	3.674
1149	3.559	62.90	3.673	-----	-----	-----	3.671	-----	-----	-----	-----	3.671
1150	3.556	62.90	3.670	-----	-----	-----	3.668	-----	-----	-----	-----	3.669
1151	3.552	62.90	3.667	-----	-----	-----	3.666	-----	-----	-----	-----	3.666
1152	3.549	62.90	3.665	-----	-----	-----	3.663	-----	-----	-----	-----	3.663
1153	3.546	62.90	3.662	-----	-----	-----	3.660	-----	-----	-----	-----	3.660
1154	3.543	62.90	3.659	-----	-----	-----	3.657	-----	-----	-----	-----	3.657
1155	3.539	62.90	3.656	-----	-----	-----	3.654	-----	-----	-----	-----	3.654
1156	3.536	62.90	3.653	-----	-----	-----	3.651	-----	-----	-----	-----	3.651
1157	3.533	62.90	3.650	-----	-----	-----	3.648	-----	-----	-----	-----	3.648
1158	3.530	62.90	3.647	-----	-----	-----	3.645	-----	-----	-----	-----	3.645
1159	3.526	62.90	3.644	-----	-----	-----	3.642	-----	-----	-----	-----	3.642
1160	3.523	62.90	3.641	-----	-----	-----	3.640	-----	-----	-----	-----	3.640
1161	3.520	62.90	3.638	-----	-----	-----	3.637	-----	-----	-----	-----	3.637
1162	3.517	62.90	3.635	-----	-----	-----	3.634	-----	-----	-----	-----	3.634
1163	3.513	62.90	3.632	-----	-----	-----	3.631	-----	-----	-----	-----	3.631
1164	3.510	62.90	3.629	-----	-----	-----	3.628	-----	-----	-----	-----	3.628
1165	3.507	62.90	3.626	-----	-----	-----	3.625	-----	-----	-----	-----	3.625
1166	3.504	62.90	3.623	-----	-----	-----	3.622	-----	-----	-----	-----	3.622
1167	3.500	62.89	3.621	-----	-----	-----	3.619	-----	-----	-----	-----	3.619
1168	3.497	62.89	3.617	-----	-----	-----	3.616	-----	-----	-----	-----	3.616
1169	3.494	62.89	3.615	-----	-----	-----	3.613	-----	-----	-----	-----	3.613
1170	3.491	62.89	3.611	-----	-----	-----	3.610	-----	-----	-----	-----	3.610
1171	3.487	62.89	3.608	-----	-----	-----	3.607	-----	-----	-----	-----	3.607
1172	3.484	62.89	3.606	-----	-----	-----	3.604	-----	-----	-----	-----	3.604
1173	3.481	62.89	3.602	-----	-----	-----	3.601	-----	-----	-----	-----	3.601
1174	3.478	62.89	3.599	-----	-----	-----	3.598	-----	-----	-----	-----	3.598
1175	3.474	62.89	3.596	-----	-----	-----	3.595	-----	-----	-----	-----	3.595
1176	3.471	62.89	3.593	-----	-----	-----	3.592	-----	-----	-----	-----	3.592
1177	3.468	62.89	3.590	-----	-----	-----	3.589	-----	-----	-----	-----	3.589
1178	3.465	62.89	3.587	-----	-----	-----	3.585	-----	-----	-----	-----	3.585
1179	3.461	62.89	3.584	-----	-----	-----	3.582	-----	-----	-----	-----	3.582
1180	3.458	62.89	3.581	-----	-----	-----	3.579	-----	-----	-----	-----	3.579
1181	3.455	62.89	3.578	-----	-----	-----	3.576	-----	-----	-----	-----	3.576
1182	3.452	62.89	3.575	-----	-----	-----	3.573	-----	-----	-----	-----	3.573
1183	3.448	62.89	3.572	-----	-----	-----	3.570	-----	-----	-----	-----	3.570
1184	3.445	62.89	3.569	-----	-----	-----	3.567	-----	-----	-----	-----	3.567
1185	3.442	62.89	3.566	-----	-----	-----	3.564	-----	-----	-----	-----	3.564

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1186	3.439	62.89	3.563	-----	-----	-----	3.561	-----	-----	-----	-----	3.561
1187	3.435	62.89	3.560	-----	-----	-----	3.558	-----	-----	-----	-----	3.558
1188	3.432	62.89	3.556	-----	-----	-----	3.555	-----	-----	-----	-----	3.555
1189	3.429	62.89	3.553	-----	-----	-----	3.552	-----	-----	-----	-----	3.552
1190	3.425	62.89	3.550	-----	-----	-----	3.548	-----	-----	-----	-----	3.548
1191	3.422	62.89	3.547	-----	-----	-----	3.545	-----	-----	-----	-----	3.545
1192	3.419	62.89	3.544	-----	-----	-----	3.542	-----	-----	-----	-----	3.542
1193	3.416	62.89	3.541	-----	-----	-----	3.539	-----	-----	-----	-----	3.539
1194	3.412	62.89	3.538	-----	-----	-----	3.536	-----	-----	-----	-----	3.536
1195	3.409	62.89	3.535	-----	-----	-----	3.533	-----	-----	-----	-----	3.533
1196	3.406	62.89	3.532	-----	-----	-----	3.530	-----	-----	-----	-----	3.530
1197	3.403	62.89	3.528	-----	-----	-----	3.527	-----	-----	-----	-----	3.527
1198	3.399	62.89	3.525	-----	-----	-----	3.523	-----	-----	-----	-----	3.523
1199	3.396	62.89	3.522	-----	-----	-----	3.520	-----	-----	-----	-----	3.520
1200	3.393	62.89	3.519	-----	-----	-----	3.517	-----	-----	-----	-----	3.517
1201	3.390	62.89	3.516	-----	-----	-----	3.514	-----	-----	-----	-----	3.514
1202	3.386	62.89	3.513	-----	-----	-----	3.511	-----	-----	-----	-----	3.511
1203	3.383	62.89	3.510	-----	-----	-----	3.508	-----	-----	-----	-----	3.508
1204	3.380	62.89	3.506	-----	-----	-----	3.505	-----	-----	-----	-----	3.505
1205	3.377	62.89	3.503	-----	-----	-----	3.501	-----	-----	-----	-----	3.501
1206	3.373	62.89	3.500	-----	-----	-----	3.498	-----	-----	-----	-----	3.498
1207	3.370	62.89	3.497	-----	-----	-----	3.495	-----	-----	-----	-----	3.495
1208	3.367	62.89	3.494	-----	-----	-----	3.492	-----	-----	-----	-----	3.492
1209	3.363	62.89	3.491	-----	-----	-----	3.489	-----	-----	-----	-----	3.489
1210	3.360	62.89	3.487	-----	-----	-----	3.486	-----	-----	-----	-----	3.486
1211	3.357	62.89	3.484	-----	-----	-----	3.482	-----	-----	-----	-----	3.482
1212	3.354	62.89	3.481	-----	-----	-----	3.479	-----	-----	-----	-----	3.479
1213	3.350	62.89	3.478	-----	-----	-----	3.476	-----	-----	-----	-----	3.476
1214	3.347	62.89	3.475	-----	-----	-----	3.473	-----	-----	-----	-----	3.473
1215	3.344	62.89	3.472	-----	-----	-----	3.470	-----	-----	-----	-----	3.470
1216	3.341	62.89	3.468	-----	-----	-----	3.467	-----	-----	-----	-----	3.467
1217	3.337	62.89	3.465	-----	-----	-----	3.463	-----	-----	-----	-----	3.463
1218	3.334	62.89	3.462	-----	-----	-----	3.460	-----	-----	-----	-----	3.460
1219	3.331	62.89	3.459	-----	-----	-----	3.457	-----	-----	-----	-----	3.457
1220	3.327	62.89	3.456	-----	-----	-----	3.454	-----	-----	-----	-----	3.454
1221	3.324	62.89	3.452	-----	-----	-----	3.451	-----	-----	-----	-----	3.451
1222	3.321	62.89	3.449	-----	-----	-----	3.447	-----	-----	-----	-----	3.447
1223	3.318	62.89	3.446	-----	-----	-----	3.444	-----	-----	-----	-----	3.444
1224	3.314	62.89	3.443	-----	-----	-----	3.441	-----	-----	-----	-----	3.441
1225	3.311	62.89	3.440	-----	-----	-----	3.438	-----	-----	-----	-----	3.438
1226	3.308	62.89	3.436	-----	-----	-----	3.435	-----	-----	-----	-----	3.435
1227	3.305	62.89	3.433	-----	-----	-----	3.431	-----	-----	-----	-----	3.431
1228	3.301	62.89	3.430	-----	-----	-----	3.428	-----	-----	-----	-----	3.428
1229	3.298	62.89	3.427	-----	-----	-----	3.425	-----	-----	-----	-----	3.425
1230	3.295	62.89	3.424	-----	-----	-----	3.422	-----	-----	-----	-----	3.422
1231	3.291	62.89	3.420	-----	-----	-----	3.418	-----	-----	-----	-----	3.419
1232	3.288	62.89	3.417	-----	-----	-----	3.415	-----	-----	-----	-----	3.415
1233	3.285	62.89	3.414	-----	-----	-----	3.412	-----	-----	-----	-----	3.412
1234	3.282	62.89	3.411	-----	-----	-----	3.409	-----	-----	-----	-----	3.409
1235	3.278	62.89	3.408	-----	-----	-----	3.406	-----	-----	-----	-----	3.406
1236	3.275	62.89	3.404	-----	-----	-----	3.402	-----	-----	-----	-----	3.402
1237	3.272	62.89	3.401	-----	-----	-----	3.399	-----	-----	-----	-----	3.399
1238	3.269	62.89	3.398	-----	-----	-----	3.396	-----	-----	-----	-----	3.396
1239	3.265	62.89	3.395	-----	-----	-----	3.393	-----	-----	-----	-----	3.393
1240	3.262	62.89	3.391	-----	-----	-----	3.390	-----	-----	-----	-----	3.390
1241	3.259	62.89	3.388	-----	-----	-----	3.386	-----	-----	-----	-----	3.386

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1242	3.255	62.89	3.385	-----	-----	-----	3.383	-----	-----	-----	-----	3.383
1243	3.252	62.89	3.382	-----	-----	-----	3.380	-----	-----	-----	-----	3.380
1244	3.249	62.88	3.378	-----	-----	-----	3.377	-----	-----	-----	-----	3.377
1245	3.246	62.88	3.375	-----	-----	-----	3.373	-----	-----	-----	-----	3.373
1246	3.242	62.88	3.372	-----	-----	-----	3.370	-----	-----	-----	-----	3.370
1247	3.239	62.88	3.369	-----	-----	-----	3.367	-----	-----	-----	-----	3.367
1248	3.236	62.88	3.366	-----	-----	-----	3.364	-----	-----	-----	-----	3.364
1249	3.232	62.88	3.362	-----	-----	-----	3.360	-----	-----	-----	-----	3.360
1250	3.229	62.88	3.359	-----	-----	-----	3.357	-----	-----	-----	-----	3.357
1251	3.226	62.88	3.356	-----	-----	-----	3.354	-----	-----	-----	-----	3.354
1252	3.223	62.88	3.353	-----	-----	-----	3.351	-----	-----	-----	-----	3.351
1253	3.219	62.88	3.349	-----	-----	-----	3.348	-----	-----	-----	-----	3.348
1254	3.216	62.88	3.346	-----	-----	-----	3.344	-----	-----	-----	-----	3.344
1255	3.213	62.88	3.343	-----	-----	-----	3.341	-----	-----	-----	-----	3.341
1256	3.209	62.88	3.340	-----	-----	-----	3.338	-----	-----	-----	-----	3.338
1257	3.206	62.88	3.336	-----	-----	-----	3.335	-----	-----	-----	-----	3.335
1258	3.203	62.88	3.333	-----	-----	-----	3.331	-----	-----	-----	-----	3.331
1259	3.200	62.88	3.330	-----	-----	-----	3.328	-----	-----	-----	-----	3.328
1260	3.196	62.88	3.327	-----	-----	-----	3.325	-----	-----	-----	-----	3.325
1261	3.193	62.88	3.323	-----	-----	-----	3.322	-----	-----	-----	-----	3.322
1262	3.190	62.88	3.320	-----	-----	-----	3.318	-----	-----	-----	-----	3.318
1263	3.186	62.88	3.317	-----	-----	-----	3.315	-----	-----	-----	-----	3.315
1264	3.183	62.88	3.314	-----	-----	-----	3.312	-----	-----	-----	-----	3.312
1265	3.180	62.88	3.310	-----	-----	-----	3.309	-----	-----	-----	-----	3.309
1266	3.177	62.88	3.307	-----	-----	-----	3.305	-----	-----	-----	-----	3.305
1267	3.173	62.88	3.304	-----	-----	-----	3.302	-----	-----	-----	-----	3.302
1268	3.170	62.88	3.301	-----	-----	-----	3.299	-----	-----	-----	-----	3.299
1269	3.167	62.88	3.297	-----	-----	-----	3.296	-----	-----	-----	-----	3.296
1270	3.163	62.88	3.294	-----	-----	-----	3.292	-----	-----	-----	-----	3.292
1271	3.160	62.88	3.291	-----	-----	-----	3.289	-----	-----	-----	-----	3.289
1272	3.157	62.88	3.288	-----	-----	-----	3.286	-----	-----	-----	-----	3.286
1273	3.154	62.88	3.284	-----	-----	-----	3.283	-----	-----	-----	-----	3.283
1274	3.150	62.88	3.281	-----	-----	-----	3.279	-----	-----	-----	-----	3.279
1275	3.147	62.88	3.278	-----	-----	-----	3.276	-----	-----	-----	-----	3.276
1276	3.144	62.88	3.275	-----	-----	-----	3.273	-----	-----	-----	-----	3.273
1277	3.140	62.88	3.271	-----	-----	-----	3.269	-----	-----	-----	-----	3.269
1278	3.137	62.88	3.268	-----	-----	-----	3.266	-----	-----	-----	-----	3.266
1279	3.134	62.88	3.265	-----	-----	-----	3.263	-----	-----	-----	-----	3.263
1280	3.131	62.88	3.262	-----	-----	-----	3.260	-----	-----	-----	-----	3.260
1281	3.127	62.88	3.258	-----	-----	-----	3.256	-----	-----	-----	-----	3.256
1282	3.124	62.88	3.255	-----	-----	-----	3.253	-----	-----	-----	-----	3.253
1283	3.121	62.88	3.252	-----	-----	-----	3.250	-----	-----	-----	-----	3.250
1284	3.117	62.88	3.249	-----	-----	-----	3.247	-----	-----	-----	-----	3.247
1285	3.114	62.88	3.245	-----	-----	-----	3.243	-----	-----	-----	-----	3.243
1286	3.111	62.88	3.242	-----	-----	-----	3.240	-----	-----	-----	-----	3.240
1287	3.107	62.88	3.239	-----	-----	-----	3.237	-----	-----	-----	-----	3.237
1288	3.104	62.88	3.235	-----	-----	-----	3.234	-----	-----	-----	-----	3.234
1289	3.101	62.88	3.232	-----	-----	-----	3.230	-----	-----	-----	-----	3.230
1290	3.098	62.88	3.229	-----	-----	-----	3.227	-----	-----	-----	-----	3.227
1291	3.094	62.88	3.226	-----	-----	-----	3.224	-----	-----	-----	-----	3.224
1292	3.091	62.88	3.222	-----	-----	-----	3.220	-----	-----	-----	-----	3.220
1293	3.088	62.88	3.219	-----	-----	-----	3.217	-----	-----	-----	-----	3.217
1294	3.084	62.88	3.216	-----	-----	-----	3.214	-----	-----	-----	-----	3.214
1295	3.081	62.88	3.212	-----	-----	-----	3.211	-----	-----	-----	-----	3.211
1296	3.078	62.88	3.209	-----	-----	-----	3.207	-----	-----	-----	-----	3.207
1297	3.075	62.88	3.206	-----	-----	-----	3.204	-----	-----	-----	-----	3.204

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1298	3.071	62.88	3.203	-----	-----	-----	3.201	-----	-----	-----	-----	3.201
1299	3.068	62.88	3.199	-----	-----	-----	3.198	-----	-----	-----	-----	3.198
1300	3.065	62.88	3.196	-----	-----	-----	3.194	-----	-----	-----	-----	3.194
1301	3.061	62.88	3.193	-----	-----	-----	3.191	-----	-----	-----	-----	3.191
1302	3.058	62.88	3.190	-----	-----	-----	3.188	-----	-----	-----	-----	3.188
1303	3.055	62.88	3.186	-----	-----	-----	3.184	-----	-----	-----	-----	3.184
1304	3.051	62.88	3.183	-----	-----	-----	3.181	-----	-----	-----	-----	3.181
1305	3.048	62.88	3.180	-----	-----	-----	3.178	-----	-----	-----	-----	3.178
1306	3.045	62.88	3.177	-----	-----	-----	3.175	-----	-----	-----	-----	3.175
1307	3.042	62.88	3.173	-----	-----	-----	3.171	-----	-----	-----	-----	3.171
1308	3.038	62.88	3.170	-----	-----	-----	3.168	-----	-----	-----	-----	3.168
1309	3.035	62.88	3.167	-----	-----	-----	3.165	-----	-----	-----	-----	3.165
1310	3.032	62.88	3.163	-----	-----	-----	3.161	-----	-----	-----	-----	3.161
1311	3.028	62.88	3.160	-----	-----	-----	3.158	-----	-----	-----	-----	3.158
1312	3.025	62.88	3.157	-----	-----	-----	3.155	-----	-----	-----	-----	3.155
1313	3.022	62.88	3.154	-----	-----	-----	3.152	-----	-----	-----	-----	3.152
1314	3.018	62.88	3.150	-----	-----	-----	3.148	-----	-----	-----	-----	3.148
1315	3.015	62.88	3.147	-----	-----	-----	3.145	-----	-----	-----	-----	3.145
1316	3.012	62.88	3.144	-----	-----	-----	3.142	-----	-----	-----	-----	3.142
1317	3.009	62.88	3.140	-----	-----	-----	3.138	-----	-----	-----	-----	3.138
1318	3.005	62.87	3.137	-----	-----	-----	3.135	-----	-----	-----	-----	3.135
1319	3.002	62.87	3.134	-----	-----	-----	3.132	-----	-----	-----	-----	3.132
1320	2.999	62.87	3.131	-----	-----	-----	3.129	-----	-----	-----	-----	3.129
1321	2.995	62.87	3.127	-----	-----	-----	3.125	-----	-----	-----	-----	3.125
1322	2.992	62.87	3.124	-----	-----	-----	3.122	-----	-----	-----	-----	3.122
1323	2.989	62.87	3.121	-----	-----	-----	3.119	-----	-----	-----	-----	3.119
1324	2.985	62.87	3.117	-----	-----	-----	3.115	-----	-----	-----	-----	3.115
1325	2.982	62.87	3.114	-----	-----	-----	3.112	-----	-----	-----	-----	3.112
1326	2.979	62.87	3.111	-----	-----	-----	3.109	-----	-----	-----	-----	3.109
1327	2.975	62.87	3.108	-----	-----	-----	3.106	-----	-----	-----	-----	3.106
1328	2.972	62.87	3.104	-----	-----	-----	3.102	-----	-----	-----	-----	3.102
1329	2.969	62.87	3.101	-----	-----	-----	3.099	-----	-----	-----	-----	3.099
1330	2.966	62.87	3.098	-----	-----	-----	3.096	-----	-----	-----	-----	3.096
1331	2.962	62.87	3.094	-----	-----	-----	3.092	-----	-----	-----	-----	3.092
1332	2.959	62.87	3.091	-----	-----	-----	3.089	-----	-----	-----	-----	3.089
1333	2.956	62.87	3.088	-----	-----	-----	3.086	-----	-----	-----	-----	3.086
1334	2.952	62.87	3.084	-----	-----	-----	3.083	-----	-----	-----	-----	3.083
1335	2.949	62.87	3.081	-----	-----	-----	3.079	-----	-----	-----	-----	3.079
1336	2.946	62.87	3.078	-----	-----	-----	3.076	-----	-----	-----	-----	3.076
1337	2.942	62.87	3.075	-----	-----	-----	3.073	-----	-----	-----	-----	3.073
1338	2.939	62.87	3.071	-----	-----	-----	3.069	-----	-----	-----	-----	3.069
1339	2.936	62.87	3.068	-----	-----	-----	3.066	-----	-----	-----	-----	3.066
1340	2.933	62.87	3.065	-----	-----	-----	3.063	-----	-----	-----	-----	3.063
1341	2.929	62.87	3.061	-----	-----	-----	3.059	-----	-----	-----	-----	3.059
1342	2.926	62.87	3.058	-----	-----	-----	3.056	-----	-----	-----	-----	3.056
1343	2.923	62.87	3.055	-----	-----	-----	3.053	-----	-----	-----	-----	3.053
1344	2.919	62.87	3.052	-----	-----	-----	3.050	-----	-----	-----	-----	3.050
1345	2.916	62.87	3.048	-----	-----	-----	3.046	-----	-----	-----	-----	3.046
1346	2.913	62.87	3.045	-----	-----	-----	3.043	-----	-----	-----	-----	3.043
1347	2.909	62.87	3.042	-----	-----	-----	3.040	-----	-----	-----	-----	3.040
1348	2.906	62.87	3.038	-----	-----	-----	3.036	-----	-----	-----	-----	3.036
1349	2.903	62.87	3.035	-----	-----	-----	3.033	-----	-----	-----	-----	3.033
1350	2.899	62.87	3.032	-----	-----	-----	3.030	-----	-----	-----	-----	3.030
1351	2.896	62.87	3.029	-----	-----	-----	3.027	-----	-----	-----	-----	3.027
1352	2.893	62.87	3.025	-----	-----	-----	3.023	-----	-----	-----	-----	3.023
1353	2.889	62.87	3.022	-----	-----	-----	3.020	-----	-----	-----	-----	3.020

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1354	2.886	62.87	3.019	-----	-----	-----	3.017	-----	-----	-----	-----	3.017
1355	2.883	62.87	3.015	-----	-----	-----	3.013	-----	-----	-----	-----	3.013
1356	2.880	62.87	3.012	-----	-----	-----	3.010	-----	-----	-----	-----	3.010
1357	2.876	62.87	3.009	-----	-----	-----	3.007	-----	-----	-----	-----	3.007
1358	2.873	62.87	3.005	-----	-----	-----	3.003	-----	-----	-----	-----	3.003
1359	2.870	62.87	3.002	-----	-----	-----	3.000	-----	-----	-----	-----	3.000
1360	2.866	62.87	2.999	-----	-----	-----	2.997	-----	-----	-----	-----	2.997
1361	2.863	62.87	2.996	-----	-----	-----	2.994	-----	-----	-----	-----	2.994
1362	2.860	62.87	2.992	-----	-----	-----	2.990	-----	-----	-----	-----	2.990
1363	2.856	62.87	2.989	-----	-----	-----	2.987	-----	-----	-----	-----	2.987
1364	2.853	62.87	2.986	-----	-----	-----	2.984	-----	-----	-----	-----	2.984
1365	2.850	62.87	2.982	-----	-----	-----	2.980	-----	-----	-----	-----	2.980
1366	2.846	62.87	2.979	-----	-----	-----	2.977	-----	-----	-----	-----	2.977
1367	2.843	62.87	2.976	-----	-----	-----	2.974	-----	-----	-----	-----	2.974
1368	2.840	62.87	2.972	-----	-----	-----	2.970	-----	-----	-----	-----	2.970
1369	2.836	62.87	2.969	-----	-----	-----	2.967	-----	-----	-----	-----	2.967
1370	2.833	62.87	2.966	-----	-----	-----	2.964	-----	-----	-----	-----	2.964
1371	2.830	62.87	2.962	-----	-----	-----	2.960	-----	-----	-----	-----	2.961
1372	2.827	62.87	2.959	-----	-----	-----	2.957	-----	-----	-----	-----	2.957
1373	2.823	62.87	2.956	-----	-----	-----	2.954	-----	-----	-----	-----	2.954
1374	2.820	62.87	2.953	-----	-----	-----	2.951	-----	-----	-----	-----	2.951
1375	2.817	62.87	2.949	-----	-----	-----	2.947	-----	-----	-----	-----	2.947
1376	2.813	62.87	2.946	-----	-----	-----	2.944	-----	-----	-----	-----	2.944
1377	2.810	62.87	2.943	-----	-----	-----	2.941	-----	-----	-----	-----	2.941
1378	2.807	62.87	2.939	-----	-----	-----	2.937	-----	-----	-----	-----	2.937
1379	2.803	62.87	2.936	-----	-----	-----	2.934	-----	-----	-----	-----	2.934
1380	2.800	62.87	2.933	-----	-----	-----	2.931	-----	-----	-----	-----	2.931
1381	2.797	62.87	2.929	-----	-----	-----	2.927	-----	-----	-----	-----	2.927
1382	2.793	62.87	2.926	-----	-----	-----	2.924	-----	-----	-----	-----	2.924
1383	2.790	62.87	2.923	-----	-----	-----	2.921	-----	-----	-----	-----	2.921
1384	2.787	62.87	2.920	-----	-----	-----	2.917	-----	-----	-----	-----	2.918
1385	2.783	62.87	2.916	-----	-----	-----	2.914	-----	-----	-----	-----	2.914
1386	2.780	62.87	2.913	-----	-----	-----	2.911	-----	-----	-----	-----	2.911
1387	2.777	62.87	2.910	-----	-----	-----	2.908	-----	-----	-----	-----	2.908
1388	2.773	62.87	2.906	-----	-----	-----	2.904	-----	-----	-----	-----	2.904
1389	2.770	62.87	2.903	-----	-----	-----	2.901	-----	-----	-----	-----	2.901
1390	2.767	62.87	2.900	-----	-----	-----	2.898	-----	-----	-----	-----	2.898
1391	2.763	62.86	2.896	-----	-----	-----	2.894	-----	-----	-----	-----	2.894
1392	2.760	62.86	2.893	-----	-----	-----	2.891	-----	-----	-----	-----	2.891
1393	2.757	62.86	2.890	-----	-----	-----	2.888	-----	-----	-----	-----	2.888
1394	2.753	62.86	2.887	-----	-----	-----	2.884	-----	-----	-----	-----	2.884
1395	2.750	62.86	2.883	-----	-----	-----	2.881	-----	-----	-----	-----	2.881
1396	2.747	62.86	2.880	-----	-----	-----	2.878	-----	-----	-----	-----	2.878
1397	2.744	62.86	2.877	-----	-----	-----	2.875	-----	-----	-----	-----	2.875
1398	2.740	62.86	2.873	-----	-----	-----	2.871	-----	-----	-----	-----	2.871
1399	2.737	62.86	2.870	-----	-----	-----	2.868	-----	-----	-----	-----	2.868
1400	2.734	62.86	2.867	-----	-----	-----	2.865	-----	-----	-----	-----	2.865
1401	2.730	62.86	2.863	-----	-----	-----	2.861	-----	-----	-----	-----	2.861
1402	2.727	62.86	2.860	-----	-----	-----	2.858	-----	-----	-----	-----	2.858
1403	2.724	62.86	2.857	-----	-----	-----	2.855	-----	-----	-----	-----	2.855
1404	2.720	62.86	2.853	-----	-----	-----	2.851	-----	-----	-----	-----	2.851
1405	2.717	62.86	2.850	-----	-----	-----	2.848	-----	-----	-----	-----	2.848
1406	2.714	62.86	2.847	-----	-----	-----	2.845	-----	-----	-----	-----	2.845
1407	2.710	62.86	2.843	-----	-----	-----	2.841	-----	-----	-----	-----	2.841
1408	2.707	62.86	2.840	-----	-----	-----	2.838	-----	-----	-----	-----	2.838
1409	2.704	62.86	2.837	-----	-----	-----	2.835	-----	-----	-----	-----	2.835

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1410	2.700	62.86	2.833	-----	-----	-----	2.831	-----	-----	-----	-----	2.831
1411	2.697	62.86	2.830	-----	-----	-----	2.828	-----	-----	-----	-----	2.828
1412	2.694	62.86	2.827	-----	-----	-----	2.825	-----	-----	-----	-----	2.825
1413	2.690	62.86	2.824	-----	-----	-----	2.821	-----	-----	-----	-----	2.821
1414	2.687	62.86	2.820	-----	-----	-----	2.818	-----	-----	-----	-----	2.818
1415	2.684	62.86	2.817	-----	-----	-----	2.815	-----	-----	-----	-----	2.815
1416	2.680	62.86	2.814	-----	-----	-----	2.812	-----	-----	-----	-----	2.812
1417	2.677	62.86	2.810	-----	-----	-----	2.808	-----	-----	-----	-----	2.808
1418	2.674	62.86	2.807	-----	-----	-----	2.805	-----	-----	-----	-----	2.805
1419	2.670	62.86	2.804	-----	-----	-----	2.802	-----	-----	-----	-----	2.802
1420	2.667	62.86	2.800	-----	-----	-----	2.798	-----	-----	-----	-----	2.798
1421	2.664	62.86	2.797	-----	-----	-----	2.795	-----	-----	-----	-----	2.795
1422	2.660	62.86	2.794	-----	-----	-----	2.792	-----	-----	-----	-----	2.792
1423	2.657	62.86	2.790	-----	-----	-----	2.788	-----	-----	-----	-----	2.788
1424	2.654	62.86	2.787	-----	-----	-----	2.785	-----	-----	-----	-----	2.785
1425	2.650	62.86	2.784	-----	-----	-----	2.782	-----	-----	-----	-----	2.782
1426	2.647	62.86	2.780	-----	-----	-----	2.778	-----	-----	-----	-----	2.778
1427	2.644	62.86	2.777	-----	-----	-----	2.775	-----	-----	-----	-----	2.775
1428	2.640	62.86	2.774	-----	-----	-----	2.772	-----	-----	-----	-----	2.772
1429	2.637	62.86	2.771	-----	-----	-----	2.768	-----	-----	-----	-----	2.768
1430	2.634	62.86	2.767	-----	-----	-----	2.765	-----	-----	-----	-----	2.765
1431	2.630	62.86	2.764	-----	-----	-----	2.762	-----	-----	-----	-----	2.762
1432	2.627	62.86	2.761	-----	-----	-----	2.758	-----	-----	-----	-----	2.758
1433	2.624	62.86	2.757	-----	-----	-----	2.755	-----	-----	-----	-----	2.755
1434	2.620	62.86	2.754	-----	-----	-----	2.752	-----	-----	-----	-----	2.752
1435	2.617	62.86	2.751	-----	-----	-----	2.748	-----	-----	-----	-----	2.749
1436	2.614	62.86	2.747	-----	-----	-----	2.745	-----	-----	-----	-----	2.745
1437	2.610	62.86	2.744	-----	-----	-----	2.742	-----	-----	-----	-----	2.742
1438	2.607	62.86	2.741	-----	-----	-----	2.739	-----	-----	-----	-----	2.739
1439	2.604	62.86	2.737	-----	-----	-----	2.735	-----	-----	-----	-----	2.735
1440	2.600	62.86	2.734	-----	-----	-----	2.732	-----	-----	-----	-----	2.732
1441	2.594	62.86	2.731	-----	-----	-----	2.728	-----	-----	-----	-----	2.729
1442	2.583	62.86	2.727	-----	-----	-----	2.725	-----	-----	-----	-----	2.725
1443	2.570	62.86	2.723	-----	-----	-----	2.721	-----	-----	-----	-----	2.721
1444	2.552	62.86	2.719	-----	-----	-----	2.717	-----	-----	-----	-----	2.717
1445	2.531	62.86	2.715	-----	-----	-----	2.713	-----	-----	-----	-----	2.713
1446	2.507	62.86	2.710	-----	-----	-----	2.708	-----	-----	-----	-----	2.708
1447	2.479	62.86	2.705	-----	-----	-----	2.703	-----	-----	-----	-----	2.703
1448	2.448	62.86	2.699	-----	-----	-----	2.697	-----	-----	-----	-----	2.697
1449	2.413	62.86	2.692	-----	-----	-----	2.690	-----	-----	-----	-----	2.690
1450	2.375	62.86	2.685	-----	-----	-----	2.683	-----	-----	-----	-----	2.683
1451	2.334	62.86	2.677	-----	-----	-----	2.675	-----	-----	-----	-----	2.675
1452	2.289	62.86	2.668	-----	-----	-----	2.665	-----	-----	-----	-----	2.665
1453	2.240	62.86	2.658	-----	-----	-----	2.655	-----	-----	-----	-----	2.655
1454	2.188	62.85	2.647	-----	-----	-----	2.644	-----	-----	-----	-----	2.644
1455	2.133	62.85	2.634	-----	-----	-----	2.632	-----	-----	-----	-----	2.632
1456	2.074	62.85	2.621	-----	-----	-----	2.619	-----	-----	-----	-----	2.619
1457	2.012	62.85	2.607	-----	-----	-----	2.605	-----	-----	-----	-----	2.605
1458	1.946	62.85	2.591	-----	-----	-----	2.589	-----	-----	-----	-----	2.589
1459	1.877	62.85	2.574	-----	-----	-----	2.572	-----	-----	-----	-----	2.572
1460	1.804	62.85	2.556	-----	-----	-----	2.554	-----	-----	-----	-----	2.554
1461	1.728	62.85	2.536	-----	-----	-----	2.534	-----	-----	-----	-----	2.534
1462	1.654	62.85	2.515	-----	-----	-----	2.513	-----	-----	-----	-----	2.513
1463	1.581	62.85	2.493	-----	-----	-----	2.491	-----	-----	-----	-----	2.491
1464	1.511	62.85	2.469	-----	-----	-----	2.467	-----	-----	-----	-----	2.467
1465	1.441	62.85	2.445	-----	-----	-----	2.443	-----	-----	-----	-----	2.443

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1466	1.374	62.85	2.419	-----	-----	-----	2.417	-----	-----	-----	-----	2.417
1467	1.308	62.84	2.392	-----	-----	-----	2.390	-----	-----	-----	-----	2.390
1468	1.243	62.84	2.364	-----	-----	-----	2.362	-----	-----	-----	-----	2.362
1469	1.181	62.84	2.336	-----	-----	-----	2.333	-----	-----	-----	-----	2.333
1470	1.120	62.84	2.306	-----	-----	-----	2.304	-----	-----	-----	-----	2.304
1471	1.060	62.84	2.276	-----	-----	-----	2.273	-----	-----	-----	-----	2.273
1472	1.002	62.84	2.245	-----	-----	-----	2.242	-----	-----	-----	-----	2.242
1473	0.946	62.84	2.213	-----	-----	-----	2.211	-----	-----	-----	-----	2.211
1474	0.892	62.84	2.181	-----	-----	-----	2.178	-----	-----	-----	-----	2.178
1475	0.839	62.83	2.148	-----	-----	-----	2.146	-----	-----	-----	-----	2.146
1476	0.788	62.83	2.115	-----	-----	-----	2.112	-----	-----	-----	-----	2.112
1477	0.738	62.83	2.081	-----	-----	-----	2.079	-----	-----	-----	-----	2.079
1478	0.690	62.83	2.047	-----	-----	-----	2.045	-----	-----	-----	-----	2.045
1479	0.644	62.83	2.013	-----	-----	-----	2.010	-----	-----	-----	-----	2.010
1480	0.599	62.83	1.978	-----	-----	-----	1.976	-----	-----	-----	-----	1.976
1481	0.556	62.83	1.943	-----	-----	-----	1.941	-----	-----	-----	-----	1.941
1482	0.515	62.82	1.908	-----	-----	-----	1.906	-----	-----	-----	-----	1.906
1483	0.475	62.82	1.873	-----	-----	-----	1.870	-----	-----	-----	-----	1.870
1484	0.437	62.82	1.838	-----	-----	-----	1.835	-----	-----	-----	-----	1.835
1485	0.400	62.82	1.802	-----	-----	-----	1.800	-----	-----	-----	-----	1.800
1486	0.365	62.82	1.767	-----	-----	-----	1.764	-----	-----	-----	-----	1.764
1487	0.332	62.82	1.732	-----	-----	-----	1.729	-----	-----	-----	-----	1.729
1488	0.300	62.82	1.696	-----	-----	-----	1.694	-----	-----	-----	-----	1.694
1489	0.270	62.81	1.661	-----	-----	-----	1.659	-----	-----	-----	-----	1.659
1490	0.242	62.81	1.626	-----	-----	-----	1.624	-----	-----	-----	-----	1.624
1491	0.215	62.81	1.591	-----	-----	-----	1.589	-----	-----	-----	-----	1.589
1492	0.189	62.81	1.557	-----	-----	-----	1.554	-----	-----	-----	-----	1.554
1493	0.166	62.81	1.522	-----	-----	-----	1.520	-----	-----	-----	-----	1.520
1494	0.143	62.81	1.488	-----	-----	-----	1.486	-----	-----	-----	-----	1.486
1495	0.123	62.81	1.454	-----	-----	-----	1.452	-----	-----	-----	-----	1.452
1496	0.104	62.80	1.421	-----	-----	-----	1.418	-----	-----	-----	-----	1.418
1497	0.087	62.80	1.388	-----	-----	-----	1.385	-----	-----	-----	-----	1.385
1498	0.071	62.80	1.355	-----	-----	-----	1.353	-----	-----	-----	-----	1.353
1499	0.057	62.80	1.324	-----	-----	-----	1.321	-----	-----	-----	-----	1.321
1500	0.044	62.80	1.307	-----	-----	-----	1.304	-----	-----	-----	-----	1.304
1501	0.033	62.80	1.289	-----	-----	-----	1.287	-----	-----	-----	-----	1.287
1502	0.024	62.80	1.272	-----	-----	-----	1.269	-----	-----	-----	-----	1.269
1503	0.016	62.79	1.255	-----	-----	-----	1.252	-----	-----	-----	-----	1.252
1504	0.009	62.79	1.238	-----	-----	-----	1.235	-----	-----	-----	-----	1.235
1505	0.005	62.79	1.221	-----	-----	-----	1.218	-----	-----	-----	-----	1.218
1506	0.002	62.79	1.204	-----	-----	-----	1.202	-----	-----	-----	-----	1.202
1507	0.000	62.79	1.187	-----	-----	-----	1.185	-----	-----	-----	-----	1.185
1508	0.000	62.79	1.171	-----	-----	-----	1.169	-----	-----	-----	-----	1.169
1509	0.000	62.79	1.155	-----	-----	-----	1.153	-----	-----	-----	-----	1.153
1510	0.000	62.79	1.139	-----	-----	-----	1.137	-----	-----	-----	-----	1.137
1511	0.000	62.78	1.124	-----	-----	-----	1.121	-----	-----	-----	-----	1.121
1512	0.000	62.78	1.108	-----	-----	-----	1.106	-----	-----	-----	-----	1.106
1513	0.000	62.78	1.093	-----	-----	-----	1.091	-----	-----	-----	-----	1.091
1514	0.000	62.78	1.078	-----	-----	-----	1.076	-----	-----	-----	-----	1.076
1515	0.000	62.78	1.063	-----	-----	-----	1.061	-----	-----	-----	-----	1.061
1516	0.000	62.78	1.049	-----	-----	-----	1.046	-----	-----	-----	-----	1.046
1517	0.000	62.78	1.034	-----	-----	-----	1.032	-----	-----	-----	-----	1.032
1518	0.000	62.78	1.020	-----	-----	-----	1.018	-----	-----	-----	-----	1.018
1519	0.000	62.78	1.006	-----	-----	-----	1.004	-----	-----	-----	-----	1.004
1520	0.000	62.77	0.992	-----	-----	-----	0.990	-----	-----	-----	-----	0.990
1521	0.000	62.77	0.978	-----	-----	-----	0.977	-----	-----	-----	-----	0.977

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1522	0.000	62.77	0.965	-----	-----	-----	0.963	-----	-----	-----	-----	0.963
1523	0.000	62.77	0.952	-----	-----	-----	0.950	-----	-----	-----	-----	0.950
1524	0.000	62.77	0.939	-----	-----	-----	0.937	-----	-----	-----	-----	0.937
1525	0.000	62.77	0.926	-----	-----	-----	0.924	-----	-----	-----	-----	0.924
1526	0.000	62.77	0.913	-----	-----	-----	0.911	-----	-----	-----	-----	0.911
1527	0.000	62.77	0.901	-----	-----	-----	0.899	-----	-----	-----	-----	0.899
1528	0.000	62.77	0.888	-----	-----	-----	0.886	-----	-----	-----	-----	0.886
1529	0.000	62.77	0.876	-----	-----	-----	0.874	-----	-----	-----	-----	0.874
1530	0.000	62.77	0.864	-----	-----	-----	0.862	-----	-----	-----	-----	0.862
1531	0.000	62.76	0.852	-----	-----	-----	0.850	-----	-----	-----	-----	0.850
1532	0.000	62.76	0.840	-----	-----	-----	0.839	-----	-----	-----	-----	0.839
1533	0.000	62.76	0.829	-----	-----	-----	0.827	-----	-----	-----	-----	0.827
1534	0.000	62.76	0.817	-----	-----	-----	0.816	-----	-----	-----	-----	0.816
1535	0.000	62.76	0.806	-----	-----	-----	0.805	-----	-----	-----	-----	0.805
1536	0.000	62.76	0.795	-----	-----	-----	0.794	-----	-----	-----	-----	0.794
1537	0.000	62.76	0.784	-----	-----	-----	0.783	-----	-----	-----	-----	0.783
1538	0.000	62.76	0.774	-----	-----	-----	0.772	-----	-----	-----	-----	0.772
1539	0.000	62.76	0.763	-----	-----	-----	0.761	-----	-----	-----	-----	0.761
1540	0.000	62.76	0.752	-----	-----	-----	0.751	-----	-----	-----	-----	0.751
1541	0.000	62.76	0.742	-----	-----	-----	0.741	-----	-----	-----	-----	0.741
1542	0.000	62.76	0.732	-----	-----	-----	0.730	-----	-----	-----	-----	0.730
1543	0.000	62.75	0.722	-----	-----	-----	0.720	-----	-----	-----	-----	0.720
1544	0.000	62.75	0.712	-----	-----	-----	0.711	-----	-----	-----	-----	0.711
1545	0.000	62.75	0.702	-----	-----	-----	0.701	-----	-----	-----	-----	0.701
1546	0.000	62.75	0.693	-----	-----	-----	0.691	-----	-----	-----	-----	0.691
1547	0.000	62.75	0.683	-----	-----	-----	0.682	-----	-----	-----	-----	0.682
1548	0.000	62.75	0.674	-----	-----	-----	0.672	-----	-----	-----	-----	0.672
1549	0.000	62.75	0.664	-----	-----	-----	0.663	-----	-----	-----	-----	0.663
1550	0.000	62.75	0.655	-----	-----	-----	0.654	-----	-----	-----	-----	0.654
1551	0.000	62.75	0.646	-----	-----	-----	0.645	-----	-----	-----	-----	0.645
1552	0.000	62.75	0.637	-----	-----	-----	0.636	-----	-----	-----	-----	0.636
1553	0.000	62.75	0.629	-----	-----	-----	0.627	-----	-----	-----	-----	0.627
1554	0.000	62.75	0.620	-----	-----	-----	0.619	-----	-----	-----	-----	0.619
1555	0.000	62.75	0.611	-----	-----	-----	0.610	-----	-----	-----	-----	0.610
1556	0.000	62.75	0.603	-----	-----	-----	0.602	-----	-----	-----	-----	0.602
1557	0.000	62.74	0.595	-----	-----	-----	0.594	-----	-----	-----	-----	0.594
1558	0.000	62.74	0.587	-----	-----	-----	0.585	-----	-----	-----	-----	0.585
1559	0.000	62.74	0.579	-----	-----	-----	0.577	-----	-----	-----	-----	0.577
1560	0.000	62.74	0.571	-----	-----	-----	0.569	-----	-----	-----	-----	0.570
1561	0.000	62.74	0.563	-----	-----	-----	0.562	-----	-----	-----	-----	0.562
1562	0.000	62.74	0.555	-----	-----	-----	0.554	-----	-----	-----	-----	0.554
1563	0.000	62.74	0.547	-----	-----	-----	0.546	-----	-----	-----	-----	0.546
1564	0.000	62.74	0.540	-----	-----	-----	0.539	-----	-----	-----	-----	0.539
1565	0.000	62.74	0.533	-----	-----	-----	0.531	-----	-----	-----	-----	0.531
1566	0.000	62.74	0.525	-----	-----	-----	0.524	-----	-----	-----	-----	0.524
1567	0.000	62.74	0.518	-----	-----	-----	0.517	-----	-----	-----	-----	0.517
1568	0.000	62.74	0.511	-----	-----	-----	0.510	-----	-----	-----	-----	0.510
1569	0.000	62.74	0.504	-----	-----	-----	0.503	-----	-----	-----	-----	0.503
1570	0.000	62.74	0.497	-----	-----	-----	0.496	-----	-----	-----	-----	0.496
1571	0.000	62.74	0.490	-----	-----	-----	0.489	-----	-----	-----	-----	0.489
1572	0.000	62.74	0.483	-----	-----	-----	0.482	-----	-----	-----	-----	0.482
1573	0.000	62.74	0.477	-----	-----	-----	0.476	-----	-----	-----	-----	0.476
1574	0.000	62.74	0.470	-----	-----	-----	0.469	-----	-----	-----	-----	0.469
1575	0.000	62.73	0.464	-----	-----	-----	0.463	-----	-----	-----	-----	0.463
1576	0.000	62.73	0.457	-----	-----	-----	0.456	-----	-----	-----	-----	0.456
1577	0.000	62.73	0.451	-----	-----	-----	0.450	-----	-----	-----	-----	0.450

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1578	0.000	62.73	0.445	-----	-----	-----	0.444	-----	-----	-----	-----	0.444
1579	0.000	62.73	0.439	-----	-----	-----	0.438	-----	-----	-----	-----	0.438
1580	0.000	62.73	0.433	-----	-----	-----	0.432	-----	-----	-----	-----	0.432
1581	0.000	62.73	0.427	-----	-----	-----	0.426	-----	-----	-----	-----	0.426
1582	0.000	62.73	0.421	-----	-----	-----	0.420	-----	-----	-----	-----	0.420
1583	0.000	62.73	0.415	-----	-----	-----	0.414	-----	-----	-----	-----	0.414
1584	0.000	62.73	0.409	-----	-----	-----	0.409	-----	-----	-----	-----	0.409
1585	0.000	62.73	0.404	-----	-----	-----	0.403	-----	-----	-----	-----	0.403
1586	0.000	62.73	0.398	-----	-----	-----	0.398	-----	-----	-----	-----	0.398
1587	0.000	62.73	0.393	-----	-----	-----	0.392	-----	-----	-----	-----	0.392
1588	0.000	62.73	0.387	-----	-----	-----	0.387	-----	-----	-----	-----	0.387
1589	0.000	62.73	0.382	-----	-----	-----	0.381	-----	-----	-----	-----	0.381
1590	0.000	62.73	0.377	-----	-----	-----	0.376	-----	-----	-----	-----	0.376
1591	0.000	62.73	0.372	-----	-----	-----	0.371	-----	-----	-----	-----	0.371
1592	0.000	62.73	0.367	-----	-----	-----	0.366	-----	-----	-----	-----	0.366
1593	0.000	62.73	0.362	-----	-----	-----	0.361	-----	-----	-----	-----	0.361
1594	0.000	62.73	0.357	-----	-----	-----	0.356	-----	-----	-----	-----	0.356
1595	0.000	62.73	0.352	-----	-----	-----	0.351	-----	-----	-----	-----	0.351
1596	0.000	62.73	0.347	-----	-----	-----	0.346	-----	-----	-----	-----	0.346
1597	0.000	62.73	0.342	-----	-----	-----	0.341	-----	-----	-----	-----	0.341
1598	0.000	62.73	0.337	-----	-----	-----	0.337	-----	-----	-----	-----	0.337
1599	0.000	62.73	0.333	-----	-----	-----	0.332	-----	-----	-----	-----	0.332
1600	0.000	62.72	0.328	-----	-----	-----	0.328	-----	-----	-----	-----	0.328
1601	0.000	62.72	0.324	-----	-----	-----	0.323	-----	-----	-----	-----	0.323
1602	0.000	62.72	0.319	-----	-----	-----	0.319	-----	-----	-----	-----	0.319
1603	0.000	62.72	0.315	-----	-----	-----	0.314	-----	-----	-----	-----	0.314
1604	0.000	62.72	0.311	-----	-----	-----	0.310	-----	-----	-----	-----	0.310
1605	0.000	62.72	0.306	-----	-----	-----	0.306	-----	-----	-----	-----	0.306
1606	0.000	62.72	0.302	-----	-----	-----	0.302	-----	-----	-----	-----	0.301
1607	0.000	62.72	0.298	-----	-----	-----	0.297	-----	-----	-----	-----	0.297
1608	0.000	62.72	0.294	-----	-----	-----	0.293	-----	-----	-----	-----	0.293
1609	0.000	62.72	0.290	-----	-----	-----	0.289	-----	-----	-----	-----	0.289
1610	0.000	62.72	0.286	-----	-----	-----	0.285	-----	-----	-----	-----	0.285
1611	0.000	62.72	0.282	-----	-----	-----	0.281	-----	-----	-----	-----	0.281
1612	0.000	62.72	0.278	-----	-----	-----	0.278	-----	-----	-----	-----	0.277
1613	0.000	62.72	0.274	-----	-----	-----	0.274	-----	-----	-----	-----	0.274
1614	0.000	62.72	0.270	-----	-----	-----	0.270	-----	-----	-----	-----	0.270
1615	0.000	62.72	0.267	-----	-----	-----	0.266	-----	-----	-----	-----	0.266
1616	0.000	62.72	0.263	-----	-----	-----	0.263	-----	-----	-----	-----	0.263
1617	0.000	62.72	0.259	-----	-----	-----	0.259	-----	-----	-----	-----	0.259
1618	0.000	62.72	0.256	-----	-----	-----	0.255	-----	-----	-----	-----	0.255
1619	0.000	62.72	0.252	-----	-----	-----	0.252	-----	-----	-----	-----	0.252
1620	0.000	62.72	0.249	-----	-----	-----	0.248	-----	-----	-----	-----	0.248
1621	0.000	62.72	0.246	-----	-----	-----	0.245	-----	-----	-----	-----	0.245
1622	0.000	62.72	0.242	-----	-----	-----	0.242	-----	-----	-----	-----	0.242
1623	0.000	62.72	0.239	-----	-----	-----	0.238	-----	-----	-----	-----	0.238
1624	0.000	62.72	0.236	-----	-----	-----	0.235	-----	-----	-----	-----	0.235
1625	0.000	62.72	0.232	-----	-----	-----	0.232	-----	-----	-----	-----	0.232
1626	0.000	62.72	0.229	-----	-----	-----	0.229	-----	-----	-----	-----	0.229
1627	0.000	62.72	0.226	-----	-----	-----	0.225	-----	-----	-----	-----	0.226
1628	0.000	62.72	0.223	-----	-----	-----	0.222	-----	-----	-----	-----	0.222
1629	0.000	62.72	0.220	-----	-----	-----	0.219	-----	-----	-----	-----	0.219
1630	0.000	62.72	0.217	-----	-----	-----	0.216	-----	-----	-----	-----	0.216
1631	0.000	62.72	0.214	-----	-----	-----	0.213	-----	-----	-----	-----	0.213
1632	0.000	62.72	0.211	-----	-----	-----	0.210	-----	-----	-----	-----	0.210
1633	0.000	62.72	0.208	-----	-----	-----	0.208	-----	-----	-----	-----	0.208

Continues on next page...

Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1634	0.000	62.72	0.205	-----	-----	-----	0.205	-----	-----	-----	-----	0.205
1635	0.000	62.72	0.202	-----	-----	-----	0.202	-----	-----	-----	-----	0.202
1636	0.000	62.72	0.200	-----	-----	-----	0.199	-----	-----	-----	-----	0.199
1637	0.000	62.71	0.197	-----	-----	-----	0.196	-----	-----	-----	-----	0.196
1638	0.000	62.71	0.194	-----	-----	-----	0.194	-----	-----	-----	-----	0.194
1639	0.000	62.71	0.191	-----	-----	-----	0.191	-----	-----	-----	-----	0.191
1640	0.000	62.71	0.189	-----	-----	-----	0.188	-----	-----	-----	-----	0.188
1641	0.000	62.71	0.186	-----	-----	-----	0.186	-----	-----	-----	-----	0.186
1642	0.000	62.71	0.184	-----	-----	-----	0.183	-----	-----	-----	-----	0.183
1643	0.000	62.71	0.181	-----	-----	-----	0.181	-----	-----	-----	-----	0.181
1644	0.000	62.71	0.179	-----	-----	-----	0.178	-----	-----	-----	-----	0.178
1645	0.000	62.71	0.176	-----	-----	-----	0.176	-----	-----	-----	-----	0.176
1646	0.000	62.71	0.174	-----	-----	-----	0.173	-----	-----	-----	-----	0.173
1647	0.000	62.71	0.171	-----	-----	-----	0.171	-----	-----	-----	-----	0.171
1648	0.000	62.71	0.169	-----	-----	-----	0.169	-----	-----	-----	-----	0.169
1649	0.000	62.71	0.167	-----	-----	-----	0.166	-----	-----	-----	-----	0.166
1650	0.000	62.71	0.164	-----	-----	-----	0.164	-----	-----	-----	-----	0.164
1651	0.000	62.71	0.162	-----	-----	-----	0.162	-----	-----	-----	-----	0.162
1652	0.000	62.71	0.160	-----	-----	-----	0.160	-----	-----	-----	-----	0.160
1653	0.000	62.71	0.158	-----	-----	-----	0.157	-----	-----	-----	-----	0.157
1654	0.000	62.71	0.156	-----	-----	-----	0.155	-----	-----	-----	-----	0.155
1655	0.000	62.71	0.153	-----	-----	-----	0.153	-----	-----	-----	-----	0.153
1656	0.000	62.71	0.151	-----	-----	-----	0.151	-----	-----	-----	-----	0.151
1657	0.000	62.71	0.149	-----	-----	-----	0.149	-----	-----	-----	-----	0.149
1658	0.000	62.71	0.147	-----	-----	-----	0.147	-----	-----	-----	-----	0.147
1659	0.000	62.71	0.145	-----	-----	-----	0.145	-----	-----	-----	-----	0.145
1660	0.000	62.71	0.143	-----	-----	-----	0.143	-----	-----	-----	-----	0.143
1661	0.000	62.71	0.141	-----	-----	-----	0.141	-----	-----	-----	-----	0.141
1662	0.000	62.71	0.139	-----	-----	-----	0.139	-----	-----	-----	-----	0.139
1663	0.000	62.71	0.137	-----	-----	-----	0.137	-----	-----	-----	-----	0.137
1664	0.000	62.71	0.135	-----	-----	-----	0.135	-----	-----	-----	-----	0.135
1665	0.000	62.71	0.134	-----	-----	-----	0.133	-----	-----	-----	-----	0.133
1666	0.000	62.71	0.132	-----	-----	-----	0.132	-----	-----	-----	-----	0.132
1667	0.000	62.71	0.130	-----	-----	-----	0.130	-----	-----	-----	-----	0.130
1668	0.000	62.71	0.128	-----	-----	-----	0.128	-----	-----	-----	-----	0.128
1669	0.000	62.71	0.126	-----	-----	-----	0.126	-----	-----	-----	-----	0.126
1670	0.000	62.71	0.125	-----	-----	-----	0.124	-----	-----	-----	-----	0.124
1671	0.000	62.71	0.123	-----	-----	-----	0.123	-----	-----	-----	-----	0.123
1672	0.000	62.71	0.121	-----	-----	-----	0.121	-----	-----	-----	-----	0.121
1673	0.000	62.71	0.120	-----	-----	-----	0.119	-----	-----	-----	-----	0.119
1674	0.000	62.71	0.118	-----	-----	-----	0.118	-----	-----	-----	-----	0.118
1675	0.000	62.71	0.116	-----	-----	-----	0.116	-----	-----	-----	-----	0.116
1676	0.000	62.71	0.115	-----	-----	-----	0.115	-----	-----	-----	-----	0.115
1677	0.000	62.71	0.113	-----	-----	-----	0.113	-----	-----	-----	-----	0.113
1678	0.000	62.71	0.112	-----	-----	-----	0.111	-----	-----	-----	-----	0.111
1679	0.000	62.71	0.110	-----	-----	-----	0.110	-----	-----	-----	-----	0.110
1680	0.000	62.71	0.109	-----	-----	-----	0.108	-----	-----	-----	-----	0.108
1681	0.000	62.71	0.107	-----	-----	-----	0.107	-----	-----	-----	-----	0.107
1682	0.000	62.71	0.106	-----	-----	-----	0.105	-----	-----	-----	-----	0.105
1683	0.000	62.71	0.104	-----	-----	-----	0.104	-----	-----	-----	-----	0.104
1684	0.000	62.71	0.103	-----	-----	-----	0.103	-----	-----	-----	-----	0.103
1685	0.000	62.71	0.101	-----	-----	-----	0.101	-----	-----	-----	-----	0.101
1686	0.000	62.71	0.100	-----	-----	-----	0.100	-----	-----	-----	-----	0.100
1687	0.000	62.71	0.099	-----	-----	-----	0.098	-----	-----	-----	-----	0.098
1688	0.000	62.71	0.097	-----	-----	-----	0.097	-----	-----	-----	-----	0.097
1689	0.000	62.71	0.096	-----	-----	-----	0.096	-----	-----	-----	-----	0.096

Continues on next page...

Detention pond outflow

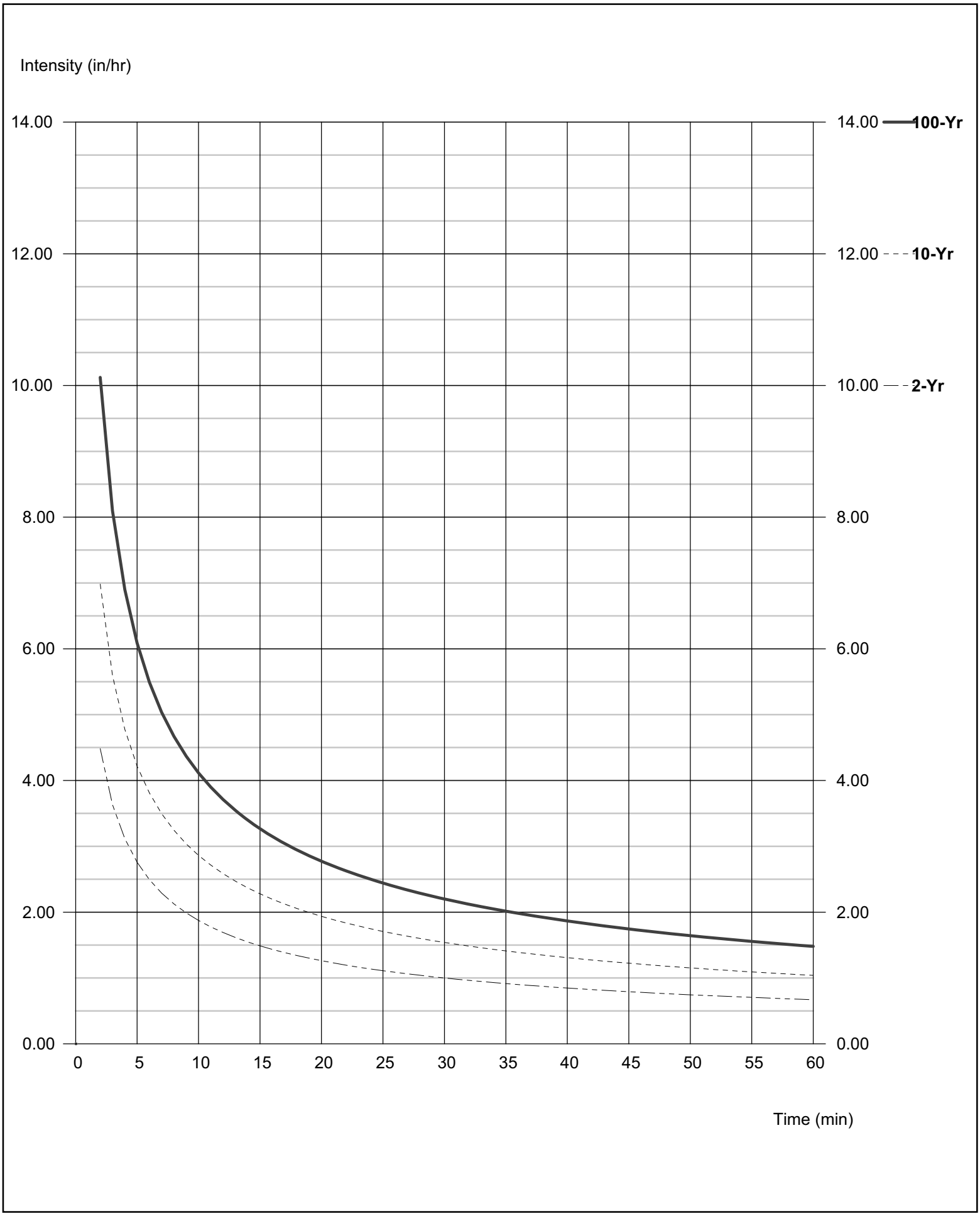
Hydrograph Discharge Table

Time (min)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
1690	0.000	62.71	0.095	-----	-----	-----	0.094	-----	-----	-----	-----	0.094
1691	0.000	62.71	0.093	-----	-----	-----	0.093	-----	-----	-----	-----	0.093
1692	0.000	62.71	0.092	-----	-----	-----	0.092	-----	-----	-----	-----	0.092
1693	0.000	62.71	0.091	-----	-----	-----	0.091	-----	-----	-----	-----	0.091
1694	0.000	62.71	0.089	-----	-----	-----	0.089	-----	-----	-----	-----	0.089
1695	0.000	62.71	0.088	-----	-----	-----	0.088	-----	-----	-----	-----	0.088
1696	0.000	62.71	0.087	-----	-----	-----	0.087	-----	-----	-----	-----	0.087
1697	0.000	62.71	0.086	-----	-----	-----	0.086	-----	-----	-----	-----	0.086
1698	0.000	62.71	0.085	-----	-----	-----	0.084	-----	-----	-----	-----	0.084
1699	0.000	62.71	0.084	-----	-----	-----	0.083	-----	-----	-----	-----	0.083
1700	0.000	62.71	0.082	-----	-----	-----	0.082	-----	-----	-----	-----	0.082
1701	0.000	62.71	0.081	-----	-----	-----	0.081	-----	-----	-----	-----	0.081
1702	0.000	62.71	0.080	-----	-----	-----	0.080	-----	-----	-----	-----	0.080
1703	0.000	62.71	0.079	-----	-----	-----	0.079	-----	-----	-----	-----	0.079
1704	0.000	62.71	0.078	-----	-----	-----	0.078	-----	-----	-----	-----	0.078
1705	0.000	62.71	0.077	-----	-----	-----	0.077	-----	-----	-----	-----	0.077
1706	0.000	62.71	0.076	-----	-----	-----	0.076	-----	-----	-----	-----	0.076
1707	0.000	62.71	0.075	-----	-----	-----	0.075	-----	-----	-----	-----	0.075

...End

Hydraflow IDF Curves

IDF file: Vacaville_ISO_22.IDF



BIO-SWALE TREATMENT CALCULATIONS

Storm water runoff swale residence time calculation

Southern Swale

Area	582000.00	ft^2
i	0.20	in/hr
C	0.65	
Q=CiA	1.75	CFS

Swale geometry
Trapezoidal section 1' flat bottom with 3:1 side slopes

Slope	0.002	
Velocity	0.28	ft/sec
Swale length	570	ft
Residence time	**33.9**	**min**

Northern Swale

Area	340000.00	ft^2
i	0.20	in/hr
C	0.65	
Q=CiA	1.02	CFS

Swale geometry
Trapezoidal section 1' flat bottom with 3:1 side slopes

Slope	0.002	
Velocity	0.27	ft/sec
Swale length	310	ft
Residence time	**19.1**	**min**

Channel Report

Hydraflow Express Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. Thursday, Jul 2 2009

Southern Swale

Trapezoidal

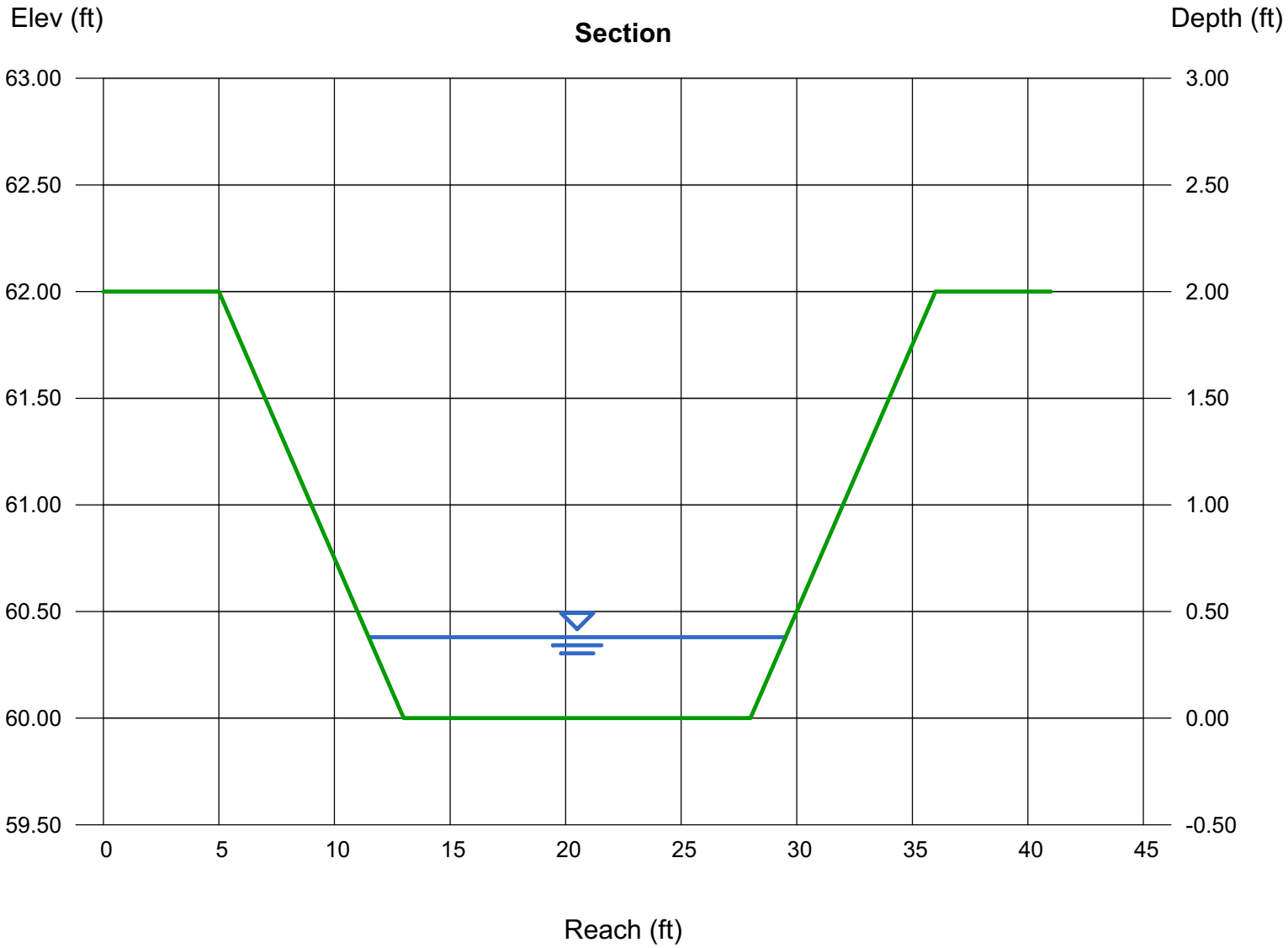
Bottom Width (ft)	=	15.00
Side Slopes (z:1)	=	4.00, 4.00
Total Depth (ft)	=	2.00
Invert Elev (ft)	=	60.00
Slope (%)	=	0.35
N-Value	=	0.150

Calculations

Compute by:		Known Q
Known Q (cfs)	=	1.75

Highlighted

Depth (ft)	=	0.38
Q (cfs)	=	1.750
Area (sqft)	=	6.28
Velocity (ft/s)	=	0.28
Wetted Perim (ft)	=	18.13
Crit Depth, Yc (ft)	=	0.08
Top Width (ft)	=	18.04
EGL (ft)	=	0.38



Channel Report

Hydraflow Express Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. Thursday, Jul 2 2009

Northern Swale

Trapezoidal

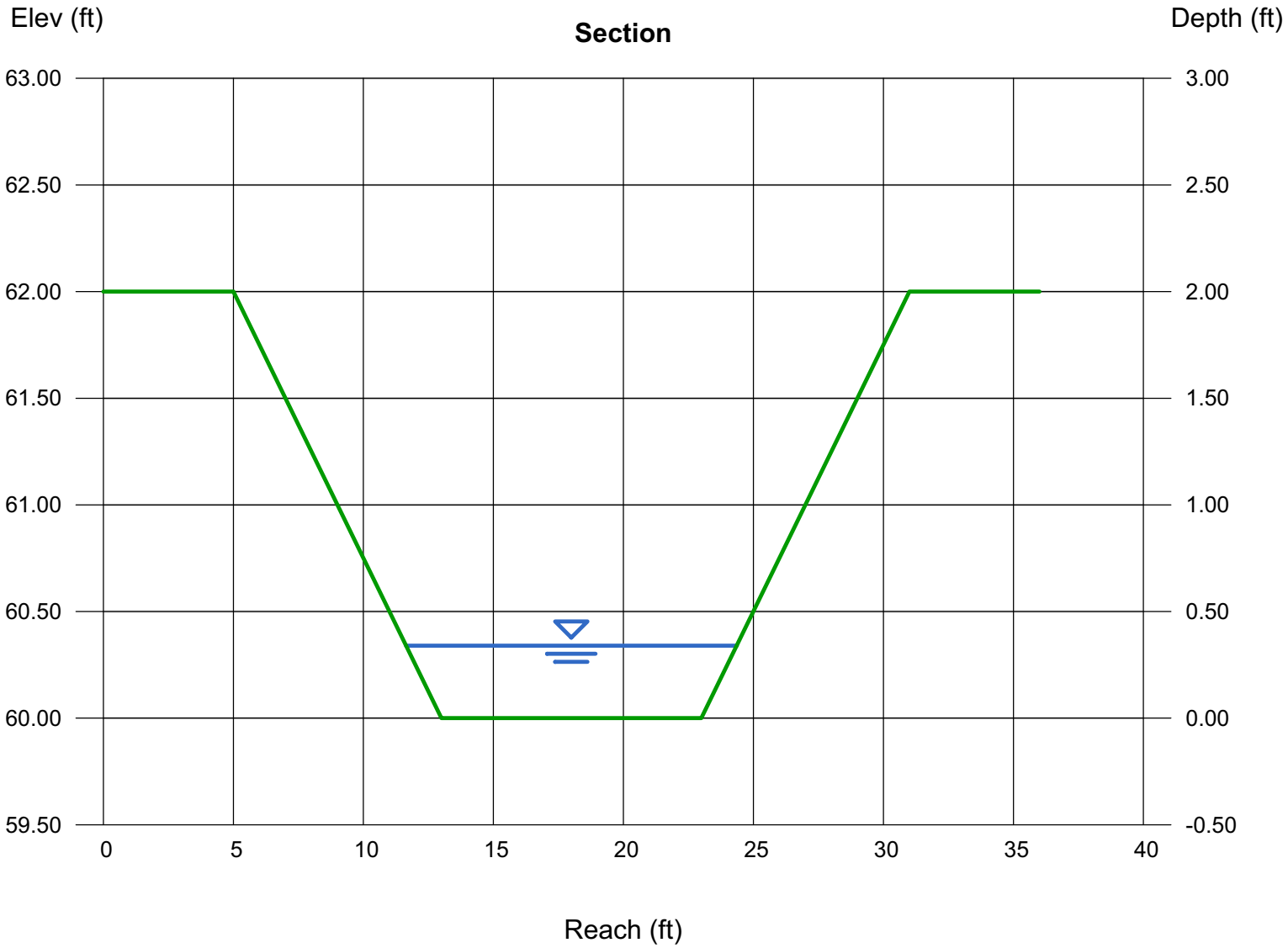
Bottom Width (ft)	=	10.00
Side Slopes (z:1)	=	4.00, 4.00
Total Depth (ft)	=	2.00
Invert Elev (ft)	=	60.00
Slope (%)	=	0.40
N-Value	=	0.150

Calculations

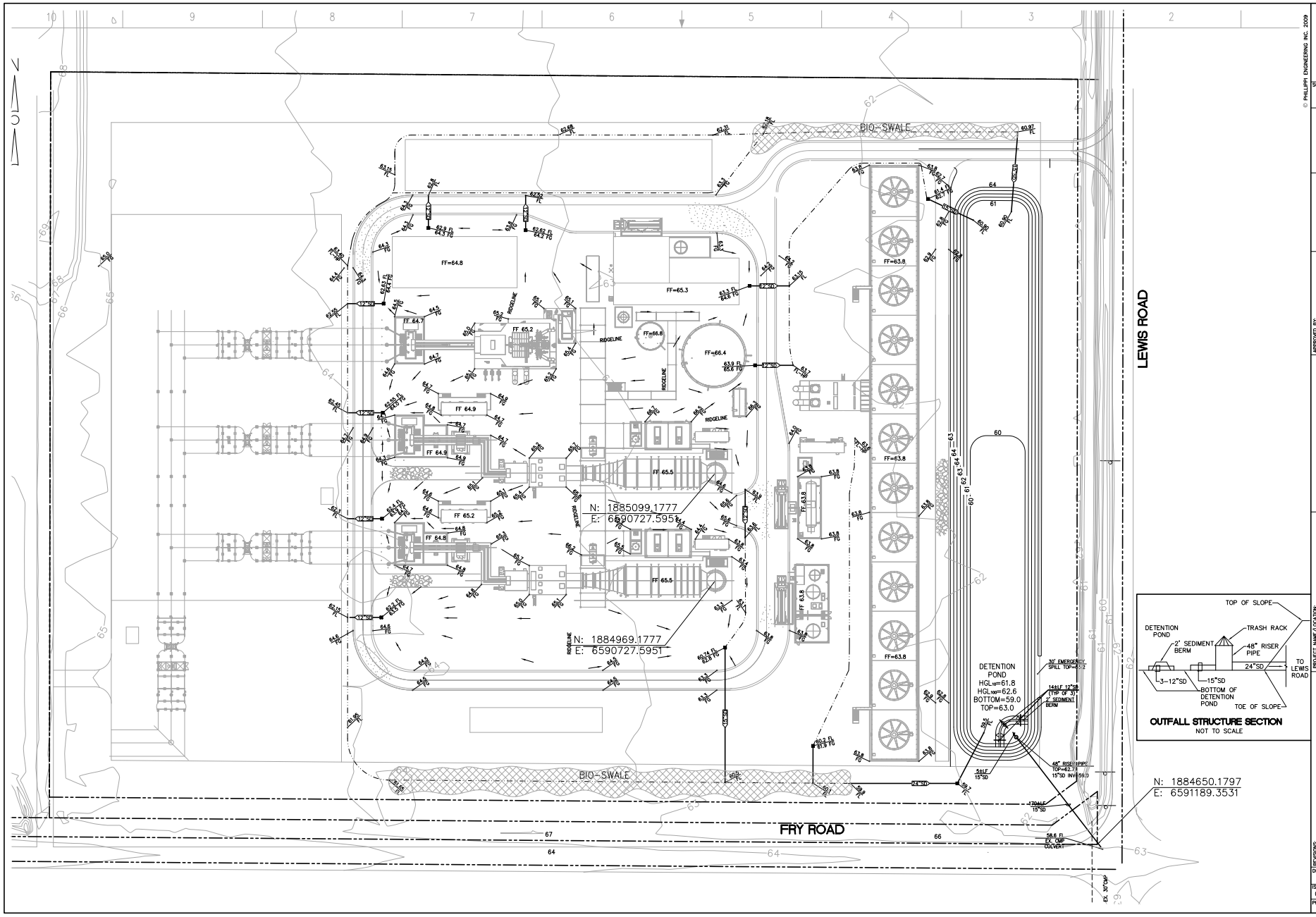
Compute by:		Known Q
Known Q (cfs)	=	1.05

Highlighted

Depth (ft)	=	0.34
Q (cfs)	=	1.050
Area (sqft)	=	3.86
Velocity (ft/s)	=	0.27
Wetted Perim (ft)	=	12.80
Crit Depth, Yc (ft)	=	0.07
Top Width (ft)	=	12.72
EGL (ft)	=	0.34



Attachment DR88-2
Revised Drainage Plan



© PHILLIPPI ENGINEERING INC. 2009

SCALE: 1"=50'

REGISTERED PROFESSIONAL ENGINEER — REGISTERED PROFESSIONAL ENGINEER — STATE OF CALIFORNIA

APPROVED BY:
CITY ENGINEER — DATE OF APPROVAL
CE NO.:

PHILLIPPI ENGINEERING
CIVIL ENGINEERING - LAND SURVEYING
425 MERCHANT STREET VACAVILLE, CA 95688
P.O. BOX 1146 VACAVILLE, CA 95696
OFFICE (707) 451-6556 FAX (707) 451-6555

DESIGNED BY: VAB
DRAFTED BY: VAB
CHECKED BY: APH, II

PRELIMINARY

PROJECT NAME/LOCATION:
COMPETITIVE POWER VENTURES
VACAVILLE CALIFORNIA

DRAWING TITLE:
GRADING AND DRAINAGE PLAN

REVISIONS:

NO.	DESCRIPTION	DATE

DRAWING FILE:

ISSUE DATE: 07/06/09
SHEET NO.:
PROJECT NO.: 271120
OF

Attachment DR93-1
Draft Drainage, Erosion, and Sediment Control Plan

Draft

Drainage, Erosion, and Sedimentation Control Plan for the CPV Vaca Station Project

Prepared for

CPV Vacaville, LLC

CPV Vacaville, LLC

July 2009

CH2MHILL
2485 Natomas Park Drive
Suite 600
Sacramento, CA 95833

Contents

Section **Page**

Acronyms and Abbreviations v
A. Vicinity Map 2
B. Site Delineation 2
C. Watercourses and Critical Areas 4
D. Drainage Map 6
E. Drainage Narrative 7
F. Clearing and Grading Plans 9
G. Clearing and Grading Narrative 9
H. Best Management Practices 10
I. Best Management Practices Narrative 11
J. References 22

Tables

1 Summary of CPVVS Permanent and Temporary Disturbance Areas (in acres) 3
2 Soil Mapping Unit Descriptions and Characteristics 5
3 CPVVS Construction Soil Loss Estimates Using the Revised Universal Soil Loss Equation 7
4 Rational Hydrograph Summary 9
5 Clearing and Grading 10
6 Key Construction Events 11
7 BMP Implementation and Maintenance Schedule 11
8 Environmental Emergency Telephone List 19

Figures

1 Location Map
2A Vicinity Map (Overview)
2B Vicinity Map (Recycled Water Pipeline/Construction Laydown/Power Plant Site)
2C Vicinity Map (Electrical Transmission Line and Substation)
2D Vicinity Map (Natural Gas Pipeline)
3A Project Site and Laydown Area
3B Site Plan
3C General Arrangement
4 Surface Water Resources
5 Drainages and Watercourses
6 Grading and Drainage Plan
7 Rough Grading Plan (to be provided)
8 Erosion Control Plan (to be provided)
9 Erosion Control Notes and Details (to be provided)
10 Erosion Control Plan – Laydown Areas (to be provided)

Acronyms and Abbreviations

BMPs	best management practices
cfs	cubic feet per second
City	City of Vacaville
CPV	CPV Vacaville, LLC
CPVVS	CPV Vaca Station
DESCP	Drainage, Erosion and Sedimentation Control Plan
DTSC	Department of Toxic Substances Control
EWTP	Easterly Wastewater Treatment Plant
LORS	laws, ordinances, regulations, and standards
MW	megawatt(s)
NPDES	National Pollutant Discharge Elimination System
OES	Office of Emergency Services
PG&E	Pacific Gas and Electric Company
RWQCB	Regional Water Quality Control Board
SWPPP	Stormwater Pollution Prevention Plan
SWRCB	State Water Resources Control Board
yd^3	cubic yards

CPV Vaca Station Project Drainage, Erosion, and Sedimentation Control Plan

CPV Vacaville, LLC (CPV) is currently developing and constructing the CPV Vaca Station (CPVVS) project. The CPVVS will be a 660-megawatt (MW), combined-cycle power generation facility located in Vacaville, Solano County, California on a 24-acre parcel and 6-acre substation in Solano County. The CPVVS site includes the main 24-acre CPVVS power plant, the adjacent 24-acre temporary construction laydown area, the 230-kV transmission line and 6-acre substation to the west of the CPVVS facility, and the natural gas pipeline east of the CPVVS facility. Approximately 1.03 miles of 16-inch-diameter underground natural gas pipeline will convey gas from PG&E line 401 to the project site. This natural gas line will run in a 70-foot-wide easement along Fry Road east to the connection point. A 2,600–foot-long recycled water pipeline will be placed between CPVVS and the adjacent Easterly Wastewater Treatment Plant (EWTP) to supply water to the power plant. The CPVVS facility and its associated features will be constructed, owned, and operated by CPV. The project location is shown in Figure 1 (all figures are provided at the end of this report).

CPV has prepared this Drainage, Erosion and Sedimentation Control Plan (DESCP) for the CPVVS project to demonstrate that construction activities associated with the project will not result in an increase in offsite flooding potential or sedimentation and that the project will meet all local, state, and federal regulatory requirements associated with the protection of water quality and soil resources. The DESCP includes the following elements:

- A vicinity map showing the location of all project elements with depictions of all significant geographic features including swales, storm drains, and sensitive areas.
- A site delineation that includes the boundary lines of all areas subject to disturbance and the location of existing and proposed structures, pipelines, roads, and drainage facilities.
- Watercourses and critical areas including water courses, critical areas, and existing/proposed drainage systems.
- Site maps showing existing drainage measures to be taken to protect the site and downstream facilities. Interim and proposed drainage systems and drainage area boundaries will be provided in a future DESCP update.
- Narrative of the project site drainage including appropriate measures to be taken to protect the site and downstream facilities.
- Preliminary Grading and Drainage Plan discharging to an onsite retention pond.

The following elements will be provided in the DESCP update:

- Clearing and grading plans including delineation of all areas to be cleared of vegetation and areas to be preserved. The plans will provide elevations, slopes, locations, and the extent of all proposed grading. Contours and cross sections will be indicated on drawings.
- A Best Management Practices (BMPs) Plan will identify the location of specific BMPs to be implemented during construction on a topographic site map.

A. Vicinity Map

The CPVVS generating facility is proposed for a 24-acre site on land owned by the City of Vacaville (City) (Assessor's Parcel Number 0142-200-040) at the intersection of Lewis and Fry roads in a rural area. Surrounding land uses include the City's wastewater treatment plant to the northwest, and agricultural uses to the east, west, and south. Primary access to the project site will be provided via an access lane in Lewis Road. The small town of Elmira is approximately 0.5 mile northwest of the CPVVS. The developed, suburban residential area of Vacaville is approximately 1.75 miles to the west. Project vicinity maps are shown in Figures 2A through 2D with project features identified including the power plant site, pipeline routes, electrical transmission line, recycled water pipeline utility corridor, substation, and the construction laydown area.

A 24-acre parcel located north of and adjacent to the project site is planned to be the project construction laydown area. The project site and adjacent laydown area are currently vacant and unused parcels that are owned by the City. The new 6-acre substation site, the proposed electrical transmission line route, and the proposed natural gas pipeline route will be located on land that is currently in agricultural production within rural Solano County.

B. Site Delineation

Figures 3A, 3B, and 3C show the areas subject to soil disturbance for the project site, laydown area, linear facilities, landscaping areas, and other project features. Boundary lines of all construction/demolition areas will be further defined in the final design phase of the project and the DESCP will be updated to reflect any changes including facilities external to the 24-acre project site (pipelines and substation).

The project site contains the CPVVS generating facility (power plant equipment, two industrial buildings, and series of cooling towers), other associated features, and an access road. Table 1 summarizes the acreage of land associated with the project that will be disturbed.

TABLE 1
Summary of CPVVS Permanent and Temporary Disturbance Areas (in acres)

Project Feature	Habitat Type	Permanent	Temporary	Total
CPVVS site	Inactive agriculture	24	0	24
Construction laydown area	Inactive agriculture	—	24	24
Gas pipeline	Active agriculture	—	6.2	6.2
Substation	Active agriculture	6	0	6
230-kV electrical transmission line	Active and inactive agriculture	0.003	0.01	0.013
Potable water supply pipeline*	Inactive agriculture	—	—*	—
Total		**31.003**	**31.21**	**62.213**

*Occurs within the temporary construction laydown area.

Activities such as grading can potentially increase rates of erosion during construction. Additionally, construction materials could contaminate runoff or groundwater if not properly stored and used. Compliance with engineering and construction specifications, following approved grading and drainage plans, and adhering to proper material handling procedures will ensure effective mitigation of these short-term impacts. BMPs for erosion control will be implemented. Erosion and sediment controls, surface water pollution prevention measures, and other BMPs will be developed and implemented for both construction and operational phases. These plans will be prepared in accordance with local agency requirements and the National Pollutant Discharge Elimination System (NPDES) construction permit issued by the State Water Resources Control Board (SWRCB).

To qualify for the NPDES statewide General Permit for Storm Water Discharges Associated with Construction Activity (General Construction Permit), prior to construction CPVVS will be required to develop a Stormwater Pollution Prevention Plan (SWPPP) to prevent the offsite migration of sediment and other pollutants, and to reduce the effects of runoff from the construction site to offsite areas.

The project laydown area will be adjacent to the project site. The CPVVS will connect with the Pacific Gas and Electric Company (PG&E) electrical transmission system via a 0.95-mile-long transmission line that will run west from the project site along Fry Road to a transmission corridor. Connections to PG&E's existing high-pressure natural gas pipeline will be through a new pipeline that will run for 1.03 mile east along Fry Road to a PG&E gas transmission line. The project will connect with the EWTP for supplies of potable water, sanitary sewer, and recycled water through a utility corridor linking the project and the EWTP.

The factors that have the largest effect on soil loss include steep slopes, lack of vegetation, and erodible soils composed of large proportions of fine sands. The soils found in the project area are nearly level, with an estimated average slope of less than 2 percent.

C. Watercourses and Critical Areas

Most of the county, particularly in the east and north, is characterized by hot, dry summers and cool winters. The areas to the south and west are influenced by the Pacific Ocean, having cool, humid summers and moderate winters. In the summer, there is a steady marine wind that blows up the Carquinez Strait. The mean annual precipitation is about 16 to 20 inches, practically all as rainfall. About 95 percent of the total precipitation falls in October through April.

Sensitive biological resources, including natural communities and special-status plant and wildlife species, have the potential to occur in the project area. Nine wildlife species could occur at the CPVVS site including northern harrier (*Circus cyaneus*), Swainson's hawk (*Buteo swainsoni*), mountain plover (*Charadrius montanus*), western burrowing owl (*Athene cunicularia*), short-eared owl (*Asio flammeus*), saltmarsh common yellowthroat (*Geothlypis trichas sinuosa*), yellow-breasted chat (*Icteria virens*), Suisun song sparrow (*Melospiza melodia maxillaries*), and tricolored blackbird (*Agelaius tricolor*). To avoid permanent impacts, the temporary construction laydown area will be re-contoured and restored following project construction to provide suitable nesting and foraging habitat for special-status bird and bat species. All habitats within the CPVVS site have been previously altered, and there are no natural plant communities within areas of ground disturbance for the CPVVS main facility site, the construction laydown area, the 230-kV transmission line, or the natural gas pipeline. Based on the results of the field surveys for rare plants, it is unlikely that special-status plant species occur within the CPVVS construction disturbance areas. Site preparation and construction activities would not occur until a biologist conducts pre-construction and clearance surveys for plant and wildlife species. No significant, unmitigated impacts to special-status wildlife are expected to result from the construction and operation of the CPVVS subsequent to the implementation of awareness training; pre-construction and clearance surveys; avoidance, mitigation, and compensation measures proposed by the Applicant, suggested by the natural resource agencies, and summarized in the Biological Resources Implementation Monitoring Plan.

Proximity of watercourses, swales, storm drains, and ditches are shown in Figures 4 and 5. The agricultural drainages in the area eventually discharge into Alamo Creek. The western primary drainage flows to the east from the project site (at the intersection of Lewis and Fry roads) along Lewis Road, and then flows south to New Alamo Creek.

The project site and the laydown area is on land that was formerly used for agriculture but that has not been cultivated for more than a decade and has been redesignated for community facilities. A few rural residential properties are located within 1 mile of the proposed CPVVS site, mostly off Lewis Road, Fry Road, and Chicorp Lane, with the closest residential properties located approximately 0.7 mile northwest of the project site.

All nearby watercourses including swales, storm drains, and drainage ditches will be further identified in construction drawings for the construction, laydown, and landscape areas including transmission and pipeline corridors. The CPVVS construction activity does not discharge directly to a water body listed as impaired for sedimentation/siltation or turbidity under the Clean Water Act Section 303(d).

In general, soils at the project site are medium to fine in texture, ranging from sandy loam to clay (NRCS, 2008). The erosion potential of these soils will vary, based on the wetness of the soil, soil compaction, sizes of soil particles, and other site-specific properties. The soils at the project site are expected to have relatively high water erosion potential and a moderate wind erosion potential for the following reasons:

- There are nearly level conditions at the site and laydown areas; however, some of the soil units are expected to have slow to very slow permeability (and consequently, high runoff).
- The silty clay and clay surface materials of the Capay soils are not expected to be readily transported by wind. The sandy loam and loam surface materials of the San Ysidro and Yolo soils may be more readily transported by wind. It is expected that the laydown areas will be covered (by gravel or paving) immediately after grading to prevent subsequent wind erosion losses.

The soil mapping units in the project area are primarily fine-textured soils formed from sedimentary deposits. These soils are moderately well to well drained and have moderate to very low permeability. All of the soils within the vicinity of the CPVVS project are considered to have high shrink-swell potential. A geotechnical investigation of the construction suitability of these soils is in progress and will be completed before construction begins.

As shown in Table 2, the entire project site lies within soil mapping unit Ca - Capay silty clay loam. The laydown area is also partially within the Ca mapping unit, and also includes mapping units SeA - San Ysidro sandy loam and Yr - Yolo loam, clay substratum. The linear features cross soil map units Ca, SeA, Yr, and also M-W - Miscellaneous Water and Cc-Capay clay.

Soil map unit characteristics for the area potentially affected by project construction are summarized in Table 2.

TABLE 2
Soil Mapping Unit Descriptions and Characteristics

Map Unit	Description	
Ca	Capay silty clay loam:	
	The entire CPVVS project site, portions of the laydown area, and all three utility corridors cross this soil unit.	
	Formation:	In mod. fine and fine textured alluvium derived from sandstone and shale
	Typical profile:	Silty clay loam over clay and clay loam
	Shrink-swell capacity:	High
	Depth and drainage:	Very deep; moderately well drained
	Permeability:	Slow to very slow
	Runoff:	Negligible to high
	Inherent fertility:	Moderately high
	Capability class:	2s (irrigated), 4s (non irrigated)
	Taxonomic class:	Fine, smectitic, thermic Typic Haploxererts

TABLE 2
Soil Mapping Unit Descriptions and Characteristics

Map Unit	Description	
Cc	Capay clay:	
	The proposed transmission line and natural gas corridors traverse this soil unit	
	Formation:	In mod. fine and fine textured alluvium derived from sandstone and shale
	Typical profile:	Clay over clay loam
	Shrink-swell capacity:	High
	Depth and drainage:	Very deep; moderately well drained
	Permeability:	Slow to very slow
	Runoff:	Negligible to high
	Inherent fertility:	Moderately high
	Capability class:	2s (irrigated), 4s (non irrigated)
	Taxonomic class:	Fine, smectitic, thermic Typic Haploxererts
M-W	Miscellaneous water:	
	A small part of the utility corridor between the CPVVS project site and the EWTP falls within this soil unit. This is an anthropogenic map unit.	
SeA	San Ysidro sandy loam, 0 to 2 percent slopes:	
	The proposed utility corridor and natural gas pipeline traverse this soil unit.	
	Formation:	In alluvium from sedimentary rocks
	Typical profile:	Sandy loam over clay loam and sandy clay loam
	Shrink-swell capacity:	High
	Depth and drainage:	Very deep; moderately well drained
	Permeability:	Very slow
	Runoff:	Slow to medium
	Inherent fertility:	Moderate
	Capability class:	4s (irrigated), 4e (non irrigated)
	Taxonomic class:	Fine, smectitic, thermic Typic Palexeralfs
Yr	Yolo loam, clay substratum:	
	The proposed utility corridor traverses this soil unit.	
	Formation:	In fine loamy alluvium derived from sedimentary formations
	Typical profile:	Loam over clay
	Shrink-swell capacity:	High
	Depth and drainage:	Very deep; well drained
	Permeability:	Moderate
	Runoff:	Slow to medium
	Inherent fertility:	Moderately high
	Capability class:	2s (irrigated), 4e (non irrigated)
	Taxonomic class:	Fine-silty, mixed, superactive, nonacid, thermic Mollic Xerofluvents

Soil characteristics are based on soil mapping descriptions provided in the online soil survey (http://websoilsurvey.nrcs.usda.gov).

D. Drainage Map

Figure 5 shows the location of nearby drainages and watercourses in relation to CPVVS construction and laydown areas, including transmission and pipeline alignments.

Drainage from the site will be directed to the detention pond. A preliminary grading and drainage plan is presented in Figure 6.

E. Drainage Narrative

The Ulatis Creek Watershed is the primary watershed in the project area and includes the Alamo Creek sub-watershed. It comprises many smaller creeks, including Alamo, Ulatis, Horse, Gibson Canyon, Sweeney, and McCune creeks (Ulatis Resource Conservation District, 2002) and covers about 150 square miles within the northwestern portion of Solano County. New Alamo Creek is an engineered earthen channel designed to convey flood flows from just above Leisure Town Road to the confluence with Ulatis Creek. Cache Slough begins at the terminus of Ulatis Creek, about 5.5 miles downstream of the confluence of New Alamo and Ulatis creeks. The Cache Slough channel morphology changes dramatically downstream of the confluence with Ulatis Creek, widening from about 300 to 1,500 feet because of tributaries entering from the north and east. Cache Slough, being a tributary to the Sacramento-San Joaquin Delta, is tidally influenced; therefore, flows from Ulatis Creek and other creeks entering Cache Slough are affected by the Delta's tidal gradient (SWRCB, 2007).

Currently, no structures exist on the proposed site, and the site has no stormwater system other than percolation into the existing soils or runoff into existing culverts and the terrain is fairly flat. Stormwater from the equipment drains will go to the oil/water separator for treatment and will be recovered for use as part of the cooling tower makeup. All other stormwater from the site will drain into the retention pond that will be built as part of the project, therefore there will be no discharge of stormwater to any nearby waterways, and impacts due to stormwater runoff and drainage will not occur. The CPVVS construction site totals 24 acres. Active soil grading will occur over a 4-month period. The soil in this area will then be exposed for an additional 20-month construction period, after which the majority of the site will be paved or covered with CPVVS facilities. It is assumed that about one-half of the project site will have bare soil exposure during the construction period.

The site grading and drainage will be designed to comply with all applicable laws, ordinances, regulations, and standards (LORS). The general site grading will establish a working surface for construction and plant operating areas, and will provide positive drainage from buildings and structures, as well as adequate ground coverage for subsurface utilities. An estimate of soil loss during construction by water erosion is provided in Table 3.

TABLE 3
CPVVS Construction Soil Loss Estimates Using the Revised Universal Soil Loss Equation[a]

Feature and Acreage[b]	Activity	Duration (months)	Soil Loss without BMPs (tons)	Soil Loss with BMPs (tons)	Soil Loss No Project (tons/year)
Project Site–24 acres	Grading	4	26.4	0.04	0.336
	Construction	20	6.4	0.18	—
Laydown Area–18.9 acres	Grading	1	5.4	0.00	0.27
	Construction	22	85.1	2.40	—
New Substation–6 acres	Grading	1	1.7	0.00	0.084
	Construction	9	0.7	0.02	—

TABLE 3
CPVVS Construction Soil Loss Estimates Using the Revised Universal Soil Loss Equation[a]

Feature and Acreage[b]	Activity	Duration (months)	Soil Loss without BMPs (tons)	Soil Loss with BMPs (tons)	Soil Loss No Project (tons/year)
Transmission Line–6.14 acres (plus 0.0098 acre for poles)	Grading	1	0.002	0.001	0.000
	Construction	2	0.096	0.003	—
Natural Gas Line–9.67 acres (plus 0.55 acre for trench)	Grading	1	0.151	0.018	0.01
	Construction	2	1.283	0.036	—
Utility Corridor–4.97 acres (plus 0.28 acre for trench)	Grading	1	0.0736	0.00875	0.004
	Construction	2	0.624	0.018	—
Project Soil Loss Estimates		**22**	**127.83**	**2.83**	**0.70**

[a] Soil losses (tons/acre/year) are estimated using RUSLE2 software available online at http://fargo.nserl.purdue.edu/rusle2_dataweb/RUSLE2_index.htm.

[b] Acreages assume 70-foot-wide corridors for the transmission line, natural gas, and utility construction corridors. Trenches for the natural gas and utility corridors are assumed to be 4 feet wide.

With the implementation of appropriate BMPs that will be required under the NPDES permit, the total project soil loss (estimated to be approximately 2.83 tons) is considered to be a minimal amount. It also should be recognized that the estimate of accelerated soil loss by water is very conservative (overestimate of soil loss) because it assumes only a single BMP (that is, silt fencing), whereas a SWPPP will require multiple soil erosion control measures.

Under the NPDES *General Permits for Storm Water Discharges from Construction Sites*(SWRCB, 1999), it is necessary to estimate the runoff coefficient of the site before and after construction is complete.

Stormwater runoff at the undeveloped project site is predominantly from west to east across an open field with an approximate slope of 0.33%, eventually discharging at the existing low point at the southeastern corner of the site where stormwater runoff exits into a roadside ditch. Currently, drainage from the site is discharged to New Alamo Creek via a drainage ditch running south along Lewis Road. The drainage area is approximately 25.5 acres. The pre-development site generated a 100-year peak runoff of 7.44cfs (Phillipi Engineering, 2009). Any increase in peak runoff resulting from the project will be mitigated with the onsite detention pond.

The developed site will incorporate asphalt, gravel, and landscaping. Stormwater runoff will be sheet flow to culverts and ditches that discharge into the detention pond located at the southeast corner of the site adjacent to the intersection of Fry Road and Lewis Road. The detention pond will have a gravity overflow outlet to the existing culvert draining south across Fry Road to allow emergency overflows resulting from a storm event in excess of the 100-year design storm or from an outflow structure failure. The developed site drains from the west to the east into the detention pond. Post development storm runoff peak flow rates may not exceed pre-development peak flow rates according to City of Vacaville design criteria. Table 4 provides the pre and post-construction runoff calculations for the project site. Further detailed information is available in the CPV Vaca Hydrology Study (Phillipi

Engineers, 2009). The detention pond will mitigate the concentrated peak runoff flows from the developed site.

TABLE 4
Rational Hydrograph Summary
Pre-Construction and Developed Site Storm Event Peak Flow

	2-year (cfs)	10-year (cfs)	100-year (cfs)
Pre-construction	1.03	3.56	7.44
Post-construction	7.79	14.81	23.03

Source: Phillippi Engineering, 2009
cfs = cubic feet per second

F. Clearing and Grading Plans

Rough grading plans are not available at this stage of the project. Prior to the start of construction, the DESCP will be updated to include these plans and final design information. For the final developed condition, the CPVVS site will be graded such that all runoff will be collected for discharge to the onsite detention pond.

G. Clearing and Grading Narrative

The information provided in this section is preliminary and will be updated and expanded upon once the clearing and grading plans are completed and prior to the start of construction. Site grading design will comply with applicable land development regulations. Graded areas will be smooth, compacted, free from irregular surface changes, and sloped to drain to onsite drainage features and the detention pond.

Construction impacts on soil resources can include increased soil erosion and soil compaction. Soil erosion causes the loss of topsoil and can increase the sediment load in surface receiving waters downstream of the construction site. The magnitude, extent, and duration of construction-related impact depends on the erodibility of the soil; the proximity of the construction activity to the receiving water; and the construction methods, duration, and season. Because conditions that could lead to excessive soil erosion are not present at the CPVVS site, little soil erosion is expected during the construction period.

The project site will require earthwork to construct the CPVVS and associated facilities. Soil-disturbing activities will include grubbing and clearing, rough grading, excavating, filling, and final grading. For all areas where earthwork will be executed, materials suitable for compaction will be stockpiled in designated onsite locations. Materials not suitable for compaction will be stored in separate stockpiles and reused on the site, as appropriate. Any contaminated materials encountered during excavation will be disposed of in accordance with applicable LORS. Only licensed, commercial fill will be used and there will not be a borrow or disposal site for the project.

The construction contractor will perform clearing and grubbing of the construction areas using scrapers or the equivalent. Clearing and grubbing on the 24-acre project site will last

approximately 4 months. Areas cleared and grubbed will be smoothed by earthwork equipment, possibly a grader or similar piece of equipment, and compacted by vibrating rollers. Concrete, mechanical, and electrical works will be performed over a period of 20 months, with the aid of graders, rollers, front loaders, dump trucks, trenching machines, concrete mixer and pump trucks, cranes, and pick-ups. Table 5 outlines the amount of cut and fill planned for specific components of the project (the DESCP will be updated once this information becomes available).

TABLE 5
Clearing and Grading

Description	Stockpile (yd^3)	Total Cut (yd^3)	Total Fill (yd^3)
To be determined.			
Total			

yd^3 = cubic yards

The following subsections provide a discussion of clearing and grading associated with each of the major construction elements of the project.

CPVVS Project Site

Earthwork will consist of removal of topsoil, vegetation, and debris; excavation and compaction of earth to create the plant grade; and excavation for foundations and underground systems. Information on the volume of excavation and fill will be determined prior to the start of construction. Thirty-one acres of land will be disturbed permanently, and 31.2 acres will be disturbed temporarily.

Construction Laydown and Parking Areas

A total of 24 acres east of the project site will be used for construction laydown and parking areas. The temporary construction laydown and parking areas may be graded and covered in gravel.

H. Best Management Practices

Potential impacts from construction will be controlled through implementing a SWPPP and associated BMPs, and practicing proper housekeeping at the construction site. The site grading and drainage will be designed to comply with all applicable LORS. The general site grading will establish a working surface for construction and plant operating areas, and will provide positive drainage from buildings and structures, as well as adequate ground coverage for subsurface utilities.

During project construction, erosion and sediment control measures will be implemented by the contractor to prevent sediment-laden runoff from leaving the site. During construction, the constructed detention pond will be used as a sediment basin. Construction runoff will be directed to the onsite detention basin.

BMPs will be implemented during construction in accordance with the SWPPP required for all construction projects over 1 acre by the Regional Water Quality Control Board (RWQCB). Monitoring will involve inspections to ensure that the BMPs described in the SWPPP/DESCP are properly implemented and effective.

The placement and details of the BMPs that will be utilized during project construction will be identified during project design. Placement of BMPs to be employed at the construction laydown areas will be identified in the erosion control plan provided by the contractor prior to construction. Updated BMP maps shall be provided once the SWPPP is complete. As part of the SWPPP, a current version of the BMP drawings are maintained in the project construction trailer and updated regularly to reflect modified or new BMPs that are being implemented and maintained on site.

I. Best Management Practices Narrative

The project construction schedule is provided in Table 6. An implementation and maintenance schedule for the drainage, erosion, and sediment control methods and practices that will be implemented as appropriate at the CPVVS project site are included in Table 7.

TABLE 6
Key Construction Events

Event Description	Expected Dates
Date of Certification by CEC	TBD
Start of Rainy Season	October 15 (Typical) *Project site and linears must have SWPPP protection measures implemented prior to first rain and these measures must remain in effect for years 2010 through 2012.*
End of Rainy Season	May 1 (Typical)
Clearing and Grubbing	Second quarter 2011
Rough Grading	Second quarter 2011
Construction of Storm Drain Improvements	Fourth quarter 2011
Final Grade	Second quarter 2012
Building Construction	Third quarter 2012
Paving	Second quarter 2013
Completion of Construction	Second Quarter 2013
Start of Operation	Second Quarter 2013

TABLE 7
BMP Implementation and Maintenance Schedule

Best Management Practices	Implementation	Inspection Frequency	Maintenance
Silt fence	Two weeks prior to construction	Inspect before and after storm events (and once each 24-hour period during extended storm events), once a week during rainy season, and bi-weekly during dry season	Replace torn sections, repair up-rooted sections, clean out collected soils when greater the 1/3 height of fence
Straw wattle dikes	Two weeks prior to construction	Inspect before and after storm events (and once each 24-hour period during extended storm events), once a week during rainy season, and bi-weekly during dry season	Replace crushed sections, replace rotted sections, clean out collected soil when greater than 1/3 height of roll
Coir logs (rolls)	Two weeks prior to construction	Inspect before and after storm events (and once each 24-hour period during extended storm events), once a week during rainy season, and bi-weekly during dry season	Replace crushed sections, replace rotted sections, clean out collected soil when greater than 1/3 height of roll
Erosion control blankets (geotextiles)	Two weeks prior to construction	Inspect before and after storm events (and once each 24-hour period during extended storm events), once a week during rainy season, and bi-weekly during dry season	Replace/repair as necessary
Straw bales	Two weeks prior to construction	Inspect before and after storm events (and once each 24-hour period during extended storm events) and once a week during dry periods	Clean out collected soil when greater than 1/3 height of roll
Sandbags	Two weeks prior to construction	Inspect before and after storm events (and once each 24-hour period during extended storm events), once a week during rainy season, and bi-weekly during dry season	Repair, reshape, replace bags as necessary, replace bags exposed to sunlight every 2 to 3 months, clean out collected soil when greater than 1/3 height of bag
Gravelbags	Two weeks prior to construction	Inspect before and after storm events (and once each 24-hour period during extended storm events), once a week during rainy season, and bi-weekly during dry season	Repair, reshape, replace bags as necessary, replace bags exposed to sunlight every 2 to 3 months, clean out collected soil when greater than 1/3 height of bag

TABLE 7
BMP Implementation and Maintenance Schedule

Best Management Practices	Implementation	Inspection Frequency	Maintenance
Hydraulic mulch	Two weeks prior to construction	Inspect before and after storm events (and once each 24-hour period during extended storm events), once a week during rainy season, and bi-weekly during dry season	Areas where erosion is evident shall be repaired and BMPs re-applied as soon as possible; maintain an unbroken, temporary mulched ground cover throughout the period of construction when the soils are not being reworked
Straw, wood, organic mulch	Two weeks prior to construction	Inspect before and after storm events (and once each 24-hour period during extended storm events), once a week during rainy season, and bi-weekly during dry season	Reapply mulch when bare earth becomes visible
Seeding	As soon possible after disturbance has permanently or temporarily ceased, but in no case more than 14 days after the construction activity in an area has ceased (Except when construction activity will resume on that portion of the site within 21 days)	Inspect before and after storm events (and once each 24-hour period during extended storm events), once a week during rainy season, and bi-weekly during dry season (monitored every May for the first 3 years following project completion)	Areas that do not meet revegetation criteria will be reseeded
Hydroseeding	Two weeks prior to construction (avoid use of hydroseeding in areas where the BMP would be incompatible with future earthwork activities and would have to be removed)	Inspect before and after storm events (and once each 24-hour period during extended storm events), once a week during rainy season, and bi-weekly during non-rainy season	Areas where erosion is evident shall be repaired and BMPs re-applied as soon as possible; where seeds fail to germinate, or they germinate and die, the area must be re-seeded, fertilized, and mulched within the planting season, using not less than half the original application rates
Permanent revegetation	As soon possible after disturbance has permanently or temporarily ceased, but in no case more than 14 days after the construction activity in an area has ceased (Except when construction activity will resume on that portion of the site within 21 days)	Inspect before and after storm events (and once each 24-hour period during extended storm events), once a week during rainy season, and bi-weekly during dry season (monitored every May for the first 3 years following project completion or until the site has been successfully revegetated to 75 percent coverage)	Areas that do not meet revegetation criteria will be reseeded

TABLE 7
BMP Implementation and Maintenance Schedule

Best Management Practices	Implementation	Inspection Frequency	Maintenance
Aggregate surfacing	Two weeks prior to construction	Once a week during rainy season and bi-weekly during dry season	Keep all temporary roadway ditches clear, periodically apply additional aggregate on gravel roads, active dirt construction roads are commonly watered three or more times per day during the dry season.
Stockpile management	Place prior to the commencement of associated activities	Once a week during rainy season and bi-weekly during dry season	Repair and/or replace perimeter controls and covers as needed to keep them functioning properly
Stabilized construction entrance/exit	Two weeks prior to construction	Once a week during rainy season and bi-weekly during dry season	Inspect local roads adjacent to the site daily, remove aggregate, separate and dispose of sediment if construction entrance/exit is clogged with sediment, keep all temporary roadway ditches clear, check for damage and repair as needed, replace gravel material when surface voids are visible, remove all sediment deposited on paved roadways within 24 hours, remove gravel and filter fabric at completion of construction
Street sweeping, vacuuming	Once construction commences	Inspect before and after storm events (and once each 24-hour period during extended storm events), when actively in use, points of ingress and egress must be inspected daily, otherwise once a week	When tracked or spilled sediment is observed outside the construction limits, it must be removed at least daily; after sweeping is finished, properly dispose of sweeper wastes at an approved dumpsite

The following describes the BMPs that will be implemented at the CPVVS project site and the construction laydown area as necessary during the pre-construction, construction, and post-construction phases of the project.

Scheduling. Construction shall be scheduled to minimize construction activities impacts during the rainy season consistent with local and resource agency regulations.

Preservation of Natural Features. Prior to the commencement of soil-disturbing activities, areas of existing vegetation that are to remain and environmentally sensitive areas shall be

fenced for protection. In general, site designs shall preserve existing vegetation to the maximum extent possible. During construction, existing vegetation shall be preserved and protected by fencing for as long as possible to minimize erosion.

Stormwater Run-on and Concentrated Flows. Existing watercourses shall be protected. To the extent feasible, all concentrated water flows shall be channeled away from disturbed soil areas and stockpiles. Concentrated water flows shall be conveyed in a non-eroding fashion. Erosion in areas of concentrated flow paths shall be controlled by applying erosion control blankets, erosion control seeding, and lining of swales.

Stockpile Management. Stockpiles shall be managed according to the type of material being stockpiled and the season, as follows:

- Soil stockpiles shall be covered or protected with soil stabilization measures and perimeter sediment barriers during the rainy season and covered or protected with perimeter sediment barriers during the non-rainy season.
- Concrete/asphalt rubble, rock, and aggregate base and sub-base stockpiles shall be covered or protected with perimeter sediment barriers year-round.
- Cold mix asphalt stockpiles shall be covered year-round.

Disturbed Soil Area Management. Disturbed soil areas shall be protected with an effective combination of measures including soil stabilization, sediment barriers, and basins/traps.

- Soil Stabilization – Hydraulic mulch; hydroseeding; suitably stabilized, non-polluting straw/wood/organic mulch; geotextiles; stabilized construction roadways
- Sediment Barriers – Silt fences; sand and gravel bag barriers; straw bale barriers; fiber rolls
- Basin/Traps – sediment traps

Temporary erosion control shall be applied to remaining active and non-active areas as needed. Temporary erosion control measures will be implemented prior to the start of the rainy season (defined as October 15 to May 1). Vegetative stabilization shall occur as soon as possible after disturbance has permanently or temporarily ceased, generally no more than 14 days after the construction activity in an area has ceased.

Disturbed areas will be provided with permanent vegetative cover once construction in that area is complete. A successfully revegetated site must achieve 75 percent coverage. Seeding operations will take place after areas have received final grading.

Offsite Sediment Tracking. The construction entrance and exit will be constructed and maintained to reduce tracking of sediments onto public streets. Excess material tracked onto public streets will be removed as necessary using a street sweeper with a water supply. Dump trucks hauling material from the site will be covered with tarpaulin. These BMPs will be implemented during the rainy and non-rainy seasons as needed.

Petroleum Products. Construction equipment will require use of diesel fuel and oil on a regular basis. While a potential exists for spills or leaks, all onsite vehicles will be monitored for leaks and receive regular preventive maintenance to ensure proper operation and reduce

the chance of leakage. No "topping off' of fuel tanks will be allowed to further reduce the possibility of spills.

Petroleum products will be stored in clearly labeled and tightly sealed containers or tanks. Any asphalt used on site will be applied according to the manufacturer's recommendations. Any soil impacted by fuel or oil spills will be removed and disposed of by the contractor at an approved disposal site. It will be the contractor's responsibility to ensure that secondary containment around fuel/oil tanks (stationary or mobile) will meet the minimum requirements of U.S. Environmental Protection Agency 40 Code of Federal Regulations Part 112 with regard to secondary containment or more stringent state requirements, if applicable. Any spills will be contained and cleaned up immediately.

Sanitary Wastes. A licensed sanitary waste management contractor will collect all construction or temporary sanitary wastes from the portable units. The units will be maintained on a regular basis. Portable units shall be anchored to prevent blowing or tipping over and all leaks or spills shall be reported immediately (sampling may be required).

Hazardous Wastes. Potentially hazardous waste associated with construction of the project will be limited to small quantities of liquids and solids such as lubricating oils, acids for equipment cleanup, concrete curing compounds, and waste paint. These wastes are typical of industrial construction activities and will be placed in containers on site and disposed of in accordance with applicable LORS and with the manufacturer's recommendations. Hazardous wastes will be either recycled or disposed of in a licensed Class I disposal facility, as appropriate. Waste oil and used oil filters will be recycled if the maintenance activities take place on site. Waste generated during each chemical cleaning operation will be temporarily stored on site in portable tanks and disposed of offsite by the chemical cleaning contractor at an appropriate disposal facility. Site personnel will be instructed of these procedures and the contractor's site manager will be responsible for implementing these practices.

To prevent contact of hazardous wastes with stormwater runoff, secondary containment will be provided, such as curbs and berms. As much as possible, all materials will be kept in a dry covered area.

Paints. All containers will be tightly sealed and properly stored to prevent leaks or spills. Excess paint will not be discharged to the stormwater system. Unused paints will be disposed of in labeled original containers according to applicable local, state, and federal laws and regulations. Spray painting will not occur on windy or rainy days, and a drop cloth will be used to collect and dispose of drips associated with painting activities. All paints will be mixed indoors, in a containment area. If using water-based paints, equipment will be cleaned in a sink that is connected to the sanitary sewer.

Concrete Trucks. Concrete trucks will not be allowed to discharge surplus concrete and drum wash at the site, unless these materials are fully contained in an engineered structure that can contain all free liquid until dry. Dried concrete shall then be removed and disposed of at an offsite location. Alternatively, concrete washout will be taken offsite for disposal by the concrete contractor. No surplus concrete or drum wash water will be disposed of onto the ground surface.

Waste Materials. All construction waste material, trash, and construction debris will be collected and stored in a metal dumpster, leased from a licensed solid waste management contractor. The dumpster will meet all local and state solid waste management regulations. The dumpster will be emptied a minimum of twice per week or more often if necessary, and the trash will be hauled to the local dump. No construction waste will be buried on site. All site personnel will be instructed regarding the correct procedure for waste disposal. The site manager will be responsible for seeing that these procedures are followed. All dumpsters will be covered, where possible.

Good Housekeeping. Good housekeeping practices are designed to maintain a clean and orderly work environment. The good housekeeping practices listed below will be followed to reduce the risk of potential pollutants entering stormwater discharges. All construction personnel will be responsible for monitoring and maintaining housekeeping tasks and reporting potential problems to the contractor's site manager:

- Store only enough products required for doing the job.
- Store all materials in a neat and orderly manner in the appropriate containers. Materials that may adversely impact stormwater, such as paint, oils, greases, sealers, etc., will be stored in covered areas such as temporary/permanent buildings or trailers, in accordance with the SWPPP.
- Keep products in the original container with the original manufacturer's label.
- Do not mix products unless recommended by the manufacturer.
- Use all of a product before disposing of the container.
- Use and dispose of products according to the contractor's site manager's direction or manufacturer's recommendations.
- Perform regular inspections of the stormwater system and the material storage areas.
- When and where appropriate, use posters, bulletin boards, or meetings to remind and inform construction personnel of required procedures.
- Preventive maintenance includes regular inspection and maintenance of structural stormwater controls (catch basins, oil/water separators, etc.) as well as other facility equipment and systems.

Storage areas for hazardous materials such as oils, greases, paints, fuels, and chemicals will be provided with secondary containment to ensure that spills in these areas do not reach stormwater. All hazardous chemical storage areas will be surrounded by curbs or dikes to contain the chemicals in the event of leaks or spills. The contractor shall establish contingencies for the proper disposal of contaminated soils (use of licensed hauler, approved landfill) early in the construction period. Secondary containment will be designed to hold the entire contents of the largest single storage container plus rainfall from a 50-year, 24-hour storm for all outdoor storage areas. Curbs and dikes will be provided around all chemical storage areas, hazardous waste products, areas with possibility of oil spill, and washout areas.

Spills and leaks are one of the largest potential sources of stormwater pollutants at industrial facilities. Chemicals will be stored in chemical storage facilities appropriately designed for their individual characteristics. Bulk chemicals will be stored outdoors in aboveground storage tanks. Other chemicals will be stored and used in their delivery containers. All hazardous chemical storage areas will be surrounded by curbs or dikes to contain the chemicals in the event of leaks or spills. Secondary containment will be sized to hold the entire contents of the largest single storage tank. All drains and vent piping for volatile chemicals will be trapped and isolated from other drains. Containment areas for bulk storage tanks will not be drained. Any chemical spills in these areas will be removed with portable equipment and reused or disposed of properly. It is anticipated that all substances will be applied/dispensed at manufacturer's recommendations.

In addition to the housekeeping and hazardous materials storage procedures described, spill prevention and cleanup practices will be as follows:

- CPV's site manager or appointee is responsible for informing construction personnel of the manufacturer's recommended spill cleanup methods, and the location of that information and cleanup supplies.
- Materials and equipment for the cleanup of a relatively small spill will be kept in the materials storage area. These facilities may include brooms, rags, gloves, shovels, goggles, sand, sawdust, absorbent, plastic or metal trash containers, and protective clothing.
- All containers will be labeled, tightly sealed, and stacked or stored neatly and securely.

Spill response procedures will be as follows:

- Step 1: Upon discovery of a spill, stop the source of the spill.
- Step 2: Cease all spill material transfer until the release is stopped and waste removed from the spill site.
- Step 3: Initiate containment to prevent spill from reaching State waters.
- Step 4: Notify supervisor and CPV's site manager of the spill.
- Step 5: CPV's site manager will immediately notify the CPV emergency coordinator, and coordinate further cleanup activities
- Step 6: Any significant spill of hazardous material will be reported to the appropriate state and/or local agencies by CPV personnel or qualified contractors. Table 8 lists the project's environmental emergency contacts.
- Step 7: Review the construction SWPPP and amend, if needed. Record a description of the spill, cause, and cleanup measures taken.

Inspection, Maintenance, and Recordkeeping Procedures. Site inspection and facility maintenance are important features of an effective stormwater management system. The contractor's qualified personnel will inspect disturbed areas of the site that have not been stabilized, storage areas exposed to precipitation, all control measures, and site access areas

to determine if the control measures and stormwater management system are effective in preventing significant impacts to receiving waters.

Inspections will be performed during the non-rainy season once every 2 weeks. Maintenance shall be performed as necessary.

TABLE 8
Environmental Emergency Telephone List

Company/Organization	Telephone Numbers
CPV Vacaville, LLC (During Construction)	
Primary Facility Emergency Coordinator: Name, Manager	tbd
24-Hour Telephone Number: CPVV Dispatch	
Alternate Facility Emergency Coordinator: Name, Principal Engineer	tbd
CPVV Environmental Specialist: Name CPVV Media Representative: Name CPVV Headquarters Telephone Operator	
CPV Vacaville, LLC (During Operation)	
Primary Facility Emergency Coordinator: Name, Manager	tbd
24-Hour Telephone Number: CPVV Dispatch	
Alternate Facility Emergency Coordinator: Name, O&M Supervisor	
CPVV Environmental Specialist: Onsite Employee CPVV Media Representative: name CPVV Headquarters Telephone Operator	
Other Resources	
3E Company (MSDS by FAX):	(800) 451-8346
Chemtrec (emergency chemical information):	(800) 424-9300
Poison Control Center:	(800) 662-9886
Federal Agency	
U.S. Coast Guard/National Response Center:	(800) 424-8802
State Agencies	
California Office of Emergency Services (OES):	(800) 852-7550
California Department of Toxic Substances Control (DTSC):*	(800) 852-7550
California Department of Fish and Game:*	(800) 852-7550
California State Lands Commission:	(562) 590-5201
Regional Water Quality Control Board*:	(800) 852-7550
Local Contacts	
Solano County Environmental Health Department:	(707) 421-6765
Fire – Vacaville Fire District:	911 or (707) 447-2252
Police – Vacaville Police Department:	911 or (707) 449-5200
Hospital – Vaca Valley Hospital:	911 or (707) 446-4000
Ambulance/Paramedics:	911

*DTSC, RWQCB and California Department of Fish and Game have requested that emergency notifications to these offices be made through the OES 800 number.

Inspections will be performed before and after storm events and once each 24-hour period during extended storm events to identify BMP effectiveness and implement repairs or design changes as soon as feasible depending on field conditions. The discharger will complete an inspection checklist, which will include the following information:

- Inspection date
- Weather conditions
- A description of any inadequate BMPs
- List of observations of all BMPs
- Corrective actions required, including any changes to the DESCP
- Inspector name, title, and signature

Erosion and Sediment Controls. The following procedures will be used to maintain erosion and sedimentation controls:

- All control measures will be inspected before and after storm events and once each 24-hour period during extended storm events.
- All measures will be maintained in good working order; if a repair is necessary, that repair will be initiated within 24 hours of the report.
- Sediment will be removed from the silt barriers when it has reached one-third of the height of the barrier.
- Silt barriers will be inspected for depth of accumulated sediment, tears, attachment to posts, and stability on a weekly basis.
- Aggregate-covered areas will be inspected for bare spots and washouts.
- The CPV site manager will select individuals to be responsible for inspections, maintenance, repairs, and reporting. The designated inspectors will receive the necessary training from CPV's site manager to properly inspect and maintain the controls in good working order.
- An inspection form will be completed after each inspection.
- The completed inspection forms will be retained on site.

Non-stormwater Controls. The following procedures will be used to maintain the non-stormwater controls:

- All control measures will be inspected before and after storm events and once each 24-hour period during extended storm events.
- All measures will be maintained in good working order; if a repair is necessary, that repair will be initiated within 24 hours of the report.
- The designated inspector will visually observe all drainage areas for the presence of unauthorized non-stormwater discharges and their sources.

- If a spill occurs that cannot be cleaned up before the next rain event, or under other circumstances warranting sample collection, the designated inspector will collect stormwater samples during the first 2 hours (including weekends or holidays) of discharge. Similarly, if it appears that BMPs have failed or been damaged to the extent that they could result in discharge of pollutants in stormwater, and are discharging potentially impacted water, samples should be collected. Sampling will also be performed in cases where stormwater comes in contact with exposed materials that could potentially contaminate stormwater runoff. The samples should be analyzed for visible and non-visible compounds with the analytical testing suite determined from the specific materials spilled or not contained properly, and for any constituents in the spill that occur in high enough concentrations to cause an impact to water quality.
- The CPV site manager will select individuals to be responsible for inspections, maintenance, repairs, and reporting. The designated inspectors will receive the necessary training from CPV's site manager to properly inspect and maintain the controls in good working order.
- An inspection form will be completed after each inspection.
- The completed inspection forms will be retained on site.

Recordkeeping. Two inspection forms will be completed demonstrating that inspections and maintenance of the control measures are implemented: Erosion and Sedimentation Controls, and Non-stormwater Source Controls. All disturbed areas and materials storage areas require inspection at least daily before and after storm events and once each 24-hour period during extended storm events. After each inspection, the inspector will complete an inspection report and retain a copy of the report. Any maintenance required will be initiated within 24 hours of the inspection.

A copy of this DESCP and any supporting materials must be maintained at the construction site from the date of California Energy Commission approval to the date of final stabilization. All records and supporting documents will be compiled in an orderly manner and maintained on site until final site stabilization is completed.

The generation of reports, as part of the construction process and inspection or amendment procedures, provides accurate records, which can be used to evaluate the effectiveness of this DESCP and document compliance. Changes in design or construction of the stormwater management system are documented and included with the DESCP to facilitate review or evaluation.

Post-construction Stormwater Management. Final erosion and sediment control measures for final stabilization or exposed soil will be in place prior to final sign-off of improvements. The following post-construction erosion and sediment control measures will be used at the site once all construction is complete:

- Seeding
- Hydroseeding
- Mulching
- Removal of debris from drain inlet bags
- Removal of temporary erosion sediment control measures

- Permanent turf on all unprotected soil surface
- Removal of temporary erosion and sediment control measures (if necessary)

J. References

Phillippi Engineering. 2009. CPV Vaca Station Hydrology Study.

Soil Survey Staff. 2008. Official Soil Series Descriptions (Online). Available at http://soils.usda.gov/technical/classification/osd/index.html.

SWRCB. 1999. National Pollutant Discharge Elimination System (NPDES) General Permit for Storm Water Discharges Associated with Construction Activity (General Permit) Water Quality Order 99-08-DWQ

State Water Resources Control Board Central Valley Region 5 Basin Plans. 2007. Alamo Creek, Ulatis Creek and Cache Slough, Solano County. CEQA Scoping Meeting. Evaluating water quality standards for the protection of human health in Alamo and Ulatis creeks and Cache Slough, Solano County. Information Document 2007.

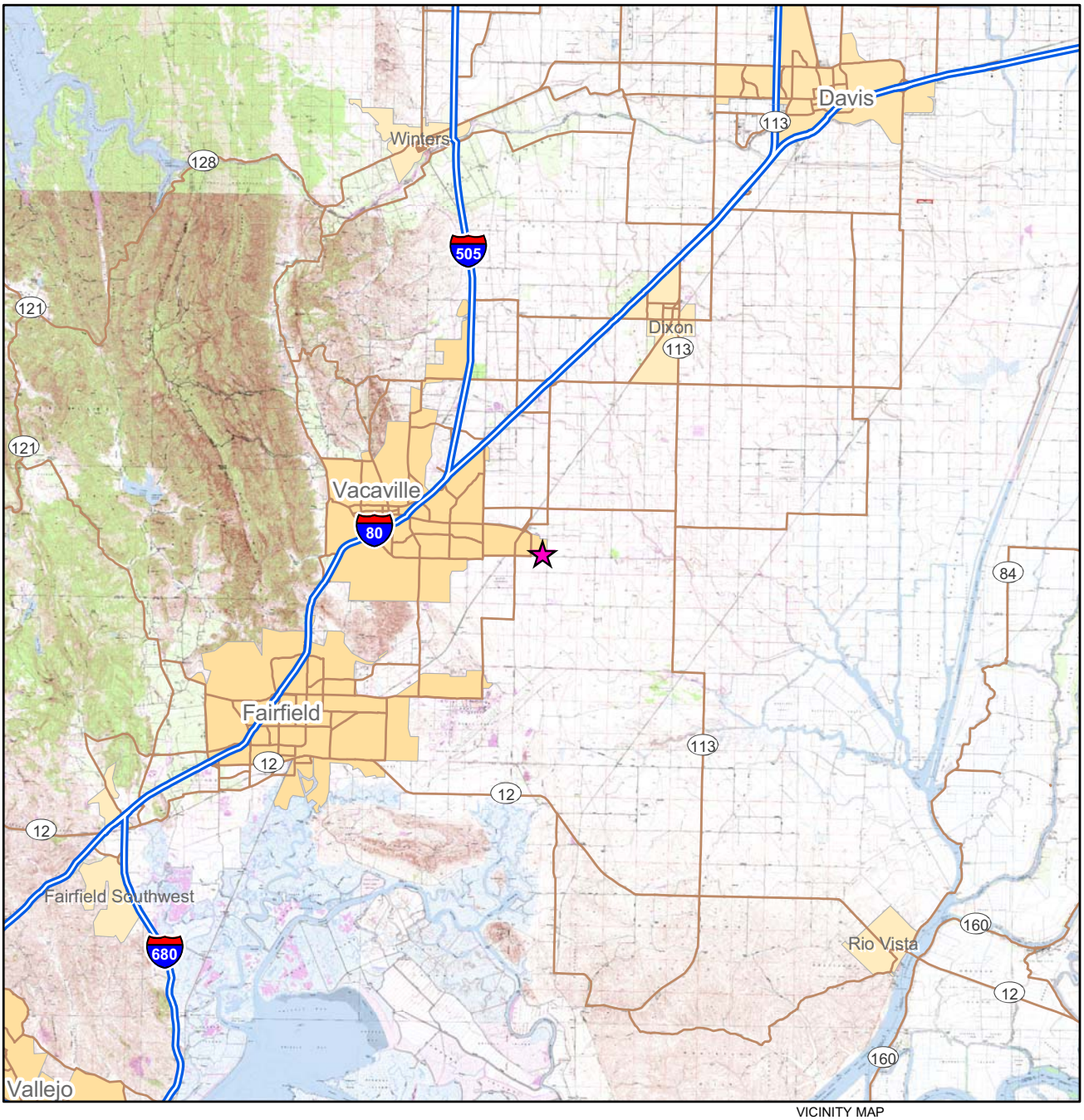
State Water Resources Control Board. 2007. http://swrcb2.swrcb.ca.gov/centralvalley/water_issues/basin_plans/alamocreek.shtml website accessed May 18, 2008.

Ulatis Resource Conservation District 2002. http://www.carcd.org/wisp/ulatis/index.htm Website accessed May 18, 2008.

USDA-NRCS. 1992. Soil Survey of Solano County, California. In cooperation with the Regents of the University of California (Agricultural Experiment Station) and the California Department of Conservation. October.

USDA-NRCS. 2008. Soil Survey Geographic (SSURGO) database for Solano County, California [Online]. Available at http://soildatamart.nrcs.usda.gov.

Figures



LEGEND

Project Site

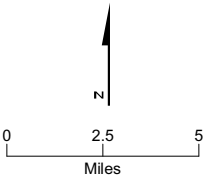
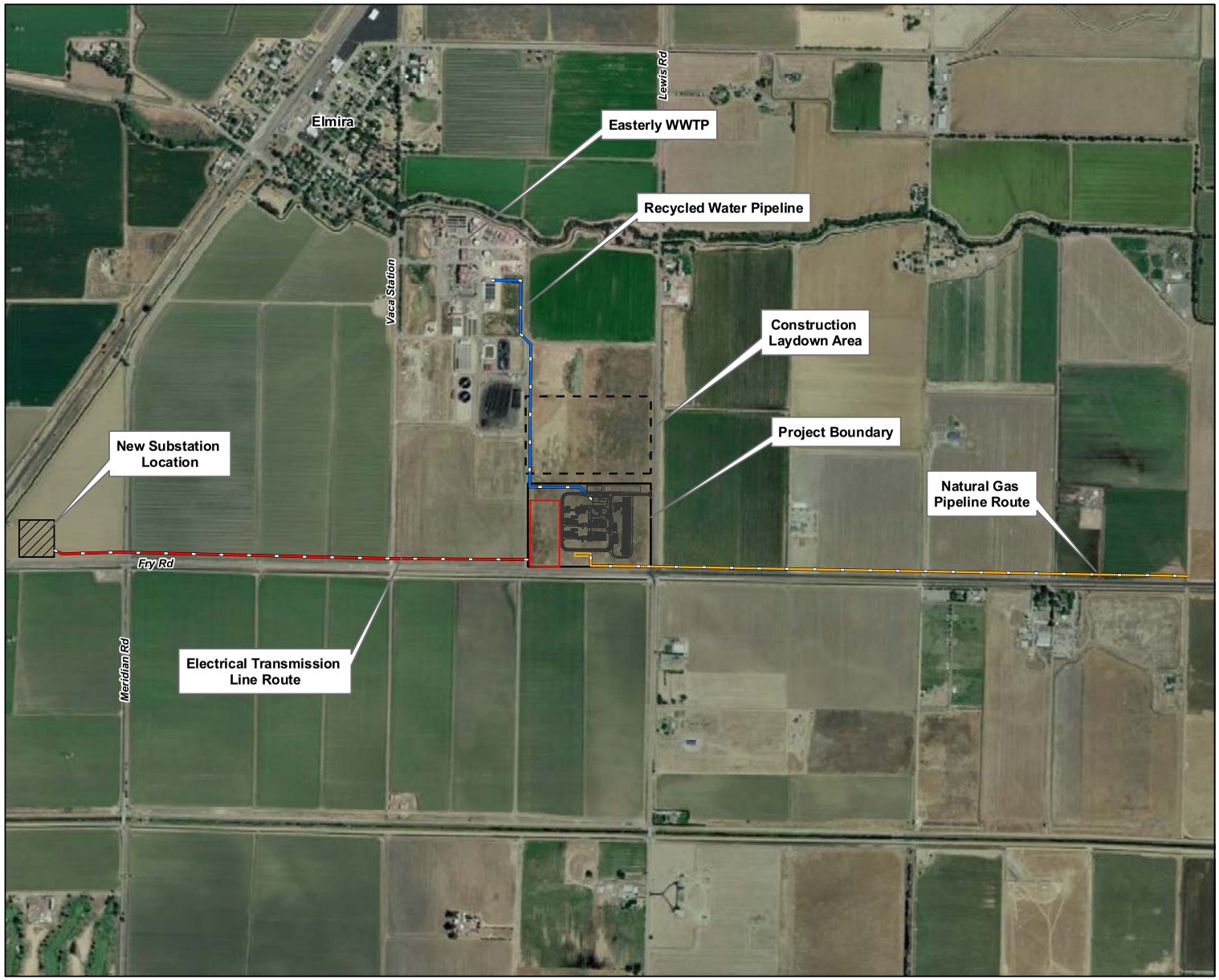
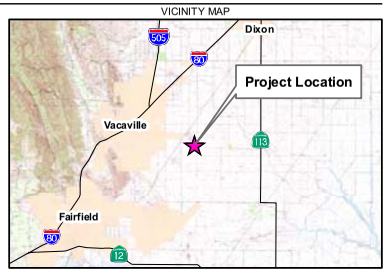


FIGURE 1
LOCATION MAP
CPV VACA STATION
VACAVILLE, CA

CH2MHILL

SAC\\ZION\SACGIS\PROJ\VACAVILLE_AFC_370668\MAPFILES\LOCATIONMAP.MXD MHASKELL 7/6/2009 13:38:54





LEGEND

- Natural Gas Pipeline Route
- Electrical Transmission Line Route
- Recycled Water Pipeline
- General Layout
- Natural Gas Metering Yard
- Switchyard
- New Substation Location
- Construction Laydown Area
- Project Boundary

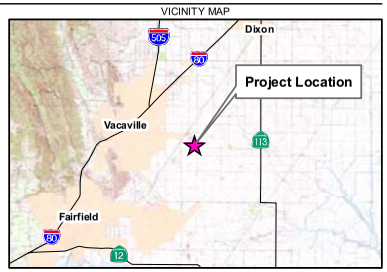
N

0 500 1,000
Feet

FIGURE 2A
VICINITY MAP
CPV VACA STATION
VACAVILLE, CA

SAC\ZION\SACGIS\PROJ\VACAVILLE_AFC_370668\MAPFILES\VICINITYMAP.MXD MHASKELL 7/7/2009 13:09:06

CH2MHILL



LEGEND

- Spot Elevation Points
- Natural Gas Pipeline Route
- Electrical Transmission Line Route
- Recycled Water Pipeline
- General Layout
- Natural Gas Metering Yard
- Switchyard
- New Substation Location
- Construction Laydown Area
- Project Boundary

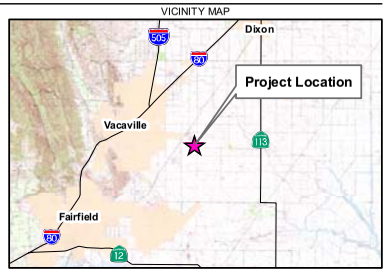
N

0 200 400
Feet

FIGURE 2B
VICINITY MAP
CPV VACA STATION
VACAVILLE, CA

SAC\ZION\SACGIS\PROJ\VACAVILLE_AFC_370668\MAPFILES\VICINITYMAP.MXD MHASKELL 7/7/2009 13:09:06

CH2MHILL



LEGEND

- Spot Elevation Points
- Natural Gas Pipeline Route
- Electrical Transmission Line Route
- Recycled Water Pipeline
- General Layout
- Natural Gas Metering Yard
- Switchyard
- New Substation Location
- Construction Laydown Area
- Project Boundary

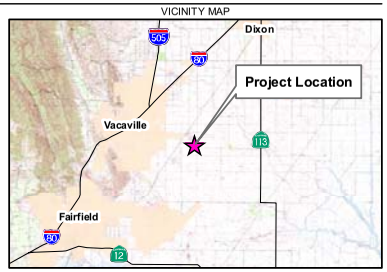
N

0 250 500
Feet

FIGURE 2C
VICINITY MAP
CPV VACA STATION
VACAVILLE, CA

CH2MHILL

SAC\ZION\SACGIS\PROJ\VACAVILLE_AFC_370668\MAPFILES\VICINITYMAP.MXD MHASKELL 7/7/2009 13:09:06



LEGEND

- Spot Elevation Points
- Natural Gas Pipeline Route
- Electrical Transmission Line Route
- Recycled Water Pipeline
- General Layout
- Natural Gas Metering Yard
- Switchyard
- New Substation Location
- Construction Laydown Area
- Project Boundary

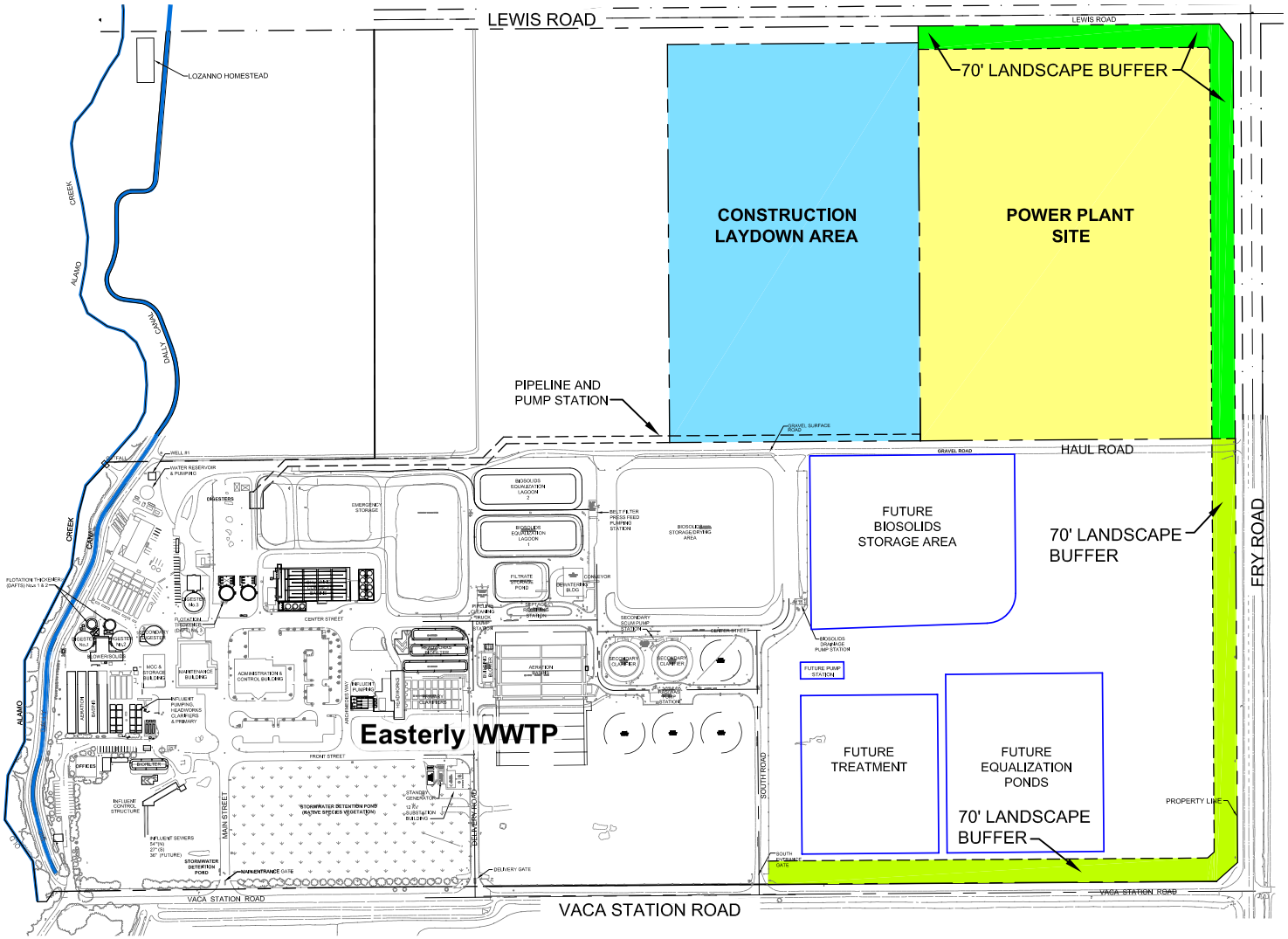
N

0 300 600
Feet

FIGURE 2D
VICINITY MAP
CPV VACA STATION
VACAVILLE, CA

SAC\ZION\SACGIS\PROJ\VACAVILLE_AFC_370668\MAPFILES\VICINITYMAP.MXD MHASKELL 7/7/2009 13:09:06

CH2MHILL



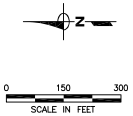


FIGURE 3A
PROJECT SITE AND LAYDOWN AREA
CPV VACA STATION
VACAVILLE, CA

Source: West Yost and Associates

EY052008001SAC Figure_3A.ai 07.08/2009 tdaus

CH2MHILL

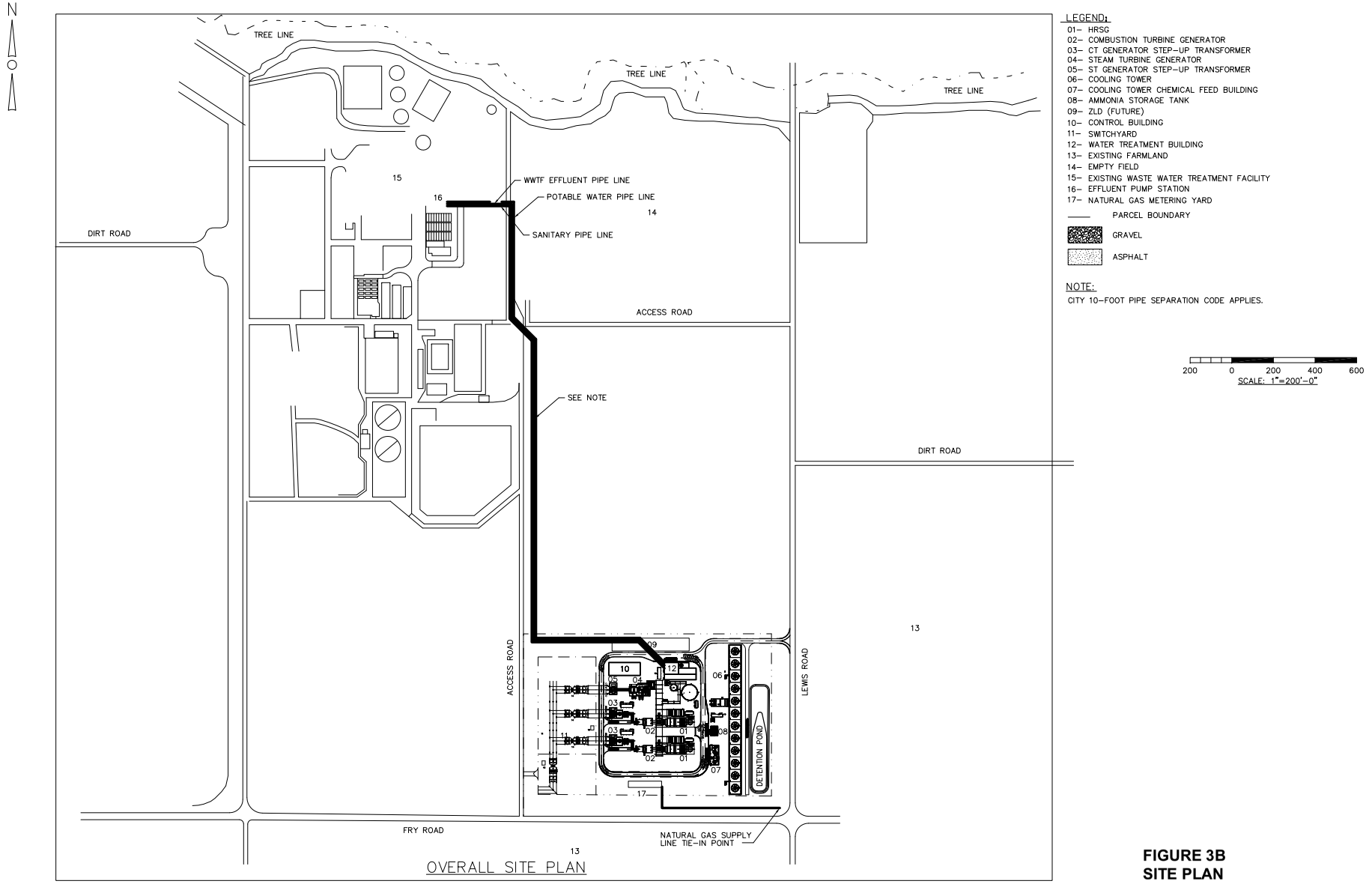
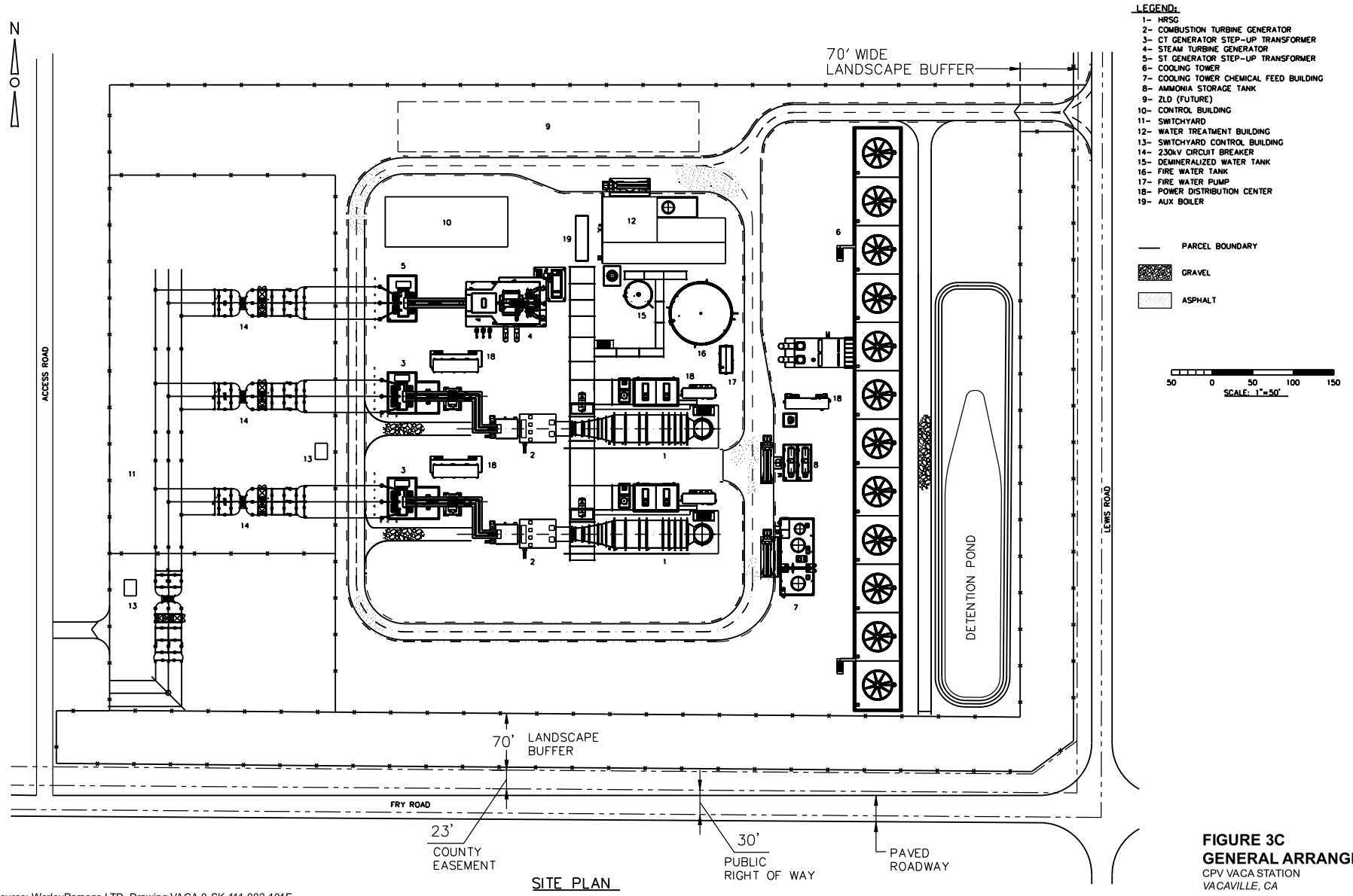


FIGURE 3B
SITE PLAN
CPV VACA STATION
VACAVILLE, CA

Source: WorleyParsons LTD, Drawing VACA-0-SK-111-002-100D

EY052008001SAC Figure_3B.ai 06/23/2009 tdaus

CH2MHILL

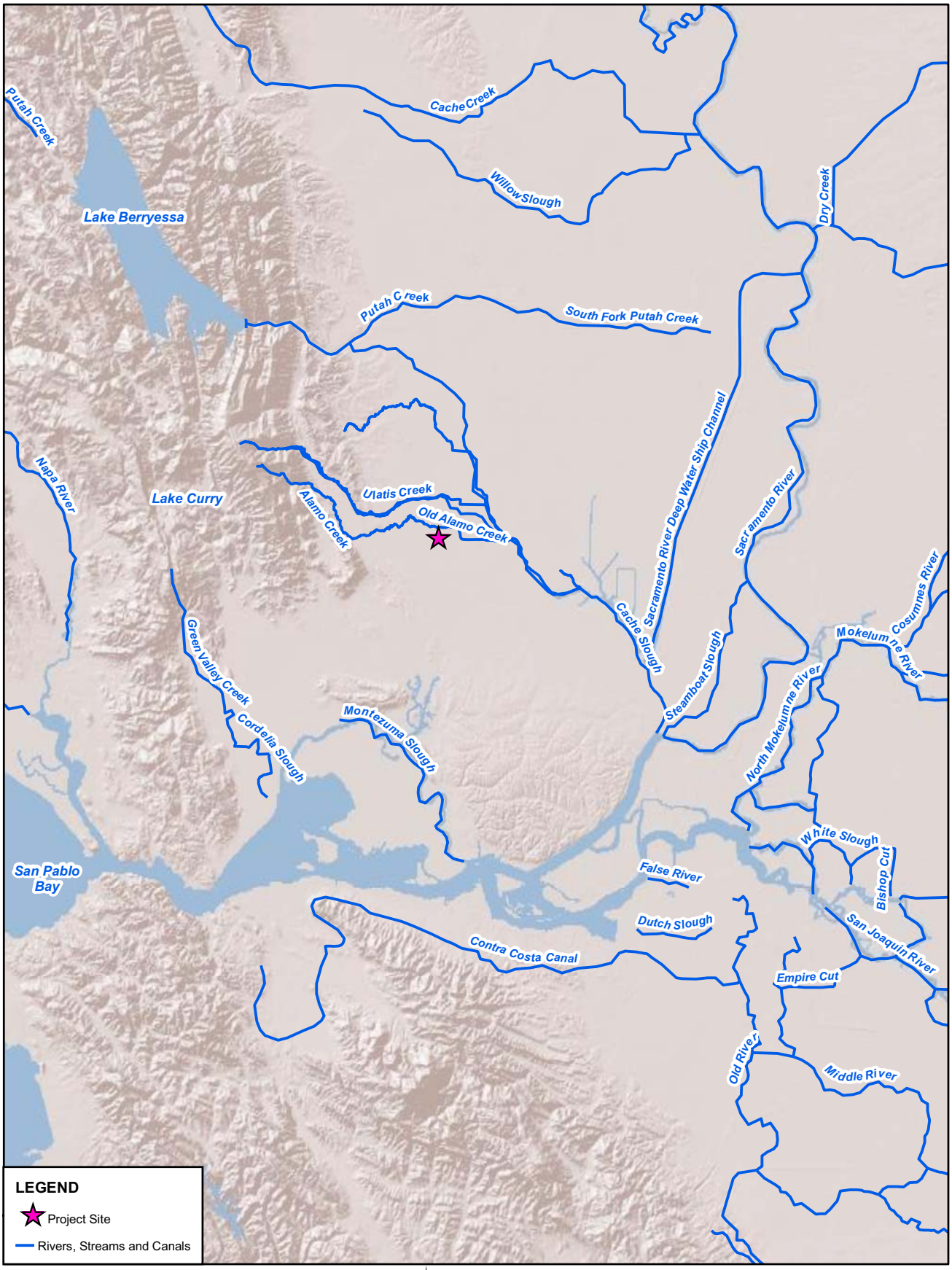


Source: WorleyParsons LTD, Drawing VACA-0-SK-111-002-101E

FIGURE 3C
GENERAL ARRANGEMENT
CPV VACA STATION
VACAVILLE, CA

CH2MHILL

EY052008001SAC Figure_3C.ai 06/23/2009 tdaus



Notes:
1. Source: The Califorina Watershed Map (CALWATER version 2.2) 2004.

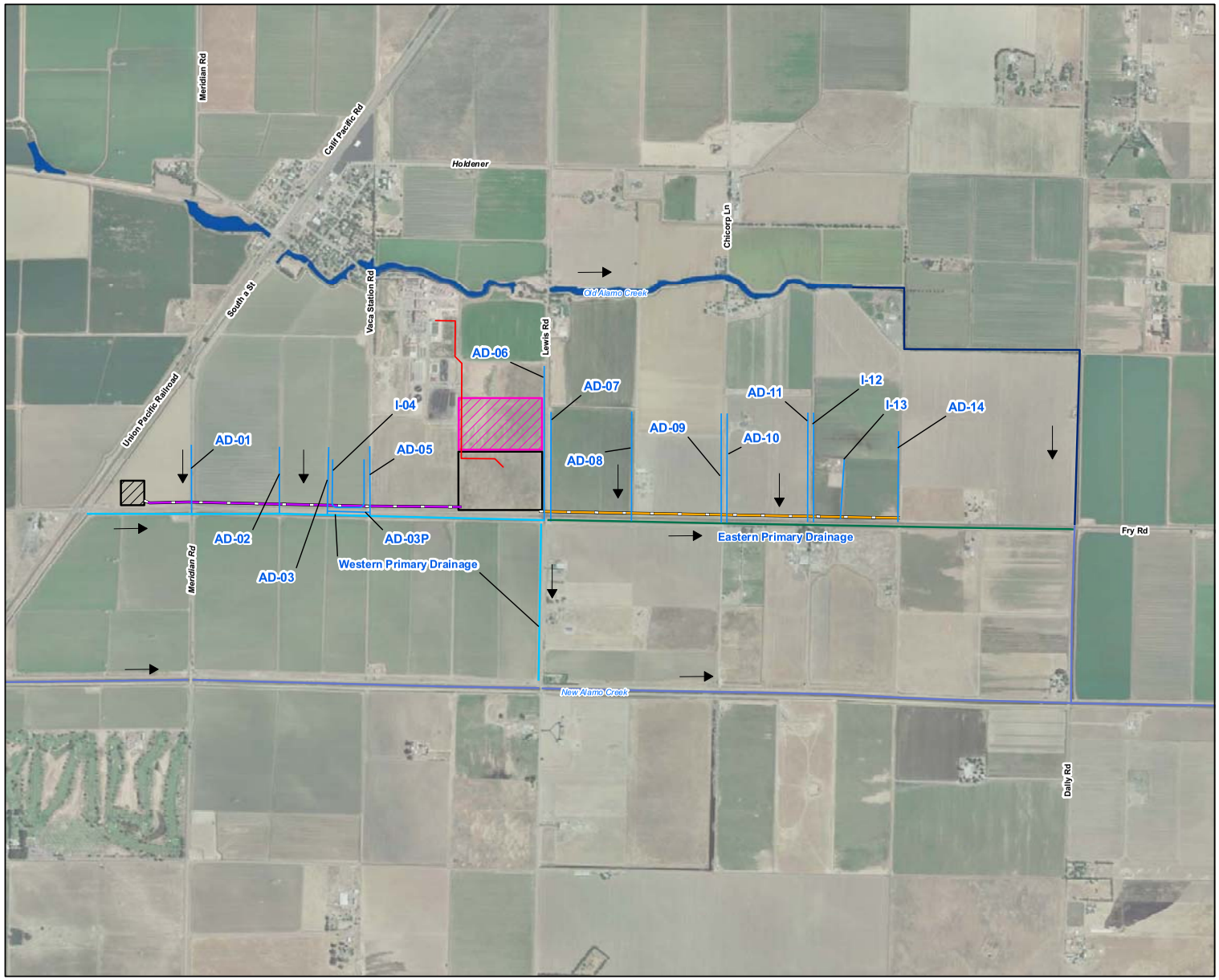
N

0 4 8
Miles

FIGURE 4
SURFACE WATER RESOURCES
CPV VACA STATION
VACAVILLE, CA

CH2MHILL

SAC\\ZION\SACGIS\PROJ\VACAVILLE_AFC_370668\MAPFILES\SURFACEWATERFEATURES.MXD MHASKELL 7/7/2009 15:21:21



LEGEND
- Utility Corridor to WWTP
- Natural Gas Pipeline Route
- Electrical Transmission Line Route
- Direction of Flow
- Agricultural Drainage Ditch
- Eastern Primary Drainage
- New Alamo Creek
- Old Alamo Creek
- Western Primary Drainage
- New Substation
- Old Alamo Creek
- Laydown Area
- Project Site

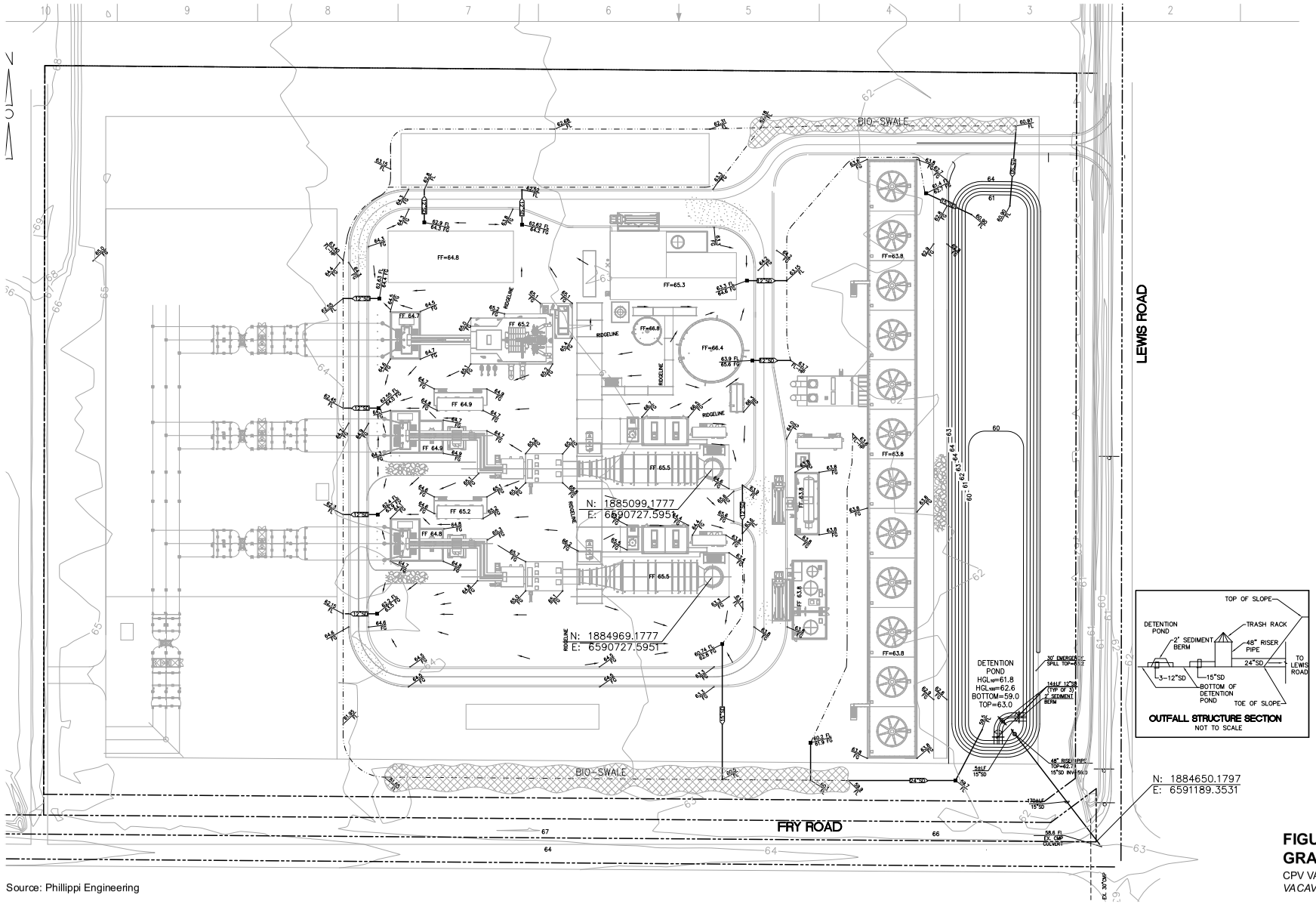
N

0 750 1,500
Feet

FIGURE 5
DRAINAGES AND WATERCOURSES
CPV VACA STATION
VACAVILLE, CALIFORNIA

CH2MHILL

SAC\ZION\SACGIS\PROJ\VACAVILLE_AFC_370668\MAPFILES\DRAINAGESHEDMAP.MXD MHASKELL 7/7/2009 15:35:33



Source: Phillippi Engineering

FIGURE 6
GRADING PLAN
CPV VACA STATION
VACAVILLE, CA

EY052008001SAC Figure_6.ai 07/29/2009 tdaus

CH2MHILL

Visual Resources (96)

High Resolution Copies of Simulations

96. Please provide high-resolution digital copies of the simulations prepared for the AFC.

Response: High resolution digital copies of the simulations prepared for the AFC are provided in electronic format on a CD-ROM, under separate cover, as Attachment DR96-1.

Attachment DR96-1
Digital Simulations

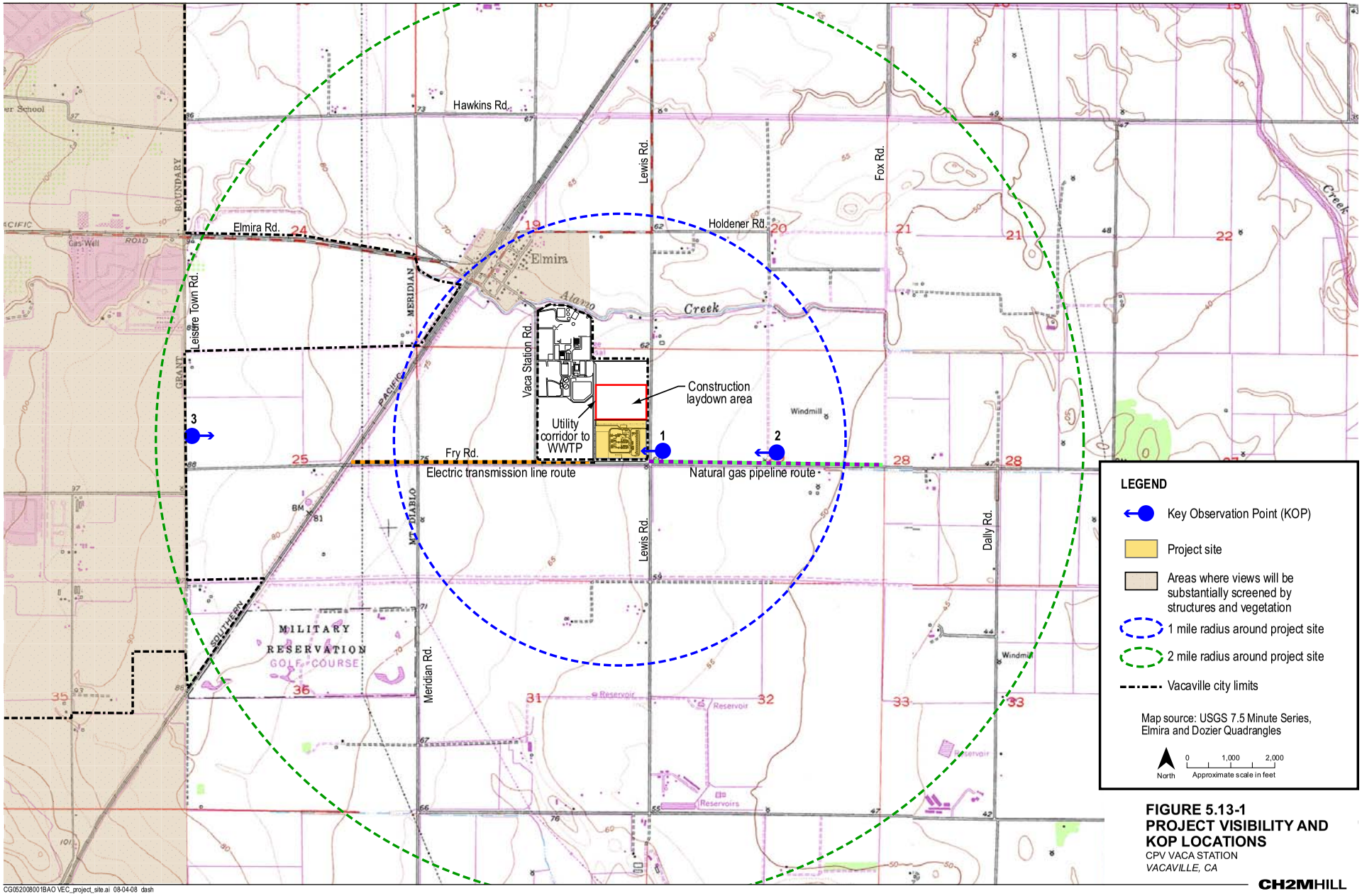


FIGURE 5.13-1
PROJECT VISIBILITY AND KOP LOCATIONS
CPV VACA STATION
VACAVILLE, CA

CH2MHILL

CG05200800 1BAO VEC_project_site.ai 08-04-08 dash

A. KOP-1. Existing view toward the project site from Fry Road at Lewis Road.

B. KOP-1. Simulated view toward the project site from Fry Road at Lewis Road.

FIGURE 5.13-2
KOP 1
CPV VACA STATION
VACAVILLE, CA

A. KOP-2. Existing view toward the project site from closest residence.

B. KOP-2. Simulated view toward the project site from closest residence.

FIGURE 5.13-3
KOP 2
CPV VACA STATION
VACAVILLE, CA

A. KOP-3. Existing view toward the project site from Leisure Town Road.

B. KOP-3. Simulated view toward the project site from Leisure Town Road.

FIGURE 5.13-4
KOP 3
CPV VACA STATION
VACAVILLE, CA

FIGURE 5.13-5
CONCEPTUAL LANDSCAPING AT 5 YEARS FROM PLANTING
CPV VACA STATION
VACAVILLE, CA

CH2MHILL

EY052008001SAC Figure_5.13-5.ai 08-20-08 tdaus

FIGURE 5.13-6
CONCEPTUAL LANDSCAPING AT MATURITY
CPV VACA STATION
VACAVILLE, CA

CH2MHILL

EY052008001SAC Figure_5.13-6.ai 08-20-08 tdaus

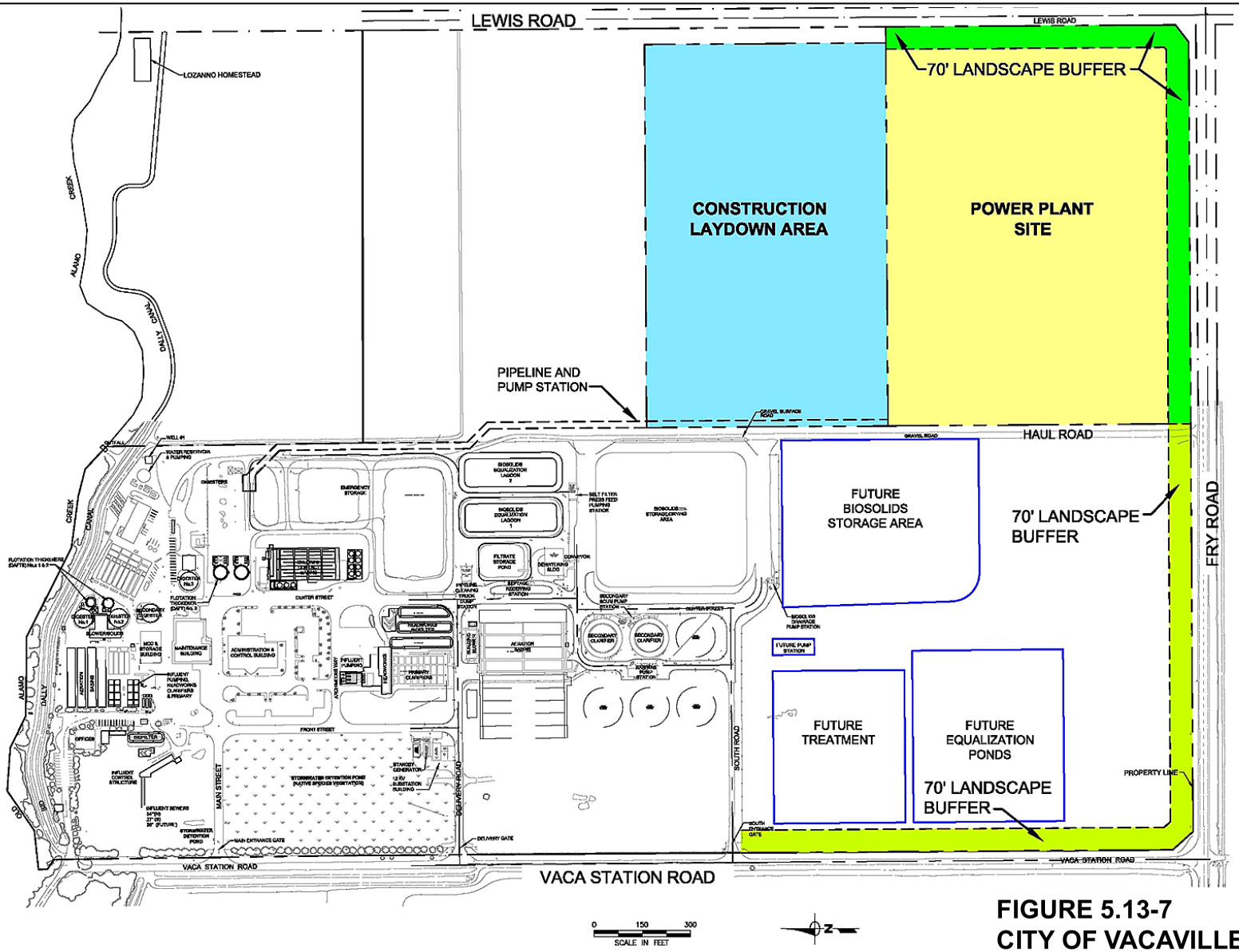


FIGURE 5.13-7
CITY OF VACAVILLE
CONCEPTUAL LANDSCAPE PLAN
CPV VACA STATION
VACAVILLE, CA

Figure source: West Yost Associates

CH2MHILL

EY052008001SAC Figure_5.13-7.ai 08-04-08 dash

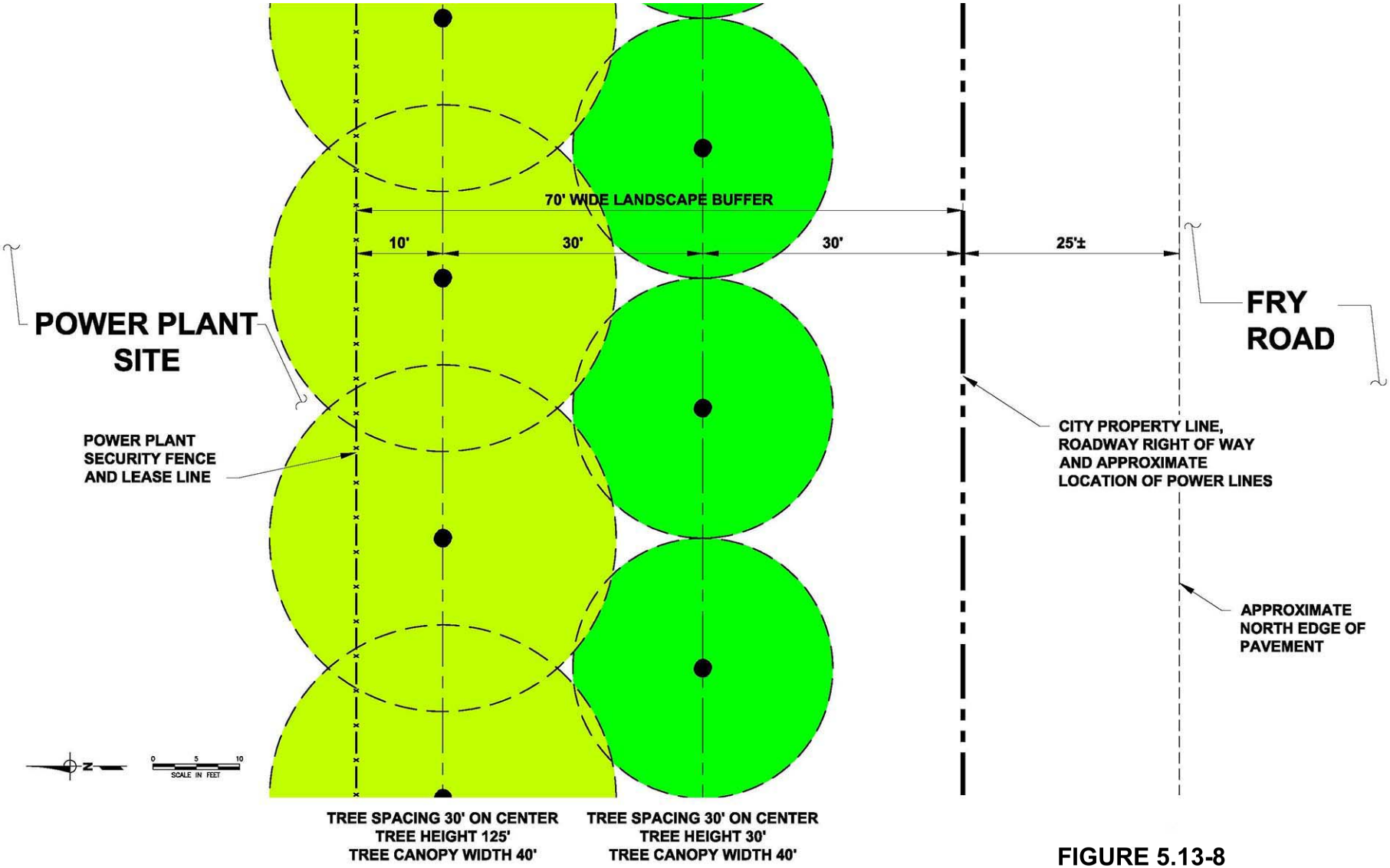


FIGURE 5.13-8
CITY OF VACAVILLE
LANDSCAPE PLAN DETAIL
CPV VACA STATION
VACAVILLE, CA

Figure source: West Yost Associates

CH2MHILL

EY052008001SAC Figure_5.13-8.ai 08-04-08 dash